WAR DEPARTMENT TECHNICAL MANUAL

SEMIPERMANENT
HIGHWAY AND
RAILWAY TRESTLE
BRIDGES

OPPOINT EFRICK FEER
OPPOINT FERNOWELLE

WAR DEPARTMENT, WASHINGTON 25, D. C., 30 April 1945.

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SEMIPERMANENT HIGHWAY AND RAILWAY TRESTLE BRIDGES

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PART ONE

GENERAL

CHAPTER I

SCOPE OF MANUAL

- 1. PURPOSE. a. This manual gives technical information on semipermanent highway and railway trestle bridges. It covers their construction from advance planning to actual fabrication and erection. It is designed as a source of detailed instructions and drawings for particular structures in the field as well as a reference handbook and text for training.
- **b.** The standard designs in this manual are intended to replace non-standard designs and reduce design work in the field to a minimum. Therefore, the manual does not discuss design *methods*. Where field-designed bridges are to be constructed, reference should be made to FM 5–10, for appropriate design methods.
- 2. ORGANIZATION OF MANUAL. a. Text. The text covers procedure for selecting location, type and length of spans, and type and height of supports. It explains methods of fabricating steel, of framing timber, and of erecting steel and timber bridges. It describes special tools and construction equipment used, and gives instructions for maintenance and repair of bridges.
- b. Drawings. General drawings show assembly of parts in standard units of construction. Detail drawings cover fabrication of steel parts and cutting and framing of timber parts from stock materials. General and detail drawings are given for special equipment that can be made in the field for erecting high towers and long spans.
- c. Tables. Tables on drawings list specific materials used in each unit of construction. Tables in text list materials, quantities, tool and equipment requirements, and give time and labor estimates for different units of construction and for different combinations of construction units used in completed bridges.
- d. Appendix. The appendix includes guides to design of plate girders, information on truck- and crawler-mounted cranes, and construction equipment, cofferdam details for foundation repairs in water not over 10 feet deep, and useful tabular data.
- 3. USE OF MANUAL. a. General Background. General information on the bridges is given in Part One. This includes general description of the bridges, advance planning data for staff use, design specifications and limitations, and information on capacities and traffic control.
- **b. Planning.** Three phases of planning are discussed in different parts of the manual:
- (1) Advance staff planning to determine theater stockage or task force requirements is treated in chapter 3.
- (2) Site selection, bridge lay-out, and detailed construction plans for the benefit of the engineer section and commanders responsible for construction are discussed in chapters 6 to 9.
- (3) Erection schemes that may be used by construction officers are dealt with in chapter 14.

TABLE I. Range of bridge spans, supports, and foundations for semipermanent trestle bridges1

Construction	High	nway bridges	Rail	way bridges
Spans: Material Designs for span length	Timber Stringers 11 ¹ , 13 ¹ , 15 ¹	Steel Stringers 15 ¹ , 20 ¹ , 30 ¹ , 40 ¹ , 50 ¹ 60 ¹ , 70 ¹ , 80 ¹ , 90 ¹	Timber Stringers 12 ¹ , 14 ¹ , 16 ¹	Steel Stringers 151, 201, 251, 301, 351 401, 451, 501
Intermediate pile bents and piers: Timber pile bents	301	No design ³	201	No design
Timber pile piers ⁵	Not shown ²	1 0		15 ¹
Steel pile bents ⁵	1	301		231
Steel pile piers	Not shown			231
Timber towers:		801		
On spread footings		L Concre	te pedestals	
On spread roomigs	1	Timbe	0 0	
On timber piling	1	Tim		
		Concrete ped		
On steel piling		Timber sills, no design;		
Steel towers:		801) 80 ¹
On spread footings		Concrete pedestals		Concrete pedestals
	No design	Steel grillage	No design	Steel grillage
On timber piling		Concrete pedestals		
On steel piling		Concrete pedestals		Concrete pedestals
		Steel framed caps		J Steel framed caps
Abutments with end dam:	61 4	61	61	61
ZIORIMENIS WIN CHW WAITE.	Not shown			Concrete
On spread footing				Over 15 ¹ 15 ¹ span span
	Timber grillage and	l end dam	 	
				Up to Over 251
On timber piles	Pile bent and timbe	r end dam		25 ¹ span span Pile pier
On steel piles	Not shown	Steel pile bent and timber end dam	Not shown	Steel pile bent and

- c. Construction. Preliminary work, details of fabrication and assembly, methods of erection, and erection equipment are discussed in chapters 10 to 16. Design drawings in Part Six include necessary working drawings for fabrication and assembly. Tables accompanying the text give material and man-hour requirements.
- d. Maintenance and repair. Maintenance and repair are covered in Part Three.

4. RELATED PUBLICATIONS. a. General.

Engineer Troops	FM	5–5
Operations of Engineer Units	FM	5–6
Construction and Routes of Communication	FM	5-10

Explosives and Demolitions	FM	5-25
Reference Data	FM	5-35
Rigging and Engineer Hand Tools	TM	5-225
Carpentry	TM	5-226
Topographic Drafting	TM	5-230
Surveying	TM	5-235
Interpretation of Aerial Photographs	TM	5-246
Construction in the Theater of Operations	TM	5-280
Standard Plans-Roadway, Track, and Structures	TM	55-276
b. Fixed bridge equipment.		
Portable Steel Highway Bridges, H-10 and H-20	TM	5-274
Fixed Steel Panel Bridge, Bailey type	TM	5-277

Semipermanent	Highway	Steel	Fixed	Bridges,	30-,	60-,			
and 90-foot	Spans	• • • • • • • • • • • • • • • • • • • •					TM	5-285	
I-Beam Railway	Bridge	• • • • • • • • • • • • • • • • • • • •	····				TM	5-371	

c. Erection equipment. See FM 21-6 for list of latest War Department publications covering operation, repair, and lubrication of engineer mechanical equipment and special tools.

CHAPTER 2

GENERAL DESCRIPTION OF BRIDGES

- **5. PURPOSE OF BRIDGES. a.** The semipermanent highway and railway trestle bridges described in this manual are intended primarily for use in:
- (1) Replacing existing temporary or inadequate bridges.
- (2) Crossing gaps on new lines of communication.
- b. These bridges usually replace:
- (1) Temporary earth-filled bypasses.
- (2) Temporary bridges with structural limitations.
- (3) Demolished bridges temporarily repaired.
- (4) Portable tactical bridges needed for operations farther forward.
- 6. LOAD CLASSIFICATION AND WIDTH OF BRIDGES. a. Highway bridge designs in this manual are for semipermanent bridges of the following U. S. load classes and widths:

Class 50, single-lane, 121/2-foot roadway	(sheets 1-43)
Class 50, double-lane, 22-foot roadway	(sheets 44–90)
(Also used as class 80 single-lane bridge)	(

Class 25, double-lane, 22-foot roadway(sheets 91-127)

b. Railway bridge designs are for only one class of semipermanent bridge: E-45, single-track, 4-foot 8½-inch and narrower gauges

(sheets 156-225)

- c. The class 50 double-lane bridge is adequate for single-lane class 80 traffic. Traffic control conditions under which other bridges can carry loads beyond their rated weight-class are given in chapter 5.
- d. Twenty-percent reduction in capacity is required if machine bolts are substituted for rivets or structural ribbed bolts in certain steel construction units. (See par. 224.)
- 7. TRESTLE BRIDGE NOMENCLATURE. This paragraph gives nomenclature of the principal parts of a trestle bridge as used in this manual. For other terms see index.

Braced bents. Pile bents connected by longitudinal bracing. (See fig. 16.) Framed bent. A single transverse row of timber columns connected by transverse bracing and a cap and sill. Two or more framed bents connected by longitudinal bracing form a framed tower. (See fig. 10).

Grade. Elevation of top of tread on highway bridges, or top of cross tie on railway bridges.

Pile bent. A support consisting of a single transverse row of piles connected by transverse bracing and a cap. (See fig. 1.)

Pile pier. A support consisting of pile bents connected by longitudinal bracing and corbels or diaphragms. (See fig. 5.)

TABLE II. Illustrations of combinations of units for trestle bridges.

Combination				Railway	
	class 50	class 50	class 25	E-45	
		PILE F	OOTINGS		
Timber-stringer spans,	Fig. 1	Fig. 2		Fig. 15	
timber pile bents.	_ 1 1g. 1	rig. 2		Fig. 15	
Steel-stringer spans	Fig. 3	Fig. 4	Fig. 4	Fig. 16	
steel pile bents.	8. 3	1.8.	1.6. 1	1 /g. 10	
Steel-stringer spans,		Fig. 5		Fig. 17	
timber pile piers.				8 - 1	
Steel-stringer spans,	Fig. 6	Fig. 7	Fig. 7	Fig. 18	
steel pile piers. Steel-stringer spans,					
framed timber towers,		Fig. 8(1),			
timber sill, timber piles.		Fig. 8(2)		Fig. 19(1)	
Steel-stringer spans,	1				
framed steel towers,		Fig. 0(1)	Fig. 0(1)	E:~ 20/2)	
concrete pedestal, timber piles.		Fig. 9(1)	Fig. 9(1)	Fig. 20(2)	
Steel-stringer spans,					
framed steel tower,		Fig. 9(2)	Fig. 9(2)	Fig. 20(3)	
concrete pedestal, steel piles.		118. 9(2)	11g. 9(2)	11g. 20()	
Steel-stringer spans,					
framed steel tower,			-	Fig. 20(1)	
steel frame, steel piles.					
Timber-stringer spans,					
framed timber towers,	Fig. 10(2)	Fig. 11(1)		Fig. 21(1)	
timber sill, timber piles.					
		SPREAD F	OOTINGS		
Timber-stringer spans,					
framed timber towers,	Fig. 10(3)			Fig. 21(2)	
concrete pedestals.	0 (1)				
Steel-stringer spans,					
framed timber towers,	Fig. 12		Fig. 13	Fig. 19(2)	
concrete pedestals.					
Steel-stringer spans,					
framed steel tower,		Fig. 9(3)	Fig. 9(3)	Fig. 20(4)	
concrete pedestals.					
Timber-stringer spans,					
framed timber tower,	Fig. 10(1)	Fig. 11(2)		Fig. 21(3)	
timber grillage.					
Steel-stringer spans,		W: 0(0)		Ti- 10/2)	
framed timber tower,		Fig. 8(3)		Fig. 19(3)	
timber grillage.					
Steel-stringer spans,	Ti~ 14	•		Fig. 20(5)	
framed steel tower,	Fig. 14			rig. 20(3)	
steel grillage.]	

Span. The distance between two supports holding up a structure. Also used to mean superstructure.

Substructure. The parts of a structure which provide support for the super-structure.

Superstructure. The part of a structure above and between supports. Also called span.

Tower. Two or more framed timber or steel bents tied together by bracing to form a supporting unit for spans. Towers are supported on timber, concrete, or steel foundation units.

Trestle bridge. A structure consisting of a series of supports and decked stringer spans.

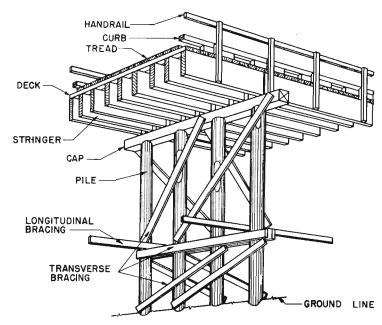


Figure 1. Highway bridge, class 50, single-lane, timber stringers on timber pile bent.

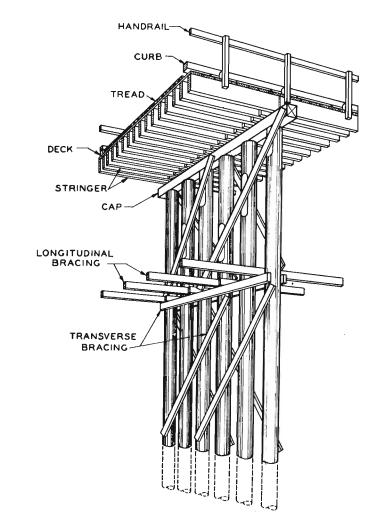


Figure 2. Highway bridge, class 50, double-lane, timber stringers on timber pile bent.

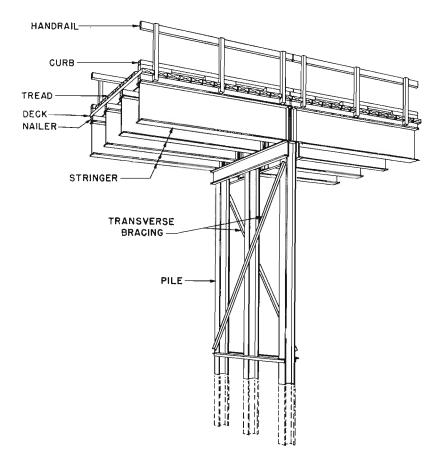


Figure 3. Highway bridge, class 50, single-lane, steel stringers on steel pile bent.

Unit of construction. A structural assembly consisting of a span, a support, or a foundation. Units of construction are combined to make a bridge. Interchangeable designs for each of the three classes of construction unit are given in this manual. The proper selection and combination of construction units are discussed in chapters 3 and 7.

- **8.** TYPES OF CONSTRUCTION. a. General. (1) All bridges in this manual are trestle type bridges. Complete drawings of units of construction (par. 7) are furnished for various spans, supports, and foundations. Types of units of construction covered in this manual are listed below. Principles governing selection of different types of construction units are given in paragraph 17.
- (2) Construction units are combined as specified in table I to provide bridges of standard load class and width. (See par. 6.) These bridge types are shown in figures 1 to 21. (See table II.)
- (3) For a particular bridge site, suitable foundations, supports, and spans are combined into a single- or multiple-span trestle bridge. Typical highway and railway bridge lay-outs for typical gaps are described in chapter 9.
- b. Spans. Units of construction for spans are of two types:

Туре	Maximum span (ft.)			
	Highway	Railway		
(1) Timber stringer	15	16		
(2) Steel stringer	90	50		
Standard span lengths of each type are given in table	I.			

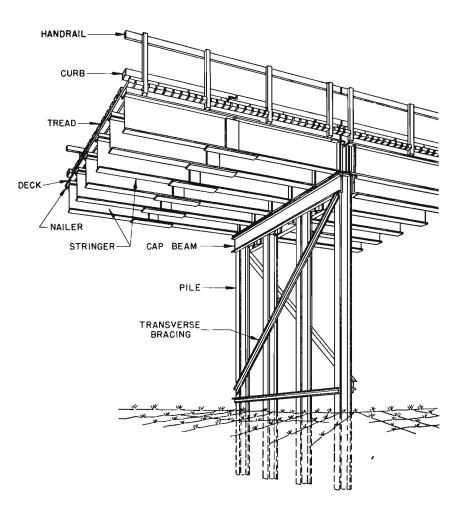


Figure 4. Highway bridge, class 50, double-lane, steel stringers on steel pile bent; class 25 similar except 3 piles in bent.

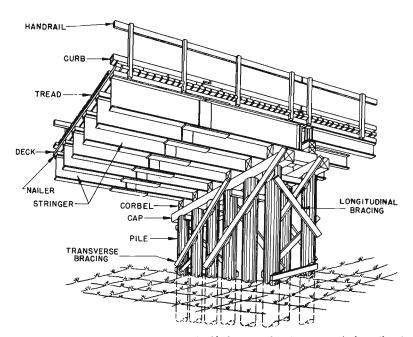


Figure 5. Highway bridge, class 50, double-lane, steel stringers on timber pile pier.

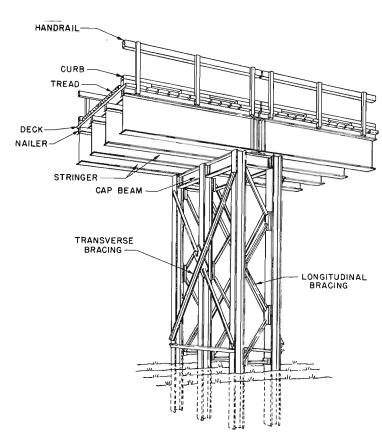


Figure 6. Highway bridge, class 50, single-lane, steel stringers on steel pile pier.

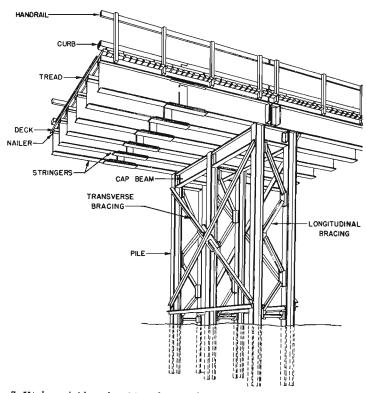


Figure 7. Highway bridge, class 25 or class 50, double-lane, steel stringers on steel pile pier.

c. Supports. Units of construction for supports are of the following types:

Type		Туре		fe height from cround (ft.)	Maximum he	eight detailea s, ground to
				Railway	bottom of st Highway	ringers (ft.)
	(1)	Timber pile bents	30	30	28	28
	(2)	Timber pile piers	30	15	14	111/2
	(3)	Steel pile bents	30	23	20	20
	(4)	Steel pile piers	35	23	20	20
	(5)	Framed timber towe	ers 80	80	76	76
	(6)	Steel towers	80	80	77	77
	(7)	Timber grillage abu	ıt-			
		ment	61	61	4	4
	(8)	Timber pile abutme	nt 61	61	4	4
	(9)	Steel pile and timb	er			
		abutment	61	61	4	31/2
	(10)	Concrete abutment	61	61	41/2	41/2

¹ Height of fill retained behind abutment.

The types of spans and range of span lengths with type and limiting height of supports are given in table I. For limitation of span length by high supports, see paragraph 223e.

d. Foundations. Units of construction for foundations under both highway and railway towers are of the following types:

Type

- (1) Timber grillage.
- (2) Steel grillage.
- (3) Concrete pedestals on ground.
- (4) Timber piles and timber sills.
- (5) Timber piles capped with concrete pedestals.
- (6) Steel piles capped with concrete pedestals.
- (7) Steel piles capped with steel frames.

The types and ranges of spans and supports for each type of foundation are given in table I.

- 9. FEATURES OF DESIGN. a. Standardization. Use of the standard designs in this manual for construction of the four standard bridge classes in paragraph 6 is intended to:
 - (1) Eliminate structural design work and capacity estimation in the field.
 - (2) Provide balanced designs which save materials and construction time.
 - (3) Utilize available stock-pile materials.
- (4) Reduce to a minimum the variety of sizes, shapes, and types of material required.
- (5) Simplify planning, stock piling, erection, and maintenance.
- (6) Indicate the necessary scope of training for construction of semipermanent trestle bridges.
- b. Flexibility. Designs are provided for widely different conditions. Units of construction can be combined to satisfy different requirements at different points on the same bridge. Selection of the type of construction best-suited to conditions in the theater is simplified by tables V to VIII. Wide deviations of final construction from original advance staff approximations or from bridge lay-out to meet unforeseeable or difficult conditions are possible because of

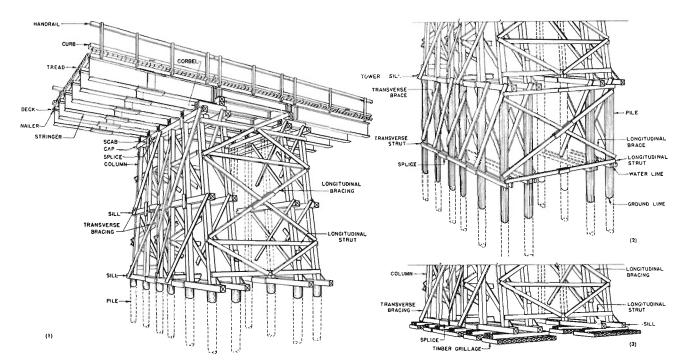


Figure 8. Highway bridge, class 50, double-lane, steel stringer spans, framed timber tower:

- (1) On timber piles constructed on ground or in shallow water.
- (2) On braced timber piles constructed in deep water.
- (3) On timber grillages.

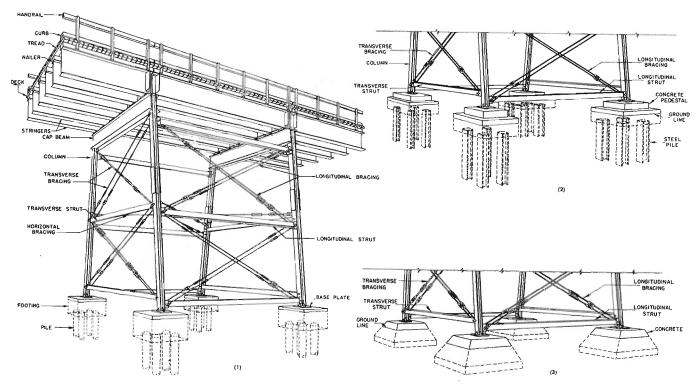


Figure 9. Highway bridge, class 25 or class 50, double-lane, steel stringer spans, steel tower:

- (1) On concrete pedestals, timber piles.
- (2) On concrete pedestals, steel piles.
- (3) On concrete pedestals.

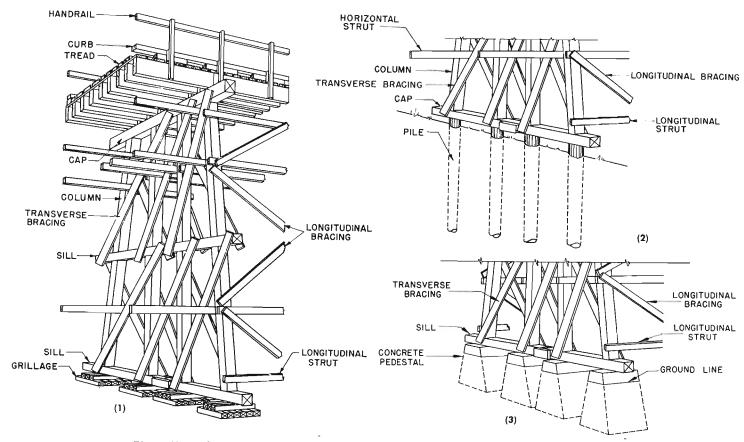


Figure 10. Highway bridge, class 50, single-lane, timber stringer spans, framed timber tower:

- (1) On timber grillages.
- (2) On timber sills, timber piles.
- (3) On concrete pedestals.

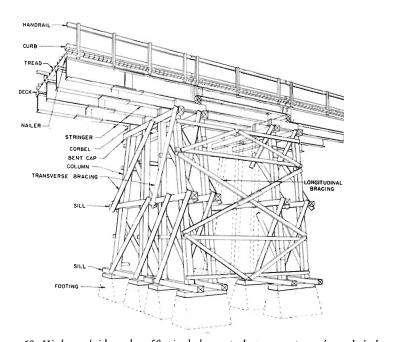


Figure 12. Highway bridge, class 50, single-lane, steel stringer spans, framed timber tower on concrete pedestals.

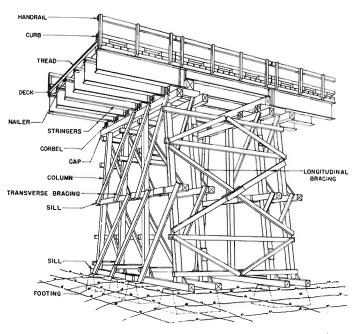


Figure 13. Highway bridge, class 25, double-lane, steel stringer spans, framed timber tower on concrete pedestals.

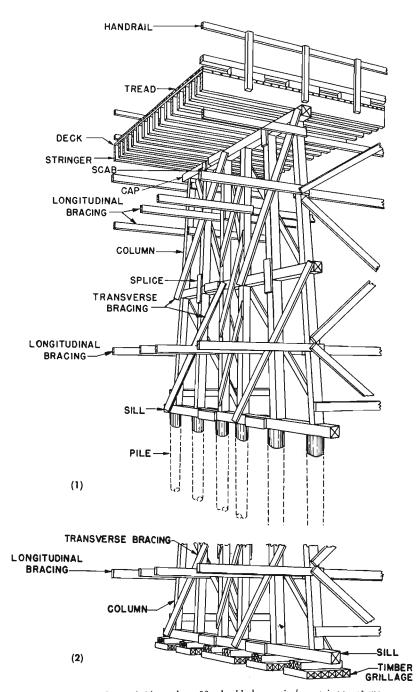


Figure 11. Highway bridge, class 50, double-lane, timber stringer spans, framed timber tower:

- (1) On timber sills, timber piles.
- (2) On timber grillages.

flexibility of designs, use of identical sections in different units of construction, and provision of alternative designs.

c. Economy of materials. Economy of materials results from balanced design of units of construction, use of materials commonly available locally, and flexibility of designs.

- 10. DESIGN LIMITATIONS. a. Semipermanent bridges. (1) Bridges in this manual are classed as *semipermanent* bridges which differ in design from *civilian* bridges and *tactical* bridges.
- (2) The following design restrictions distinguish semipermanent bridges from civilian structures:
- (a) Designs are for specific military load limits and for controlled traffic. (See ch. 5.)
- (b) Allowable stresses are greater than normally used in civilian practice. (See ch. 4.)
- (3) The following characteristics distinguish semipermanent bridges from most tactical bridges:
- (a) Designs are for standard load classes and roadway widths (par. 6) which usually exceed the frequently critical clearance and load capacity of tactical bridges.
- (b) Bridges are not temporary structures. They are not intended to be dismantled for use farther forward in the combat zone as front lines advance.
- (c) Erection time generally is greater than for tactical bridges.
- (d) Transportation requirements generally exceed those for tactical bridges because larger and heavier units are used.
- (e) More deliberate erection methods and special erection equipment and tools not organic in engineer troops units are required.
- (4) The semipermanent trestle bridges in this manual are also distinguished from *prefabricated* semipermanent bridges such as the H20 box-girder steel fixed bridge or the semipermanent highway bridge, 30-, 60-, and 90-foot spans. The bridges in this manual are not issued prefabricated, but are fabricated in the field from class IV materials (par. 12) so span length and height of supports can be varied in small increments and various types of construction can be used to suit the site. However, the supports described in

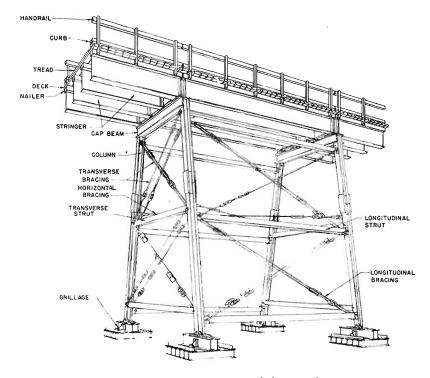


Figure 14. Highway bridge, class 50, single-lane, steel stringer spans, steel tower on steel grillages.

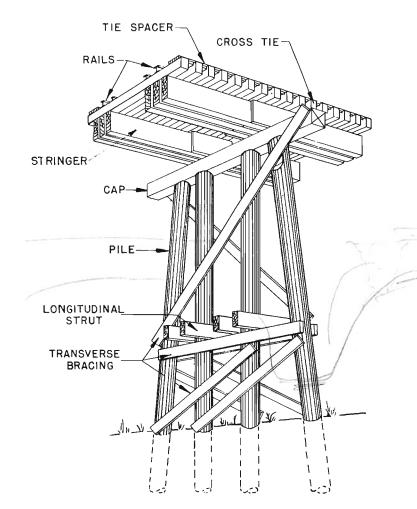


Figure 15. Railway bridge, timber stringers on timber pile bents.

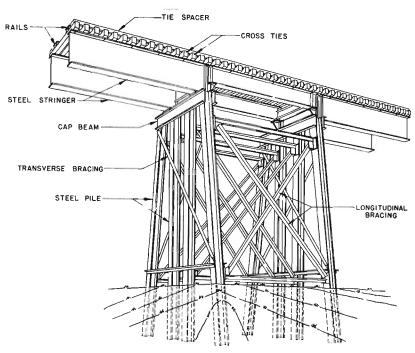


Figure 16. Railway bridge, steel stringers on braced steel pile bents.

this manual can be adapted for use with *prefabricated* semipermanent spans. (See par. 11.)

- b. Stream characteristics. The bridges in this manual are suitable for crossing shallow tidal waters, shallow streams, deep streams not over 80 feet wide, and deep valleys or ravines. They are not intended for use where foundations must be constructed in deep water, where drift or ice is heavy, scour is excessive, or where large flood flows are frequent.
- c. Unbraced lengths of pile foundations. Bridges with pile foundations can be built in water where the unbraced length of piles from firm stream-bed material to the lowest point of bracing, with allowance for probable scour (par. 75), does not exceed the following:

Distance grade	Maximum unbraced lengt
to ground (ft.)	of pile (ft.)
Less than 30	20
30 to 50	15
50 to 80	10

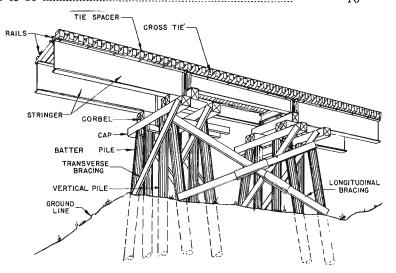


Figure 17. Railway bridge, steel stringers on braced timber pile piers.

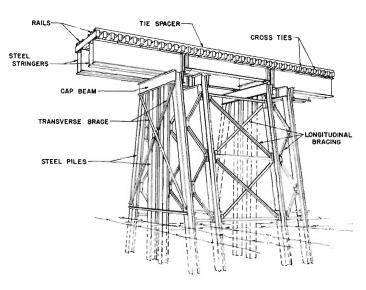


Figure 18. Railway bridge, steel stringers on braced steel pile piers.

I'I. DESIGN ALTERNATIVES, MODIFICATIONS, AND ADAPTATIONS.

- **a.** General. This manual does not include design methods. Changes in designs should not be made except by qualified engineer officers trained in bridge design. Design methods are specified in FM 5-10.
- **b.** Alternatives. Data on alternative nonstandard connections, decking, and stringer sections are given in chapter 18.
- **c.** Modifications. The standard designs show level grades, straight alignment, and symmetrical towers. Chapter 18 gives methods of modifying designs for grades, curved alignment, and sloping banks. Grades on structures are limited to normal operating grades.
- **d.** Adaptations. (1) Details are given (sheets 235 to 245) for adapting. substructure units to the following standard prefabricated highway superstructures:
- (a) Semipermanent highways, steel fixed bridges, 30-, 60-, and 90-foot spans (TM 5-285).
- (b) Panel steel fixed bridge, Bailey-type (TM 5-277).
- (c) Box-girder steel fixed bridges, H10 and H20 (TM 5-274).
- (2) By modifying the end bearings of the I-beam railway bridges (TM 5-371), they can be used with any of the standard railway supports in this manual, except timber pile bents. The unit construction railway bridge (spans 50 to 85 feet) (TM 5-372) and through truss railway bridge (spans 90 to 150 feet) (TM 5-373) cannot be used on any of the railway supports in this manual. They must be supported respectively on light standard (L-type)

and standard (T-type) unit steel trestles (TM 5-374) or on specially designed piers.

- 12. MATERIALS AND EQUIPMENT. a. Class IV supplies. Bridges in this manual can be fabricated in the field from class IV material and with organic equipment normally issued to engineer troops or class IV tools and equipment available in communications zone depots.
 - b. Timber. Designs use timber in:
 - (1) All bridge flooring, curbs, and handrails.
 - (2) Stringers up to 16-foot spans.
 - (3) Framed bents and towers under all spans.
 - (4) Pile bents, piers, and foundation piles.
 - (5) Abutments under all spans.
 - (6) Grillages under timber towers.
- c. Structural steel. Designs are prepared for steel furnished in 40-foot lengths. Designs use steel in:
- (1) Stringers in spans.
- (2) Framed steel towers.
- (3) Pile bents and pile piers.
- (4) Abutments.
- (5) Grillages under towers.
- (6) Steel frame on steel piles.
- d. Concrete. Reinforced concrete is not used in these bridge designs.

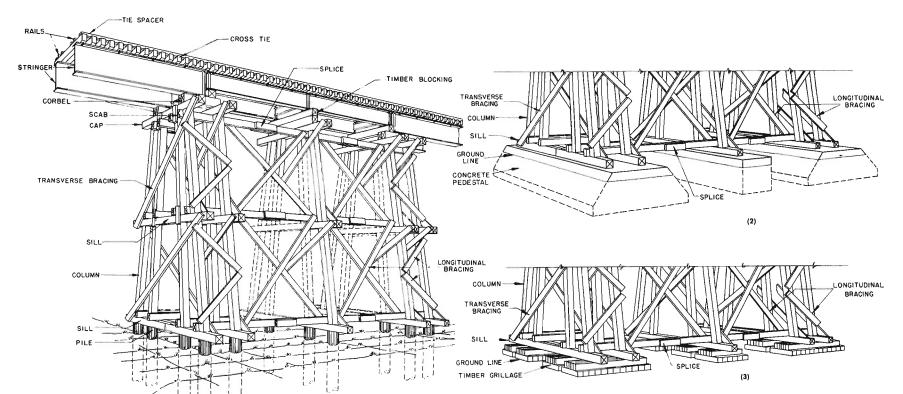


Figure 19. Railway bridge, steel stringer spans, framed timber tower.

- (1) On timber sills, timber piles.
- (2) On concrete pedestals.
- (3) On timber grillages.

Designs use unreinforced concrete in:

- (1) Abutments.
- (2) Foundation pedestals on ground under:
- (a) Framed timber towers.
- (b) Framed steel towers.
- (3) Grout under steel grillages.
- (4) Pedestals supported on timber or steel foundation piles.
- e. Hardware. Black, unpainted hardware is used throughout.
- f. Paint. Semipermanent bridges are painted only when necessary for

TABLE III. Sizes, lengths, and principal uses of timber in semipermanent bridges.

Size (inches)	Length (feet)	Use
12 x 12	10, 12, 14, 16, 18	
	or random	Pile bent and pier cap
10 x 12	12, 20, or ran-	
	dom	Class 25 tower cap. Blocking under stringers
10 x 10	12, 14, 16, 18, 20,	
	22, or random	Tower caps and sills. Columns. Abutment cap
8 x 12	16, 20, or random	Corbels on piers and double bents
8 x 10	Random	Blocking under stringers
8 x 8	8, 12, 14	Abutment bulkhead posts
6 x 18	16	Railway stringer, 14- and 16-foot span
6 x 16	16	Highway stringer
6 x 12	10, 12, 16, or	•
	random	Blocking under stringers
6 x 10	12, 14, 16, 18, 20	Railway tower struts
6 x 8	12, 16, 20, or	
	random	Abutment footing and bulkhead posts.
		Timber grillage
6 x 6	10, 12, 14, 16, or	
	random	Curb. Nailer
4 x 12	14, 16, 18, 20, 22,	
	24, or random	Deck on steel stringers. Bulkhead
4 x 10	16, 18, 20, 22, 24,	
	or random	Railway tower longitudinal bracing. Scabs
4 x 8	14, 16, 18, 20, 22,	
	24, 26, or ran-	_
	dom	Bent, pier, and tower bracing. Railway walkway
	Random	Handrail posts. Walkway
	12	Spacers between stringers.
3 x 12	12, 14, 16, 20, 24,	
l	or random	Tread plank. Deck plank on timber stringers
3 x 10	8, 12, 14, 16, or	
	random	Scabs for columns. Railway pier and tower brac-
		ing. Tie spacers.
3 X 8	8, 10, 12, 14, or	Constant of the second
1 4	random	Spacers and scabs for timber stringers
	Random	Handrail post fill.
2 x 12	12, 14, 16, 20, or	75 1 - 1 1 1 1 1 - 1 -
	random	Tread plank on laminated deck. Scabs for railway stringers
2 x 10	14, 16, or ran-	
	dom	Railway walkway, scabs on bracing
2 x 8	Random	Scabs for highway bracing
2 x 6	10, 12, 14, 16, or	
	random	Handrail. Walkway. Railway tie spacers
2 x 4	14	Laminated deck on steel stringers
2 x 4	24	Laminated deck on timber stringers

long-time protection of steel. Painting may be justified in localities with high precipitation and salt-water spray. (See par. 197.)

- 13. CONNECTIONS. a. Timber. Nailed, drifted, and bolted connections are used exclusively. Special timber connectors are not required for these designs.
- **b. Steel.** Details are provided for three methods of making splices and connections.
- (1) Bolting (a) Structural ribbed bolts (table LXXVII), %-inch diameter can be used for all splices, stiffeners, and diaphragms.
- (b) Standard machine bolts (table LXXV), can be used for temporary connections. If standard machine bolts are used in stringer or column splices, bridge ratings must be reduced. (See par. 224.)
- (2) Riveting. All permanent connections, except pinned and welded connections, are designed for \(\frac{7}{8} \)-inch structural rivets. Structural ribbed bolts and rivets can be used interchangeably. Rivets are listed in bills of materials. Structural ribbed bolts of appropriate length may be substituted. (See table XLIV.)
 - (3) Welding. (a) Structural welding is used for:
 - 1. Clips welded to tops of beams for attachments or nailers.
 - 2. Shims to support nonuniform stringers.
 - 3. Base plates welded to tower columns.
 - 4. Attachment of tower bracing connections.
 - 5. Splicing of tower bracing rods.
- (b) Welded designs are also prepared as alternative to bolted or riveted construction for all fabrication of structural steel.
- 14. PERSONNEL TRAINING AND QUALIFICATIONS. a. Simple bridges with only abutments, bents, and short spans can be built by troops trained in the use of common tools and supervised by officers and noncommissioned officers experienced in building minor structures.
- **b.** Bridges with high towers and long spans require troops trained in steel fabrication, timber framing, and erection, and officers and noncommissioned officers experienced in supervision of heavy timber and structural steel work. The experience and necessary qualifications of troops and supervisors employed on big bridges must not be minimized.
- c. The labor estimates in chapters 3 and 8 assume troops are adequately trained in steel-bridge construction. Although these man-hour tables do not include operators who accompany equipment, such operators must be fully trained in use of the special organic or class IV equipment.

CHAPTER 3

ADVANCE PLANNING

- 15. PURPOSE. The information given in this chapter will aid in advance staff planning of trestle-crossing requirements and in developing stock-pile needs.
- 16. BRIDGE REQUIREMENTS. General requirements for trestle crossings in theaters of operations are determined from the basic information supplied by intelligence sources, reconnaissance maps, aerial surveys, and hydrological

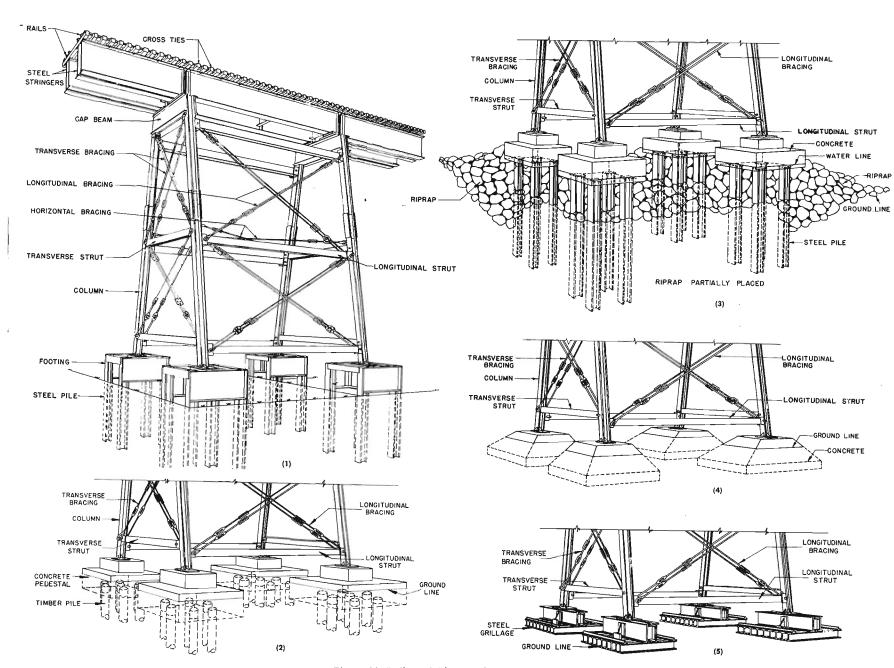


Figure 20. Railway bridge, steel stringer spans, steel tower:

- (1) On steel frames, steel piles.
- (2) On concrete pedestals, timber piles.
- (3) On concrete pedestals, steel piles.
- (4) On concrete pedestals.
- (5) On steel grillages.

reports. From these data, estimates are made of:

- a. Number and character of trestle crossings required in the theater.
- b. Probable length and average height of bridges required at these crossings.
- c. Crossings that can be made with the designs given in this manual. The kinds of crossings for which these designs can be used are described in chapter 2
- d. Type of construction suited to each crossing.

- 17. SELECTION OF TYPE. a. Conditions for which the different types of construction are best suited are:
- (1) Spans on pile bents. Best where short spans can be used, as in shallow streams, swamps, tidal waters, and floodways in wide valleys. (See table XVII.) They are usually not economical if piles must be over 60 feet long.
- (2) Spans on pile piers. Best for bridges of intermediate height and longer span (table XVII) across narrow streams and floodways.

TABLE IV. Sizes and principal uses of steel in semipermanent bridges.

Abbreviations: 50S, class 50, single-lane. 50D, class 50, double-lane. 25D, class 25, double-lane. RR, railway.

- (3) Spans on framed towers. Used for high bridges. (See table XVII) across deep valleys and ravines.
 - (a) On pile footings in soft, marshy, or loose sandy soil.
- (b) On spread footings in firm soil, compacted sand, gravel, boulders, and rock.
- (4) Timber spans. Designs limited to 15-foot-long highway spans and 16-foot-long railway spans.
- (5) Steel spans. Use required for all spans exceeding length limit for timber spans.
- b. Except where span length is the controlling factor, choice between timber and steel is based on economy in construction, materials and equipment available, transportation and skill of construction forces.
- 18. CLASS IV MATERIALS USED IN BRIDGES. a. Timber. Sizes, lengths, and principal uses of timbers required in all construction units (par. 8) provided by the manual are listed in table III.
- b. Steel. Rolled steel shapes required in all units of construction and their principal uses are tabulated in table IV.

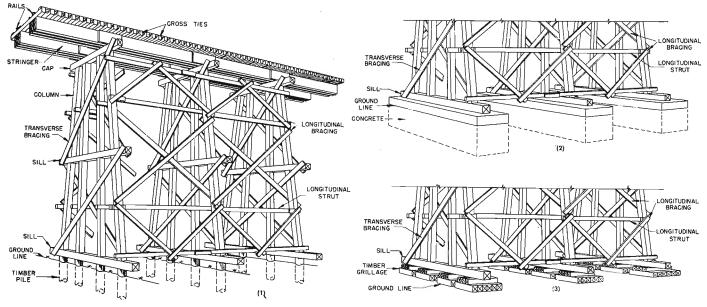


Figure 21. Railway bridge, timber stringer spans, framed timber tower:

- (1) On timber sills, timber piles.
- (2) On concrete pedestals.
- (3) On timber grillages.

- 19. EQUIPMENT USED IN CONSTRUCTION. Tools and equipment normally needed to construct semipermanent highway and railway bridges of stockpile materials are listed in table XXXIA.
- 20. COMPARATIVE ECONOMY OF BRIDGE TYPES. Tables V to VIII inclusive give material quantities and man-hours of labor required per foot of bridge to build each type and height of structure for which designs are provided. These tables permit quick comparison of the economy with which different types of bridges of the same height can be built, and aid in selecting the bridge type best suited to material, transportation, and personnel available in the theater.
- 21. ESTIMATES. Quantities of principal materials and man-hours of labor needed to build a bridge of any type covered in the manual are estimated in the following manner:
- **a.** Length and average height are approximated and type is selected. (See par. 16.)
- b. Unit quantities for the type and average height of the bridge are taken from tables V to VIII inclusive, and are multiplied by the bridge length. The quantity allowances for end spans and abutments given in the tables are added or subtracted as shown.
- 22. ANTICIPATING STOCK-PILE NEEDS. a. Estimates of materials of each kind needed for the bridges in the theater are obtained by approximating the number of each unit of construction required; that is, the number of each type of foundation unit, the number and average height of each type of tower unit, and the number and length of each type of span required. From the bills of materials given on the detail drawings for each unit, quantities of all materials needed to build that unit are taken. These quantities are multiplied by the number of units to be built in the theater. Quantities are combined into lists of stock-pile requirements.

Caution: In preparing lists of stock-pile requirements, allowance must be made for loss and damage in transit.

b. Because the designs are flexible, alternatives are provided, and identical sections can be used in different units, final construction can deviate widely from original estimates without wasting stocked materials.

CHAPTER 4

DESIGN SPECIFICATIONS

Section I. GENERAL CONDITIONS

- 23. LOADS AND FORCES. The bridges in this manual are designed to withstand various combinations of the following loads and forces:
- a. Dead load. The weight of the bridge itself.
- **b. Live load.** The weight of traffic on the bridge, including troops, vehicles, or trains.
- c. Impact. The dynamic effect of moving live load expressed as a percentage of the live load.
- d. Longitudinal forces. Horizontal longitudinal forces representing the

effects of wind and of the motion, stopping, or starting of vehicles or trains on the bridge.

- e. Lateral forces. Horizontal lateral forces representing the nosing effect of the locomotive and the effect of wind on the structure and on live load for railway bridges and the effect of wind on the structure only for highway bridges.
- 24. DEAD-LOAD WEIGHTS. Weights used in computing dead loads are: Steel—490 pounds per cubic foot.

Timber—50 pounds per cubic foot.

Concrete—150 pounds per cubic foot.

Rails and fastenings—200 pounds per linear foot of railway bridge.

- 25. WIND FORCES ON BRIDGES. The bridges are designed for a lateral wind load of 30 pounds per square foot on 1½ times the area of the bridge as seen in elevation. This represents the effect of an 85-mph wind. They are also designed for a longitudinal wind load of 15 pounds per square foot on 3¼ times the area of spans as seen in elevation and on 1½ times the area of towers and bents as seen in cross section. See paragraph 38 for wind forces on live load.
- 26. EXPANSION AND CONTRACTION. No provision is made for expansion and contraction of timber spans. Steel stringers are fixed at one end with slotted holes at the other end to allow for changes in length resulting from temperature variations between 120° F and —30° F. Stresses due to expansion and contraction are disregarded.
- 27. FOOTWALKS. Walks are not part of the basic designs for highway and railway bridges. Footwalks, which may be added to all bridges, and refuge bays for railway bridges are designed for pedestrian loads of 85 pounds per square foot. Increased stresses in stringers and supports to which footwalks are attached are disregarded.

Section II. HIGHWAY CLEARANCES AND LOADS

- **28. BRIDGE CLASSES. a.** Highway bridge designs in this manual include the following classes:
 - (1) Class 50, single-lane bridge.
- (2) Class 50, double-lane bridge, usable also as class 80 single-lane bridge.
 - (3) Class 25, double-lane bridge.
- b. The hypothetical vehicles used for designing these bridges are shown in figures 22 and 23. All weights and loads are in short (US) tons of 2,000 pounds. Assumed spacing of vehicles is 90 feet center-to-center. The hypothetical class 80 vehicle is a tracked vehicle 14 feet 8 inches wide with 14 feet 0 inches ground contact and 36-inch tracks.
- 29. CLEARANCES. a. The width between curbs is:

Double-lane bridges	22'-0"
Class 50, single-lane bridge	12'-6"
Class 25, single-lane bridge	
	included)

b. The height of curb is 10 inches for all bridges.

c. Abutments are designed for the following widths between edges of approach-road shoulders:

Double-lane bridges	26' 0"
Class 50, single-lane bridge	16'-6"
d. Handrails are 3 feet high. The width between handrails is:	
Double-lane bridges, timber stringers	23′-8″
Double-lane bridges, steel stringers	22'-8"
Class 50, single-lane bridge, timber stringers	
Class 50, single-lane bridge, steel stringers	13'-2"

- 30. LIVE LOAD. a. Highway bridge floors are designed for the tracked-vehicle and wheel loads given in table IX for class 25 and 50 loadings.
- **b.** Stringers and supports are designed for the loadings shown in figure 22 for class 25 and in figure 23 for class 50.
- (1) The axle and track loads of critical vehicles shown in the figures determine maximum shears and reactions.
- (2) The diagrams show concentrated load equivalents used in computing bending moments. Concentrated load equivalent (CLE) is the single-axle load which at midspan causes the same maximum moment as the actual vehicle. (See par. 211, FM 5–10.)
- c. Lateral distribution of track or wheel loads on stringers is assumed to be the following:
- (1) For interior stringers, fraction of track or wheel load carried by each stringer is:

		3" tread 4" deck
(a) For single-lane bridges	S	<u>s</u>
()	4.5	5.0
(b) For double-lane bridges	<u>s</u>	S
(-)	4.0	4.25

Where, S=average spacing of stringers in feet.

- (2) For an outside stringer, load equals reaction of the track or wheel load, assuming the deck to act as a simple beam between stringers.
- 31. IMPACT. Impact loads are assumed to be 15 percent of live load. Impact loads are applied in designing all steel members except steel piles; they are disregarded for all timber members, piles, and foundations.
- 32. TRACTION AND BRAKING FORCES. In addition to longitudinal wind forces given in paragraph 25, highway bridges are designed for a horizontal longitudinal braking force equal to 5 percent of the live load acting at the surface of the bridge floor. This force represents the effect of moving, starting, and stopping vehicles on the bridge.

Section III. RAILWAY TRACK AND LOADS

- 33. GAUGE AND CLEARANCE. a. Railway bridges are designed for standard 4-foot 8½-inch gauge track. The same designs are used for narrower track. Placing of rails for 1-meter (3-foot 33%-inch) gauge track is shown on the drawings.
- **b.** The structure gauge or clearance of bridge parts for standard track is shown on figure 24. Only handrails and braces for footwalks and refuge

TABLE V. Class 50, single-lane highway bridges. Approximate quantities per linear foot of bridge.

Combination		1			2			:	3			4			_	5				6				7				8			9			10			11				12			13			14			15	
Distance grade		per string mber pil bents			el string steel pil bents			timbe	tringers, er pile iers			el string steel pil piers		tis	eel strin nber tov sill, tin	vers, ti	mber	s	teel to	wers, co	s, frame oncrete ber piles		Steel s tower	tringers, s, concre steel p	te pedes	tals.	Steel ste ste steel fra	el cower	rs.	framed tin	oer string timber t mber sill mber pile	owers,	framed ti	r stringe imber to te pedes	wers,	frame	teel stri ed timbe acrete pe	r towers	•	fram	teel stris sed steel screte pe	towers,		Timb string framed to cowers, t grilla	timber f	framed t	el stringers timber tov ser grillag	wers.	framed	stringe steel to l grillag	wers,
to ground (feet)	Timber piling ² (1 in. ft.)	Timber (mbm)	Man- hours	Metal ² (lb.)	Timbe (mbm	Man- hours	Metal (lb.)	Timber	Timber piling ² (1 in. ft.)	Man- hours	Metal (lb.)	² Timbe	Man hour	Meta (lb.)	Timber (mbm)	Timber piling (1 in ft.)	Man- hours	Metal (lb.)	Timbe (mbm	er pilin	er Con- g ² crete (cu. yd.)	Man-	Metal ² (lb.)	Timber (mbm)	Concrete (cu. yd.)	Man- hours	Metal ² (lb.)	Timber (mbm)	Man- hours	Timber	Timber piling ² (1 in. ft.)	Man- hours	Timber (mbm)	Con- crete l (cu. li yd.)	Man- I	Metal T (lb.)	'imber	Con- crete M (cu. h yd.)			Timber (mbm)	Con- crete (cu. yd.)	Man- 7 hours ((imber (mbm)	Man- hours	Metal (lb.)	Timber M (mbm) h	Man- 1 nours	Metal (lb.)	Timber (mbm)	Man- hours
10 20 30 40 50 60 70 80 Add per bridge	7.2 10.7 12.5 +140	.18 .22 .22 +0.7	8.7 9.5 9.5 	573 583 +10,00	.16 .15		315 3728	.19 .188 +0.7		10.28 	813 830 +300	.15	22.1 23.0 -10	270 320 415 472 508 584 738	 .30 .34 .37 .39 .40 .42 .44 -5.0	7.1 5.8 4.9 4.3 3.8 3.4 3.0 +90	23.0 25.7 26.6 29.7 31.5 33.2	582 620 766 813 892 950 1,134 —10,00	.15 .15 .15 .15 .15	4.6 4.6 4.0 3.6 3.2 2.9 3.3	.29 .29 .25 .22 .20 .18 .19 -10	23.5 25.2 27.6 26.9	840 868 945 1,001 1,080 1,200 1,2%	 .15 .15 .15 .15 .15 .15 .15 .15	 .29 .29 .26 .23 .20 .19 .17 -10.0	21.2 22.0 26.2 27.7 29.8 29.2 33.4 -200	955 970 1,036 1,082 1,165 1,275 1,458 —5,000	 .15 .15 .15 .15 .15 .15 .15 .15	26.3 27.9 29.9 29.2 31.0 33.8 35.1 -300	 .35 .42 .49 .56 .64 .70 -1.0	5.3 5.3 5.3 5.3 5.3 5.3 5.3 +220	16.5 20.0 23.5 27.3 31.0 34.1 -40	 .29 .35 .42 .49 .56 .64 .70	.67 .67 .72 .72 .80 .80	27.7 33.6 34.4	321 415 472 508 585 740 740	 .27 .31 .34 .36 .38 .40 .44 -7.0	.66 1 .64 .56 .48 .50 .50 .46	19.1 24.9 28.2 30.3 31.4 35.5 37.2	582 620 766 804 892 950 1,134	.15 .15 .15 .15 .15 .15 .15	.37 .41 .36 .33	16.8 18.3 23.1 25.6 28.3 27.5 32.0 +80	 .32 .39 .46 .53 .61 .68 .74	11.1 13.9 17.0 20.1 23.7 26.9 29.5		.35 1 .38 1 .41 2 .42 2 .44 2 .45 2 .46 3		798 838 955 972 1,083 1,123 1,294 -17,000	.15 .15 .15 .15	16.8 17.7 22.5 24.4 27.5 27.1 31.6 100

TABLE VI. Class 50, double-lane highway bridges. Approximate quantities per linear toos of bridge.

																																					,		_	$\overline{}$	$\overline{}$	$\overline{}$			$\overline{}$				_
10	12.0		10.4	860	.23		528		12.0		1,190	.21	29.3										****								_				_ _	_ -	.	. .=		=	-	27.6		160				25 23	26.8
2 0	16.0		12.2	915	.22	17.2	6128	.268	12.08	15.78	1,325	.21	34.2	478	.44		26.3	956	.22	4.6	.29	25.6	1,200	.22	.29	27.8	1,334	.22	31.8	.45	8.0	16.8	.45	1.04 2	2.0 47	78 .4	4 1.2		9/1	1.43		27.6	.51	10.0	4/0	.51 27	7.0 1 1,2	22	27.0
30	20.0	.38	13.4			-					****			547	.47	8.7	27.2	990	.22	4.6	.29	25.5	1,230	.22	.29	29.4	1,370	.22	33.4	.53	8.0	20.5	.53	1.04 2		47 .4	7 1.0	3 32.5	990	, ,44	.52	26.8	.59	19.8	547	.53 25	3.8 1,34	20 .22	32.0
40]								740	.51	7.4	33.0	1,210	.21	5.0	.29	32.6	1,425	.22	.25	34.0	1,545	.21	37.4	.62	8.0	24.3	.62	1.04 25		40 .5	1 0.9	0 38./	1,210		.40	35.3	.00	27.5	910	.5/ 51	76 15	10 22	35.5
50					l –				****	*		****		810	.54	6:4	38.6	1,245	.22	4.5	.26	35.7	1,435	.22	.23	37.4	1,545	.22	40.5	.71	8.0	28.4	.71	1.11 3	4.4 81	10 .5	4 0.8		1 360		7,40	38.9	1.77	1 33.0	810	.50 1	00 16	15 22	38.0
60											****			810	.61	6.4	41.7	1,360	.22	5.3	.32	39.5	1,550	.22	.23	40.0		.22	42.9	.80	8.0	32.6	.80	1.11 30	8.6 8	0 0	0.8	0 4/./	4,500		1.40	30.9	.07	36.0	020	.67	48 16	54 22	40.2
70	****													920	.63	5.6	45.5	1,425	.22	4.8	.28	41.1	1,595	.22	.20	41.9	1,690	.22	44.5	.90	8.0	36.9	.90	1.21 4	5.7 92	20 .0	0.8	4 31./	1,425		1 .43	41.0	1.90	30.3	920	.07	7.5 1.7	55 22	42.5
80							****		****					920	.68	5.6	48.2	1,526	.22	4.8	.28	43.7	1,695	.22	.20	44.1	1,791	.22	46.8	.98	8.0	40.3	.98	1.21 4		20 .6	8 0.8	4 54.5	1,526		1,43	43.0	1.04			.73	150 - 26	نئت اس	9 -300
Add per brids	e. +18	0 +1.2	≀ +50	+10,00	十2.2	+170	٠	+0.6	60		+2,400) +2.2	60		8.0	+100	-500 ·	-15,000	+2.9	+260	-10.0	-300	-1,000	+2.2	-10.0	0 - 200	-6,000	+2.2	-300	-1.0	+300	-100	-4.0 -	+49.0 +	300 .	-1	.0.0 + 2	7.0 -200) 15,0	00	+ 40.1	1 +100) -		- -	-7.0 -	.330 - 20,	,000 74.	/ -300
			1		1	1 1		1		1		1	1							·				1		1	1	1 '					- 1		- 1		- 1	- 1		- 1	1	1	1	1 1	1			<u>l</u>	

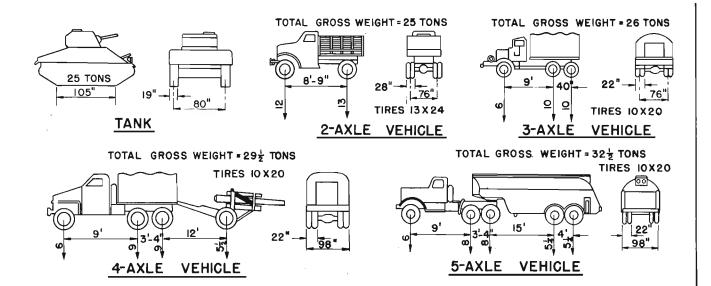
TABLE VII. Class 25, double-lane highway bridges. Approximate quantities per linear foot of bridge?

10 20 30	8.0 10.7 13.3	.26 .32 .32	8.3 10.0 10.8		.24	20.0	431	.29	8.	0 14	.9 .8 ³ 1	883 ,040	.21	26.7 31.0	392 577	.38	5.8	20.2 28.2	760 860		4.6		23.1	1,002	.23	.29	26.3 31.0	1,138 1,150		29.7	.38	5.3	13.8 17.0	.38	.67 .67	17.1	392	.38	.66	23.5	758	.23	.42	22.5	.41	13.4	392	.42	19.3	975	.23	22.0
40 50 60 70											1				577 669 669 760	.43 .45 .52	4.3 3.8 3.8	30.6 35.1 38.0 34.0	968 1,031 1,130 1,195	.22	3.6 3.2 3.2 3.6	.22	30.6 33.1 35.6	1,150 1,201 1,300	.22	.23 .20 .20	33.4 35.8 38.0 33.5	1,238 1,296 1,395 1,435	.22	33.6 35.9 38.0 40.1 35.7	.52 .60 .68	5.3 5.3 5.3	20.3 23.9 27.5	.43 .52 .60 .68		24.2 27.7 32.0	530 575 575 670	.43 .49 .52	.56 .56 .57		976 996 1,105	.22	.37 .40 .40	20.7 29.4 31.9 34.3	.49 .56 .64 .72	19.9 23.4 27.2	575 575 670	.44 .46 .52 .55	30.0 32.6 37.6	1,045 1,135 1,165 1,282		30.0 30.8 35.2
Add per brid	ge. +200	+1.1	+50	+12,00	0 +2.	2 +20	0	+0.9	+4	0 +	40 +	2,400	+2.2		830	.53 -6.0	3.1	38.3	1.310	+2.6	33	.19 -10.0	36 0	1,445	.21 +2.2	.17 -10.0	18 1	1,525 -1,000	.21 +2.2	1 4AA 9 J	.83 -1.0	5.3 +280	34.1 -100	.83 +1.5	.80 -10	35.8 38.7 	830	.53 -9.0	.46 +38.0	42.0	1,158 1,290 13,000	.22	.33	36.8 34.2 +200	.87 	33.9	830 —	.55 -5.0	33.7 38.0 -200	1,385 1,500 - 20,000	.22	37.0 34.3 100

TABLE VIII. E-45 railway bridges. Approximate quantities per linear foot of bridge!

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10	7.5	.11	5.2	765	.0	4 27	2 236	.09	13.	7 12.0	1,0	30 .0	14 29.	.0					***			-						****														1			****						
20	10.0	.15	5 6.6	840	.0	4 22	4 295	.104	1 12.5	54 12.1	14 1,3	0. 14	14 32.	.3 288	.20	6.15	17.5	632	.04	7.38	.44	21.8	890	.04	.31	22.4		.04	26.7	.23	5.0	12.0	.23	.91	18.0	274	.21	1.15	25.3	620	.04		22.0	.27	16.6	274	.26	17.7 1,0	000 .	.04	21.1
30	12.4	.15	5 7.3			_	.	l _				.	.,	. 326	.25	8.56	21.4	682	.04	8.60	.57	24.5	940	.04	.31	24.0	1,090	.04	28.2	.30	9.2	17.3	.30	1.00	21.7	274	.28	1.28	30.3	680	.04	.80		.35				21.4 1,1			
40		` l	.				. _					.		. 326	.32	8.57	25.2	875	.04	8.60	.57	28.8	1,090	.04	.31	28.3	1,235	.04	32.4	.37	9.2	20.9	.37	1.20	27.7	295	.35	1.46 1.52	35.3	825	.04	.80						24.6 1,2			
50	I _		.			_ l	. _	-			_	.		_ 404	.38	10.15	31.6	925	.04	9.14	.53	33.0	1,165	.04	.29	31.4	1,300	.04	35.3	.43	9.2	24.2	.43	1.35	31.8	334	.40	1.52	38.5	925	.04	.86		.49				28.6 1,3			
60	·	l	.					_		ļ		.	.,	. 404	.45	10.15	35.3	1,068	.04	11.45	.99	39.5	1,310	.04	.29	35.7	1,445	.04	39.5	.50	9.2	27.9	.50	1.35	35.5	334	.48	1.66	44.0	1,070	.04	.86		.56	26.4	334	.55 3	32.8 1,5	500	.04	34.9
70					- 1	_						.		. 512	.50	9.50	39.4	1,182	.04	11.80	.92	42.2	1,410	.04	.27	37.9	1,530	.04	40.1	.58	9.2	31.7	.58			410	.53	1.75	50.0	1,185	.04	.80		.67	31.7		.60	37.8 1,5	590	.04	37.1
80		"							1		1	.		. 512	.57	9.50	43.2	1,328	.04	11.80	.92	46.4	1,550	.04	.27	42.0	1,680	.04	45.5	.64	9.2	35.0	.64	1.47	43.7	410	.60	1.75	53.7	1,325	.04	.80	42.5	.73	34.8	410	.67	41.5 1,3	730	.04	41.2
Add per brid	oc +14	n Lin	4 1 76	1 +2,9	ت∔ ا ۱۰۰	ï 2	00	+ 19	1 + 10	57 1-30	0 -19	$\infty + 1$	1.2 -5	00	-6.0	+340	-300	-12.00	1 +2.1	+200	-23.0	ol —400	-4.000	+1.2	-12.0	-200	- 10.00	0 +1.2	-300	-2.0	+153	-100	I	-16	-200	_	8.0	+2.0	300	-10,000	L	+15.0	-200	-1.0 -	-100	-	6.0 -	-400 - 2	5.000 H	-3.1	-400
read por bird	1.1	" ' "	۳' ۱	′	~ I ' .	-		' ''	´ ' ``	" '1	" <i>"</i> "	, ,				1,3.	"	,	1 , =	,		-	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1.	"			1 '	-		'		1					1 · 1	-	· 1		(

¹ Quantities shown are based on recommended span lengths shown in the selection diagrams, tables XVII to XXIV.
2 Pile length based on 20-foot penetration.
3 For height of 18-feet.
4 For height of 15-feet.



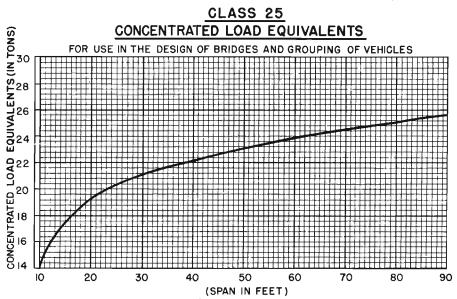
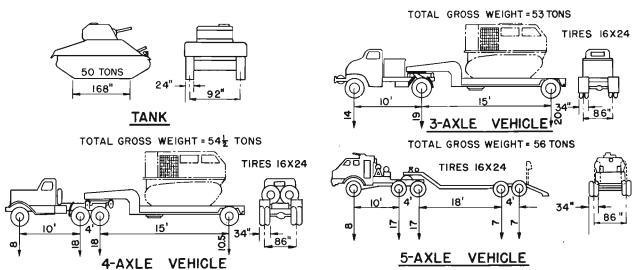
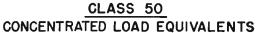


Figure 22. Class 25, track, axle, and wheel loads, and concentrated load equivalents for design of military bridges, 10- to 90-foot spans.

bays extend above track. Handrail is 12 feet from bridge center line.

- c. Abutments are designed for a 15-foot-wide embankment.
- **34.** LIVE LOAD. These bridges are designed for Cooper's E-45 loading and a maximum speed of 40 mph. Figure 24 shows details of this loading and the relation between Cooper's loadings and British standard unit (BSU) loadings. Cooper's E-45 is equivalent to BSU 20. Note that British loads are given in long tons (2,240 pounds).
- (1) Structure-clearance diagram for straight track.
- (2) Locomotive and train, Cooper's E-45 loading.
- (3) Alternative concentrated loads for short spans.
- (4) Relation between Cooper's E- loading and British standard unit (BSU) loading.
- (5) BSU 20 loading.
- 35. IMPACT. Impact loads are assumed to be a percentage of live load as





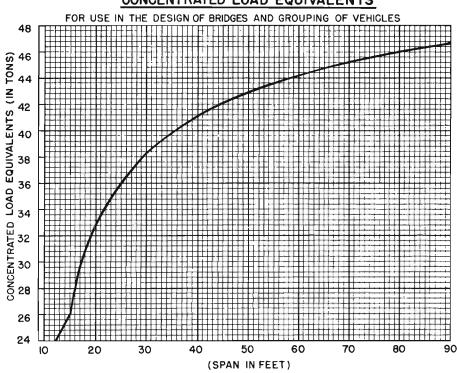


Figure 23. Class 50, track, axle, and wheel loads, and concentrated load equivalents for design of military bridges, 10- to 90-foot spans

expressed by the formula: l=100 - 0.60 L Where,

- I = percent addition to static live load.
- L = length of span in feet.

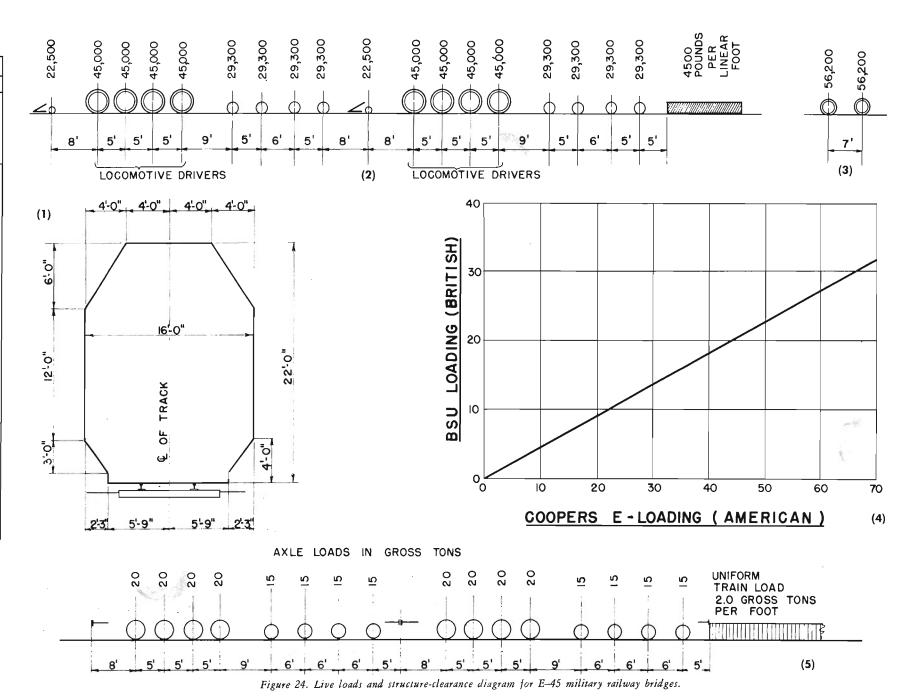
This impact load includes the effects of uneven rail joints and unbalanced locomotive driver wheels. Impact loads are applied in designing all steel members except steel piles; they are disregarded for all timber members, piles, and foundations.

TABLE IX. Track, axle, and wheel loadings for design of flooring of military bridges.

Bridge classification	Class 25	Class 50
Clear roadway	128"	150".
Track vehicle:		-
Weight of critical tank	25 tons	50 tons.
Length of ground contact	105"	168".
Width of each track	19"	24".
Distance c to c of tracks	80"	92".
Axle load:		
Single axle:		
Axle load	13 tons	20 tons.
Wheel:		
Width		34".
Number of tires	4 (dual)	4 (dual).
Width out-to-out of wheels	100"	124".
Bogie axle:		
Maximum axle load when total num-		
ber of axles are:		
3	10 tons	19 tons.
4	9 tons	18 tons.
5 or more	8 tons	17 tons.
Wheel:		
Width	22"	34".
Tires (dual)		16 x 24.
Spacing, c to c		86".
Width out-to-out of wheels		120".
Axle spacing	40"	48"
Wheel load:		•
Single tire:		
Load	4 tons	5 tons.
Tire size	16 x 24	16 x 24.
Dual tire:		
Load		
Tire size		16 x 24.
Wheel width	28"	34".

Note: Loadings for class 80 bridges are described in paragraph 28.

- 36. NOSING OF LOCOMOTIVES. To withstand the effect of nosing of moving locomotives, bridges are designed for a concentrated moving horizontal lateral force of 20,000 pounds applied at top of rail at any point in the span. Vertical effects of this lateral force are disregarded.
- 37. TRACTION AND BRAKING FORCES. In addition to longitudinal wind forces (par. 25), railway bridges are designed for a horizontal longitudinal force representing the effects of train traction or braking. The design force used is the larger of the following:
- a. Twenty-five percent (25%) of the weight on locomotive drivers, representing traction effect.
- b. Fifteen percent (15%) of the total live load on the bridge, representing braking effect.
- **38.** WIND ON TRAIN. In addition to the lateral wind forces (par. 25), railway bridges are designed for a lateral horizontal wind load of 300 pounds per foot of track applied 8 feet above top of rail. This force represents the effect of wind on the side of a train on the bridge.



Section IV. MATERIALS AND WORKING STRESSES

39. STEEL MATERIALS. a. Structural and rivet steel. The designs are based on steel with the following physical properties:

	Structural	Rivet: steel
Tensile strength (pounds per square inch=psi)	steel 60,000= 72,000 psi	52,000= 62,000 psi
Minimum yield point, one-half of tensile strength but not less than	33,000 psi	28,000 psi

These properties are characteristic of the American structural steel normally available in depots. Where steel of uncertain origin or lower strength is used, load capacities must be reduced in proportion to the lower yield point, or the size of members and connections shown on the drawings must be increased. This must be done because of the relatively high allowable working unit stresses (par. 40) used in the designs. For example, a basic tensile working stress of 27,000 psi has been adopted for semipermanent military bridges, as compared to 18,000 psi used for civilian highway and railway bridges. (See table L for moments and shears.)

b. Structural ribbed bolts. Structural ribbed bolts (table LXXVII) are made of steel having a tensile strength of 70,000 psi. They are \%-inch size

with 15 longitudinal ribs and .95-inch outside diameter of the ribbed shank and are used in 15/16-inch holes. They have full buttonheads and are threaded with special screw threads for 7/8-inch self-locking nuts 11/8 inches thick.

- c. Machine bolts and nuts. (table LXXV). Designs using black or unfinished machine bolts are based on common bolts with a yield point of approximately 45,000 psi.
- d. Welding rods and electrodes. Welding rods for oxyacetylene welding are mild-steel rods. Electric-arc welding electrodes must be heavily coated, mild-steel, shielded-arc electrodes for all-position, general-purpose work. They are used with reverse-polarity (electrode positive) direct-current welders.
- 40. STEEL WORKING STRESSES. Steel bridge designs in this manual are based on the allowable working unit stresses shown below. These stresses are not exceeded by any combination of design loads and forces excluding lateral and longitudinal forces. Where lateral and longitudinal forces are considered in combination with other loads and forces, allowable working unit stresses 15 percent higher than those listed below are permitted. All stresses are in pounds per square inch unless otherwise noted.

a. Structural and rivet steel. (1) Tension. Axial tension on	net section.
(a) Structural members	27,000
(b) Machine bolts, at root of thread	20,000
(2) Axial compression. On gross section	
for length of member	—L inches
and radius of gyration	-r inches
(a) For values of L not greater than 140.	

1. Riveted or bolted ends	$22,500 - \frac{3}{8} \left(\frac{L}{r}\right)^2$
2. Pinned ends	22,500— $\frac{1}{2} \left(\frac{L}{r} \right)^2$

(6)	For values of \underline{L} over 140 but not
	to exceed 200, bolted or pinned ends.

to exceed 200, bolted or pinned ends.		56,000
		L^2
		1 + $\overline{_{5,750}}$
Compression, splice material	24,000	

24,000

(")	otimeners of place girders
(3)	Bending. On extreme fiber of rolled and
	built-up sections.

- - (Double-plank floors or laminated floors securely nailed and held to steel stringers by welded or bolted connections are assumed to furnish continuous lateral support.)

commuous faterar support.)	
(b) Tension on net section	27,000
(c) Pins, structural-grade hot-rolled steel	33,000
(d) Pins, cold-rolled steel	45,000

(e) Bolts	27,000
(4) Diagonal tension. In webs of girders of rolled beams; at sections where maxi-	
mum shear and moment occur simul-	
taneously	27,000
(5) Shear.	
(a) Girder webs, gross section	16,500
(b) Pins	17,000
(c) Power-driven rivets and structural ribbed	
bolts in tight-fitting holes	15,000
(d) Unfinished bolts	12,000
(6) Bearing.	
(a) Pins, steel parts in contact	33,000
(b) Power-driven rivets and structural ribbed	
bolts in tight-fitting holes	30,000
(c) Unfinished bolts	25,000
b. Welds. (1) Fillet welds. On throat area,	-
tension, compression or shear	9,600
(This is 425 pounds per linear inch of	
weld for each 1/16 inch of size.)	
(2) Butt welds. On weld area.	
(a) Shear	12,000
(b) Compression	16,000
(v) compression	-0,000

- 41. TIMBER MATERIALS. Timber bridge designs in this manual are based on use of seasoned, dry timber of American species of 1,400-pound stress grade as shown in table LVIII. This grade includes select structural Douglas fir, merchantable structural longleaf southern pine, or dense structural shortleaf southern pine. The designs cannot be used with unseasoned or wet timber and timber of lower grades, unless sizes and connections are increased or load capacities decreased proportionately.
- **42. TIMBER WORKING STRESSES.** The following allowable working unit stresses govern the design of wood members of bridges in this manual. These stresses are not exceeded by any combination of design loads and forces. (See par. 23.) Values are in pounds per square inch.

a. Extreme fiber stress in bending	2,100
b. Horizontal shear (parallel to grain)	150
c. Compression perpendicular to grain	500
d Compression parallel to grain on cross section of members	

d. Compression, parallel to grain, on cross section of members with:

length	L inches	
least dimension	d inches	
(1) For L — values not great	ter than 11	750
(2) For L — values over 11 b	out not greater than 21.5	750
\overline{d}	$\left[1 - \frac{1}{3} \left(\frac{L}{21.5 \text{ d}}\right)^4\right]$	

(3) For L — values	over 21.5	but not to	exceed 50.
\overline{d}			

 $\frac{535,000}{\left(\frac{L}{d}\right)^2}$

- 43. CONCRETE MATERIALS. Designs for concrete caps, footings, and abutments are based on unreinforced concrete having a 28-day compressive breaking strength of 2,500 psi. Concrete of this quality should have a maximum water-cement ratio of 61/4 gallons of water per sack of cement. (See ch. 8, FM 5–10, for detailed information on proportioning, mixing, placing, and curing concrete.)
- **44.** CONCRETE WORKING STRESSES. The following allowable working unit stresses govern the design of concrete parts of bridges in this manual. Values are in pounds per square inch.

a. Compression in pedestals, height to thickness ratios not to	
exceed 3 to 1	750
b. Bending stress in extreme fiber.	
(1) Compression	1,250
(2) Tension	
c. Shear	75
d. Punching shear	200
e. Bond to timber or steel piles	15

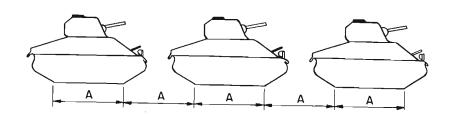
- **45. SOIL PRESSURES.** Designs for spread footings and abutments are based on soils capable of developing a safe allowable bearing pressure of 3,000 pounds per square foot. (See par. 70.) This value is used in proportioning footings for combinations of dead and live loads. However, for combinations of lateral and longitudinal forces with dead and live loads, a maximum bearing pressure of 4,000 pounds per square foot is allowed on these soils.
- **46. BEARING-PILE LOADS.** a. Designs for pile bents and piers, foundation piles, and pile abutments are based on piles driven to the bearing values shown on the drawings. Pile bearing values are determined in accordance with section III, chapter 12. The maximum pile loads in these designs are:
 - (1) Timber piles, 18 tons.
 - (2) Steel piles, 50 tons.
- **b.** These pile capacities are used for combinations of dead and live loads. However, for combinations of lateral and longitudinal forces with dead and live loads, permitted loads on piles are:
- (1) Timber piles, 25 tons.
- (2) Steel piles, 60 tons.
- **47. FIELD DESIGN.** Field designs are necessary for scaffolding, concrete forms, ramps, and other temporary construction: See TM 5–225 for detailed information on rigging and TM 5–226 for information on carpentry.

CHAPTER 5

CAPACITIES AND TRAFFIC CONTROL

- 48. NORMAL LOADS FOR CONTROLLED TRAFFIC. a. The normal movement of all vehicles across bridges is governed by military traffic regulations. The designs in this manual are based on controlled traffic having the following normal restrictions:
- (1) Weight-class of vehicles does not exceed posted capacity of bridges. For definition of weight class and equivalent weight class, see FM 5-10, paragraphs 239 and 245.

- (2) Vehicle spacing 30 yards, the closest military-vehicle spacing normally permitted.
- (3) Maximum speed 25 mph, normally not exceeded by heavy military vehicles. The vehicles may veer from side to side, and move in both lanes of double-lane bridges.
- (4) Only these normal restrictions are necessary when class 50 double-lane bridges are used for single-lane traffic by class 80 vehicles. (See par. 28.)
- **b.** The normal traffic regulations given in a cannot be violated without risk of overstressing these bridges.
- 49. POSTING BRIDGES. a. Bridges are marked with their capacity under controlled traffic as defined above. (See tables X, XI, and XII.) This is referred to as posted capacity, US class 50, or US class 25. Class 50 double-line bridges may also be posted as US class 80 for single-lane traffic only. (See par. 239 FM 5–10.)
- **b.** The hypothetical vehicles used as design loads for class 50 and class 25 bridges are shown in figures 22 and 23. The hypothetical class 80 vehicle is described in paragraph 28.
- **50.** OVERLOADS. a. Excessive stresses may be caused by:
- (1) Loads of weight-class exceeding posted capacity of the bridge if crossed without special traffic restrictions.
- (2) Loads less than or equal to posted capacity of the bridge crossed at excessive speeds or decreased spacing of vehicles.
- b. Loads of weight-class exceeding posted capacity are permitted provided additional traffic restrictions are enforced. For such overloads there are two types of crossing, each with special traffic restrictions:
 - (1) Caution crossing. (See par. 51.)



SPACING OF TRACKED VEHICLES FOR UNRESTRICTED CROSSING

CLASS	WEIGHT (TONS)	A (INCHES)
4	4 TONS	80"
99	9 TONS	80"
12	12 TONS	80"
16	16 TONS	105"
20	20 TONS	105"
25	25 TONS	105"
35	35 TONS	132"
50	50 TONS	168"
65	65 TONS	216"
80	80 TONS	264"

Figure 25. Tank loads used in rating bridges for unrestricted traffic.

- (2) Risk crossing. (See par. 52.)
- **c.** If normal traffic restrictions as to speed and spacing are violated, the bridge must be restricted to vehicles of weight-class less than normal posted capacity. Crossings of such decreased loads are known as *unrestricted* crossings.
- d. Design loads of the following weight-classes have been considered in rating the bridges for caution, risk, or unrestricted crossings: 80, 65, 35, 20, 16, 12, 9, and 4.
- **51. CAUTION CROSSING. a.** Overloads cross with *caution* if the following traffic restrictions are enforced:
- (1) Speed not over 5 mph, to reduce effect of impact.
- (2) Distance between vehicles at least 50 yards, to reduce load on spans.
- (3) Vehicle centered on bridge, to avoid overstress in outside stringers.
- (4) Single-lane traffic on two-lane bridges, to reduce loads concentrated near center line of roadway. (Note that this is the only restriction necessary to permit class 80 traffic (par. 28) on class 50 double-lane bridges. This is not a caution crossing.)
- (5) No braking or gear shifting on bridge, to reduce longitudinal forces on bridge.
- **b.** Maximum weight-classes of vehicles that can cross with *caution* are listed in separate columns in tables X, XI, and XII. If these vehicles comply with the restrictions in *a* above, allowable stresses given in chapter 4, section IV will not be exceeded.
- **52. RISK CROSSING. a.** Overloads cross with *risk* if the following traffic restrictions are enforced:
 - (1) Speed not over 3 mph.
 - (2) Only one vehicle allowed on bridge at a time.
- (3) Vehicle centered on bridge deck.
- (4) No braking or gear shifting on bridge.
- (5) Vehicle guided across bridge by man on foot to insure observance of restrictions (1), (3), and (4).
- b. Maximum weight-classes of vehicles that can cross with risk are listed in separated columns in tables X, XI, and XII. If these vehicles cross the bridge, the allowable stresses in section IV, chapter 4, are exceeded, even if all restrictions in a are observed. Such loads involve a definite risk of bridge failure, since the values of maximum permissible weight-class for crossing with risk have been computed using stresses at or near the yield point of the materials. Risk crossings should be permitted only on well-maintained bridges when specifically authorized by the responsible headquarters.
- **53. UNRESTRICTED CROSSING, DECREASED LOADS. a.** Normally, unrestricted traffic is not permitted on military bridges. If the situation requires or justifies relaxing normal restrictions, the maximum weight-class of vehicles must be reduced on long bridge spans. (See par. 53c.)
- b. The permissible weight-class of vehicles for unrestricted traffic was computed for columns of tanks of the weights, ground-contact lengths, and spacings shown in figure 25. The capacities for unrestricted traffic of single spans are listed in tables X, XI, and XII. The capacities for unrestricted traffic bridges of two or more spans are limited by the substructure capacities and are shown in tables XIII and XIV for combined lengths up to 180 feet of two spans on a common support.

- c. Capacity is not reduced for unrestricted crossings on:
- (1) Single-span, single-lane, class 50 bridges, up to 40 feet long. Single-span, double-lane, class 50 bridges, up to 50 feet long. Single-span, double-lane, class 25 bridges, up to 30 feet long.
- (2) Multiple-span, class 50 bridges, with combined length of two spans on a common support 53 feet or less.

Multiple-span, class 25 bridges, with combined length of two spans on a common support 35 feet or less.

54. CAPACITY TABLES. a. Superstructure. Capacities of spans, with timber stringers and steel stringers, are given in tables X, XI, and XII.

TABLE X. Single-lane, class 50 bridges, capacities of superstructures.

		Traffic condition			
Span length	Stringer	Controlled	With caution	With risk	Unrestricted
(feet)		Posted capacity ²	Maximum class of loading ²	Maximum class of loading ²	Maximum class of loading
11	Timber	50	80		50
13	Timber	50	80		50
15 .	Timber	50	80		50
15	Steel	50	80		50
20	Steel	50	80		50
30	Steel	50	80		50
40	Steel	50	80		50
50	Steel	50	80		35
60	Steel	50	80		. 35
70	Steel	50	80		. 25
80	Steel	50	80		20
90	Steel	. 50	80		20
ļ					

¹ To determine over-all capacity of bridge for unrestricted crossings, see table XIII for capacity of substructure.

TABLE XI. Double-lane, class 50 bridges, capacities of superstructures.

Span	Stringer		trolled capacity)2	Caution or risk one lane	Unrestricted¹ two lanes
length (feet)	Stringer	Two lanes	One lane	Maximum class of loading ²	Maximum class of loading
11	Timber	50	80		50
13	Timber	50	80		50
15	Timber	50	80		50
15	Steel	50	80		50
20	Steel	50	80		50
30	Steel	50	80		50
40	Steel	50	80		50
50	Steel	50	80		50
60	Steel	50	80		35
70	Steel	50	80		. 20
80	Steel	50	80		. 20
90	Steel	50	80		20

¹ To determine over-all capacity of bridge for "unrestricted" crossings, see table XIII for capacity of substructure.

² Capacity of substructure same as capacity of superstructure.

² Capacity of substructure same as capacity of superstructure.

TABLE XII. Double-lane, class 25 bridges, capacities of superstructures.

			Traffic	condition	
Span length	Stringer	Controlled two lanes	With caution one lane	With risk one lane	Unrestricted ¹ two lanes
(feet)		Posted capacity ²	Maximum class of loading ²	Maximum class of loading ²	Maximum class of loading
11	Timber	25	35	50	25
13	Timber	25	35	50	25
15	Timber	25	35	50	25
15	Steel	25	50	65	25
20	Steel	25	50	65	25
30	Steel	25	50	65	25
40	Steel	25	35	50	16
50	Steel	25	35	50	16
60	Steel	25	35	50	12
70	Steel	25	35	50	9
80	Steel	25	35	- 50	9
90	Steel	25	35	50	4

¹ To determine over-all capacity of bridge for unrestricted crossings, see table XIV for capacity of substructure.

- **b. Substructure.** (1) For "controlled," "with caution," and "with risk" crossings, the superstructure governs bridge capacity.
- (2) For "unrestricted" crossings, the substructure generally governs capacity. These capacities are given in tables XIII and XIV.

TABLE XIII. Class 50 bridges, capacities of substructures for unrestricted crossings.

Combined length of two spans on common support (feet)	Maximum class of loading	Combined length of two spans on common support (feet)	Maximum class of loading
53	50	105	16
58	35	120	12
68	25	160	9
84	20	over 180	4

TABLE XIV. Double-lane, class 25 bridges, capacities of substructures for unrestricted crossings, two lanes.

Combined length of two spans on common support (feet)	Maximum class of loading	Combined length of two spans on common support (feet)	Maximum class of loading
35	25	59	12
46	20	82	9
56	16	180	4

- **c.** Loads and stresses. Stresses caused by loads under "controlled," "with caution," and "unrestricted," are within the allowable limits stipulated in this chapter.
- **55.** APPLICATION OF CAPACITY TABLES. a. The capacity of a bridge depends on:
- (1) Longest span in bridge, for "controlled," "with caution," and "with risk" crossings.
- (2) Longest span in bridge or the longest combined length of two spans on a common support for "unrestricted" crossings.

b. To illustrate the use of capacity tables for determining over-all bridge capacity, reference is made to figure 35, chapter 9, showing a class 50 single-lane bridge.

Longest span = 50' (span 8)

Longest combined length
of two spans on a common support = 65' (span 7 + span 8 on pier 7.)

Posted capacity US Class 50 (See table X, column 3.)

Crossing
With caution US Class 80 (See table X, column 4.)

Since vehicles of the heaviest load classification can cross "with caution," no

"with risk" classification is required. For "unrestricted" crossings, bridge capacity is:

Superstructure Class 35 (See table X, column 6,

Superstructure

Class 35

(See table X, column 6, for 50-foot span.)

Substructure

Class 25

(See table XIII for loaded length not exceeding 65 feet.)

The capacity of the bridge under various classes of traffic control is then:

Traffic control Class of	loadi
"Controlled" (posted capacity)	50
"With caution"	
"Unrestricted"	25

PART TWO

CONSTRUCTION OPERATIONS

CHAPTER 6

SITE SELECTION, RECONNAISSANCE, AND SURVEYS

Section I. SITE SELECTION

- 56. GENERAL. a. Semipermanent bridges are usually built to:
- (1) Replace demolished bridges, bridges of limited capacity, or standard stream-crossing equipment.
- (2) Provide crossings at new sites for new routes or for relocated existing routes.
- **b.** If the bridge replaces a demolished structure, the original site is usually chosen so approaches and undamaged parts of the replaced bridge can be used. However, a bypass bridge may be more practicable where debris is difficult to move and damaged parts require extensive repair. (See fig. 26(2).)
- (1) Reconstruction by replacing demolished spans with timber trestle construction.
- (2) A new bridge with new approaches built alongside a partly demolished structure. Use of standing parts of the demolished bridge was not practicable because of its height and the large amount of debris to be moved.
- c. If a new location is chosen, alternate sites are considered and the advantages or disadvantages of each compared. The site should provide a suitable crossing at the least cost in time, labor, and material. Tables V to

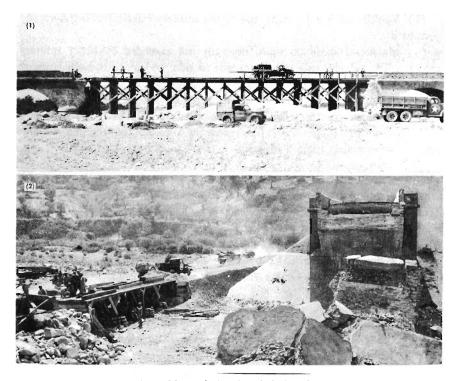


Figure 26. Replacing demolished bridges.

VIII give approximate quantities of labor and materials to help make comparisons. Important factors in site selection are discussed below.

- **57.** APPROACH ROADS. In comparing sites, the amount of construction involved in building access roads and approaches must be considered. Unless the crossing presents particularly difficult construction problems or requires a large structure, its location is usually less important than that of approach and access roads. Factors to be considered in location of roads are discussed in FM 5–10.
- **58.** ALIGNMENT. a. Bridge and stream. A site at which a stream can be crossed at right angles is best. Other crossings require longer structures with construction skewed or towers and bents set at an angle to the stream flow. Such crossings are to be avoided because skewed construction is more difficult, and towers and bents at an angle to the current obstruct the flow and tend to catch more debris than if parallel to the stream.
- **b. Bridge and approaches.** Alignment of a bridge and its approaches should be as straight as possible. (1) Curves on or close to railway bridges are avoided if at all possible, and in no event should curvature on a bridge exceed 6° 30.' With that curvature, train speeds must be limited to 20 mph.
- (2) Sharp curves in approaches to highway bridges must end at least 60 feet from the bridge, if it is to be crossed by long trailer units. Preferably, approaches are straight for 150 feet.
- **59. STREAM CHANNEL.** a. A site on a narrow, straight, and uniform reach of a stream is preferred because:
 - (1) A narrow channel requires a shorter bridge.
- (2) Banks of straight and uniform channels are less apt to erode and cave in. Erosion is particularly severe below sharp bends in a channel.
- (3) Islands or other obstructions interrupt smooth flow and tend to cause

² Capacity of substructure same as capacity of superstructure.

destructive cross currents during floods.

- **b.** Uniform depth of water is desirable because scour is less apt to occur during floods.
- c. Deep water requires special construction methods which are avoided wherever possible. The limiting conditions for construction outlined in this manual are given in paragraph 10.
- **60. FOUNDATION CONDITIONS. a.** Foundation conditions are an important factor in site selection. This manual provides foundation types for all conditions ordinarily encountered; their adaptation is discussed in chapter 7. Material, labor, and equipment requirements for foundations vary widely; requirements are given in chapter 8.
- **b.** Firm, gently sloping banks are preferred as they permit more efficient use of truck- and crawler-mounted erection equipment. Soft, muddy, or steep banks limit the efficiency of both men and equipment.
- c. Sliding or heaving banks should be avoided. Even the most substantial construction cannot successfully resist displacement by large masses of moving earth.
- (1) Slides are most often caused by the saturation and softening of heavily loaded layers of clay or mud. Evidences of their occurrence are easily recognized.
- (2) Heaving is usually caused by embankments overloading soft clay or mud. Except in the softest soils, it can be avoided by placing abutments well back of the bank line and by limiting the height of embankments.
- 61. CONSTRUCTION FACILITIES. The site should include a firm, level area suitable as a material and fabrication and framing yard. It should also have a nearby bivouac area for construction forces, and an access road over which materials, equipment, and supplies can be brought to the work.

Section II. RECONNAISSANCE

- **62. PURPOSE.** The purpose of a reconnaissance is to get the information necessary for selecting a site and for determining the type and principal features of the construction. If a demolished structure is to be replaced, the condition and extent of any standing parts that might be used in reconstruction should also be determined.
- 63. PERSONNEL. Reconnaissance for sites of semipermanent bridges should be assigned to an officer experienced in bridge reconnaissance. He must know what information is necessary and be able to recognize the relative importance of the various factors so he can compare sites. This requires that he be able to visualize at each prospective site the completed bridge and all principal steps in its construction. He must, furthermore, be thoroughly familiar with the communication requirements of the installation, and with the adaptability, limitations, and labor, material, and equipment requirements of various type bridges.
- **64. RECONNAISSANCE INSTRUCTIONS.** For general information on reconnaissance instructions, see FM 5–6. Reconnaissance instructions for these bridges should specifically cover the points listed below; if they do not, the information should be requested before going into the field:
 - a. Vehicle weight-class requirements.

- b. Number of lanes required.
- c. Minimum clearance requirements over canals, streams, roads, or railroads.
- d. Existing limitations on availability of construction materials and equipment.
- e. Availability and experience of construction troops.
- f. Time for construction.
- 65. PRELIMINARY STUDY. a. Review the requirements listed in the statement of theater construction policy. Gather all available information on the stream including maps and stream-flow data. Request stream data, particularly information on floods, from intelligence section. If a choice of sites is permitted, make an initial map study to determine which sites best fit the communication network. Ordinarily this study discloses factors which limit the choice of locations and suggests other factors requiring special investigation on the ground.
- **b.** Investigate the source and availability of materials and construction equipment; also the means of bringing these to the various sites. Determine limitations on construction imposed by lack of certain equipment or material.
- c. Preparations for reconnaissance include assembly of necessary surveying instruments, tools and transportation, including some means of crossing the stream if necessary. Picks, shovels, bars, mauls, rope, and an earth auger should be included for prospecting and sounding foundations. Photographic equipment is desirable to take pictures of the sites.
- **66. RECONNAISSANCE METHODS. a.** Reconnaissance should be as deliberate and complete as time permits. Through reconnaissance reduces the likelihood of picking a poor location or of having to abandon work because of unfavorable conditions not disclosed until construction is underway.
- **b.** Topographic features need not be obtained in great detail or with extreme exactness. They may be determined by stadia or with tape, compass, and hand level by survey methods described in FM 5–10 and TM 5–235.
- c. Stream characteristics are determined by observing velocity and evidences of flood heights on banks and buildings and of drift lodged in trees and brush. Where possible, these observations are supplemented by inquiry and checked against available stream-flow records.
- **d.** Foundation conditions are estimated by visual examination of exposed banks and by soundings in the stream bed.
- e. Location and alignment of approaches are determined by rough ground survey, by aerial survey, or by paper location on contour maps of the area.
- 67. RECONNAISSANCE REPORTS. A reconnaissance report in brief written form conforming to the general requirements given in FM 5–6 is submitted for each site. A form like that shown in table XV serves as a guide to prevent omitting important items from the investigations or from the report. To provide complete site information, maps, sketches, photographs, and brief descriptions should supplement the data on the form.

Section III. SITE SURVEY

68. PURPOSE. A detailed survey is made after the site has been selected from the information furnished by reconnaissance. Its purpose is to furnish exact information from which the bridge lay-out can be determined,

materials requisitioned, and construction procedure outlined. It is submitted as drawings of the site in plan and profile, with graphical presentation of subsurface conditions. (See fig. 27.)

- 69. TOPOGRAPHY. a. The center line of the bridge is established on the ground and reference points are established on it to which all topographic features are tied by survey. The survey should fix the location of all topographic features which may have bearing on lay-out or construction.
- b. The survey drawings should include the following:
- (1) Location map showing relation of the site to:
- (a) Communication routes.
- (b) Bivouac areas for construction troops.
- (c) Nearest water supplies.
- (d) Local sources of sand, gravel, timber, and other construction materials.
- (2) Detailed plan of the site to a scale of not less than 1 inch to 40 feet showing:
- (a) Alignment of the proposed structure and tentative position of towers, bents, and abutments.
- (b) Position of piers and abutments of any existing structure. If these are to be used in the new construction, enlarged details are attached giving complete measurements and notes on condition and repair needed.
- (c) Course of the stream with bank lines and direction and distribution of flow.
- (d) Natural features of the site such as caving banks, exposed rock ledges, dirt piles, drainage courses, and trees and wooded areas.
- (e) Works of man such as dikes, walls, fences, power and utility lines, sewers, drainage structures, buildings, and roads and streets.
- (f) Elevation contours extending at least 100 feet each side of the bridge center line and 200 feet beyond each abutment.
- (g) Location of all bench marks and their elevations; all reference points; and all borings and soil tests.
- (3) Profile to equal horizontal and vertical scales of not less than 1 inch to 40 feet, showing:
- (a) Ground surface on center line of the proposed bridge, extending not less than 200 feet back of each abutment.
- (b) Elevation of high and low water.
- (c) Foundation materials as disclosed by test pits and borings.
- 70. FOUNDATION INVESTIGATION. a. Rod soundings. Foundation conditions can be explored to depths of 12 to 15 feet with a pointed steel sounding rod. In soft ground, much greater depths can be reached.
- (1) Round rods 3/4 or 1-inch in diameter are used in lengths of 5, 10, and 15 feet. They are preferably driven with a sleeve driver, such as can be made by capping and weighting a short length of pipe. An 8-pound hammer can also be used. As the limit of each rod is reached, the rod is withdrawn and the next longer rod driven into the hole. Rods are pulled with a lever fastened to the rod with a chain. (See fig. 28.) They can be pulled more easily if first turned with a pipe wrench. Where soundings deeper than 15 feet are made, threaded rod sections are joined and driven with the aid of a clamped cross arm.
- (2) Differences in type, consolidation, and moisture content of soils penetrated by the rod are judged by the sound and speed of driving.
 - (3) In making soundings to bed rock through soils containing boulders

Reference Reconnaissance Instruction No
(See table 11, FM 5-6)
Purpose of reconnaissance:
Facility required.
(Single- or double-track railway and gauge; single- or double
lane highway, load capacity, and width between curbs; side
walks and widths)
Date and time of reconnaissance:
Date and time of report:
1. Stream crossed:
2. Designation of crossing:
3. Highway or railroad:
4. Near:
a. Distance:
b. Direction:
5. Bridge replaced:
a. Kind:
(Single- or double-track railway and gauge; single- or double
lane highway and width between curbs; sidewalks and
widths)
•
b. Type:
c. Load capacity:
d. Construction: (steel, timber, concrete, masonry)
(1) Substructure:
(2) Superstructure:
e. Span lengths:
f. Over-all length:
g. Maximum height above stream bed:
b. Height at abutments:
i. Alignment:
j. Grade:
k. Condition:
(1) Substructure:
(2) Superstructure:
1. Parts usable in new construction:
(1) Substructure:
(2) Superstructure:
m. Approaches:
(1) Alignment:
(2) Grade:
(3) Width:

or logs, at least three soundings spaced about 3 feet apart are made at each test to insure that soundings are not being stopped by an obstruction before reaching bed rock.

(4) A party of 3 men can make 15 to 20 soundings a day through 15 feet of usual alluvial soil.

b. Borings. For pile- supported construction, foundation materials must

	(4) Character of surface:
	(5) Condition:
6.	Stream characteristics:
	a. Depth:
	(1) Observed:
	(2) Low water:
	(3) High water:
	b. Width:
	(1) Observed:
	(2) Low water:
	(3) High water:
	c. Velocity:
	(1) Observed:
	(2) Low water:
	(3) High water:
	d. Flood periods and duration:
	e. Amount and character of debris carried during flood:
	f. Character of bed and banks:
	g. Height of banks:
7.	Foundation conditions:
	a. Stream bed:
	b. Right bank:
	c. Left bank:
8.	Topographic and man-made features:
	a. Buildings:
	b. Walls and fences:
	c. Utility lines:
	d. Wooded areas:
	e. Other features:
9.	
	a. Length:
	b. Character of ground traversed:
	c. Grades:
	d. Alignment:
10	. Construction features:
	a. Communication routes:
	(1) Designation or description:
	(2) Classification:
	(3) Width:
	(4) Character of surface:
	(5) Condition:

be investigated to depths of 20 to 40 feet to get the information necessary for requisitioning piles. This investigation is made by either auger or water-jet borings.

- (1) Auger borings. Auger borings are most effective for shallow exploration of soils free from coarse gravel or loose rock.
- (a) The motorized gasoline-engine-driven earth auger can be used for

<i>t</i>	P. Fabrication and storage areas:
	(1) Location:
	(2) Size:
· • •	(3) Character:
··· c	. Bivouac areas:
	(1) Location:
	(2) Size:
	(3) Character:
6	d. Areas for parking vehicles:
	(1) Location:
	(2) Size:
	(3) Character:
	e. Water supply:
	(1) Location:
	(2) Quality:
-	(3) Quantity:
1	f. Construction materials available locally:
···) ·	(1) Kind:
	(timber, stone, gravel, sand)
	(2) Location:
	(2) Location:
···	(2) Location:
···	(2) Location: (3) Quality: (4) Quantity: General remarks:
 11.	(2) Location: (3) Quality: (4) Quantity: General remarks:
 11.	(2) Location: (3) Quality: (4) Quantity: General remarks:
 11.	(2) Location: (3) Quality: (4) Quantity: General remarks:
11.	(2) Location: (3) Quality: (4) Quantity: General remarks:
 11.	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:
11.	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:
 11. 12.	(2) Location: (3) Quality: (4) Quantity: General remarks:
 11. 12.	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:
11.	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:
11 12 12	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:
11.	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation: (name, grade, organization
11 12 12	(2) Location: (3) Quality: (4) Quantity: General remarks: Recommendation:

(6) Alignment and grade:

Annexes:

- 1. Maps and photographs
- 2. Sketches and drawings
- 3. Lay-outs
- 4. Estimates

boring to depths of 15 feet in soils free of boulders over 3 inches in diameter. Unless immediately available, however, its use is usually not justified.

(b) The handled post-hole augers shown in figure 29 can be used for boring to depths of 20 to 25 feet by lengthening the stem with \(\frac{3}{4}\)-inch-diameter pipe extensions. Extension sections should be threaded and should be in 3- or 4-foot lengths; they should be added as the depth of the hole increases.

LEGEND

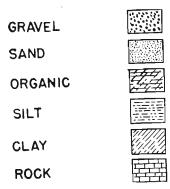


Figure 27. Symbols used in representing soil classifications.

In ordinary material, a party of three men can bore two holes a day to depths of 20 feet or more.

- (2) Wash borings. Wash borings can be made to considerable depths through any fine-grained soil; gravel or gravelly soils are penetrated with difficulty. The boring is made by driving a casing pipe a few feet at a time and then washing the material from inside the pipe to the surface by churning a smaller water jet up and down inside the casing. The overflow of wash water is caught in a bucket as it leaves the casing pipe and the suspended material is allowed to settle for analysis.
- (a) The sand content of the sample is always higher than that of the soil in its natural state, since the fine silt and clay particles are carried away in the wash water. The experienced driller judges the material penetrated not by the samples alone, but also by the color of the wash water, the speed of drilling, and the resistance of the casing to driving. Accurate determination of materials penetrated requires that the casing be driven ahead of the jet so material brought to the surface is only that forced into the casing by driving.
- (b) The usual party for making wash borings is four men. In ordinary material, they can make two borings a day to depths of 30 to 40 feet.
- (c) Equipment for making wash borings is shown in figure 30. It consists essentially of 2-inch-diameter black pipe for casing, a 3/4-inch-diameter black pipe for the jet, a hammer and drive head for driving the casing, a tripod from which a block is suspended for handling the hammer and jet

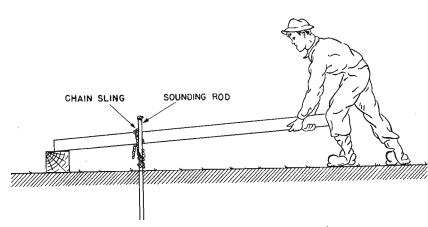


Figure 28. Method of pulling sounding rods.

- pipe, a pump to supply water to the jet, and clamps, tackle, and jacks for pulling the casing after the hole is completed. Casing and jet pipe should be in about 5-foot lengths for easy handling. The tip of the jet should be flattened to a chisel point for boring through clay, but need not be flattened when working in sandy soil.
- (3) Core borings. In soft soils and clays containing boulders, core drilling may be necessary to find the true foundation conditions. Similarly it may be necessary to bore into subsurface rock to learn whether it is a thin ledge or bed rock and to judge the quality of the rock. The gasoline-engine-driven lightweight rotary well-drilling machine model 43–5 (fig. 31) can be used to advantage for such foundation explorations. In soils it will auger holes up to 10 inches in diameter; in rock it will drill 3-inch holes producing 2-inch cores. Depending on the nature of the rock, cores can be drilled at rates of ½ to 1 foot per minute in holes up to 40 feet deep. The drill is capable of drilling holes over 100 feet deep. The equipment weighs about 3,000 pounds complete without mud pump. For complete details, see the Technical Manual on this equipment.
- c. Test pits. Test pits are dug to explore foundation materials for spread footings and sills. Pits are made only large enough for one man to work in. They should be extended beyond the expected bottom of the footing to make sure that the foundation strata is thick enough to carry the intended loads and is not immediately underlain by softer material. They should be shored and braced. (See par. 160.)
- d. Load tests. Before spread footings and sills are built on soils whose adequacy is in doubt, load tests (fig. 32) are necessary to determine the bearing capacity of the foundation material. These are made by test-loading a small area at the elevation of the proposed footings.
- (1) A square bearing plate is set and leveled in a shallow depression just large enough to receive the plate. A post supporting the loading platform is centered on the plate and braced against tipping. The platform is loaded with sandbags of measured weight until the foundation material is subjected to the unit load at which it is to be tested.
- (2) The size of the bearing plate differs with the type of soil being tested.
- (a) On cohesionless soils, gravel, confined sand or sandy soil, a plate 8½-inches square, having an area of ½-square foot can be used.

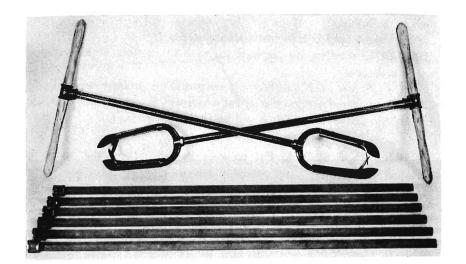


Figure 29. Post-hole auger with handle and extensions for 6-inch diameter holes.

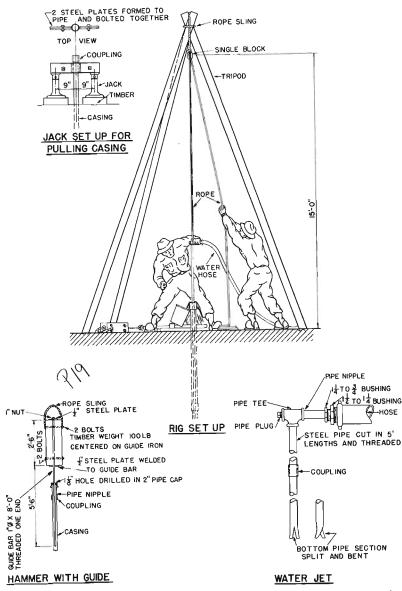


Figure 30. Use of wash-boring equipment for subsurface exploration. Inset views show equipment made up in the field of class IV materials.

- (b) On firm cohesive soils, clays, and silts, the test area should be increased to at least 1 square foot.
- (c) On plastic soils, soft clay, or mud, the test area should be at least 2 square feet.
- (3) If cohesive and plastic soils are tested during dry periods, they should be wetted to the maximum moisture expected during the wet season.
- (4) The initial settlement under load is determined by observations before and immediately after loading, and the test is allowed to stand for 12 hours while additional observations are made. If at the end of the test period, no appreciable settlement is observed in addition to that at the initial loading, the loading is increased and the test repeated. The critical capacity of the soil is exceeded when settlement continues at a constant rate after the addition of load. Foundation loads exceeding 75 percent of the critical capacity of the soil should not be used.

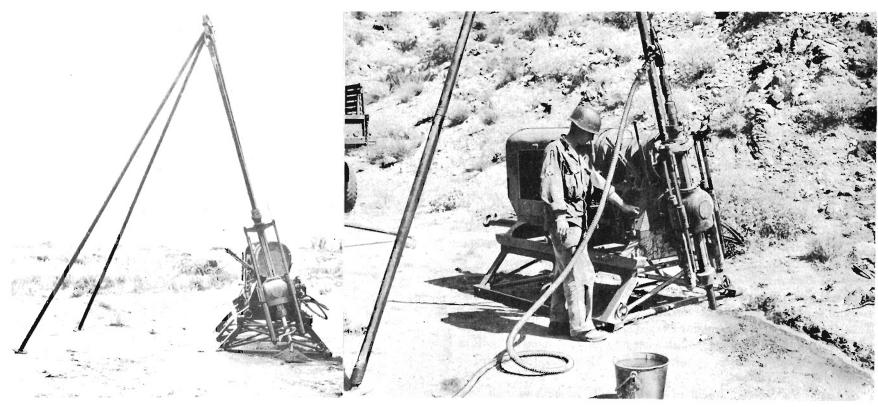


Figure 31. Lightweight rotary well-drilling machine. Used as earth auger and core drill.

CHAPTER 7

BRIDGE LAY-OUT

Section I. GENERAL CONSIDERATIONS

- 71. LAY-OUT DEFINED. a. Bridge lay-out is the process of determining all principal features of the construction including:
 - (1) Height of bridge.
- (2) Location of abutments and foundations.
- (3) Lengths and positions of spans.
- (4) Type and units of construction.
- **b.** Lay-out requires preparing sketches of the bridge in plan and elevation, and assembling complete plans of all units of construction.
- c. The lay-out also provides all information needed for planning construction operations and for requisitioning materials and equipment.
- 72. INFORMATION REQUIRED. To make the bridge lay-out as defined above, it is necessary to have complete data on the bridge site including the approved reconnaissance report (par. 67) and site survey. (See pars. 68 to 70.)
- **73. MECHANICS OF LAY-OUT. a.** A bridge lay-out is worked out in the following sequence:
- (1) Grade line of top of bridge deck is drawn on the ground profile as

determined by approach grades, flood levels, or clearances under the bridge.

- (2) Position of each abutment is determined and shown on the profile.
- (3) Position and lengths of principal openings are indicated as required by flood water or traffic under the bridge.
- (4) Type and units of construction and span lengths are chosen. Units are sketched in on the profile.
- (5) Outlines of foundations and approach roads are drawn on the contour map.
- (6) Principal dimensions and notes concerning construction are added.
- (7) Listing is made of working drawings for each unit of construction used in the bridge.
- (8) Consolidated bills of materials are prepared.
- (9) Detail sketches are prepared to cover adjustments in dimensions of standard designs.
- b. Difficult site conditions may require preparing alternate bridge lay-outs. These are compared to select the lay-out which will carry traffic most efficiently, cost least in materials and labor, and be fastest to construct.
- 74. HEIGHT OF BRIDGE. For economy in construction, the bridge floor elevation (grade line) is set as low as clearance requirements and approach grades allow.
- a. Clearance. (1) The bottom of stringers must be above the level of the highest probable flood expected during the required life of the bridge. In addition, a suitable allowance should be made for drift carried at that flood stage. In view of the semipermanent nature of the bridges, they are not built to withstand the highest floods of extremely infrequent occurrence.

- (2) If the stream is open to navigation, stringers must be high enough to allow boats to pass under the bridge at normal high water. Where this is not practicable, a removable floating section is used or a draw span is improvised.
- (3) Over roadways or railway tracks, usual vertical clearance requirements are:
- (b) Railway:
- 22 feet above top of rail. See figure 24 (1) for clearance diagram. b. Approach grades. (1) Preferred maximum approach grades are:

- not to be exceeded in any case, are:

 Percent
- (a) Highways
 12

 (b) Railways
 2
- (3) Transition curves should be provided to avoid sudden changes of grades at the ends of the bridge. Grades should not be so great that washing of the road surface occurs during rains.
- **75. LENGTH OF BRIDGE.** a. Low bridges. (1) Generally, low trestle bridges should be only long enough to reach from one overflow bank to the other. The approach roads are placed on fill or are permitted to flood during high water.
- (2) In shallow or slow-moving streams, the channel between banks can be restricted by approach embankments only if enough waterway is left to pass flood flows at velocities that will not cause scour. Water velocities at which scour occurs are given in table XVI.
- b. High bridges. (1) Length of high trestle bridges is fixed by economic height of approach embankments. If adequate earth-moving equipment is available, embankments up to 15 feet high can usually be made quicker than trestles of equal height can be built.

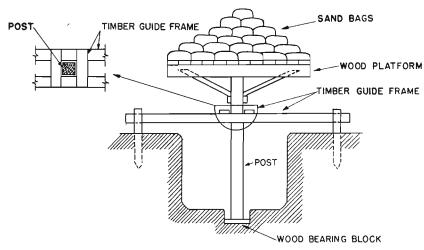


Figure 32. Load test to determine bearing capacity of soil.

TABLE XVI. Scouring velocities of water.

Material	Current (fps)	Material	Current (fps)
Fine sand or silty sand	0.50	Small boulders	8.00 - 10.00
Coarse sand	1.50 - 2.00	Soft rock	6.00 - 10.00
Silt	2.50 - 4.00	Hard rock	10.00 - 15.00
Stiff clay	4.00 - 6.00	Concrete	15.00 - 20.00
Gravel	2.00 - 8.00		

- (2) Maximum height of retained fill behind abutments is 6 feet. Where the bridge deck is more than 6 feet above ground, abutments are set on fill. Fill must be well compacted. Where compaction is difficult, pile abutments (sheet 21) are preferred. Piles should penetrate the ground beneath the fill far enough to develop required capacity. (See ch. 12.) Where scour may occur, fills and abutments are protected with riprap.
- 76. LOCATION AND LENGTHS OF PRINCIPAL OPENINGS. a. Traffic requirements. (1) Navigation. Openings required over navigable waterways vary with the water traffic and with stream conditions. Conditions of the site must be examined and openings located to satisfy the particular navigational requirements.
- (2) Highways and railways. (a) Usual horizontal clearance required for highways and railways are as follows:
- 1. Single-lane highway—12 feet 6 inches.
- 2. Double-lane highway—22 feet.
- 3. Single-track railway—16 feet (fig. 24 (1)).
- 4. Multiple-track railway-—16 feet plus distance center-to-center of outside tracks.
- (b) If roadways or tracks are curved or pass under the bridge at an angle, openings must be increased to maintain the required clearance. Width must also be increased if space for walkways or road-side drainage is required.
- **b.** Foundations. (1) Openings are located so obstructions and unfavorable foundation conditions are avoided. Unfavorable foundation locations may be caused by steep banks, shelving ledges, debris, or underground utilities.
- (2) The foundation designs in this manual are not intended for use in deep water (par. 10) or in locations subject to unusual scour.
- (3) Supports are located to avoid strong currents and maximum drift during high water.

Section II. SELECTING TYPE AND UNITS OF CONSTRUCTION

- 77. GENERAL. Principal factors to be considered in selecting types and units of construction are:
 - a. Material limitations.
- **b.** Equipment limitations.
- c. Labor limitations.
- d. Flood problems.
- e. Foundation problems.
- f. Economy in construction.
- 78. SELECTION DIAGRAMS. a. Diagrams to aid in selecting type of construction are given in tables XVII to XXIV. Two diagrams are given for each bridge class, one showing combinations of units with spread footings and

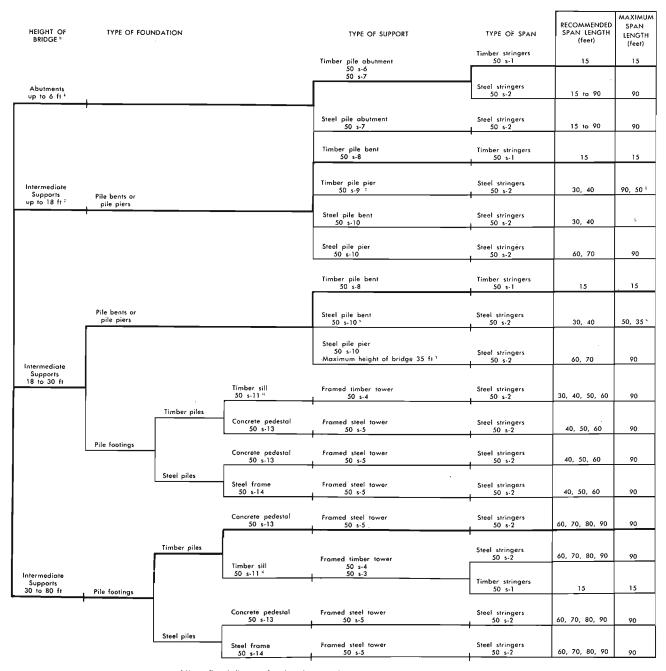
- one showing combinations of units with pile foundations. Sets of drawings covering each type of construction are also listed.
- **b.** Diagrams may be entered from the left with height of structure, or from the right with span length. Preferred combinations of units are indicated by heavy lines. Order of preference in each bracket is given by order of listing from top of diagrams.
- 79. MATERIALS LIMITATIONS. a. General. Principal materials used in semipermanent trestle bridges are timber and steel. Concrete is used only in foundation units; designs in timber or steel are also provided. Timber is usually easiest to obtain and when not available at engineer depots can often be obtained locally.
- b. Span lengths. Material for stringers determines the maximum span that can be used. The lengths of timber and steel spans for which designs are provided are listed in table I. Maximum span lengths are given also in the selection diagrams, tables XVII to XXIV.
- c. Tower heights. Towers up to 80 feet high can be built of either timber or steel if necessary sections are available.
- d. Pile foundations. If piles for bents and piers do not extend far enough above ground after securing necessary penetration, they must be spliced. Designs are provided for pile bents and piers up to the limiting heights from ground or water surface to top of cap listed in chapter 2 and in the selection diagrams.
- e. Grillages. Sections required for steel grillages are the same as those used in steel towers. For timber grillages 6- by 8-inch timber only is used.
- f. Concrete foundations. Concrete for foundations requires cement from engineer depots, and aggregates and mixing water from sources close to the site.
- 80. EQUIPMENT LIMITATIONS. a. Framing and fabrication. Timber bridges can be framed with organic equipment of construction troops. Fabrication of steel requires special equipment for cutting, drilling, and riveting or welding, much of which must be secured from depots. Tools and equipment required for fabrication of steel are described in chapter 11.
- **b. Erection.** Timber bridges can be erected with organic equipment and, if necessary, without powered equipment. Steel members are heavier and generally longer; their handling and erection requires heavy equipment. Difficult erection problems require special equipment. Erection equipment is described in chapter 14.
- **c.** Pile driving. Pile construction requires standard pile-driving equipment. Safe construction of the designs given cannot be obtained with light, expedient pile drivers.
- 81. LABOR LIMITATIONS. a. Engineer troops are familiar with the use of carpentry tools in framing timber. Timber framing does not require the specialized skills needed for fabricating steel. Template making, lay-out of steel, cutting, drilling, riveting, and welding, all require special training.
- **b.** Erection of long spans on high towers is hazardous. It should be undertaken only by well-trained and properly equipped erection crews.
- **82. FLOOD PROBLEMS.** Choice of construction type is influenced by characteristics of the stream at flood stage. The flood channel should be obstructed as little as possible. Units requiring longitudinal bracing should not be used where they will be subjected to strong currents, drift, or ice.

- **a.** Span lengths over floodways should be made as long as practicable to reduce stream obstructions.
- **b.** Pile bents and pile piers offer least obstruction and greatest strength against transverse loads imposed by current, drift, and ice.
- c. Steel towers present less obstruction to stream flow than wood towers and are more stable than timber towers during floods. Steel frame pedestals on steel piles provide very secure anchorage; their construction is justified if frequent, extreme flash floods are expected.
- d. Because of their buoyancy, timber towers should not be used where they will be fully submerged at flood stage, unless weighted down to prevent flotation
- **e.** If the stream bed is subject to scour, pile foundations are preferred. Spread footings, if used, are protected with riprap.
- 83. FOUNDATION PROBLEMS. a. Spread footings. Spread footings require stable foundation material able to support a unit load of not less than 3,000 pounds per square foot. Bearing capacity of soil should be determined by the load tests described in chapter 6. If test data are not available, approximate bearing capacities of soils given in table XXV can be used.

TABLE XXV. Bearing capacity of soils.

General description	Condition	Safe allowable pressure (psf)
Fine-grained soils:	Soft, unconsolidated, having high mois-	
Clays, silts, very fine sands, or mix-	ture content (mud)	1,000
tures of these containing few	Stiff, partly consolidated, medium mois-	
coarse particles of sand or gravel.	ture content	4,000
Classification: MH, CH, OH, ML,	Hard, well-consolidated, low moisture	
CL, OL.	content (slightly damp to dry).	8,000
Sands and well-graded sandy soils con-	Loose, not confined	3,000
taining some silt and clay. Classi-	Loose, confined	5,000
fication: SW, SC, SP, SF.	Compact	10,000
Gravel and well-graded gravelly soils	Loose, not confined	4,000
containing some sand, silt, and	Loose, confined	6,000
clay. Classification: GW, GC, GP.	Compact	12,000
	Cemented sand and gravel	16,000
Rock	Poor quality rock, soft and fractured;	
	also hardpan	10,000
	Good quality; hard and solid	20,000

- b. Pile foundations. Pile foundations are used if the soil will not safely support spread footings, if deep excavation is required to reach a satisfactory bearing for spread footings if scour may occur, or if currents or floods make lateral support necessary. Pile foundations may also be used where depth of water makes construction of spread footings difficult. Usual depths to which piles must be driven to develop satisfactory bearing capacity are obtained from table XXVI.
- 84. ECONOMY IN CONSTRUCTION. a. Proportions. Span lengths should be balanced against height of supports to secure the most economic proportions. Recommended span lengths for each type of supporting structure based on least expenditure in materials and labor are shown on the selection diagrams. Where a range of values is shown, shorter spans in lower structures and longer spans in higher structures give maximum economy.



¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

HEIGHT OF BRIDGE ³		TYPE OF SUPPORT	TYPE OF SPAN	RECOMMENDED SPAN LENGTH (feet)	MAXIMUM SPAN LENGTH (feet)
		Timber Grillage abutment	Timber stringers 50 s-1	15	15
Abutments		50 s-6 50 s-7	Steel stringers 50 s-2	15 to 90	90
Up to 6 ft '	·	Concrete abutment 50 s-7	Steel stringers	15 to 90	90
			Timber stringers 50 s-1	15	15
	Concrete pedestal	Framed timber tower 50 s-3 50 s-4	Steel stringers		
	50 s-12 50 s-13	Framed steel tower	50 s-2 Steel stringers	30, 40, 50	90
		50 s-5	50 s-2	40, 50, 60	90
Intermediate Supports Up to 30 ft	Timber grillage 50 s-16	Framed timber tower 50 s-3 50 s-4	Timber stringers 50 s-1	15	15
		'	Steel stringers 50 s-2	30, 40, 50	90
	Steel grillage 50 s-16	Framed steel tower 50 s-2	Steel stringers 50 s-2	40, 90, 60	90
	Concrete pedestal 50 s-13	Framed steel tower 50 s-5	Steel stringers 50 s-2	50, 60, 70, 80, 90	90
	Steel grillage 50 s-15	Framed steel tower	Steel stringers 50 s-2	50, 60, 70, 80, 90	90
Intermediate	Carrent and total	Framed timber tower	Steel stringers 50 s-2	50, 60, 70, 80, 90	90
Supports 30 to 80 ft	Concrete pedestal 50 s-12	50 s-4 50 s-3	Timber stringers 50 s-1	15	15
		Framed timber tower	Steel stringers 50 s-2	50, 60, 70, 80, 90	90
	Timber grillage 50 s-16	50 s-4 50 s-3	Timber stringers		

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

 $^{^{2}}$ Drawing-set number listed on sheet 1 is noted under each construction unit in table,

³ Height of structure from grade to ground.

⁵ Average length of two spans on bent.

[&]quot;Where built over water, use braced piles as shown on sheet 36.

⁷ Timber pile piers can be built to 30 feet maximum height from grade to ground. When height exceeds 18 ft the average length of two spans on pier is not to exceed 50 feet, and additional bracing similar to that detailed for lower piers is to be provided.

Steel pile bents can be built to 30 feet maximum height from grade to ground. For heights up to 23 feet the average length or two spans on bent is not to exceed 35 feet.

² Drawing-set number listed on sheet 1 is noted under each construction unit in table.

³ Height of structure from grade to ground.

Height of retained fill.

RECOMMENDED MAXIMUM
SPAN LENGTH
(Feet) LENGTH HEIGHT OF BRIDGE 3 TYPE OF FOUNDATION TYPE OF SUPPORT TYPE OF SPAN (Feet) Timber pile abutment 50 D-6 50 D-6 15 15 Steel stringers 50 D-2 Abutments up to 6 ft 15 to 90 90 Steel stringers 50 D-2 15 to 90 90 Timber pile pier 50 D-9 30, 40 90, 50 supports up to 18 ft ? Pile bents or Steel stringers Steel pile pier 50 D-10 60, 70 90 Timber pile bent 50 D-8 Timber stringers 50 D-1 15 15 Pile bents or pile piers Steel pile bent 50 D-10 * Steel stringers 50 D-2 30. 40 50, 35 Steel pile pier 50 D-10 Maximum height of bridge 35 ft ³ 60, 70 90 Intermediate supports 18 to 30 ft Timber sills 50 D-11 ⁹ Steel stringers 50 D-2 Framed timber tower 50 D-4 30, 40 50 90 Timber piles ncrete pedesto 50 D-13 Framed steel tower 50 D-5 Steel stringers 50 D-2 40, 50, 60 90 Pile footings Steel stringers 50 D-2 40, 50, 60 90 Steel piles Steel stringers 50 D-2 40, 50, 60 90 Concrete pedestal Framed steel tower 50 D-5 Steel stringers 50 D-2 40, 50, 60, 70 Timber piles Steel stringers 50 D-2 Framed timber tower 50 D-4 50 D-3 40, 50, 60, 70 90 Timber sills 50 D-11 ⁶ Intermediate supports 30 to 80 ft Timber stringers 50 D-1 15 15 Pile footings Framed steel tower 50 D-5 Steel stringers 50 D-2 Concrete pedestal 50 D-13 40, 50, 60, 70 90 Steel stringers 50 D-2 Framed steel tower 50 D-5 Steel frame 50 D-14 40, 50, 60, 70

TABLE XX. Selection diagram, class 50, double-lane highway bridges with spread footings.

HEIGHT OF BRIDGE 1	FOOTING	TYPE OF SUPPORT	TYPE OF SPAN	RECOMMENDED SPAN LENGTH (Feet)	MAXIMU SPAN LENGTH (Feet)
			Timber stringers	15	
		Timber grillage abutment 50 D-6 50 D-7	50 D-1	13	15
Abutments up to 6 ft			Steel stringers 50 D-2	15 to 90	90
op 10 0 11		Concrete abutment	Steel stringers	15 to 90	90
		Framed timber lower 50 D-3	Timber stringers 50 D-1	15	15
	Concrete pedestal 50 D-12	50 D-4	Steel stringers 50 D-2	20, 30, 40	90
	50 D-13	Framed steel tower	Steel stringers		
		50 D-2	50 D-2	40, 50	90
Intermediate		Framed timber tower	Timber stringers 50 D-1	15	15
supports up to 30 ft	Timber grillage 50 D-16	50 D-3 50 D-4	Steel stringers	30, 40	
			50 D-2	30, 40	90
	Steel grillage 50 D-15	Framed steel tower 50 D-5	Steel stringers 50 D-2	30, 40, 50	90
		Framed steel tower 50 D-5	Steel stringers 50 D-2	50, 60, 70	90
	Steel grillage 50 D-15	Framed steel tower 50 D-5	Steel stringers 50 D-2	50, 60, 70	90
		-	Steel stringers		
ntermediate supports 30 to 80 ft		Framed timber tower 50 D-4 50 D-3	50 D-2	40, 50, 60, 70	90
			Timber stringers 50 D-1	15	15
		Framed timber tower	Steel stringers 50 D-2	40, 50, 60, 70	90
	Timber grillage 50 D-16	50 D-4 50 D-3	Timber stringers		
			50 D-1	15	15

Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

^{*} Drawing-set number listed on sheet 44 is noted under each construction unit in table.

 $^{^{\}mathrm{3}}$ Height of structure from grade to ground.

^{&#}x27; Height of retained fill.

 $^{^{\}circ}$ Average length of two spans on bent.

⁴ Where built over water, use braced piles as shown on sheet 81.

Timber pile piers can be built to 30 feet maximum height from grade to ground. When height exceeds 18 ft the average length of two spans on pier is not to exceed 50 feet, and additional bracing similar to that detailed for lower piers is to be provided.

Steel pile bents can be built to 30 feet maximum height from grade to ground. For heights up to 23 feet the average length of two spans on the bent is not to exceed 50 feet. When height exceeds 23 feet the average length of two spans on bent is not to exceed 35 feet.

² Drawing-set number listed on sheet 44 is noted under each construction unit in table.

³ Height of structure from grade to ground.

^{*} Height of retained fill.

TABLE XXI. Selection diagram, class 25, double-lane highway bridges with pile foundations.

HEIGHT OF BRIDGE 3 TY	PE OF FOUNDATION			TYPE OF SUPPORT	TYPE OF SPAN	RECOMMENDED SPAN LENGTH (feet)	MAXIMUM SPAN LENGTH (feet)
				Timber pile abutment 25 D-6	Timber stringers 25 D-1	15	15
Abutments up to 6 ft 1				25 D-7	Steel stringers 25 D-2	15 10 90	90
	-	-		Steel pile abutment 25 D-7	Steel stringers 25 D-2	15 10 90	90
				Timber pile bent 25 D-8	Timber stringers 25 D-1	15	15
Intermediate supports	Pile bents or			Timber pile pier 25 D-9 :	Steel stringers 25 D-2	20, 30, 40, 50	90, 60
up to 18 ft	pile piers			Steel pile bent 25 D-10	Steel stringers 25 D-2	20, 30, 40	50
				Steel pile pier 25 D-10	Steel stringers 25 D-2	60, 70	90
				Timber pile bent 25 D-8	Timber stringers 25 D-1	15	15
	Pile bents or pile piers			Steel pile bent 25 D-10 `	Steel stringers 25 D-2	20, 30, 40	50, 35
•				Steel pile pier 25 D-10	Steel stringers 25 D-2	60, 70	90
Intermediate supports 18 to 30 ft			Max Timber sill 25 D-11 "	imum height of bridge 35 ft : Framed timber tower 25 D-4	Steel stringers 25 D-2	30, 40, 50, 60	90
		Timber piles	Concrete pedestal 25 D-13	Framed steel tower 25 D-5	Steel stringers 25 D-2	40, 50, 60	90
	Pile footings	Concrete pedestal 25 D-13	Framed steel tower 25 D-5	Steel stringers 25 D-2	40, 50, 60	90	
		Steel piles	Steel frame 25 D-14	Framed steel tower 25 D-5	Steel stringers 25 D-2	40, 50, 60	90
			Concrete pedestal 25 D-13	Framed steel tower 25 D-5	Steel stringers 25 D-2	60, 70, 80, 90	90
		Timber piles		Framed timber tower	Steel stringers 25 D-2	60, 70, 80, 90	90
Intermediate supports 30 to 80 ft	Pile footings		Timber sill 25 D-11 "	25 D-4 25 D-3	Timber stringers 25 D-1	15	15_
<u> </u>	1	-	Concrete pedestal 25 D-13	Framed steel tower 25 D-5	Steel stringers 25 D-2	60, 70, 80, 90	90
		Steel piles	Steel frame 25 D-14	Framed steel tower 25 D-5	Steel stringers 25 D-2	60, 70, 80, 90	90

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

TABLE XXII. Selection diagram, class 25, double-lane highway bridges with spread footings.

HEIGHT OF BRIDGE ³	FOOTING	TYPE OF SUPPORT	TYPE OF SPAN	RECOMMEND SPAN LENGTH (feet)	MAXIMU. SPAN LENGTH
			Timber stringers		(feet)
		Timber grilfage abvIment	25 D-1	15	15
		25 D-6 25 D-7			
			Steel stringers	15 to 90	90
Abutments up to 6 ft '			25 D-2	13 16 70	,,,
		Concrete abutment	Steel stringers		
		25 D-7	25 D-2	15 to 90	90
			•		
			Timber stringers 25 D-1	15	15
		Framed timber tower 25 D-3	25 0-1	15	13
		25 D-4			
	Concrete pedestal 25 D-12		Steel stringers 25 D-2	30, 40, 50	90
	25 D-13				
		Framed steel tower	Steel stringers		
		25 D-5	25 D-2	40, 50, 60	90
Intermediate		Francis de Control de La control	Timber stringers 25 D-1	1.5	15
supports up to 30 ft	Timber grillage 25 D-16	Framed timber tower 25 D-3 25 D-4			
-	25 0-16	17 0-4	Steel stringers		
			25 D·2	30, 40, 50,	90
	Steel grillage 25 D-15	Framed steel tower 25 D-2	Steel stringers 25 D-2	40, 50, 60	90
			+		
	Concrete pedestal	Framed steel tower	Steel stringers		
	25 D-13	25 D-5	25 D-2	50, 60, 70, 80	90
	Steel grillage 25 D-15	Framed steel tower 25 D-5	Steel stringers 25 D-2	50, 60, 70, 80	90
		1000	13 5-2	33, 33, 73, 60	
			Stool at-		
Intermediate		Framed timber tower	Steel stringers 25 D-2	50, 60, 70, 80, 90	90
supports 30 to 80 ft	Concrete pedestal 25 D-12	25 D-3 25 D-4			
		1	Timber stringers 25 D-1	15	15
			20 0-1	1	
			Sanal rad		
		Framed timber tower	Steel stringers 25 D-2	50,60, 70, 80, 90	90
•	Timber grillage 25 D-16	25 D-3 25 D-4			
		+	Timber stringers	.	
			25 D-1	15	15

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

^{*} Drawing-set number listed on sheet 91 is noted under each construction unit in table.

³ Height of structure from grade to ground.

Height of retained fill.

 $^{^{\}circ}$ Average length of two spans on bent.

⁶ Where built over water use braced piles as shown on sheet 121.

Timber pile piers can be built to 30 feet maximum height from grade to ground. When height exceeds 18 feet the average length of two spans on pier is not to exceed 60 feet and the additional bracing similar to that detailed for low piers is to be provided.

Steel pile bents can be built to 30 feet maximum height from grade to ground. For heights up to 23 feet the average length of two spans on bent is not to exceed 50 feet. When height exceeds 23 feet the average length of two spans on bent is not to exceed 35 feet.

^{*}Drawing-set number listed on sheet 91 is noted under each construction unit in table.

[·] Height of structure from grade to ground.

^{&#}x27; Height of retained fill.

TABLE XXIII. Selection diagram, E-45 railway bridges with pile foundations.

HEIGHT OF BRIDGE 3	TYPE OF FOUND	PATION		TYPE OF SUPPORT	TYPE OF SPAN	RECOMMENDED SPAN LENGTH (feet)	MAXIMUM SPAN LENGTH (feet)
				Timber pile abutment RR—6 RR—7	Timber stringers RR—1	16	16
Abutments up to 6 ft	1				Steel stringers RR-2	15 to 50	50
	1	-		Steet pile abutment RR—7	Steel stringers RR-2	15 to 50	501
				Timber pile bent RR—8	Timber stringers RR-1	16	16
Intermediate supports up to 15 ft	Pile bents or			Timber pile pier RR-9	Steel stringers RR-2	20, 25, 30	50
ор 10 13 11	pile piers			Steel pile bent RR—10	Steel stringers	20, 25, 30	30
				Steel pile pier RR-10	Steel stringers RR—2	35, 40, 45	50
				Timber pile bent RR-8 Maximum height of bridge 30 ft "	Timber stringers	16	16
	Pile bents or pile piers			Steel pile bent RR—10 Maximum height of bridge 23 ft ³	Steel stringers RR2	20, 25, 30	30
Intermediate				Steel pile pier RR—10 Maximum height of bridge 23 ft ³	Steel stringers RR-2	35, 40, 45	50
supports 15 to 30 ft	-		Timber sill RR-11 5	Fromed timber tower RR-4	Steel stringers	35, 40, 45, 50	50
		Timber piles	Concrete pedestal RR-13	Framed steel tower RR –5	Steel stringers RR—2	40, 45, 50	50
	Pile footings	\dashv	Concrete pedestal RR-13	Framed steel tower RR-5	Steel stringers RR-2	40, 45, 50	50
		Steel piles	Steel frame RR-14	Framed steel tower RR-5	Steel stringers RR-2	40, 45, 50	50
			Concrete pedestal RR—13	Fromed steel tower RR-5	Steel stringers RR-2	40, 45, 50	50
		Timber piles		Framed timber tower	Steel stringers RR-2	40, 45, 50	50
Intermediate supports 30 to 80 ft	Pile footings		Timber sill RR-11 5	RR-4 RR-3	Timber stringers RR—1	16	16
	· ··· · · · · · · · · · · · · · · · ·		Concrete pedestal RR—13	Framed steel tower RR-5	Steel stringers RR2	40, 45, 50	50.
		Steel piles	Steel frame RR-14	Framed steel tower RR-5	Steel stringers	40, 45, 50	50
				 	 		

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

TABLE XXIV. Selection diagram, E-45 railway bridges with spread footings.

HEIGHT OF BRIDGE "	FOOTING	TYPE OF SPAN		RECOMMENDED SPAN LENGTH (feet)	MAXIMUM SPAN LENGTH (feet)
		Timber avillage abutment	Timber stringers RR-1	16	16
	•	Timber grillage abutment RR—6 RR—7			
Abutments up to 6 ft			Steel stringers RR-2	15	15
		Concrete abutment RR—7	Steel stringers RR-2	15 to 50	50
			Timber stringers RR—1	16	16
		Framed timber tower RR—3			
	Concrete pedestal RR—12 RR—13		Steel stringers RR-2	30	50
		Framed steel tower RR—5	Steel stringers RR-2	35, 40, 45, 50	50
Intermediate			Timber stringers RR–1	16	16
Intermediate supports up to 30 ft	Timber grillage RR—16	Framed timber tower RR-3			e e e e e e e e e e e e e e e e e e e
		•	Steel stringers RR-2	30	50
	Steel grillage RR—15	Framed steel tower	Steel stringers RR-2	35, 40, ⁴ 45, 50	50
	Concrete pedestal RR—13	Framed steel tower RR—5	Steel stringers RR-2	40, 45, 50	50
	Steel grillage RR—15	Framed steel tower	Steel stringers	40, 45, 50	50
Intermediate		Framed timber tower	Steel stringers RR-2	30 35, 40, 45	50
supports 30 to 80 ft	Concrete pedestal RR—12	RR-3	Timber stringers RR-1	16	16
			Steel stringers		
	Timber grillage RR-16	Framed timber tower RR—4 RR—3	RR-2	30 35, 40, 45	50
	RR-10	- NN-3	Timber stringers RR—1	16	16

¹ Heavy lines indicate preferred combination of units. Other combinations shown in vertical position in brackets by order of preference.

² Drawing-set number listed on sheet 156 is noted under each construction unit in table.

⁴ Height of structure from grade to ground.

¹ Height of retained fill.

 $^{^{\}rm 5}$ Where built over water, use braced piles as shown on sheet 212 and 213.

 $^{^{\}rm 2}$ Drawing-set number listed on sheet 156 is noted under each construction unit in table.

³ Height of structure from grade to ground.

⁴ Height of retained fill.

TABLE XXVI. Approximate load capacities per foot of penetration for piles deriving their support principally from friction. Use for preliminary estimates of required length and number of piles when actual test data are not available.

Soil type	per :	Range of safe load, foot of penetration e of mean diamete	for
	9"	12"	15"
Fine grained soils: Clays, silts, very fine sands or mixtures containing few coarse sand and gravel particles. Classification: MH, CH, OH, ML, CL, OL.	Ton	Ton	Ton
Condition 1: Soft, unconsolidated, high moisture content		0.12.4.00	0.17.1-0.25
(mud). Condition 2: Stiff, partly consolidated,	0.1 to 0.15	0.13 to 0.2	0.16 to 0.25
medium moisture con- tent.	.15 to .4	.2 to .6	.25 to .8
Condition 3: Hard, well - consolidated, low moisture content (slightly damp or dry).	.4 to .9	.6 to 1.2	.8 to 1.5
Sands and well-graded sandy soils containing some silt and clay. Classification: SW, SC, SP, SF.	.6 to 1.2	.8 to 1.6	1.0 to 2.0
Gravel, well-graded sandy soils containing some sand, silt, and clay. Classification: GW, GC, GP, GF.	.7 to 2.0	1.0 to 2.5	1.2 to 3.0

- (1) Soils classification as shown in FM 5-10, 1944 edition, table I.
- (2) For other pile diameters, safe load varies in proportion to diameter.
- (3) Piles must be driven at least 8 feet in hard ground and 15 to 20 feet in soft ground.
- (4) Piles resting on a hard stratum act as columns and this table does not apply.
- (5) The above values of pile bearing capacity are used in estimates of piling, lacking more accurate information. The required pile penetration should always be based on actual driving described in paragraph 155.
- **b.** Duplication. Uniformity in type and units of construction is preferred. Repetition makes for faster and better work and limits the variety of equipment required.
- c. Transportation. Materials close at hand or readily available are preferred. Construction requiring lighter and fewer pieces of equipment is preferred for the same reason.
- d. Time. Ordinarily, timber construction requires less time than longer-span steel construction.
- 85. COMPARATIVE ESTIMATES. After alternative lay-outs have been made, estimates of materials and labor as well as principal equipment requirements are compared. Material requirements for all units of construction are given in tables XXVII to XXX. Man-hour requirements for all units are given in tables XXXIII to XXXVII. Equipment requirements are given in table XXXI.

CHAPTER 8

CONSTRUCTION PLANNING

86. GENERAL, a. Careful planning of work eliminates unnecessary delay and rehandling of materials and parts. It insures completing parts in orderly sequence and completing the bridge within the time allotted.

TABLE XXVII. Summary of materials—highway bridges, class 50, single-lane.

(1) Summary of materials for bents, piers, and abutments.

Туре					Λ	butments						Be	nts	Pi	ers
17100	Timb	er pile	Steel pile			Timber	grillage			Con	crete	Timber	Steel	Timber	Steel
Height of retained fill	6	feet	6 ft.		3 feet			6 feet		3 ft.	6 ft.	pile bent	pile bent	pile pier	pile pier
Maximum span—feet	15	90	90	15	40	90	15	40	90	90	90	15	450	90	90
Piles-each	¹ 6	16	15									(*0.19)	3	8 (61.08)	6
Timber—mbm	0.72	0.88	0.81	0.69	0.92	1.41	1.39	1.59	1.99	•		0.78		1.10	
Steel-tons			1.32										{ 50.94 } 0.99 }		{ ⁵ 2.05 2.49
Concrete—cu. yd										{ ² 11.7 14.0	218.0 \ 20.8 }				

¹ Includes 2 wing piles.

(2) 'ummary of materials for footings.

Timber į	grillages				Concrete	ped tals		Concre	te pedestals, tim	ber piles	Concrete pedes	tals, steel piles	Timber sills, timber piles	Steel frame	, steel piles
Unit		Steel (tons)	Unit	Concrete	Unit	Concrete	Unit	Piles	Concrete	Piles	Concrete	Piles	Piles	Steel	
	(mbm)	Bol	red]	(cu. yd.)		(cu. yd.)		(number)	(cu. yd.)	(number)	(cu. yd.)	(aumber)	(number)	(tons)
G113	0.32	S101	1.89	F104	11.4	F112	5.6	F134	4	5.0	4	5.1	12	4	1.19
G114	0.16	S102	2.86	F105	6.0	F113	3.0	F135	5	5.8			24		
G115	0.64	**		F106	10.2	F114	2.7	F136	6	1.1					
G116	0.32			F107	5.2	F115	2.5	F137	/	9.3					
G117	0.29			F108	9.1	F121	7.4								
G118	0.15			F109	4.5	F122	9.1								
G119	0.58			F110	6.1	F123	10.8								J
G120	0.29			F111	5.9	F124	12.9								****

(3) Summary of materials for towers and spans.

	Framed tim	ber towers1					_					Tim	ber spans ²		Steel span	•
Timber	r spans	Steel s	spans				Fr	amed steel towe	az,			Length	Timber	Length	Steel	Timber
Height (ftin.)	mbm	Height (ftin.)	mbm	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	(feet)	(mbm)	Length (feet)	(tons)	(mbm)
13-4 25-10 38-4 50-10 63-4 75-10	2.60 5.01 7.55 10.18 12.92 15.75	13-4 25-10 38-4 50-10 63-4 75-10 	5.03 9.45 14.18 19.08 24.20 29.58 	77 75 73 71 69 67 65 63 61	26.11 25.79 25.65 25.19 24.89 21.27 21.00 20.71 20.43	59 57 55 53 51 49 47 45 43	20.14 19.84 19.54 19.25 18.98 15.50 15.23 14.97 14.68	41 39 37 35 33 31 29 27 25	14.51 14.13 13.85 13.59 13.32 10.04 9.78 9.52 9.25	23 21 19 17 15 	8.99 8.74 8.43 8.22 7.98 	11 13 15 	1.90 2.21 2.55 	15 20 30 40 50 60 70 80 90	1.37 2.18 4.72 7.44 12.13 16.34 20.20 26.37 37.39	2.40 3.15 4.66 6.17 7.69 9.18 10.73 12.21 13.76

¹ Material in tower spans not included.

² For 36- and 16-inch steel stringers.

^{*} For heights of 10, 20 and 30 feet. Includes longitudinal bracing.

⁴ Average length of two spans on bent. See table LI.

⁵ For heights of 10 and 23 feet.

⁶ For heights of 10 and 18 feet.

² Includes timber in deck.

TABLE XXVIII. Summary of materials-highway bridges, class 50, double-lane.

(1) Summary of materials for bents, piers, and abutments.

						Abutm	ents						В	egts	F	iers
Туре		Timber pile		Steel pile			Timbe	r grillage			Cor	acrete	Timber pile	Stee l pile	Timber pile	Steel
Height of retained fill		6 feet		6 feet		3 feet			6 feet		3 feet	6 feet	bent	bent	pier	pile pier
Maximum span—feet Piles—each	15 18	50 18	90 110	90 16	15	40	90	15	40	90	90	90	15	⁴ 50 4	90	90 6
Timber—mbm	1.16	1.45	1.50	1.09	1.17	1.39	2.11	2.22	2.43	3.38	••••		$ \left\{ \begin{array}{c} 3.34 \\ 1.15 \\ 1.39 \end{array} \right. $		{ ⁶ 1.70 } 1.75 }	
Steel—tons			*	1.65				****						{ 51.78 }		∫ ⁵ 3.26 3.70
Concrete—cu. yd	****					*					$\left\{\begin{array}{c}218.2\\21.4\end{array}\right\}$	$\left\{\begin{array}{c} 228.1\\32.1\end{array}\right\}$				

- ¹ Includes 2 wing piles.
- ² For 36- and 18-inch steel stringers.
- ⁸ For heights of 10, 20, and 30 feet from grade to ground. Includes longitudinal bracing.

- Average length of two spans on bent. See table LI.
- ⁵ For heights of 10 and 23 feet from grade to ground.
- 6 For heights of 10 and 18 feet from grade to ground.

(2) Summary of materials for footings.

Tin grili	nber lages	Se grill	eci ages		crete estals		Concrete pedestals, timber piles			crete stals, piles	Timber sills, timber piles	Steel :	rame, piles
Unit	Timber (mbm)	Unit	Steel (tons)	Unit	Concrete (cu. yd.)	Unit	Piles (number)	Concrete (cu. yd.)	Piles (number)	Concrete (cu. yd.)	Piles (number)	Piles (number)	Steel (tons)
G113 G114	0.32 0.16	S-101 S-102	1.89 2.39	F105 F107	6.0 5.2	F134 F135	4	5.0 5.8	4	5.1	8 16	4	1.14
G117	0.29	3-102	2.39	F109	4.5							********	
G118	0.14	*******		F113 F114	3.0 2.7					*******	*******	*******	
	*******			F115 F120	2.5 6.0			*******					******
*******	********	*******		F121 F122	7.4 9.1								

(3) Summary of materials for towers and spans.

	Framed tim	iber towers?					Fram	ed steel towers?	:							
Timber	ebans	Steel:	spans		eight T Height							Length (feet)	Timber (mbm)	Length (feet)	Steel	Ţimber
Height (ftin.)	mbm	Height (ftin.)	mbm	Height (ft.)	Топз	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons			(feet)	(tons)	(mbm)
13-4 25-10 38-4 50-10 63-4 75-10	3.61 6.78 10.01 13.38 17.00 20.71	13-4 25-10 38-4 50-10 63-4 75-10	7.10 13.03 19.24 25.52 32.40 39.46	77 75 73 71 69 67 65 63 61	32.11 31.82 31.54 31.26 30.99 27.06 26.88 26.55 229	59 57 55 53 51 49 47 45	25.99 25.73 25.44 25.19 24.93 20.88 20.63 20.37 20.10	41 39 37 35 33 31 29 27 25	19 89 19.59 19.34 19.07 18.83 15.03 14.66 14.53 14.27	23 21 19 17 15 	14.03 13.79 13.53 13.29 13.06	11 13 15 	3.20 3.74 4.31 	15 20 30 40 50 60 70 80 90	2.85 4.33 7.92 12.26 21.17 27.50 36.26 50.28 72.35	3.90 4.80 6.87 8.79 10.86 12.64 14.71 16.44 18.27

- ¹ Material in tower spans not included.
- ² Includes timber in deck.

- b. Construction planning requires:
- (1) A careful estimate of the material, equipment, and personnel required to do the job.
- (2) A time schedule of construction operations covering all work to be done, equipment to be used, materials required, and labor to be employed.
- (3) A progress schedule and a simple system of periodic reports and records of progress so work done can be readily compared with the scheduled progress. This promotes effective supervision and job control.
- c. Exact material requirements for the bridge itself are established as soon as the final layout is made. (See par. 71.) Equipment and personnel requirements and materials required for temporary construction depend on the construction procedure and the schedule adopted.
- 87. MATERIAL REQUIREMENTS. a. Bridge material. The drawings list all materials required for each unit of construction. A bill of materials showing each item used for each unit is prepared from these lists. Requisitions of materials for the bridge are prepared by combining similar items from all bills of materials into listings of total quantities of each item. Bills of materials contain exact count of all pieces. In requisitioning hardware such as bolts, nuts, rivets and nails, 15 percent should be added for waste, loss, and rejections.
- b. Erection material. Materials needed for temporary use, such as concrete forms, falsework, cofferdams, and construction shelters are determined after the erection method has been chosen. When requisitioning these materials, unforeseen requirements and local sources of materials are taken into account. Wherever possible, construction is planned so material to be used in the final structure can also be used for temporary purposes. The manual does not give quantities of material which may be required in temporary construction. Material estimates for concrete forms, falsework, and scaffolding should be prepared from field construction sketches following instructions of TM 5–226.
- 88. EQUIPMENT REQUIREMENTS. a. Erection equipment requirements differ with site conditions and erection methods. Table XXXI gives tool and equipment items needed to construct each unit under usual site conditions and for the following construction procedures.
- (1) Bridges less than 35 feet high from ground to grade, erected with a crawler-mounted crane operating from ground level. (See par. 210.)
- (2) Bridges over 35 feet high from ground to grade.
- (a) Towers erected with special equipment described in paragraphs 211 and 213.
- (b) Spans not more than 50 feet long, erected with truck-mounted crane operating from deck level. (See par. 208.)
- (c) Spans over 50 feet long, erected with the special equipment described in paragraphs 212 and 214.
- (3) If other procedures are followed, equipment requirements must be modified accordingly.
- b. The number of pieces of each equipment item needed is determined after the construction schedule is prepared and the time allocated to each operation is fixed. Table XXXIA gives the number necessary to outfit a single crew or detail in each operation. Operations such as framing, drilling, riveting, welding, and the like may require several crews, all using identical items of equipment.

					Abutmer	162				Ве	ats	Pi	ers
Туре	Timbe	er pile	Steel pile		Timber	grillage		Conc	rete	Timber	Steel pile	Timber	Steel pile
Height of retained fill	6 fe	eet	6 ft.	3 fe	et	6	feet	3 ft.	6 ft.	pile bent	bent	pile pier	pier
Maximum span, feetPiles, each	15 17	90	90 1 ₆	15	90	15	90	90	90	15	450 3	90 8	90 6
Timber, mbm		1.32	1.09	1.17	1.54	2.22	2.44			$ \left\{ \begin{array}{c} 3.34 \\ 1.16 \\ 1.21 \end{array} \right\} $		$\left\{\begin{smallmatrix}61.71\\1.75\end{smallmatrix}\right\}$	
Steel, tons			1.62								$\left\{ \begin{array}{c} 51.77 \\ 1.80 \end{array} \right\}$	·	53.18 3.62
Concrete, cu. yd			<i></i> -					{ ² 18.7 22.1	² 28.8 33.0				

- ¹ Includes 2 wing piles.
- ² For 36- and 14-inch steel stringers.
- * For heights of 10, 20, and 30 feet from grade to ground. Includes longitudinal bracing.
- Average length of two spans on bent. See table LI.
- ⁶ For heights of 10 and 23 feet from grade to ground.
- ⁶ For heights of 10 and 18 feet from grade to ground.

(2) Summary of materials for footings.

Tim grill		St grilla	eel iges		crete estals	Co	ncrete pedest timber piles	als,	Concrete steel	pedestals, piles	Timber sills, timber piles	Steel f	
Unit	Timber (mbm)	Unit	Steel (tons)	Unit	Concrete (cu. yd.)	Unit	Piles (number)	Concrete (cu. yd.)	Piles (number)	Concrete (cu. yd.)	Piles (number)	Piles (number)	Steel (tons
G113 G114	0.32 0.16	S101 S102	1.89 2.86	F105 F107	6.0 5.2	F134 F135	4 5	5.0 5.8	4	5.1	8 16	4	1.19
G117	0.29			F109	4.5								
G118	0.15			F113	3.0						••••		
				F114	2.7								
				F115	2.5								
				F120	6.0			•					
] <i>.</i>	F121	7.4						•		
****				F122	9.1								****
				F123	10.8								

(3) Summary of materials for towers and spans.

I	3.19 (ftin.) (ftin.) 3.19											Timber	spans2		Steel spans	
Timber	spans	Steel	pans				Framed ste	eel towers1				Land	Timber	71	6. 1	
Height (ftio.)	mbm		mbm	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	Length (feet)	(mbm)	Length (feet)	Steel (tons)	Timber (mbm)
13-4	3.19	13-4	6.44	77	30.18	59	23.95	41	17.97	23	12.11	11	2.65	15	2.03	3.91
25-10	5.82	25-10	11.28	75	29.89	57	23.68	39	17.66	21	11.87	13	3.09	20	2.89	4.90
38-4	8.56	38-4	16.41	73	29.60	55	23.39	37	17.41	19	11.62	15	3.56	30	6.47	7.09
50-10	11.49	50-10	21.71	71	29.33	53	23.15	35	17.14	17	11.38			40	8.75	8.88
63-4	14.53	63-4	27.38	69	29.05	51	22.88	33	16.90	15	11.13			50	15.20	10.62
75-10	17.66	75-10	33.28	67	25.01	49	18.96	31	13.11					60	19.60	12.55
				65	24.78	47	18.71	29	12.75			****		70	26.37	14.62
				63	24.51	45	18.44	27	12.61					80	34.17	16.67
		****		61	24.29	43	18.18	25	12.36					90	41.62	18.50

¹ Material in tower spans not included

TABLE XXX. Summary of materials—E-45 railway bridges.

(1) Summary of materials for bents, piers, and abutments.

						Abut	ments					Ве	ents	Pi	ers
Туре		Timb	er pile		Steel pile		Timber	grillage		Con	crete	Timber	Steel	Timber	Steel
Height of retained fill		6 1	fect		6 ft.	3 :	feet	6	eet	3 ft.	6 ft.	pile bent	pile bent4	pile piers	pile pier6
Maximum span feet Piles—each	16 16	25 16	45 110	50 110	50 16	16	15	16	15	50	50	16	15 & 50	15 & 50 16	15 & 50 16
Timber—mbm	.62	.72	1.03	1.12	.58	.82	.98	1.57	1.65			$ \left\{\begin{array}{c} 3.17 \\ .80 \\ .80 \end{array}\right\} $	*	${21.61 \atop 2.81}$	
Steel—tons					.69								$\left\{ \begin{array}{c} 52.93 \\ 3.32 \end{array} \right\}$		6.31 8.71
Concrete cu. yd										213.1 14.4	² 18.9 20.4				

- ¹ Includes 2 wing piles.
- ² For 36- and 21-inch steel stringers.
- * For heights of 10, 20, and 30 feet from grade to ground. Includes longitudinal bracing.
- 4 Quantities are per tower-2 pile bents braced longitudinally.
- ⁶ For heights of 10 and 23 feet from grade to ground.
- 6 Quantities are per tower-2 pile piers braced longitudinally.
- 7 For heights of 10 and 15 feet from grade to ground.

(2) Summary of materials for footings.

	Timber (mbm)	Unit	Timber								timber pil	lestals es		pedestals, piles	timber piles	Steel f	
			(mbm)	Unit	Steel (tons)	Unit	Concrete (cu. yd.)	Unit	Concrete (cu. yd.)	Unit	Piles (number)	Concrete (cu. yd.)	Piles (number)	Concrete (cu. yd.)	Piles (number)	Piles (number)	Steel (tons)
G93 94 95 96 97 98 99 101 102 103 104 105	.29 .32 .35 .58 .64 .70 .20 .35 .24 .51	G107 108 109 110 111 112 	.35 .18 .32 .16 .29 .14 	\$101 102 103 	1.89 2.85 3.75	F81 82 83 84 85 86 87 88 89 90 91 92 93	52 46 42 38 33 29 40 36 32 29 26 22 27	F94 95 96 97 98 99 101 102 103 123 124 125	24 22 19 17 16 15 5.9 5.4 4.8 10.8 12.9 15.1	F135 136 137 138 139 140 	5 6 7 8 10 11 	5.8 7.1 9.3 9.3 17.3 17.3 	4	5.1	12 22 20 30 38 	4	1.18

(3) Summary of materials for towers and spans.

				r												
	Framed tim	ber towers1										Timb	er spans		Steel spans	ı
Timber	spans	Steel s	рапз				Framed st	eel towers1				Y	^Timber2	Y	Co I	7771
Height (ftin.)	mbm	Height (ftin.)	mbm	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	Height (ft.)	Tons	Length (ft.)	(mbm)	Length (ft.)	Steel (tons)	Timber (mbm)
13-4 25-10 38-4 50-10 63-4	4.72 8.37 12.57 16.90 21.42	13-4 25-10 38-4 50-10 63-4	8.22 13.99 20.49 27.27 34.26	77 75 73 71 69	28.4 28.0 27.7 27.3 26.9	61 59 57 55 53	22.1 21.7 21.4 21.0 20.7	45 43 41 39 37	16.0 15.7 15.4 15.0 14.7	29 27 25 23 21	10.2 9.9 9.6 9.3 9.0	12 14 16 	1.11 1.32 1.56	15 20 25 30 30	1.57 2.56 3.70 5.05 2.93	.61 .81 1.02 1.22 1.22
75-10 	26.12	75–10 	42.00 	67 65 63	23.1 22.8 22.5	51 49 47 	20.3 16.7 16.4	35 33 31 	14.4 14.0 10.6	19 17 15	8.6 8.3 8.0	 		Spec. 35 40 45 50	6.42 8.52 12.18 17.54	1.42 1.63 1.83 2.03

¹ Material in tower span not included.

² Includes timber in deck.

² Includes timber in deck.

					Abutn	nents			Ben	nts			Pier	rs	_			Foot	ngs			_		Cowers		-	Sp	203		
				Hi	ghway ac	d railwa	ıy	High	way	Railw	vay	Highwa	ау	Railwa	у		Hig	hway an	d Railw	2y			Highwa	y and Rai	lway	H	lighway :	and Rail	way	
			Number													Steel pile	T	imber pi	e	Spread fo	octings		Steel	Т	imber		Steel		Timber	
Stock Numb er	ltem	Size	for one crew	Con- crete	Steel pile	Tim- ber pile	Tim- ber grill- age	Steel pile	Tim- ber pile	Steel pile	Tim- ber pile	Steel	Tim- ber pile	Steel I	per oile p	Con- crete Ste edes- frai tals		les- si	er cre	les- ag	I- be	t 15' l- to	' 35	ns Span 12.5 to 35'	s Span: 35' to 75'	15' to 50'	60' to 90' Less than 35' high	60' to 90' More than 35' high	11' to 16'	Source
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12,	(13)	(14)	(15)	16)	(17) (18	(1	9) (2	(2	1) (22	(2)) (24) (25) (26)	(27)	(28)	(29)	(30)	(31)	(32)
78–2965.04 78–2965.07 78–7585.07	Crane, truck mounted, gasoline-engine driven	3/8 cu. yd. 3/4 cu. yd. 3/4 cu. yd.	1 1 1		 X	 X	X	 X	 X	 Х	 Х 		 X		X		. .;				.	.			X 	X X	X X 	X 	X 	T/E or class IV. T/E or class IV. T/E or class IV.
78-5785.14 69-9280.5-3 66-5335.5-18 66-3250.5 66-5340.7 11-2650.4	Mixer, concrete, gasoline-engine driven, trailer mounted. Wheelbarrow, general utility, steel tray, steel handles	3 cu. ft. 1800 pound 500 cfm 5000 pound	1 12 1 1 1	X X X	 X X 	 X X X	 X	 X X	 X X 	X X X	 X X X	X	X X X		 X	X X X X X X X X X X X X X X X X X	X X X		. } : :	X	X	X	X	X	X	X	X	 X 	X	Class IV.
11-4619.24	Pump, centrifugal, gasoline-engine driven, base mounted, 2-inch discharge.	/	1	X										1		X	- 1		-											Class IV.
66-3270.105	Compressor, air, truck or trailer mounted, gasoline- engine driven, and accessories. Drill, pneumatic, portable, woodboring	#3 Morse Taper 24 in. 12 in. 70 lb. 55 lb. 3/4" x 23/4" shank	1 1 1 1 1 1 2	X X X X X X	X X X X X	X X X X X	X X X X X X	X	X X X 	X	X X X 		X X		X X X	X X X X X X X	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	X X X X X X X X X X X X X X X X X X X) 3 3 3 3	 X X	X X X X		,	X X X	X X X 	X X X 	X X X 	X X X 	X X X 	T/E or class IV. Class IV. Class IV. Class IV. Class IV. Class IV. T/E or class IV.
66-6845.5 40-1932.5-08 40-3871.3 40-5257.5 11-7468.5 66-8425.5 66-6070.3 40-4498.3-6	Nail driver, pneumatic with nail sets and rivet-buster. Rivet set, pneumatic, buttonhead for naildriver, 6 CND. Drill, pneumatic, portable non-reversible, for steel Grinder, pneumatic, rotary type Pump, sump, pneumatic, 2½-inch discharge Tamper, backfill, pneumatic. Lead, pile-driving, steel, hanging Drill, twist, high-speed-steel, taper shank, Morse Taper	5½" blade size 6 CND 78-inch # 3 Morse Taper 5 and 8 inch 150 gpm 20-, 15-, 10-foot sections 156 inch	1 2 1 1 1 1 1 1 12	X X X	X X X X X X X	X X X X	X X X	X X X X 	x 	X X X X X	X	X X X	x	X X X 	 X	X X		 	 	X X X	X	XXX	XXX			X X X X 	X X X X	X X X 	X	T/E or class IV. Class IV. T/E or class IV. T/E or class IV. T/E or class IV. T/E or class IV. Class IV. Class IV.
40-5455.3 40-9823.5 41-2009.7-5 41-4725.5-5 79-3015.7-10 79-3015.7-25 41-4692.2-5 41-4878.5-12	Wrench, pneumatic, reversible, impact type	3 inch stroke 3/2 to 11/4 inch 4 ft. 4 ft. 5 ton 12 ton	1 1 4 4 12 12 12 1 3	X X 	X X X X X	X X X 	X X X 	X X X X	X X X X	X X X X	X X X X X	 X	X X X X	 	X X X	X X X X X X X X X X X X X X X X X X X	. 3	3 C 3		X X X X	X X X X X X X X X X X X X X X X X X X		. X	XXX	X X X	X X X X X X	X X X X 	X X X X X X	X X X 	Class IV. Class IV. Class IV. Class IV. Class IV. Class IV. Class IV. Set 640-01 or
41-4944.3-15 41-4955.5-12	Jack, ratchet-lever, double socket, with foot lift	15 ton 12 ton	2 1	X X	X X	X X	X X	X X	X X	X X	X X	X X	X X	X X	x X	X X	2	ζ 2 ζ 2		X X	X X	X	X	X	X	X X	X X	XX	X X	class IV. Set 210.50. Set 640-01 or
43-2219.08-04 43-9215.5-08	Bolt, machine, steel, square head, with hexagon nut	. 4 inch %-inch	2 2		X X			X X		X X				77		X				X			X	·		X X	X X	X X		class IV. Class IV. Class IV.
Set 970-01 Set 970-02	‰-inch thick. Welding equipment, electric-arc Welding and cutting equipment, oxyacetylene	Set No. 1, 300 amp. Set No. 2	1 1	 X	 X	x	····	X X	x	X X	X	X X	 X	X X	 X	X	: : :	 		X	 K	X	X	X	 X	X X	XX	XX	X	T/E or class IV. T/E.
	Special tools for structural work (not in class IV at time	of publication)																												
41~2312.300~065 41~5812.3 	Clamp, C-, heavy service	6½-inch capacity 156-inch 78-inch rivets 76-inch and 1-inch bolts 156-inch	6 -2 3 2 6	 X	X X X X	 X	X	X X X X X	 X	X X X X	 X		X	X X X	 X	X X X X X X		נֵ נ		Х			: X	 X	 X	X X X X	X X X X	X X X X	 X	
	Hole cutter, adjustable highspeed steel, Morse taper No. 3, Clark, No. 4 or equal, with 3 sets blades, pilot and 3/8-inch drill.	1½- to 3-inch															.				.	. x	: x	:				X		
41-49385-10	Jack, pushing and pulling, ratchet type	. 10-ton	2	Х	x	Х	x	Х	x	x	X	x	x	x	x	$\mathbf{x} \mid \mathbf{x}$. 2	()	()	x x	: [x	: x	: x	x	X	X	X	X	X	

May be used instead of multiple 105 cfm units.
 See table XXXIC.
 See table XXXIB.

TABLE XXXIB. Tool set for riveting with \(\gamma_{\text{s}}\)-inch steel rivets.

Stock No.	Description	Quantity in set
40-5488.180-610	Hammer, pneumatic, riveting, 18-pound.	1
40-5950.06-2	Holder-on, pneumatic, 8-inch closed length with	
	set.	1
40-7732.5-08	Rivet set, pneumatic, buttonhead, 1/8-inch, retainer	
1	type.	3
41-3604.11-18	Forge, coal-burning, rivet-heating, 18-inch.	1
41-6508.3-5	Rake, fire, portable forge.	1
41-7457.5-5	Shovel, blacksmith, portable forge.	1
	Tongs, rivet-heating and pitching.	1
	Tongs, rivet-sticking.	1
	Can, rivet-catching, handled.	1
	Bar, dolly, riveting 1/8-inch offset.	2
	Bar, dolly, riveting 1/8-inch heel.	2
	Chisel, rivet-buster, 11/4-inch edge.	1
	Rivet-buster, handled, 11/2-inch edge.	1
	Punch, backing-out, bar.	1
	Punch, backing-out, handled.	1
	Hammer, striking, handled, 8-pound.	1
	Wrench, structural offset, 15/18-inch opening,	
	15-inch.	2

TABLE XXXIC. Erection equipment, steel and timber, set.

Stock No.	Description	Quantity in set
	Wrench, structural offset, 15/16-inch opening,	
	18-inch.	2
	Wrench, structural offset, 1½-inch opening,	
	18-inch.	2
••••	Wrench, ratchet, reversible, 16-inch handle with:	
	Loose open socket, 6-point, 15/16-inch for	
	₹%-inch bolts.	2
	Loose open socket, 4-point, 11/2-inch for 1-	
	inch bolts.	2
41-1277.3-26	Bar, pinch, offset, 26-inch.	2
41-9537.5-5	Wrench, adjustable, crescent, 111/16-inch opening,	
	15-inch.	1
41-4347.5-08	Hammer, striking, handled, 8-pound.	1
37-2456.7-5	Belt, lineman's safety, leather.	2
21-7555.3-05	Rope, manila, 3-strand, 1/2-inch.	50 ft.

Note: Quantity of fitting-up bolts 25 percent of quantity of rivets. Two washers per bolt. Quantity of driftpins 30 percent of quantity of rivets.

TABLE XXXII. Required compressor capacity for portable pneumatic construction tools.

Compressor capacity required in percent of the total maximum possible air consumption of all tools connected.

			Nun	ber of to	ols		
Altitude	1	2	5	8	12	20	30
		Percen	t of total o	connected	tool consum	nption	•
At set level	100	90	80	75	70	60	55
3,000 feet	110	100	90	83	75	65	60
6,000 feet	120	110	100	90	80	70	65
10,000 feet	130	120	110	100	90	78	70
							<u> </u>

- c. Equipment can often be used to construct more than one unit or class of units. Cranes, special tools having only occasional use, and auxiliary equipment such as sharpening and repair tools serve several crews or details.
- d. Organic equipment should be fully utilized and class IV items drawn from depot only when necessary to supplement regularly issued equipment. Common hand tools included in engineer squad and engineer platoon sets for carpentry, pioneer, and demolition work have not been listed. They are presumed to be available on all jobs and must be increased in number if required.
- e. Table XXXIA does not include special supplies and equipment such as cordage, wire rope, rafting equipment and powerboats, diving sets, large air compressors, pipe and fittings, large pumps, hose for water and air, electric light plants, maintenance tools, goggles for welders, chippers, and grinders, safety belts for men working aloft, or other personal protective equipment. Those must be requisitioned in accordance with the job requirements
- **f.** The special tool sets listed below for manufacture and maintenance of small tools, jigs and fixtures should be available for all bridge construction. Trained specialists to operate this equipment must also be provided.

Blacksmith equipment, set No. 1.

Pipefitting equipment, set No. 1.

Rigging equipment, set No. 1.

Sign painting equipment, set No. 1.

Surveying equipment, set No. 6 (general-purpose).

- g. Large-capacity compressors operating several air tools can be used instead of the 105cfm truck-counted compressors of organic equipment. However, a single unit should not be depended on where a breakdown of that unit would stop the entire operation.
- (1) Volumes of air required to operate different pneumatic tools at sea level are given in table LXXXI.
- (2) All tools drawing air from a single compressor are rarely in operation at one time. Capacity requirements at different altitudes for compressors driving several air tools are given in table XXXII. Compressors driving riveting equipment must be large enough to operate all hammers at full capacity.
- 89. LABOR REQUIREMENTS. a. Tables of labor requirements. Normal man-hour requirements for typical construction operations are given in table XXXIII. Man-hours of labor required to construct each unit are shown in tables XXXIV to XXXVII, inclusive. These tables also list the size crew normally required for efficient work in each operation.
- (1) Tables are based on civil construction practice under average working conditions using power tools whenever possible. In military construction, allowance must be made for:
- (a) Skill of workers, training of troops.
- (b) Working conditions, extreme heat or cold.
- (c) Adequacy of equipment.
- (2) The tables give man-hours of direct labor only. They do not make allowance for lost time, time required to deliver materials and equipment to the site, maintenance of equipment, administration, supervision, and other overhead items. Tables include foremen but do not include machine operators who accompany equipment.
- b. Use of tables. After the lay-out is determined and the units of construction chosen, man-hours of labor for each principal operation are tabulated for all units of the bridge.

TABLE XXXIII. Man-hours of labor required for principal construction operations in terms of units of quantity.

Operation	Unit	Man-hours per unit	No. of men in crew
Steel			
Bolting	Bolt	.060	2
Chipping	Lin. ft	.083	1
Cutting (oxyacetylene)	Lin. ft	.067	2
Drilling	Lin. ft	3.200	2
Driving steel piles	Lin. ft	.133	8
Handling (arrival through fabrication)	Ton	7.000	7
Span erection	Ton	2.500	9
Tower erection	Ton	3.500	9
Laying out	Hole	.040	2
Pattern making			2
Reaming (10% all holes)	Hole	.067	2
Riveting			
Erection	Rivet	.150	4
Fabrication	Rivet	.100	4
Welding	Lb	.700	2
Timber			
Bolting	Bolt	.133	2
Boring	Lin. ft	.100	2
Driving driftbolts	Bolt	.017	1
Driving nails	Nail	.003	1
Driving spikes	Spike	.008	1
Driving piles	Lin. ft	.200	8
Handling (arrival through fabrication)	Fbm	.010	7
Handling			
Span erection	Fbm	.004	9
Tower erection	Fbm	.006	9
Laying out	Fbm	.004	2
Sawing	Sq. ft	.033	2
Sawing piles	Pile	.167	2
Excavation, hand	Cu. yd	1.000	7
Handling cement	ВЫ	.133	9
Handling piles	Pile	1.000	7
Handling sand and gravel	Cu. yd	.500	5
Mixing and placing concrete	Cu. yd	2.000	24
Placing and removing scaffolds		ļ	4
	•		

- (1) Tables listing man-hours to construct abutments, bents, piers, and spans give directly the man-hours required for each unit.
- (2) Tables listing man-hours to construct footings and towers give man-hours required for each unit of quantity of principal material in that unit. This means that the quantities of principal materials must be taken from the material summaries shown in tables XXVII to XXX before labor requirements can be determined.
- (3) Man-hours and crew-hours of labor for all units are totaled to obtain the over-all requirements for each operation.
- (4) Man-hours are shown for riveted construction. Man-hours for welded construction approximate 70 and bolted construction approximate 95 percent of those required for riveted construction.
- **c.** Crews. The number of crews assigned to each operation must be sufficient to keep the work on schedule.
- 90. CONSTRUCTION SCHEDULE. a. Purpose. A construction schedule is a detailed time plan showing all operations in their proper sequence. Making a schedule is an aid to planning because it requires advance consideration of every operation and the equipment, labor, and materials associated with it.

TABLE XXXIV. Man-hours of labor to build units of class 50, single-lane, highway bridges.

(1) Labor to build abutments, bents, and piers¹

	Num- ber		_	I	Abutmen	its				В	ents					Piers	3		
Operation	of men	p	nber ile	Steel pile		mber illage	Со	ncrete	7	imber 1	oile	Steel		mber ile			Steel pil	e	
	in crew	Steel spans	Timber spans		3 ft.2	6 ft.2	3 ft.2	6 ft.2	Under 9 ft.3	9 to 17 ft. ³	17 to 28 ft. ³		Under 8 ft.3	8 to 12 ft.3	Under 6 ft.3	8 to 10 ft.3	12 to 14 ft. ³	16 to 18 ft.*	20 ft.
Sheet number		23	21	25	22	22	27	27	28	28	28	32	30	30	32	32	32	32	32
Excavation	7				14	29	53	74	•••••										
Pile driving	8	45	45	81					33	33	33	54	64	64	98	115	115,	116	116
Form building	9						59	73											
Concrete mixing and placing	24						43	59											
Steel fabrication				30								55			90	132	146	157	166
Handling	7			6								14			12	18	22	26	28
Drilling	2			17								25			45	71	79	84	90
Miscellaneous				7								16			33	43	45	47	48
Steel erection				8								44			58	81	86	92	98
Rigging and handling	9			3								26			30	35	37	39	41
Fitting up	2			1								4			7	11	12	12	13
Riveting	4			4		•						14			21	35	37	41	44
Timber framing																			
Handling	7																		
Boring and sawing	2	-			-	-												-	
Miscellaneous																			
Timber erection		18	13	21	44	55			8	34	46		47	63					
Rigging and handling	9	9	8	9	30	37			5	22	23		24	29					
Boring and sawing	2	3	1	3	4	3			1	5	9	*****	13	20					.
Miscellaneous		6	4	9	10	15			2	7	14		10	14					
Total man-hours		63	58	140_	58	84	155	206	41	67	79	153	111	127	246	328	347	365	380

¹ Man-hours of labor are total for one unit.

TABLE XXXIV. Continued

(2) Labor to build footings and towers1

West Admin 1995 (A. 1987) (A. 1987) (A. 1987)			Spread footing:	5		Pile for	otings		Tow	ers
Operation	Number of men in crew	Timber grillage	Steel grillage	Concrete pedestal	Concrete pedestal, timber piles	Concrete pedestal, steel piles	Timber sills, timber piles	Steel frame, steel piles	Framed steel tower	Frame timber tower
Sheet number		43	41	37	39	39	36	40	12	7-1
Unit of quantity		Mbm.	Ton.	Cu. yd.	Pile	Pile	Pile	Pile	Ton.	Mbn
Excavation	7	6	3	3	4	5				
Pile driving	8				7	17	8	9		
Form building	9			2	3	4				
Concrete mixing and placing	24			4	5	6				
Steel fabrication			20					28	29	
Handling	7		6					5	8	
Drilling	2		11					13	13	
Miscellaneous		**********	3					10	8	
Steel erection			6	•				11	20	
Rigging and handling	9		4					5	17	
Fitting up	2	***************************************	2		·			1	1	
Riveting	4	**********	. 0		*************			5	2	
Timber framing	*;	23								1
Handling	7	8								
Boring and sawing	2	11	••••••							•
Miscellaneous		4								
Timber erection		22			•		1			2
Rigging and handling	9	10		•			1			2
Boring and sawing	· 2	12								
Miscellaneous	•	0				*****	•			
Total man-hours		51	29	9	19	32	10	48	49	4

¹ Man-hours of labor are for one unit of quantity.

Because of this, no essential part of scheduled work is likely to be overlooked.

- **b. Preparation.** (1) The schedule is prepared from the tabulation of man-hours of labor required in each principal operation. It must take into account the following factors:
- (a) Time allowed for completion.
- (b) Equipment and troops available.
- (c) Delivery of construction materials.
- (d) Logical sequence of operations.
- (e) Necessary delays between operations.
- (f) Weather.
- (2) The construction schedule is a bar diagram with a separate bar for each principal operation. The time required to complete each operation is represented by the length of the bar for that operation. The schedule with bar diagram for a typical bridge is shown in table XL. It is prepared in the following order:
- (a) The number of crews for each operation is tentatively established. By dividing crew-days or crew-hours (taken from the tabulation of labor requirements in table XXXIX) by the number of crews used, the time in days or hours to complete the operation is found.
- (b) Starting and completion time for each operation is plotted on the date and hour chart, with attention to each of the factors listed in paragraph 90b. Schedules must be set up so preceding steps will be complete before subsequent work is to start.
- (c) After the tentative schedule is drawn up, the number of men and the essential pieces of equipment in each operation are noted. These are totaled for all operations to determine the number of men occupied each day or hour and the number of pieces of each principal equipment item required at one time.
- (d) Time allotted to the several operations is adjusted so the number of men required during the construction period is as uniform as possible, and each piece of equipment is used most efficiently.
- **c.** Use. (1) The first use of the schedule is to determine:
- (a) Number of men and amount of equipment required on whole job.
- (b) Distribution of men and equipment.
- (c) Number of men and amount of equipment required during any interval of construction period.
- (d) Time at which construction materials must be delivered to site.
- (2) During the construction period, the schedule guides the officer in charge in assigning men and materials to specific operations.
- d. Shifts. In these schedules, an 8-hour work period is referred to as a day. When two or three shifts are planned, the schedule must be prepared for shifts rather than for days. In planning such operations, full consideration must be given to the effect on efficiency of length of daylight, problems of night lighting, weather and other local conditions, and tactical problems.
- 91. REPORTS AND PROGRESS RECORDS. A simple and effective system of daily reports of work accomplished is necessary for proper job control. From these a progress report is compiled daily for submission to higher authority giving direct comparison between scheduled and actual construction progress. Figure 37(1) gives one form of construction progress chart which shows progress for the entire job as a curve in which percentage of completion is plotted against time. This graph can be used alone or together with the more detailed chart shown in figure 37(2). In the detailed chart, percentages of completion of the entire job and of each principal operation are represented by bar diagrams.

² Height from ground to grade.

⁸ Height from ground to top of cap.

92. ORGANIZATION CHART. It is advisable to prepare and post an organization chart showing specific responsibilities, channels of supervision, and coordination. Ordinarily, this is covered generally by the standing operating procedure (SOP) of the construction unit. However, each bridge project usually has some special features which necessitate modifying and elaborating specific duties to insure complete understanding by all personnel. A typical organization chart is shown in figure 33.

BRIDGE PROJECT

ORGANIZATION CHART HEADQUARTERS Commanding Officer **TROOPS EQUIPMENT** MATERIALS RESPONSIBLE CHARGE SUPPLIES Higher command function; staff action; troops assignment; labor requisitions; organic equipment assignment, loans, replacement; materials and supplies credit; expediting. Project Officer DIRECT CHARGE OF PROJECT Direct supervision of planning functions, and control: Bridge layout, design, material estimates; requisitions; surveys, staking out, sectioning, explorations; operations; construction methods; transportation and equipment assignment; construction schedules, labor estimates; progress, reports. Assistant Assistant Assistant Assistant

Heavy equipment Compressed air equipment Electrical and Welding Bolting, reaming welding equipmen Special shops and storage Riveting Figure. 33. Sample organization chart for bridge project. If more than one

Supervisor for

FABRICATION

Yard and plant

marking Timber framing

Cutting Drilling Assembly

Supervisor for

SUPPLIES AND MAINTENANCE

Material storage, receiving, issue Tool storage, issue maintenance

CHAPTER 9

Supervisor for

ERECTION

Rigging Timber and steel

Riveting Welding

Supervisor for

Site work Clearing Foundations Approaches

CONSTRUCTION

Concrete and forms

Bridge carpentry

PLANNING TYPICAL CROSSINGS

platoon is used, officer assistants supervise their work.

Section I. BRIDGE LAY-OUT

93. SCOPE. a. This chapter illustrates how to solve typical bridge problems. Determination of bridge lay-out is described for two typical crossings, one a high railway trestle bridge, the other a highway bridge. Construction planning is discussed only for the railway bridge; planning for the highway bridge or any other bridge would be similar.

TABLE XXXIV. Continued

(3) Labor to build spans.12

	<u> </u>				_	s	teel spans		-		
Operation	Size of crew	Timber spans	15 ft.	20 ft.	30 ft.	40 ft.	50 ft.	60 ft.	70 ft.	80 ft.	90 ft.
Sheet number		2	4	4	4	4	4	4	4	4	4
Steel fabrication			61	65	115	138	446	587	783	901	1352
Handling	7		8	12	28	42	67	118	116	150	256
Drilling	2		28	28	49	56	243	294	429	506	752
Miscellaneous			25	25	38	40	136	175	238	245	344
Steel erection	*******		41	43	56	62	76	272	277	301	326
Rigging and handling	9		29	31	38	44	55	242	252	267	291
Fitting up	2		3	3	4	4	7	8	10	11	12
Riveting	4		9	9	14	14	14	22	15	23	23
Timber framing	*******	40	29	35	51	67	85	105	118	128	154
Handling	7	20	15	19	29	36	45	67 .	63	69	100
Boring and sawing	2	9	6	6	8	13	17	11	23	25	14
Miscellaneous		11	8	10	14	18	23	27	32	34	40
Timber erection		24	12	16,	22	28	35	45	49	53	58
Rigging and handling	9	14	7	9	14	18	23	27	32	34	40
Boring and sawing	2	3	2	4	3	3	3	5	6	61	7
Miscellaneous	********	7	3	3	5	7	9	13	11	13	11
Total man-hours		64	143	159	244 .	295	642	1009	1227	1383	1890

¹ Man-hours of labor are total for one unit. ⁹ For walkways add 45.0 man-hours per mbm.

TABLE XXXV. Man-hours of labor to build units of class 50, double-lane, highway bridges.

(1) Labor to build abutments, bents, and piers.1

Operation	Num- ber			Abutments				Bents						Piers					
	of men	Timber pile			Timber grillage		Concrete		Timber pile				Timher pile		Steel pile				
	in crew	Steel spans	Timber spans	Steel pile	3 ft.2	6 ft.2	3 ft.2	6 ft.2	Under 9 ft.3	9 to 17 ft. ³	17 to 28 ft. ³	Steel pile	Under 8 ft.3	8 to 12 ft.3	Under 6 ft.3	8 to 10 ft. ³	12 to 14 ft. ³	16 to 18 ft. ₃	20 ft.*
Sheet number		66	64	69	65	65	71	71	72	72	72	76	74	74	76	76	76	76	76
Excavation	7				18	30	62	94	•••••										
Pile driving	8	70	57	95					45	45	45	66	89	89	98	116	117	118	119
Form building	ı					:	82	115											
Concrete mixing and placing	24						61	83											
Steel fabrication				51								90	-		140	162	176	198	212
Handling	7			8								22			19	23	28	35	38
Drilling				30								45			75	86	93	105	113
Miscellaneous				13								23			46	53	55	58	61
Steel erection				14								70			82	90	100	111	119
Rigging and handling	9			4								36			36	38	41	45	47
Fitting up	2			2								6			12	13	14	16	17
Riveting	4			8								28			34	39	45	50	55
Timber framing																			
Handling	7																		
Boring and sawing	2																		
Miscellaneous																			
Timber erection		26	18	34	60	74			12	39	57		58	76					
Rigging and handling	9	11	11	13	41	51		,	9	25	32		28	33					
Boring and sawing	2	- 5	2	9	5	4			1	6	10		17	23			-		
Miscellaneous		10	5	12	14	19			2	8	15		13	20					
Total man-hours		96	75	194	78	104	205	292	57	84	102	226	147	165	320	368	39 <u>3</u>	427	450

¹ Man-hours of labor are total for one unit.

3 Height from ground to top of cap.

² Height from ground to grade.

TABLE XXXV. Continued

(2) Labor to build footings and towers.1

Operation			Spread footing	s		Pile	footings	Towers		
	Number of men in crew	Timber grillage	Steel grillage	Concrete pedestal	Concrete pedestal, timber piles	Concrete pedestal, steel piles	Timber sills, timber piles	Steel frame, steel piles	Framed steel tower	Framed timber tower
Sheet number		89	87	83	84	85	81	86	55	50-53
Unit of quantity		Mbm.	Ton.	Cu. yd.	Pile	Pile	Pile	Pile	Ton.	Mbm.
Excavation	7	6	3	3	4	5				
Pile driving	8				7	17	8	9		
Form building	9			2	3	4				
Concrete mixing and placing	24			4	5	6				
Steel fabrication			20		***************************************			28	34	
Handling	7		6					5	4	
Drilling	2		11					13	15	
Miscellaneous		•	3					10	15	
Steel erection			6					11	16	
Rigging and handling	9		4					5	12	
Fitting up	2		2			***************************************		1	1	
Riveting	4	*	0					5	3	
Timber framing		23						T	T	18
Handling	7	8								6
Boring and sawing	2	11								8
Miscellaneous		4								4
Timber erection		22					1		1	25
Rigging and handling	9	10					1	4		16
Boring and sawing	2	12				***************************************				0
Miscellaneous		0								9
Total man-hours		51	29	9	19	32	10	48	50	43

¹ Man-hours of labor are for one unit of quantity.

TABLE XXXV. Continued

(3) Labor to build spans.12

		Timber spans	Steel spans									
Operation	Size of crew		15 ft.	20 ft.	30 ft.	40 ft.	50 ft.	60 ft.	70 ft.	80 ft.	90 f	
Sheet number		45	47	47	47	47	47	47	47	47	4 7	
Steel fabrication			93	112	177	231	607	909	1346	1874	2897	
Handling	7		19	29	43	67	116	150	195	277	395	
Drilling	2		35	41	78	97	298	502	785	1148	1857	
Miscellaneous			39	42	56	67	193	257	366	449	645	
Steel erection			48	54	72	84	109	310	334	382	435	
Rigging and handling	9		32	35	44	55	76	267	286	324	377	
Fitting up	2		4	4	5	6	10	13	18	20	20	
Riveting	4		12	15	23	23	23	30	30	38	38	
Timber framing		66	45	55	83	108	135	161	193	212	239	
Handling	7	35	30	39	45	58	74	88	108	117	131	
Boring and sawing	2	14	3	1	16	21	25	29	34	37	42	
Miscellaneous		17	12	15	22	29	36	44	51	58	66	
Timber erection		33	15	22	30	40	48	58	69	80	90	
Rigging and handling	9	21	11	15	22	29	36	44	52	59	66	
Boring and sawing	2	4	1	1	2	3	3	4	5	7	8	
Miscellaneous		8	3	6	6	8	9	10	12	14	16	
Total man-hours		99	201	243	362	463	899	1438	1942	2548	3661	

¹ Man-hours of labor are total for one unit. ² For walkways add 45 man-hours for mbm.

- **b.** It is assumed in this illustration that reconnaissance has been made, the site chosen, and surveys completed in accordance with instruction given in chapter 6.
- 94. SITE DESCRIPTION. The following assumptions are made:
- **a.** Characteristics of site. Data obtained by site survey shown in figure 34 include:
- (1) Topographic plan of site.
- (2) Location and alignment of bridge.
- (3) Ground profile on bridge center line.
- (4) Logs of borings.
- (5) Normal water level and high-water level.
- (6) Stream has fairly uniform flow.
- (7) Stream banks show evidence of scour and shifting of stream bed.
- **b.** Material. Steel, timber, cement, and aggregates are available. Adequate timber for piling cannot be found locally.
- c. Equipment. All pieces of construction equipment needed to supplement organic equipment can be drawn from depot, including crawler-mounted and truck-mounted cranes up to \(^3\)4-cubic-yard capacity.
- d. Construction period. The construction period falls between annual floods; river stage during construction will be approximately normal (elevation 131).
- e. Access to bridge site. Both banks at the bridge site are directly accessible by highway. Construction can proceed from both ends of the structure if desired.
- 95. LAY-OUT OF RAILWAY CROSSING. a. Height of bridge. The elevation of base of rail (elevation 180.0) across the bridge is determined by the grade of the approaches; in this case, the bridge will be about 40 feet high at the stream banks.
- b. Length of bridge. To avoid high approach fills, abutments are tentatively located at the rim of the stream valley. This fixes the length of the bridge at about 400 feet.
- c. Principal openings. A 50-foot center span is selected so as not to obstruct the channel and to permit foundations to be built on dry ground. This span length requires steel stringers. (See par. 8.)
- d. Foundation types. (1) Pile footings. (a) The boring logs indicate that the westerly three-fourths of the bridge will be on soft alluvial soil, either silty or sandy clay. These materials cannot safely support the load of 3,000 pounds per square foot necessary for spread footings. (See table XXV.) Pile footings must be used for this portion of the structure.
- (b) Timber friction piles are selected since bed rock is too far below the surface to justify using either timber or steel point bearing piles. (See par. 145.) Although subject to alternate wetting and drying, untreated piles would be satisfactory for semipermanent construction. However, since piling is not available locally and only creosoted piles are stocked in depot, these are requisitioned.
- (c) Penetration of about 25 feet is required to develop the needed bearing capacity of 18 tons per pile. (See table XXVI.) To allow for contingencies and cut-off, 30-foot timber piles are requisitioned.
- (d) The selection diagram (table XXIII) shows that for bridges over 30 feet high supported on timber piles, concrete pedestals are preferred.
 - (2) Spread footings. The easterly one-fourth of the bridge will be on rock

TABLE XXXVI. Man-hours of labor to build units of class 25, double-lane, highway bridges.

(1) Labor to build abutments, bents, and piers.1

	Num-				Abutmer	nts		'			Bents					Piers	3		
Operation	ber of men	Tin pi	iber le			nber llage	Cone	crete	T	imber p	ile		Tim pi			5	Steel pil	e	
	in crew	Steel spans	Timber spans	Steel pile	3 ft. ²	6 ft. ³	3 ft.2	6 ft.º	Under 9 ft.3	9 to 17 ft. ³	17 to 28 ft. ³	Steel pile	Under 8 ft.3	8 to 12 ft.	Under 6 ft.3	8 to 10 ft. ³	12 to 14 ft. ³	16 to 18 ft. ³	20 ft.3
Sheet number		106	104	109	105	105	111	111	112	112	112	116	114	114	116	116	116	116	116
Excavation	7				18	30	62	94											
Pile driving	8	51	45	95					33	33	33	54	64	64	98	115	118	118	118
Form building	9			•			82	115										•	
Concrete mixing and placing	24						61	83											
Steel fabrication				51					*			68			110	154	169	181	197
Handling	7			8								18			13	21	25	27	33
Drilling	2			30								33			57	82	91	99	107
Miscellaneous				13					*			17			40	51	53	55	57
Steel erection				14								52			66	86	93	105	112
Rigging and handling	9			4								28			32	36	38	41	45
Fitting up	2			2								5			9	12	13	18	18
Riveting	4			8								19			25	38	42	46	49
Timber framing																			
Handling	7						*												
Boring and sawing	2							1											
Miscellaneous															******				
Timber erection		22	19	34	60	74			8	34	46		47	63					
Rigging and handling	9	10	12	13	41	51			5	22	23		24	29					
Boring and sawing	2	3	1	9	5	4			1	5	9		13	20					
		99	6	12	14	19			2	7	14		10	14					
Total man-hours		73	64	194	78	104	205	292	41	67	79	174	111	127	274	355	377	404	427

¹ Man-hours of labor are total for one unit.

TABLE XXXVI. Continued

(2) Labor to build footings and towers.1

	Number		Spread foot	ings		Pile	footings		Tow	ers
Operation	of men in crew	Timber grillage	Steel grillage	Concrete pedestal	Concrete pedestal, timber piles	Concrete pedestal, steel piles	Timber sills, timber piles	Steel frame, steel piles	Framed steel tower	Framed timber tower
Sheet number		127	125	122	123	123	121	124	102	97-100
Unit of quantity	***************************************	Mbm.	Ton.	Cu. yd.	Pile	Pile	Pile	Pile	Ton.	Mbm.
Excavation	7	6	3	3	4	5				
Pile driving	8				7	17	8	9		
Form building	9			2	3	4				
Concrete mixing and placing	24			4	5	6				
Steel fabrication			20					28	34	
Handling	7		6					5	4	
Drilling	2		11					13	15	
Miscellaneous			3					10	15	
Steel erection			6					11	16	
Rigging and handling	9		4					5	12	
Fitting up	2		2					1	1	
Riveting	4		0					5	3	
Timber framing		23								17
Handling	7	8								6
Boring and sawing	2	11								7
Miscellaneous		4								4
Timber erection		22					1			27
Rigging and handling	9	10					1			26
Boring and sawing	2	12					***********	*		0
Miscellaneous		0								1
Total man-hours		51	29	9	19	32	10	40	50	44

¹ Man-hours of labor are for one unit of quantity

or sandy clay. Spread footings are satisfactory for this portion of the structure. Table XXIV shows that concrete pedestals are the preferred spread footings for bridges over 30 feet high.

- e. Superstructure. (1) The selection diagram (table XXIII) for bridges with pile foundations shows that framed steel towers are the preferred support for steel-stringer spans. The central part of the structure then will be a 50-foot steel-stringer span on framed steel towers with concrete pedestal foundations on timber piles. Tower spans will be 25 feet long. (See sheet 184.)
- (2) Two 50-foot spans and one 25-foot tower span will be needed to reach the east abutment. Similar construction is used on the west to permit duplication in fabrication. (See par. 84.) These spans are within the recommended lengths for spans on steel towers.
- (3) Tower 1 exceeds the recommended height for timber pile piers (table I) and a framed tower must be used. A steel tower conforming with the rest of the structure is chosen rather than a timber tower which also could be used.
- (4) Span 1 is made 25 feet long since this length gives a satisfactory location for the west abutment and duplicates the spans used on the towers. An 8-foot fill is used west of the abutment, since it is more economical than trestle construction and ample waterway opening has been provided. (See par. 75a.) The fill retained by the abutment is about 6 feet high.
- (5) At all tower bents, one span will have a fixed bearing and the other an expansion bearing.
- f. Selection of construction units. (1) Deck. Standard open timber deck without walkways will be used. This is shown on sheets 158 and 159. One refuge bay (sheet 174) will be provided near the center of the bridge.
- (2) Spans and towers. Lay-out of spans and towers fixes the construction unit drawing sets to be used. (See sheet 156.) These units are the following:
- (a) Towers 1, 2, 3, 4, and 5, framed steel towers, drawing set RR-5, sheet 184.
 - (b) Tower spans, 25-foot steel-stringer spans, drawing set RR-2, sheet 158.
- (c) Span 1; 25-foot steel-stringer span, drawing set RR-2, sheet 158.
- (d) Spans 2, 3, 4, 5, and 6, 50-foot steel-stringer spans, drawing set RR-2, sheet 159.
- (3) Foundations. Concrete pedestal units are determined by tower height and span length. Drawings showing these pedestals are given in set RR-13.
- (a) Pile footings. Type F138 footings are required for towers except the west bent of tower 1 where type F135 can be used. (See sheet 215.)
- (b) Spread footings. Type F124 spread footings are required to support columns of tower 5. (See sheet 216.)
- (4) West abutment. A timber pile abutment (drawing set RR-7) is chosen for the west abutment where the soil is not capable of supporting a spread footing. A six-pile abutment (four bearing piles and two wing piles) is required for a 25-foot span. (See sheet 195.)
- (5) East abutment. A concrete abutment (drawing set RR-7) is chosen for the east abutment, since the soil there has adequate bearing capacity. The large abutment (sheet 199) is required since height of retained fill is over 3 feet. A timber grillage abutment cannot be used at this location since the span supported by the abutment is over 15 feet. (See table XXIV.)
- g. Construction drawings. The general plan and elevation drawing (fig. 34) is completed by adding dimensions, elevations, and other data, including stationing of center line of substructure units, elevations of pedestals, mark number of footings, and heights of towers. Location of fixed and expansion bearings is also indicated.

² Height from ground to grade.

² Height from ground to top of cap.

- 96. LAY-OUT OF HIGHWAY CROSSING. Figure 35 illustrates a layout for a single-lane highway crossing at the location described in paragraph 94.
- a. Top of bridge deck is set to give clearance above high water. (See par. 74a.) Grades of approaches are not steeper than 10 percent.
- b. Tests have shown that the soil will not support spread footings, so pile supports must be used. Table XVII shows that timber stringers on timber pile bents are preferred for bridges less than 30 feet high. Timber pile piers will be used at each end of the central span.
- c. A 50-foot steel span is necessary across the stream, so the two piers will be above the steep banks. Stream width is then free from obstructions to drift or ice and foundations are not subject to scouring.
- d. The third span from the pile pier on the west side is over 17 feet high and the sixth span is less than 17 feet high. (See sheet 29.) Longitudinal bracing is required only under the third span.
- e. The east abutment is founded on rock. Since concrete is not needed for other units, a timber grillage abutment is used.

Section II. CONSTRUCTION PLANNING FOR A RAILWAY BRIDGE

- 97. DRAWINGS. Drawing sets for each construction unit are shown by the selection diagrams in tables XXIII and XXIV. Sheet numbers included in these sets are shown on sheet 156. The drawing sets required for the railway bridge described in section I are as follows:
- a. Abutments
 Set RR-7

 b. Pile footings
 Set RR-13

 c. Spread footings
 Set RR-13

 d. Framed steel towers
 Set RR-5

 e. Steel stringers
 Set RR-2
- 98. MATERIAL LISTS. a. Bridge materials. The drawings included in sets listed in paragraph 97 give complete bills of materials for each unit. Material quantities are shown in summary form in table XXX. The forms of typical bills of materials and of material requisitions are shown in table XXXVIII and figure 36 respectively.
- **b.** Erection materials. Quantities of materials needed for temporary construction, concrete forms, construction shelters, platforms, and scaffolding are estimated after the construction scheme has been outlined.
- **99.** MAN-HOUR REQUIREMENTS. a. Man-hour and personnel requirements are obtained from table XXXVII and are shown in table XXXIX. This data is used in making up the construction schedule shown in table XL.
- b. Table XXXIX is prepared as follows:
- (1) Entries in columns 1, 2, 5, 8, 11, 14, and 15 are taken directly from table XXXVII.
- (2) Entries in columns 3, 6, and 9 are obtained by multiplying values from table XXXVII by the number of piles in the footings for each tower.
- (3) The entry in column 12 is obtained by multiplying values from table XXXVII by 51, the cubic yards of concrete in the footings of tower 5.
- (4) Entries in columns 4, 7, 10, and 13 are obtained by multiplying values from table XXXVII by the tons of steel in each tower.
- (5) The entry in column 16 is obtained by multiplying values from table XXXVII by 5, since there are five 50-foot spans in the bridge.
 - (6) The entries in column 17 are estimated.
 - (7) The entry in column 18 is the sum of columns 1 to 17 inclusive.

TABLE XXXVI. Continued

(3) Labor to build spans.12

	C: .	m				5	iteel spans				
Operation	Size of crew	Timber spans	15 ft.	20 ft.	30 ft.	40 ft.	50 ft.	60 ft.	70 ft.	80 ft.	90 ft.
Sheet numbers	*****	92	94	94	94	94	94	94	94	94	94
Steel fabrication			83	91	147	175	589	733	1170	960	1522
Handling	7		10	15	35	48	83	106	148	187	227
Drilling	2		42	44	70	82	299	389	655	505	873
Miscellaneous			31	32	42	45	207	238	367	268	422
Steel erection			53	55	76	81	97	294	312	341	360
Rigging and handling	9		30	32	41	46	62	248	266	283	302
Fitting up	2	*	8	8	12	12	12	16	16	20	20
Riveting	4		15	15	23	23	23	30	30	38	38
Timber framing		55	42	54	80	107	139	159	185	209	235
Handling	7	29	24	30	45	59	77	88	103	117	131
Boring and sawing	2	12	6	0	13	18	24	27	31	,	38
Miscellaneous		14	12	15	22	30	38	44	51	33 59	66
Timber erection		28	19	24	32	42	52	60	71	83	
Rigging and handling	9	18	12	16	22	30	38		1		94
Boring and sawing	2	2	2	10	1 22	30	26	44	51	58	66
Miscellaneous	_	7	, ,	4	4	9	,	0	8	11	12
Total man-hours	*	83	197	224	335	405	<u>9</u> 877	1246	12 1738	14	2211

¹ Man-hours of labor are total for one unit.

TABLE XXXVII. Man-hours of labor to build units of E-45 railway bridges.

(1) Labor to build abutments, bents, and piers1

					Abu	itments					Bei	nts					Piers			
	Num- ber	Ti	mber pi	le			mber llage	Con	crete	,	Timber	pile			mber ile ⁶			steel pile	5	escioni intri
Operation .	of men in crew	Ste spa 15-25' long		Tim- ber spans	Steel pile	3 ft.²	6 ft. ²	3 ft.2	6 ft. ²	Under 9 ft.3	9 to 17 ft. ³	17 to 28 ft. ³	Steel pile4	Under 8 ft.3	8 to 12 ft. ³	Under 6 ft.3	8 to 10 ft. ³	12 to 14 ft. ³	16 to 18 ft. ³	20 ft.
Sheet number		195	195	193	197	194	194	199	199	200	200	200	204	202	202	205	205	205	205	205
Excavation	7						,	91	90											
Pile driving	8	45	70	45	92					33	33	33	59	107	107	210	210	210	210	210
Form building	9	*****						48	67											
Concrete mixing and placing	24		,					47	56											
Steel fabrication					39								504			548	611	650	727	733
Handling	7				6								82			45	58	80	88	94
Drilling	2				22								337			362	372	381	434	434
Miscellaneous					11			,					85			141	181	189	205	205
Steel erection					16								132			180	272	307	360	363
Rigging and handling	9				4								68			83	115	124	131	134
Fitting up	2				4								48			29	41	45	51	51
Riveting	4				8								16			68	116	138	178	178
Timber framing				*****			•													
Handling	7															ļ				
Boring and sawing	2																			
Miscellaneous																				******
Timber erection		15	22	13	32	31	45			8	30	41		56	124					
Rigging and handling	9	6	10	6	8	20	26			6	20	25		34	53	ļ				
Boring and sawing	2	4	5	1	8	2	4			1	4	7		11	32					
Miscellaneous		5	7	6	16	9	15			1	6	9		11	39					
Total man-hours		60	92	58	179	31	45	186	213	41	63	74	695	163	231	938	1093	1167	1297	1306

¹ Man-hours of labor are total for one unit.

² For walkways add 45 man-hours per mbm.

² Height from ground to grade.

³Height from ground to top of cap.

⁴Unit is two bents with longitudinal bracing.

⁶ Unit is two piers with longitudinal bracing.

TABLE XXXVII. Continued.

(2) Labor to build footings and towers.1

	Number		Spread footis	ngs		Pile	e footings		Tov	wers
Operation	of men in crew	Timber grillage	Steel grillage	Concrete pedestal	Concrete pedestal, timber piles	Concrete pedestal, steel piles	Timber sills, timber piles	Steel frame, steel piles	Framed steel tower	Framed timber tower
Sheet number		223	218	214	215	216	212	217	184	175–179
Unit of quantity	*	Mbm.	Ton	Cu. yd.	Pile	Pile	Pile	Pile	Ton	Mbm.
Excavation	7	6	3	3	4	6				
Pile driving	8				7	15	8	9		
Form building	9	*************		2	3	4				***********
Concrete mixing and placing	24	***********	***********	4	5 `	6				
Steel fabrication		*	20		********		***********	28	37	
Handling	7		6					5	4	
Drilling	2		11					13	25	
Miscellaneous	<u></u>		3					10	8	
Steel erection	***************************************		6					11	23	
Rigging and handling	9		4					5	16	
Fitting up	2		2					1	2	
Riveting	4		0			*********		5	5	
Timber framing		23								18
Handling	7	8				*********				6
Boring and sawing	2	11				•				8
Miscellaneous		4								4
Timber erection	**********	22					1			33
Rigging and handling	9	10					1			31
Boring and sawing	2	12					***********			0
Miscellaneous		0	***********	***********						2
Total man-hours		51	29	. 9	19	31	10	48	60	51

¹ Man-hours of labor are for one unit of quantity.

TABLE XXXVII. Continued.

(3) Labor to build spans12

								Steel Sp	ans		
Operation	Size of crew	Timber spans	15 ft.	20 ft.	25 ft.	30 ft.	Special 30 ft.	35 ft.	40 ft.	45 ft.	50 ft.
Sheet number		157	158	158	158	158	158	158	158	158	159
Steel fabrication			65	76	112	112	103	139	166	383	579
Handling	7		9	14	26	24	20	43	60	67	123
Drilling	2		30	36	53	53	60	60	68	211	292
Miscellaneous			26	26	33	35	23	36	38	105	164
Steel erection			38	41	58	54	57	63	62	85	130
Rigging and handling	9		29	30	35	38	40	40	41	55	69
Fitting up	2		2	3	4	4	4	4	4	8	12
Riveting	4		7	8	19	12	13	19	17	22	49
Timber framing		27	9	14	21	19	19	23	28	29	33
Handling	7	13	5	7	11	10	12	14	15	15	21
Boring and sawing	2	8	2	3	3	4	2	4	4	6	3
Miscellaneous		6	2	4	7	5	5	5	9	8	9
Timber erection		15	6	8	6	11	9	12	11	17	18
Rigging and handling	9	9	3	4	4	5	5	6	7	8	9
Boring and sawing	2	2	1	1	1	1	1	1	1	3	3
Miscellaneous	*********	4	2	3	1	5	3	5	3	6	6
Total man-hours		42	118	139	197	196	188	237	267	514	748

TABLE XXXVIII. Bills of materials for a typical railway bridge.

(1) Bill of materials—structural steel.

Description		Piece			Quan- tity for one	Total:	required
	Mark	Size (in.) (lb.)	Length (ftin.)	Unit Weight (lb.)	onstruc- tion unit	Quan- tity	Weight (lb.)
Six 25-foot spans:							
Stringers	404	30 I 108	24-101/2	2,686	1	6	16,116
Stringers	405	30 I 108	24-101/2	2,686	1	6	16,116
(Other items entered	from bill	of materials	, sheet 160	.)			
Five 50-foot spans:							
Stringers	414-417	36 I 150	40-0	6,000	4	20	120,000
Stringers			9-101/2	, , , , , ,		20	29,740
(Other items entered					_	-	->,, 10
·		•	· 	ĺ			
Five towers, 1 to 5-Ma	terials com	mon to all t	owers:		ĺ		
Cap beam	651	21 I 59	10-3	605	4	20	12,100
(Other items entered	l from bill	of materials	, table B, s	heet 186)		ļ
Tower 1, One-story, 15-f			for differe	nt tower	height	r:	
Tower columns	1727R L	12 I 65	15-21/4	985	4	4	3,940
(Other items entered 15-foot tower height		l of materia	ls sheet 19	2 and ta	ble A,	sheet	187 for
(Towers 2 to 5.		ich varv fo	or differen	t tower	height	s liste	d from
same sheets.)		, 1	1			 !	
West abutment:							
Bearing plates	P1	12x1	1–8	68	2	2	136
(Other items entered	d from bill	of materials	s, sheet 178	3.)			
~							
East abutment:	.						İ
Bearing plates		12x1	1-4	54	4	4	216
(Other items entered	trom bill	ot material:	s, sheet 178	3.)			

TABLE XXXVIII. Bills of materials for a typical railway bridge.

(2) Bill of materials—timber and piling.

Mark	Pi Size (in.)	ece Length (ftin.)	fbm.	Quantity for one construction unit		•
372	6x8	8–6	34	25	150	2,700
		sheet 16	1.)	-		
	ĺ	ı	,			
					ļ	
372	6x8	8–6	34	50	250	4.500
oill of m	aterials,	sheet 16	l.)			
			80	6	6	.480
oill of m	aterials,	sheet 19	6.)		! 	
		1				
					}	
		300		4	4	
		15–0		2	2	
ı		30-0		26	26	
}		30-0		32	96	
	372 pill of m 372 pill of m	Mark Size (in.) 372 6x8 oill of materials, 178 4x12 oill of materials,	372 6x8 8-6	Mark Size (in.) fbm. each 372 6x8 8-6 34 pill of materials, sheet 161.) 372 6x8 8-6 34 pill of materials, sheet 161.) 178 4x12 20-0 80 pill of materials, sheet 196.) 30-0 300 15-0 30-0	Piece Size Length fbm. construction unit	Piece Size Length fbm. fbm. Construction Quantity

¹ Man-hours of labor are total for one unit. ² For walkways and refuge bays add 45 man-hours for mbm.

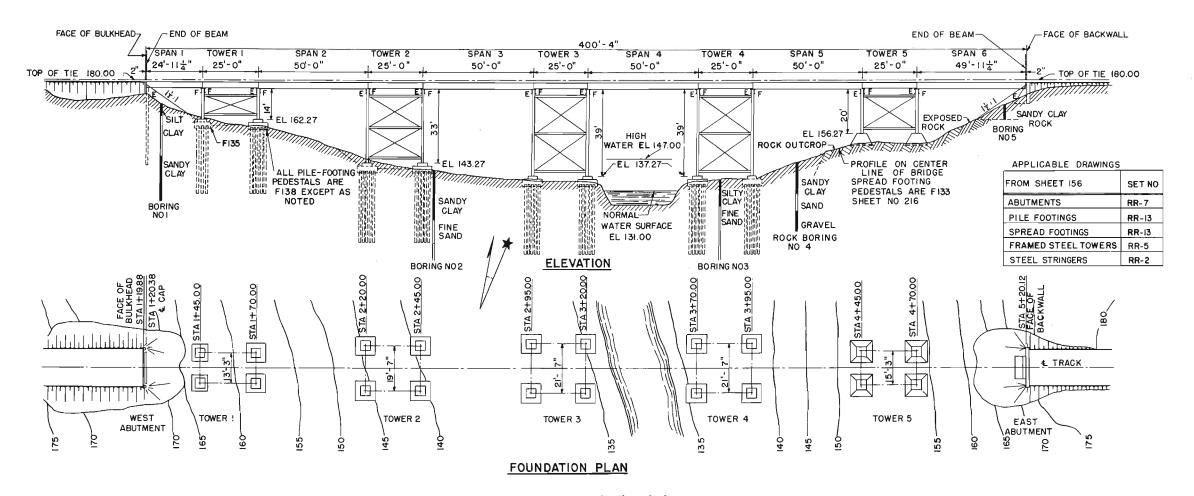


Figure 34. Lay-out of a typical railway bridge.

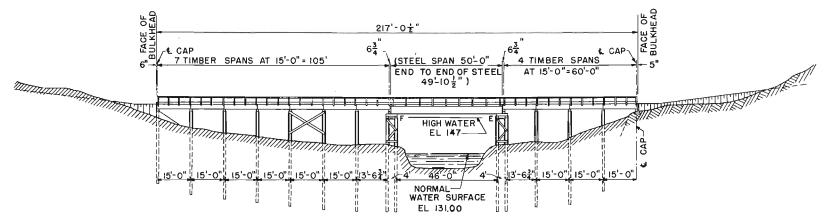


Figure 35. Lay-out of a typical highway bridge.

TABLE XXXVIII. Bills of materials for a typical railway bridge. Continued.

(3) Bill of materials—hardware

Description		Pie	ce		Quan- tity for one	Total re	quired
2.000.7.00.	Mark	Size	Length (in.)	Unit Weight (lb.)	construc- tion unit	Quantity	Weight (lb.)
Six 25-foot spans: Hook bolt with washer and nut(Other items entered fr		3/4"	13 sheet 10		16	96	202
Five 50-foot spans: (Other items entered fr	om bill of ma	terials,	sheet 1	61.)			
West abutment: Bolt with nut and two washers		3/4" aterials,	•	2.95 96.)	16	16	47
East abutment: Anchor bolt with nut and two washers		3⁄4"	24	3.5	12	12	42
Tower pedestals: Anchor bolt with nut and two washers	E24	1"	24	6.5	16	80	520

(4) Bill of materials—concrete1

	Cement sacks	Fine aggregate (cu. yd.) ²	Coarse aggregate (cu. yd.) ²
Per cubic yard	6.03	0.51	0.72
For 212.3 cu. yds	1,280	108	153
Waste 5 percent	63	5	8
Total required	1,344	113	161

 $^{^1}$ Quality of concrete: maximum size of aggregate, $2\frac{1}{2}$ -inch, water cement ratio 6 gal. per sack, slump 3 to 4 inches. See table XL, FM 5-10.

100. CONSTRUCTION SCHEDULE. Preparation of the construction schedule from the tabulation of man-hour requirements is discussed in chapter 8. The schedule of the typical railway bridge is shown by table XL.

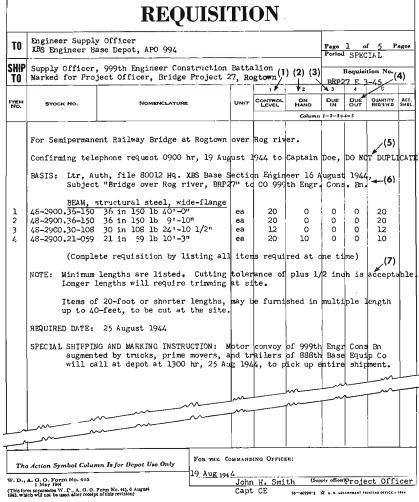
a. The entries in column 1 are taken directly from column 18 of table XXXIX. The values entered in columns 2 to 7 are computed in accordance with instructions given in chapter 8.

b. The days (par. 90d) required to complete each operation (col. 6, table XL) are plotted graphically on the schedule. In plotting these values, the necessary continuity of operations is kept in mind. The number of men employed each day should be as nearly constant as possible.

- c. The planned sequence of operations is as follows:
- (1) Clearing and earthwork are started immediately.
- (2) Fabrication, drilling particularly, requires more time than other operations and is started as early as possible.
- (3) Pile driving starts as soon as the first of the footings are excavated (normally the second day).
- (4) Form building and concreting start on the third and fifth days

respectively. Concreting is staggered with form building and excavation to balance personnel requirements.

- (5) Steel erection is started on the ninth day, as soon as the first concrete is 3 days old.
- (6) Dismantling equipment and clean-up work is done during the last few days as other operations are concluded and men become available.
- d. At the bottom of the bar graph, the total labor requirements for each day are shown. These totals do not include supervisory personnel, nor allow-



- 1. Column 1 shows total requirement for project.
- 2. Column 2 shows quantity available locally, including substitute, reclaimed, locally procured or produced materials.
- 3. Column 3 shows quantity previously requisitioned but not yet received.
- 4. Column 4 shows quantity due in or on hand which is committed to some other project or to be returned to depot as unserviceable or salvage.
- 5. Requisition confirming telephone or telegraph request is identified and marked DO NOT DUPLICATE.
- 6. Authority for issue is stated above the items on the requisition by citing the project order or showing a complete reference.
- 7. Special instructions such as grade of material, permissible substitutions, multiple or random lengths, pocking, marking, and unit load limitations are given for appropriate item numbers when necessary.

Property issue slip, ${\sf AGO}$ form 446, is preferred in some theaters, because it serves also as tally-out and shipping document.

Figure 36. Standard requisition form, showing required information, typical items, and guide for preparing material requisition.

ances for surveying, equipment maintenance, and delivery of materials to the site.

- 101. EQUIPMENT REQUIREMENTS. Tools and equipment needed in addition to organic items are shown in table XXXI A. The number of each equipment item needed is determined by the construction schedule, table XL. The special tool and equipment items for construction of the typical railway bridge are shown in table XLI. The following equipment use is planned.
- **a.** Cranes. One crane will be used in the fabrication yard and two at the site to drive piles and erect steel. Data on crawler-mounted and truck-mounted cranes are given in tables LXXXIII and LXXXII.
- (1) A 3/8-cubic-yard truck-mounted crane will be used in the fabrication yard to handle materials and finished parts.
- (2) A 3/4 cubic-yard crawler-mounted crane with 35-foot boom is needed to drive 30-foot piles. (See table LXXXIII.) This machine also will erect all parts of the structure from the ground except spans 3 and 4 and the upper story of towers 3 and 4.
- (3) Spans 3 and 4 will be erected from the deck with a $\frac{3}{4}$ -cubic-yard truck-mounted crane. The maximum load to be handled is one 50-foot stringer weighing 4 tons. It must be handled at 25-foot reach.
- b. Gin poles. Towers 3 and 4 are too high to be erected by a crane with standard 35-foot boom. Gin poles like these described in paragraph 211 will be used to erect the top stories of these towers. After erection of towers 2, 3, and 4, these poles will be cut to length and used as struts for towers 1 and 5. Towers 1 and 5 can be erected by cranes.
- c. Compressors. The number of pneumatic tools needed is obtained from the construction schedule, table XL. In the fabrication yard, most of the air required will be for drilling steel. Eight drills will be used and each drill requires 93 cfm of compressed air. (See table LXXXI.) Two 315-cmf trailermounted compressors will be needed. Additional capacity for peak requirements can be furnished by the 105-cfm truck-mounted compressors. The 105-cmf compressors will also furnish air for riveting crews. One compressor is needed for erection riveting.
- 102. PROGRESS REPORTS. Progress reports for the typical railway bridge are shown by figures 37(1) and 37(2). These are prepared from the percentage break-down of man-hour requirements. (See table XLII.)
- a. Table XLII is prepared by reducing the man-hours of labor required for each operation from table XXXIX to a percentage of the labor required to complete the entire bridge. These percentages are tabulated in columns 1 to 21 inclusive of table XLII. The work in each principal operation scheduled for completion at the end of successive periods is obtained by proportion from the construction schedule. (See table XL.) These proportions are applied to the percentages that the operations are of the entire work (col. 21) to obtain the entries in columns 22 to 27 inclusive.
- b. Total percentages from columns 22 to 27 inclusive are plotted as the schedule curve of figure 37(1) and from this curve, the graph of scheduled progress for the entire job is plotted (figure 37(2)). Scheduled progress in each operation is also plotted in figure 37(2), the length of the bar representing the duration of the operation being obtained from the construction schedule, table XL. At the end of each day percentage of work actually completed is estimated by referring to table XLII and plotted on the charts for comparison with scheduled progress.

² Damp-loose condition.

TABLE XLI. Special equipment list for constructing a typical railway bridge.

	Abut	ments]					า	owers						Sı	ans		T 4.1
Operation				No.	1		No.	2		No. 3 and 4	ļ		No. 5		Span	Spans	Gen- eral	Total man-
•	West	East	Foun- dation	Tower	Span	Foun- dation	Tower	Span	Foun- dation	Tower	Span	Foun- dation	Tower	Span	1	2 to 6		hours
	(1)	(2)	(3)	(4)	(5)	(v)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
Clearing ²																	240	240
Excavation		90	112			138			276			129						745
Pile driving	45		190			234			468									937
Form building		67	78			96			192			124						557
Concrete mixing and placing		56	133		·	163			326	·		196		•				874
Steel fabrication				296	112		518	112		1,110	224		318	112	112	2,895		5,809
Handling				32	26		56	26		120	52		34	26	26	615		1,013
Drilling				200	53		350	53		750	106		215	53	53	1,460		3,293
Miscellaneous				64	33		112	33		240	66		69	33	33	820		1,503
Steel erection				184	58	-	322	58		690	116		198	58	58	650		2,392
Rigging and handling				128	35		224	35		480	70		138	35	35	345		1,525
Fitting up				16	4		28	4		60	8		17	4	6	60		205
Riveting				40	19		70	19		150	38		43	19	19	245		662
Timber framing					21			21	*****		42			21	21	165		291
Handling					11			11			22			11	11	105		171
Boring and sawing					3			3			6			3	3	15		33
Miscellaneous					7			7			14			7	7	45		87
Timber erection	15				6			6			12			6	6	90		141
Rigging and handling	6				4			4			8			4	4	45		75
Boring and sawing	4				1			1			2			1	1	15		25
Miscellaneous	5				1			1			2			1	1	30		41
Cleanup, etc. ²									·					-			400	400
Total man-hours	60	213	513	480	197	631	840	197	1,262	1,800	394	449	516	197	197	3,800	640	12,386

Stock number	Description	Number required
78-7585.07	Crane, crawler-mounted, gasoline-engine driven,	
	35-foot boom, 3/4 cu. yd	1
78–2965.07		
	3⁄4 cu. yd	1
78-2965.04	Crane, truck-mounted, gasoline-engine driven,	
	3/8 cu. yd	1
66-6070.3	Lead, pile driving, steel hanging	1
	Hammer	1
11-2650.4	Jetting set, portable, complete with gasoline-engine	
	driven 200 gpm centrifugal pump and accessories	1
66-3250.315	Compressor, air, trailer-mounted, 315 cfm	2
78-5785.14	Mixer, concrete, gasoline-engine driven, trailer-	
	mounted, 14 cu. ft.	1
69-9280.5-3	Wheel barrow, steel tray and handles, 3 cu. ft	12
11-4619:24	Pump, 55 gpm centrifugal, gasoline engine driven,	
	base-mounted, 2-inch discharge	1
40-3871.3	Drill, penumatic, portable, nonreversible, for steel	8
	Erection equipment, steel and timber, structural, set	1
	Riveting equipment, structural, set	1
	Rigging equipment, set No. 1	1
	Blacksmith equipment, set No. 1	1
	Pipefitting equipment, set No. 1	1
	Rigging equipment, set No. 1	1
	Sign painting equipment, set No. 1	
	Surveying equipment, set No. 6	

Table XL. Construction schedule for a typical railway bridge

Operation	Total man- hours	Man- days	Size of detail	Detail- days	Number of details	Days re- quired	Men re- quired														c	onstruc	tion p e ri	od—day	5													
	(1)	(2)	(3)	(4)	(5)	(6)	(7)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
Clearing	240	30	10	3	1	3	10	X	X	x								(****		
Excavation	745	93	7	13	2	7	14	X			X		X	X		X		X	X]				
Pile driving	937	117	8	15	1	15	8		X	X	X	X	X	X	X	X	X	X	X	X	X	X	X															
Form building	557	70	9	8	1	8	9			X	X		X	X		X		X			X		X				J	•										
Concrete mixing and placing	874	109	24	5	1	6 ¹	24					X			X		X	-22		X	-:::	X		A	-:::					-::		::::						
Steel fabrication	5,809	726			J	25	29		X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	Х					
Handling	1,013	127	7	18	1 1	18	7																															
Drilling	3,293	411	2	205	8	25	16																										[****		
Miscellaneous	1,503	188					- 6						[***				····			l		x [Х	¨ X	X	X	X	X	X	X	 Х	X			v
Steel erection	2,392	299				21	15			•						X	X	A	X	A	A	^	Λ.	^	^	Λ	^	Λ.	^	_ ^	^	^	^	Α	A	^	^	Λ
Rigging and handling	1,525	191	9	21	1 1	21	9.															•						****									*	
Fitting up	205	26	2	13	†	13	Z		••••	••••					•																							
Kiveting	002	82	4	20	1	20	11		****														····	[[
Timber framing	291 171	36 21		2	';''	2	11												^		^	****	Λ										/					
HandlingBoring and sawing	1/1	4	/ /)	†	ן נ	2																			****	···· [
Missellaneous	33 87	11				2	2						- 1																									
Miscellaneous	141	18					11			****										Wor	k don e	by s	reel e	rectio	n det	ıil					****			•				
Rigging and handling	75	10		1	1	1	- 0									i						· 1												,				
Boring and sawing	25	3	2	2	i	2	ź												****																			****
Miscellaneous	41	{	-	-	1	-	-					••••																										
Clean-up, etc	400	sõ	10	5	1	5	10																							٠				X	X	X	X	X
Total ²	12,386	1,548	-	Me	n employe	ed²		24	47	56	60	61	60	60	61	75	76	75	77	76	72	76	72	68	44	44	44	44	44	44	44	44	44	25	25	25	25	25

¹ One day required for each tower and the east abutment.

¹ Man-hours required for supervision, surveying, equipment maintenance, etc. not included.

² Estimated roughly.

² Supervision, equipment maintenance, surveying, etc., not included.

c. The progress charts (fig. 37) assume the following status of work at the end of the tenth day of construction.

Clearing	complete.
West abutment	complete.
Span 1	complete.
Tower 1	complete.
Span 2	steel fabricated and timber
	framed.
Tower 2	foundations complete, steel
	fabricated, and timber framed.
Tower 3	foundations excavated, piles
	driven, forms built, and
	steel fabricated.
Tower 4	foundations excavated.

d. To prepare progress charts (fig. 37), the status of each operation as given above must be converted to percentage of completion. The calculations are shown below. (The percentages of total work represented by each operation on each unit of construction are from table XLII.)

Clearing	1.9% ÷	1.9% = 1	100%
Excavation	4.2% ÷	6.0% =	70%
Pile driving0.4 + 1.5 + 1.9 + 1.9 =	5.7% ÷	7.6% =	75%
Form building	2.2% ÷	4.6% =	48%
Concrete mixing and placing1.1 + 1.3 $=$	2.4% ÷	7.0% =	34%
Steel fabrication:			
001041001471			

$$0.9 + 2.4 + 0.9 + 4.7 + 4.2 + 0.9 + 4.5 + 0.9 = 19.4\% \div 46.9\% = 41\%$$
 Steel and timber erection:

0.1 + 0.1 + 0.5 + 0.1 + 0.5 + 1.3 =	$2.6\% \div 20.5\% =$	13%
Timber framing0.2 + 0.1 + 0.3 + 0.2 =	$0.8\% \div 2.3\% =$	35%
Clean up	$0\% \div 3.2\% =$	0%
Total work	$39.2\% \div 100\% = 3$	9.2%

CHAPTER 10

PRELIMINARY WORK AND CONSTRUCTION SURVEYS

- 103. PRELIMINARY. a. Pioneer work. The construction troops move up with pioneer tools and dozers, establish security, build pioneer access roads, prepare the site, and provide drainage.
- b. Access roads. Existing roads may have to be improved or new roads constructed to reach the site. High priority must be given to this work to permit early delivery of equipment and supplies.
- c. Preparation of site. The work area should be prepared in accordance with the approved construction plan. Preparation of site includes:
- (1) Clearing work areas of underbrush, trees, drift, and debris.
- (2) Clearing, leveling, and draining work areas for storage of materials, fabrication and framing operations, assembly of parts, turn-arounds, and tools and equipment.
- (3) Providing shelter for tools and supplies.
- (4) Providing dunnage for storage of materials.

- 104. ASSEMBLY OF EQUIPMENT. a. General. Tools and equipment should be assembled and prepared for use before they are needed. Priority should be given to tools and equipment used in early stages of construction.
- **b. Storage.** Provision should be made for sheltering tools stored at the site. Vigilant supervision is necessary to make sure that tools and equipment are returned to their storage place when not in use. Principal minimum space requirements for storage and maintenance of tools and equipment are:

- (3) Machine, blacksmith, and pipe-fitting shops, including tool sharpening 30 square yards or more.
- (4) Riggers' shop 20 square yards or more.
- c. Maintenance. Daily inspection, cleaning, lubrication, and repair are essential if tools and equipment are to be in good working order at all times. It is particularly important that ropes, slings, blocks, winches, brakes, and other equipment carrying heavy loads be checked for defects. Defective load handling equipment should be repaired or removed from service. This prevents serious accidents and delays.
- 105. ASSEMBLY OF MATERIALS. a. General. All material required for constructing the bridge is assembled at the site without delay. Priority is given to securing material needed in the early stages, particularly to assembly of steel which must be fabricated before erection. Assembly of material is coordinated with the construction schedule. (See par. 90.)
- b. Care in shipment. Care must be taken to avoid damage in assembling and transporting material. Light and heavy steel sections should not be loaded together. Small parts such as nails, bolts, rivets, and the like, should be packed in kegs or boxes. Adequate timber bracing and blocking should be provided to prevent material shifting during shipment.
- c. Storage. Materials delivered to the site should be immediately sorted and stored as described in chapter 11. Small parts like nails, bolts, nuts and washers, and rivets should be kept under cover. Cement must be off the ground

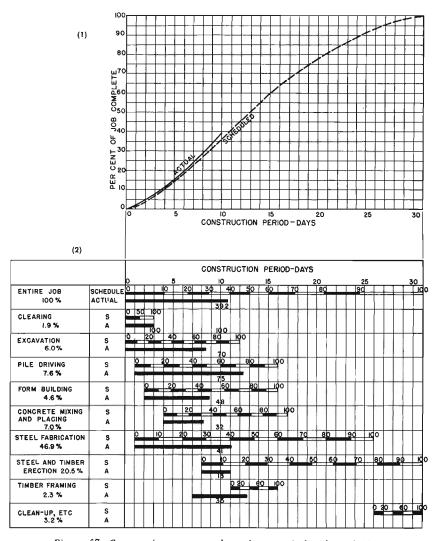


Figure 37. Construction progress charts for a typical railway bridge.

- (1) Progress graph.
- (2) Progress bar diagram.

TABLE XLII. Percentage break-down of man-hour requirements for a typical railway bridge.

	Abut	ments								Towers		_						Sp	ans				Per	cent of jo	ob compl	lete	
				No. 1			No. 2			No. 3	_		No. 4		_	No. 5		Span	Spans	Gen- eral	Per- cent of job	1st	Sth	12th	16th	26th	31st
Operation	West	East	Foun- dation	Tower	Span	Foun- dation	Tower	Span	Foun- dation	Tower	Span	Foun- dation	Tower	Span	Foun- dation	Tower	Span	1	2 to 6		0. 100	day	5th day	day	day	day	day
	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)	(24)	(25)	(26)	(27)
Clearing Excavation Pile driving Form building Concrete mixing and placing Steel fabrication Steel erection Timber framing Timber erection Clean-up, etc	0.4	0.7 0.5 0.4 	0.9 1.5 0.6 1.1 	2.4 1.5	0.9 0.5 0.1	1.1 1.9 0.8 1.3	4.2 2.6	 0.9 0.5 0.2 0.1	1.1 1.9 0.8 1.3 	 4.5 2.7	0.9 0.5 0.1	1.1 1.9 0.8 1.3	 4.5 2.8 	0.9 0.5 0.2 0.1	1.1 1.1 1.6 	2.5 1.6	0.9 0.5 0.2 0.1	0.9 0.5 0.2 0.1	23.4 5.2 1.3 0.4	1.9	1.9 6.0 7.6 4.6 7.0 46.9 20.5 2.3 3.2	0.9 Work	1.9 1.7 2.0 1.2 1.1 7.5 done	1.9 6.0 5.6 3.5 20.6 3.9 0.7 by ste			6.0 7.6 4.6 7.0 46.9 20.5 2.3 detail 3.2
Total	0.5	1.6	4.1	3.9	1.6	5.1	6.8	1.7	5.1	7.2	1.6	5.1	7.3	1.7	3.8	4.1	1.7	1.7	30.3	5.1	100.0	1.6	15.4	45.7	64.2	93.9	100.0

in a watertight shack or on a timber platform, where it should be covered with tarpaulins. Principal space requirements for storage are:

- (1) Stock-length storage adequate to handle 40-foot steel pieces and of sufficient size for tonnage in storage at one time, estimated at 1 square yard of net area per ton. Storage-pile width should not exceed 15 feet.
- (2) Timber storage estimated at 2 square yards of net area per thousand board feet (mbm).
- (3) Adequate space for storage of finished parts and fabricated or framed assemblies.
- d. Access to work and storage areas. All work and storage areas should be easily accessible to cranes with driveways 16 feet wide. No point in the storage, fabrication, or framing areas should be more than 10 feet from a driveway.
- 106. TRANSPORTATION. a. Truck-trailer. (1) Except for piles, the maximum length of stock-pile sections used in semipermanent bridges is about 40 feet. These sections can be transported by 8-ton or 16-ton full flat-bed trailers. (See fig. 38.)
- (2) Piles may be up to 90 feet long. Transportation of long piles requires two-wheel utility pole type trailers. Piles are carried by the trailer and in a pivoted cradle on the truck.
- **b.** Rail loading. (1) Units constructing these bridges ordinarily are not concerned with loading and rail transportation. However, they unload material at rail sidings or from cars at the sites of railway bridges.
- (2) All class IV materials except long piles can be carried in standard-length commercial railway cars, but some sections are too long for standard military railway cars. Where the length of pieces exceeds the length of cars, pieces are placed so their weight rests on one car, called the load car, and the overhang extends over an adjacent car, called the idler car. Extremely long piles may have to be carried in cradles on two load cars.
- **c.** Unloading. Trailers and cars are usually unloaded with a truck- or crawler-mounted crane. (See fig. 39.) However, light pieces can be unloaded by hand. Steel pieces should not be thrown from the trailer or car, but should be slid to the ground on skids. (See fig. 40.)
- 107. CONSTRUCTION SURVEYS. a. General. (1) Construction surveys with transit, level, and tape are made to stake out the work on the ground. Surveys are required to fix the elevation of sills and bearing plates and to



Figure 38. Steel-stringer sections loaded on a trailer. Timbers level the beams and chains and shoring secure the load. Stringers shown are for a 30-foot-span semipermanent highway steel bridge.

locate the position of anchor bolts and the center lines of bridge, foundations, and bearings.

- (2) The vertical distance from top of deck to top of cap or to bottom of bearing is shown on the assembly drawings for all units. Position of anchor bolts with respect to the bridge centerline and the centerline of the foundation is also shown for all units.
- (3) Bridge surveys are discussed in FM 5-10. Instructions on the use of instruments and the procedure followed in construction surveys are given in TM 5-235.
- b. Location of center lines of bridge and foundations. The position of the bridge centerline is established by the construction plan. It usually coincides with the centerline used in the site survey. The final centerline is located on the ground and marked by stakes set at each end of the line. From a starting

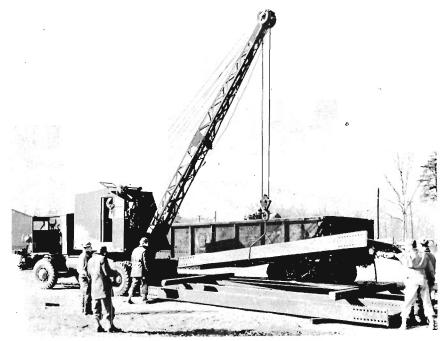


Figure 39. Unloading stringer sections from a gondola car with a \(\frac{1}{2}\)ection-yard truck-crane. The timber dunnage keeps the steel off the ground and facilitates placing wire-rope slings. Sections shown are for a 60-foot-span semipermanent highway steel bridge.

point at one abutment, also fixed in position by the construction plan, the locations of the other abutment and of each foundation unit are established.

- (1) Direct measurement. (a) Wherever conditions permit, centers of all units are established by direct lining with transit and measuring with tape. Distances between foundation units are measured and centers marked by stakes. The centerline of each bent is established by turning a 90° angle from the bridge centerline. The center of each footing or of each pile of pile bents is located by measurement from the bridge centerline and is marked. Reference stakes from which centers can be reestablished are preferably set outside the construction area where they will not be disturbed. Where this is not possible, their presence is made evident by guard stakes and flags.
- (b) Where wide streams or swampy areas are crossed and direct measurement on the ground is impossible, centerlines may be located by triangulation, or platforms from which measurements can be made, may be built on posts at the centers of each bent.
 - (2) Triangulation. (a) A base line running at approximately 90° to the

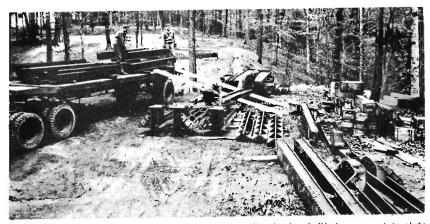


Figure 40. Unloading light steel sections from a trailer by hand. Skids are used to slide beams to the ground.

bridge centerline is laid out on firm level ground on one bank as close to the stream as practicable. The base line should be at least half the greatest distance to be measured; longer base line is preferable. One end of the base line is on the bridge centerline.

- (b) A point on the bridge centerline is established at random on the opposite bank. From each end of the base line, angles to the point on the far bank are carefully measured with a transit. From the measured angles and the known length of base line, the distance to the point on the far bank is computed.
- (c) Intermediate inaccessible points on the bridge centerline are established by turning computed angles from the base line to lines intersecting the bridge centerline at those points.
- (d) Extreme care must be used to avoid inaccuracies in triangulation. The base line and angles must be accurately measured and carefully checked.
- (e) For long triangulations, two base lines are preferred, one on each bank. Locations are made from one base line and checked from the other.
- c. Elevations of foundations and bearings. Before elevations are run to foundation units, bench marks should be established near both ends of the bridge and at other convenient locations near the construction areas. The reference elevation (datum) should be the one used in the site survey. Elevations of bearing on foundation units are given on the construction plan or may be obtained by subtracting the depth of the intervening superstructure and supports from the elevation of the bridge grade line. These elevations are marked by grade stakes set close to the construction areas. Grade stakes should be protected by guard stakes or framework.
- d. Anchor bolts and bearings. (1) Particular care must be used in setting anchor bolts. The position of anchor bolts in concrete foundations should be checked after forms are completed and immediately before concrete is placed.
- (2) After foundation units are completed, centers of bearings should be reestablished accurately on the finished foundation.
- e. Accuracy. Accurate measurements are extremely important in bridge construction and particularly for steel bridges. Steel tapes must be used for all measurements. These should be checked with the tapes used in fabrication and framing of parts. All measurements should be carefully checked to eliminate errors. Steel tacks marking the exact point of reference should be used in all survey stakes.

CHAPTER II

FABRICATION AND FRAMING

Section I. STEEL FABRICATION

- 108. GENERAL. a. Fabrication of steel for towers and superstructures consists of cutting, drilling, and assembling the shapes, plates, and bars received from engineer depots in stock sizes and lengths.
- **b.** Fabrication methods depend on the size of the structure, the tools available, and the skill of the personnel.
- c. Strength of the finished structure depends on careful fabrication and fitting, and the bolting, riveting, or welding by which parts are joined.
- d. Ease of making connections during erection is largely determined by the accuracy of fabrication.
- 109. TOOLS AND EQUIPMENT. a. Tools and equipment needed for fabricating semipermanent bridges are listed in table XXXI. This list does not include hand tools regularly issued to squads or platoons, or personal protective equipment such as goggles and safety belts.
- b. A crane, preferably the \(\frac{3}{8}\)-cubic-yard truck-mounted crane, should be available in the fabrication yard at all times for unloading steel and for moving and turning the heavier pieces during fabrication and assembly.
- 110. FABRICATION YARD. a. The fabrication yard is laid out to suit the fabrication procedure and the size of the bridge. It must be on firm, level ground, providing ample working space, and preferably should adjoin the bridge site.
- b. The yard is divided into the following areas:
- (1) Area for storage of stock-length steel.
- (2) Area for lay-out, cutting and drilling of individual parts.
- (3) Area for drilling and reaming assembled parts and for bolting, riveting, and welding.
- (4) Area for storage of fabricated subassemblies.
- 111. WORK SCHEDULE. a. Fabrication of steel should be started well ahead of erection so parts will be ready when needed.
- b. The work is divided so all available men and equipment can be employed. Maximum efficiency is obtained when work is organized on an assembly-line basis with each crew assigned the fabrication of one group or class of members.
- 112. MATERIAL RECEIVING AND STORAGE. a. Receiving. As material arrives at the site, each piece is checked to insure that its size and length are correct and that it is in good condition. Wrong-size pieces and pieces severely damaged in transit are returned for exchange.
- b. Record. A record is kept of each piece of material in the storage yard and its intended use.
- (1) Cutting lists are prepared and each piece is given the mark number or numbers in the bills of materials.
 - (2) All material taken from the yard is checked out by the stockkeeper.

- c. Storage. Time and labor are saved by storing materials carefully.
- (1) Pieces of one size and length are stored together on timber blocking. Pieces are separated so slings can be easily attached. If stacked in more than one layer, layers are separated with timber dunnage.
- (2) Pieces are stored so those needed first can be most easily reached.
- (3) All pieces are placed within easy reach of the yard crane. Stacks are not over 15 feet wide and are at least 16 feet apart.
- 113. STRAIGHTENING BENT MATERIAL. a. Bent or twisted pieces must be straightened before being used in fabrication.
- (1) If the damage is so severe that the strength of the piece is in doubt, it should be used only as miscellaneous stock to be cut up for secondary use.
- (2) No attempt should be made to reclaim pieces that have short kinks or buckles or that show surface cracks at the point of injury.

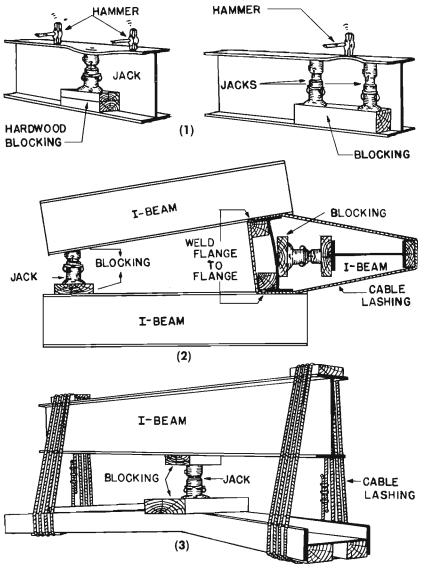


Figure 41. Methods of straightening bent beams with jacks and tackle.

- (1) Localized flange bends.
- (2) I-beam web bent longitudinally.
- (3) I-beam bent transversely.

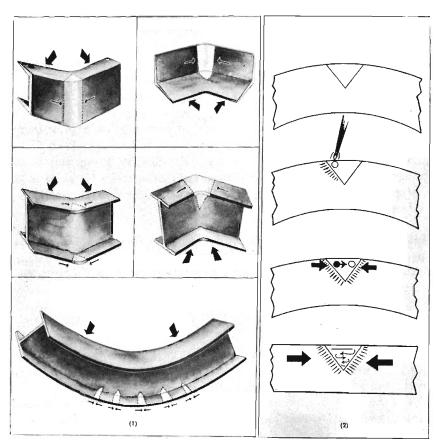


Figure 42. Heat-straightening of beams.

- (1) Areas to which heat should be applied to heat-straighten typical beams.
- (2) Sequence of operations in heat-straightening bent members.
- b. Examples of common damage to rolled beams and of methods of straightening them with jacks and tackle are shown in figure 41. Straightening is assisted by heating the metal with a blow torch or an oxyacetylene torch adjusted to a neutral flame.
- c. Members can also be heat-straightened as illustrated in figure 42. The outside of the bend is heated while the inside of the bend is kept cool. The heated metal tries to expand but is restrained by the cooler metal surrounding it. Then as the heated area cools and contracts, the member tends to straighten. By repeating the cycle of heating and cooling the metal on the outside of the bend, the member is straightened. Heat straightening procedure is as follows:
- (1) Mark with chalk the area to be heated. Usually this will be in the shape of a triangle because more heat is needed at the outside of the bend and less toward the center.
- (2) An oxyacetylene torch with a large welding tip is used. Hold the flame steady at a point near the apex of the triangle (toward the center) or at the outer edge as shown in figure 42(2) until the metal reaches a light cherry-red color.
- (3) When the area immediately under the tip has reached the proper temperature, slowly move the tip to one side so the heated area moves with it. Watch the work closely to keep the hot spot moving properly, otherwise there will be no upsetting and the metal may be burned. Under no circumstances

should the metal be heated to the melting point. Cool the metal on the inside of the bend with water, ice, or wet rags.

(4) Continue this procedure until the small circle of hot metal has covered all of the area within the triangle; then allow the member to cool. If the member is still not straight repeat the operation at the same or an adjacent point. A little heat applied several times is better than too much heat all at once. Long bends are straightened best by heating several times at intervals along the bend.

Caution: Operators should practice heat-straightening on scrap metal before attempting to straighten a structural member.

- d. If the strength of a piece is in doubt after straightening, it should be reinforced by welding on plates which extend far enough beyond the zone of apparent damage to develop their full strength.
- 114. LAY-OUT. a. General. (1) Lay-out is the process of marking material for cutting and drilling or welding. It must be done accurately for it determines the exactness of subsequent operations.



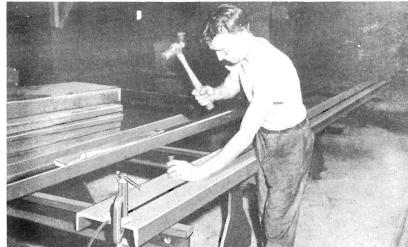


Figure 43. Lay-out procedure when little duplication is required. Steel tape clampea to the work for measurements from one end.

- (2) Only steel squares, steel rulers, and steel tapes are used. Woven metallic tapes must not be used for lay-out work. All tapes should be checked against each other to insure they are all exactly alike.
- b. Procedures. The two principal lay-out procedures are as follows:
- (1) Scratching. For members having little duplication, all cuts and holes are marked directly on the metal in the exact positions shown on the detail drawings. No guide or pattern is used, cuts and holes being located by direct measurement. (See fig. 43.) Cuts are marked with metal workers' soapstone crayon and all holes are center-punched. All measurements should be carefully checked.
- (2) Templates. Lay-out templates (fig. 44) are full-scale patterns of wood or stencil paper made to the exact size and shape of the piece for which they are used and containing all holes to be made in the finished piece. Holes are located exactly but are drilled only large enough to guide the center punching of holes in the steel with straight shank center punches. Templates are clamped to the material in exact position; all holes are center-punched and all cuts marked.

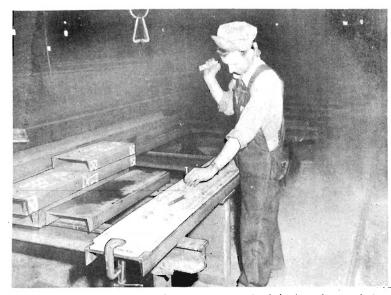
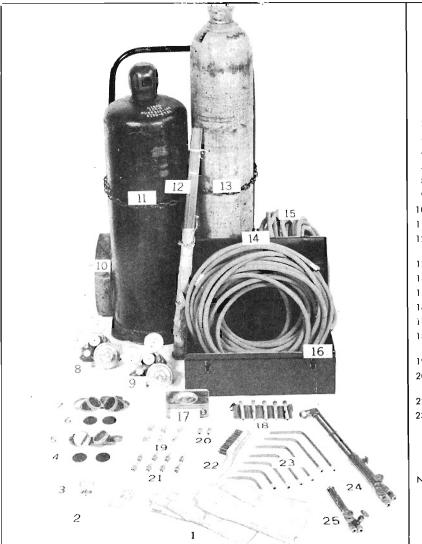


Figure 44. Wood template used to guide center-punching for holes in a short steel channel.

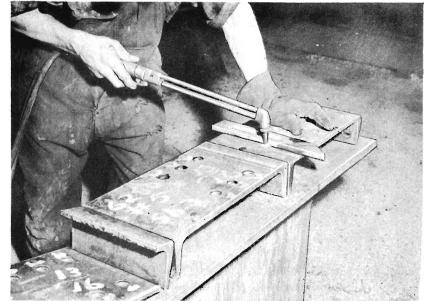


WELDING EQUIPMENT — SET NO. 2 Oxyacetylene

- Gloves, welder's leather.
- 2. Ignitor, oxyacetylene.
- Flints, ignitor, oxyacetylene.
- 4, 6. Lens, goggle, welder's, shades Nos. 5, and 6.
- 5, 7. Goggles, welder's type II.
- 8. Regulator, 2-stage, acetylene.
- 9. Regulator, 2-stage, oxygen.
- Truck, hand, gas cylinder, oxyacetylene.
- 11. Gas, acetylene, 225-cubic-foot cylinder.
- 12. Rods, welding, oxyacetylene, manganese bronze 3/16-inch, steel mild ½-inch, steel mild ½-inch.
- 13. Gas, oxygen 220- to 240-cubic-foot cylinder.
- 14. Hose, gas, acetylene, red with couplings, 5/16-inch, 50-foot.
- 15. Hose, gas, oxygen, green, with couplings, 5/16-inch, 50-foot.
- Box, welding and cutting equipment, steel.
- 17. Flux, welding, 1-lb. can.
- Torch, oxyacetylene, cutting, with 5 tips, Smith Nos. 2-4, 3-6, 4-6, 6-6, and 6SC; of Airco, Nos. 2, 4, 6, 8, and 11.
- 19. Clamp, hose, oxyacetylene, 5/16-inch.
- 20, 21. Coupling, hose, oxyacetylene, 5/16 thread; oxygen, right-hand 9/16-inch 18-thread; with nut and ¼-inch to 5/16-inch gland.
- 22. Brush, wire, scratch, with wood handle, 4 x 17 rows, 10-inch.
- 23, 25. Torch, oxyacetylene, welding with tips, Smith Nos. 50, 51, 52, 53, 54, 56, 57, B68, B69, B612; or Airco Nos. 1, 3, 5, 7, 8, 9, 10.

Not Shown: Adaptor, acetylene regulator.
Cleaners, welding and cutting equipment, cutting tip.
Wrenches, regulator; torch, cutting; torch, welding.

Figure 45. Oxyacetylene cutting and welding equipment, set No. 2.



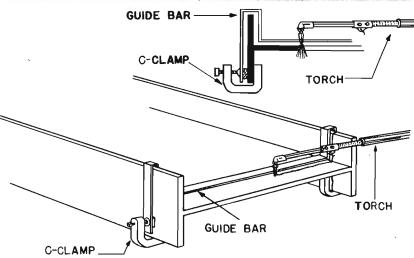
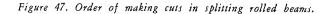


Figure 46. Guiding the oxyacetylene cutting torch.

- (1) Bar clamped to beam to guide torch.
- (2) Cutting steel channels with a torch guided by a flat bar laid on the line of the cut.
- (a) Templates for short members and plates are made in one piece of the same size as the piece to be fabricated.
- (b) For long members such as beams and columns, templates cover only the connections. Templates may be joined by a board to insure accurate spacing or may be handled separately, the template for each connection being clamped to the member after spacing and lining by measurement.
- 115. MARKING. Each part and each member of assembled parts is marked to correspond with markings on the detail drawings. The identifying number gives the principal member by mark number and the pieces attached to it in fabrication by letter and number. These marks are painted on each piece on completion of its lay-out, so pieces can be identified during fabrication, assembly, and erection.



116. CUTTING. a. General. The principal cutting tool in the field is the oxyacetylene torch. In the hands of a skilled operator, it is a fast and versatile tool. It is used in making all cuts in steel, to bevel edges for welding, and to cut rough holes for bolting and riveting, slots for anchor bolts on stringers, and anchor-bolt holes in steel-column base plates.

b. Oxyacetylene cutting torch. The oxyacetylene cutting torch is fitted with a tip containing a central jet which discharges pure oxygen surrounded by other jets which discharge mixed oxygen and acetylene. Tips are selected to suit the thickness of metal to be cut. Recommended tip sizes are given in table XLIII.

TABLE XLIII. Oxyacetylene cutting data.

Thickness of steel—inches	1/4	3/8	1/2	3/4	1
Diam, of cutting orifice—inches	.03	.03	.04	.06	.06
Cutting speed—					
lineal inches per minute	17-25	16-24	15-23	13-21	12-18
Oxygen consumption				-5	
cubic feet per hour	29-34	37-46	68-77	127-151	144-160
Acetylene consumption—		•	,,	/ -/-	*** ***
cu. ft. per hour	7-8	7–8	12-14	14-20	14-20

c. Procedure. (1) To preheat the steel to its kindling temperature in oxygen (1,400 F to 1,600 F), the torch flame is adjusted to neutral by gradually opening the oxygen valve and shortening the acetylene flame until a clearly defined inner luminous cone is visible at the end of the tip.

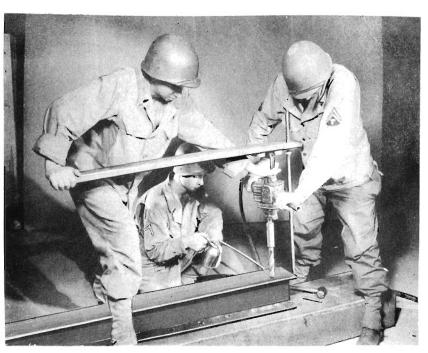
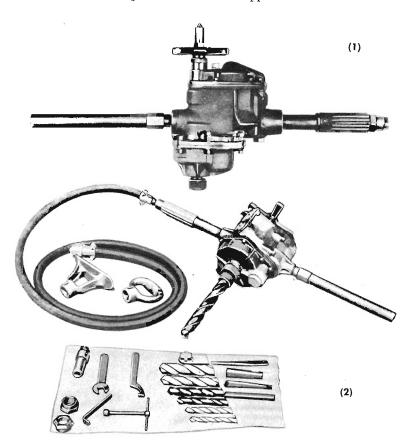


Figure 48. Drilling 15/16-inch holes in steel with the pneumatic wood borer.

- (2) To start the cut, the torch is held perpendicular to the work at the end of the cut; the inner core of the preheating flame should be about 1/16 of an inch from the metal.
- (3) The torch is held stationary until the metal under the tip is raised to a bright red heat; then the valve of the oxygen jet is slowly opened. As the cut starts, a shower of sparks falls from the opposite side of the work.



DRILL, PNEUMATIC, PORTABLE, NONREVERSIBLE, NO. 3 MORSE TAPER SOCKET, FOR STEEL, WITH ACCESSORIES

Drill, twist, high-speed steel, No 2 Morse taper, ½-, %-, and ¾-inch, each Drill, twist, high-speed steel, No 3 Morse taper, 78-, 1-, 118-, and 114-Canvas container, for twist drills Sleeve, Morse taper No 2 to No 3 Countersink, high-speed steel, No 3 Morse taper, 34-inch Breast plate, with stud and nuts Feed screw, 3%-inch travel Grip handle, with stud and nuts Leader hose, ½-inch, 20 feet long, with couplings Chuck, reamer Nipple, hose, 34- to 12-inch Pin, ejecting Wrench, socket, 7/16- and ½-inch, and spanner Gun, arease Tool box, wood or steel (3)

Figure 49. Portable pneumatic drill for up to 11/4-inch holes in steel.

- (1) Piston type, 41-pound drill with accessories.
- (2) Vane type, 35-pound drill.
- (3) Accessories for complete drill when issued with 105-cfm motorized compressor.

- (4) The flame is drawn slowly along the line of the cut. The movement should be just fast enough for the cut to continue to penetrate and cut completely. If the cutting is done properly, a clean narrow cut results.
- d. Guides. Where exactness in the finished cut is necessary, as at the ends of columns or beams, or for accurate splitting of beams, a torch guide is used. The guide can be a bar shaped to fit the beam and clamped to it (fig. 46(1)), or a straight-edged bar heavy enough to hold its position without slipping (fig. 46(2)).
- e. Splitting rolled shapes. T-shaped pieces are obtained by splitting I-beams lengthwise through the web. Release of internal stresses locked in beams during rolling causes parts to bend or warp when the beams are split unless the splitting process is carefully controlled. The proper procedure is to:
 - (1) Cut beams to length before splitting.
- (2) Make splitting cuts about 2 feet long, leaving 2 inches of undisturbed metal at the ends of the beam and between all cuts. (See fig. 47.) As the cut is made, cool the steel immediately back of the torch by laying wet burlap over the cut.
- (3) After splitting cuts have been made and the beam cooled, burn through the metal between cuts, starting at the center of the beam and working toward the ends.

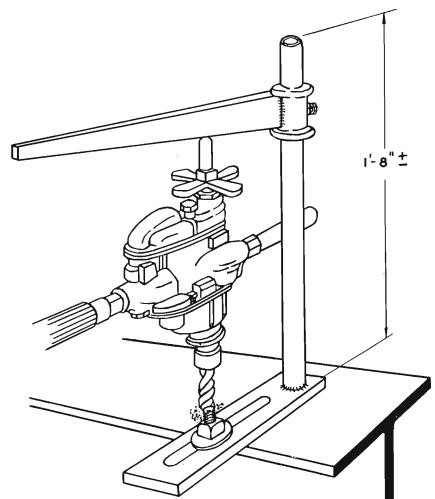


Figure 50. Adjustable clamp or "old man" used when drilling steel with pneumatic drill.

A drill bar may be used instead.

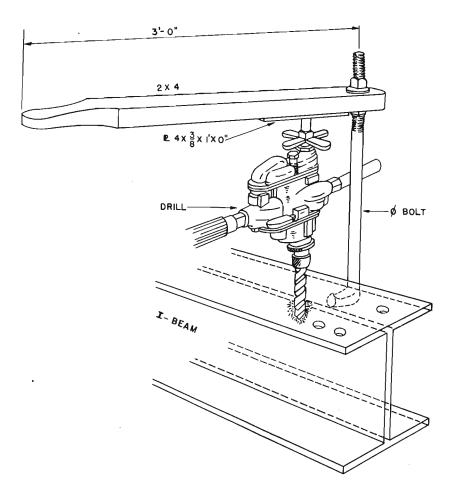


Figure 51. Drill bar used with pneumatic drill. The drill bar is less stable than the "old man" shown in figure 50.

- 117. TRIMMING. a. Cuts made with an oxyacetylene torch are rough, because melted and oxidized metal adheres to the cut edges. The oxidized metal can be removed with a chisel. Edges of the cut can be roughly smoothed by hammering; this gives edge satisfactory for most purposes.
- **b.** Where close-fitting joints are required, edges must be smoothed by chipping. Chipping is done with the pneumatic chipping hammer (stock number 40–5455) or with a cold chisel.
- c. Tolerances to which stringer sections must be cut are given in paragraph 223a (6) (b), 5 and 6.
- 118. GRINDING. It is seldom necessary to grind cut edges. However, end stiffener angles of girders and beams must fit closely against the bottom flange or be welded. The inside leg of the stiffener is shortened to clear the beam fillets and the outstanding leg is ground to an even bearing. Either portable or bench-mounted pneumatic grinders can be used. The use of power grinding tools is described in TM 5–225.
- 119. DRILLING AND CUTTING HOLES. a. Sizes of holes. (1) The following holes in steel are required for semipermanent bridges.
- (a) ½-inch-diameter holes in clips for attaching nailing strips to highway stringers.

- (b) 3/8-inch-diameter pilot holes used in cutting 1-9/16-inch-diameter and 2-1/16-inch-diameter holes.
- (c) 9/16-inch-diameter holes for $\frac{1}{2}$ -inch bolts, if nailing strips of highway stringers are attached by bolting.
- (d) 15/16-inch-diameter holes for $\frac{7}{8}$ -inch bolts and rivets.
- (e) 15/16- by $2\frac{1}{2}$ -inch slotted holes for $\frac{7}{8}$ -inch anchor bolts at expansion bearings of stringers.
- (f) $1\frac{1}{4}$ -inch-diameter holes for 1-3/16-inch pins of horizontal tower bracing connections made with clevices.
- (g) 1-9/16-inch-diameter holes for 1½-inch pins of transverse vertical bracing of railway bridge towers and longitudinal and transverse vertical bracing of highway bridge towers. The drawings show 1-9/16-inch-diameter holes for anchor bolts in tower column bearing plates; these holes can be made 1½-inch-diameter if special care is used to set anchor bolts accurately.
- (b) 2-1/16-inch-diameter holes for 2-inch pins connecting longitudinal bracing of railway bridge towers.
- b. Pneumatic drills. (1) The pneumatic reversible wood borer furnished engineer troops with the 105-cfm compressor can be used to drill holes in steel (fig. 48), but its use is not recommended if much drilling is required. The portable nonreversible pneumatic drill (stock number 40–3871.3) is preferred. (See fig. 49.) This drill is fitted with a screw-feed spindle for operation in an adjustable support (fig. 50) or is used with a drill bar. (See fig. 51.) Figure 52 shows a column press and carriage that can be made in the field to expedite drilling if much drilling is to be done.
- c. Drilling. Holes 11/4 inches in diameter and smaller are drilled with high-speed steel twist drills.
- (1) Enough pressure should be applied to the drill to make it cut a clean full chip. Slow feeding hardens the steel being drilled and spoils the drill.
- (2) Drills are cooled with mineral lard oil or a soluble oil emulsion. A good drilling compound is made by mixing 1 part by weight of soda ash dissolved in water with 4 parts lubricating oil, and adding to 50 parts of water. Free use of oil or drilling compound is necessary to prevent spoiling drills.
- (3) For efficient drilling, drills should be resharpened after every 100 holes

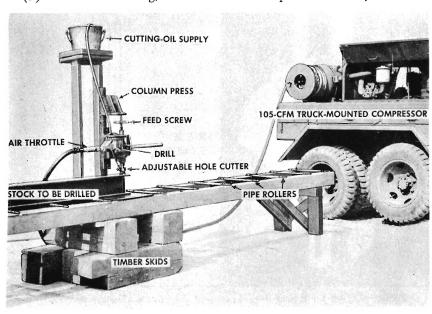


Figure 52. Production drilling. General view of production drilling lay-out.

An ample supply of twist drills and one or more drill grinders are needed on the usual job.

- (4) A crew of three men using a pneumatic drill and drill bar should drill: 30 holes per hour in ½-inch steel.
- 20 holes per hour in 1-inch steel.
- **d.** Cutting holes. Holes 1-9/16 and 2-1/16 inches in diameter are cut with an adjustable hole cutter. (See fig. 53.)
- (1) The drill must be held firmly in its support. (See fig. 52.)
- (2) A 3/8-inch-diameter pilot hole is drilled at the exact center of the hole to be cut. The pilot hole must not be oversize.
- (3) The cutter should be fed into the metal slowly to avoid excessive tooth breakage. The tool should be flooded with oil as in drilling. Five to 10 minutes, including time for setting up drill and cutter, are required for cutting a 2-1/16-inch hole in ½-inch steel.
- (4) The hole cutter cannot be used in metal over 5/8-inch thick. Holes in tower column bearing plates for anchor bolts must be burned or may be drilled 1½-inch diameter. (See par. 119.)
- e. Holes for rivets and bolts. (1) Subdrilling. Holes 13/16-inch in diameter may be subdrilled separately in all connecting parts and reamed to full size after assembly. Subdrilling is not recommended if parts can be assembled and drilled full size.
- (2) Drilling full size. Holes may be drilled full size by either of two methods.
- (a) Clamp a number of similar splice plates together and drill them all at one time. Then clamp these drilled plates to the members to which they connect to guide the drilling of full-size holes in those members. After the first holes are drilled, replace clamps with bolts to hold the parts more securely.
- (b) Clamp the undrilled splice plates to the beams and columns and drill holes through all parts in one operation. Such pieces must be match-marked

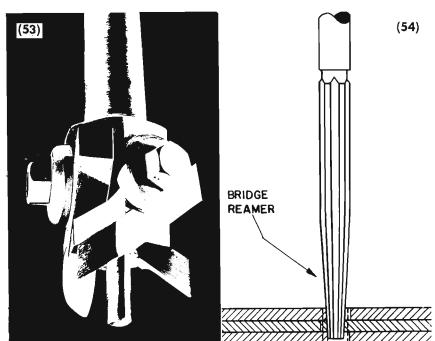


Figure 53. Tool for cutting 1-9/16-inch and 2-1/16-inch-diameter holes in steel.

Figure 54. Reaming with a taper bridge reamer.

for reassembly in the same positions. With this drilling method, hole centers need not be located with great accuracy but drills must be well plumbed.

- f. Holes for pins. Holes for pins connecting tower bracing must be located by exact measurement; each hole must be cut separately. Special care must be taken to insure that holes in opposite sides of members are in exact alignment.
- g. Slotted holes. Slotted holes, 15/16 by 2½ inches, for anchor bolts at expansion bearings of steel beams are made by drilling two 15/16-inch-diameter holes centered 1-9/16 inches apart and then cutting out the metal between with an oxyacetylene torch. Rough edges made in burning are smoothed with a file.
- 120. ASSEMBLING. After all members have been cut and holes drilled or burned, they are assembled on blocking for fitting (and when necessary, reaming) and for riveting, bolting, or welding into subassemblies. Permanent connections ordinarily made in fabrication are shown on the detail drawings.
- a. Blocking should be waist high to permit reaming, riveting, or bolting on the underside of the assembly.
- **b.** Members connecting in one plane are assembled and carefully aligned to correct angle and dimension.
- **c.** Connections are pinned with driftpins and bolted with fitting-up bolts to hold them securely.
- (1) For 15/16-inch-diameter drilled holes, driftpins are 15/16 inch in diameter, fitting-up bolts $\frac{7}{8}$ inch in diameter.
- (2) For 13/16-inch-diameter subdrilled holes, driftpins are 13/16 inch in diameter, fitting-up bolts 3/4 inch in diameter.
- d. Tower columns having connections in two planes are assembled and fitted separately with connecting members in each plane.
- 121. REAMING. Sub-l. lled, mismatching, and burned holes are reamed to clean, full-size holes while parts are assembled on the blocking.
- a. The portable, nonreversible pneumatic drill is used in reaming.
- b. Taper bridge reamers (fig. 54) are used for aligning full size but mismatching and burned holes. The bridge reamer is tapered for about half its length and its cutting edges are on the sides of the tool, permitting it to enter small or poorly matching holes and to remove the necessary metal with the least slotting of the hole.
- 122. BOLTING. Standard machine bolts and structural ribbed bolts, also referred to as rivet bolts, are used in semipermanent bridge construction.
- **a. Machine bolts.** (1) Standard machine bolts are used for temporary connections in fitting up and in crection. They should not be used for permanent connections except as shown in paragraph 224.
- (2) Seven-eighth-inch bolts are used for full-size holes. The bolts have U. S. Standard square heads and hexagon nuts. Washers are used under the nut. These are not supplied with the bolt but must be requisitioned separately. Principal dimensions and weights of standard machine bolts are given in tables LXXV and LXXVI.
- (3) Length of bolts should be such that with the nut drawn tight at least 1/4 inch of thread protrudes beyond the nut. In fitting up, any excess length of bolt shank is taken up with extra washers to save time in turning down nuts.
- (4) When used in permanent connections, nuts should be drawn as tight as possible and threads beyond the nut peened to keep the nuts tight. The

thread should be outside the parts being joined and washers should be used under nuts. Bolts should alternate in direction through the work.

- (5) A crew of 2 men working with hand wrenches can place and tighten 25 to 30 bolts per hour.
- b. Structural ribbed bolts. (1) Bolts. Structural ribbed bolts (par. 39b) can be used instead of rivets in all permanent connections.







Figure 55. Splicing beam sections preparatory to erection.

(1) Assembling beam sections preparatory to splicing. One section being moved with crane. Timber blocks and wedges adjust sections to correct fit. (2) Align bolt holes with driftpins before bolting. Machine bolts are used to hold the members tightly together until structural ribbed bolts are placed. Note the use of the pneumatic hammer for driving structural ribbed bolts. (3) Driving structural ribbed bolts in lower flange splice. Note the clearance required under the beam for the pneumatic hammer. If sledges are used for driving bolts, the beam is laid on its side.

- (a) The shanks of structural ribbed bolts are formed with ribs having an outside diameter slightly greater than that of the 15/16-inch holes into which they are driven. The ribs flatten and fill the hole, giving a tight fit.
- (b) The length of the ribbed shank should equal the thickness of the metal connected or be not over $\frac{1}{8}$ inch longer. Excess length of shank can be taken up by using a washer under the nut.
- (c) Table LXXVII gives principal dimensions and weights of structural ribbed bolts for lengths of grip used.
- (d) Lengths of rivets are given in bills of materials. Table XLIV gives equivalent lengths of structural ribbed bolts.

TABLE XLIV. Conversion of rivet lengths to lengths of structural ribbed bolts.1

Length of undriven rivet (inches)	Length of ribbed bolt (inches)	Length of undriven rivet (inches)	Length of ribbed bolt (inches)
2	1 11/16	33/4	3 3/16
21/4	2 1/16	4	3 9/16
$2\frac{1}{2}$	21/4	41/4	33/4
23/4	2 7/16	41/2	3 15/16
3	2 5/8	43/4	41/8
31/4	2 13/16	5	4 5/16
31/2	3		

- ¹ Lengths of rivets and ribbed bolts are total lengths of shanks under heads.
- (2) Fitting up. Parts being connected are aligned with drift pins and then securely, bolted with machine bolts. A bolt or a pin should be used in every second hole. The number of bolts and pins used should be about equal.
- (3) Driving. (a) Before driving any structural ribbed bolts in a joint, tighten all fitting-up bolts so all parts are drawn firmly together. Ribbed bolts must not be used to do this because the special lock threads will strip. Holes for ribbed bolts must be perpendicular to the faces of the metal connected. (See fig. 55.)
- (b) Structural ribbed bolts are driven into all open holes in a joint before removing any driftpins or fitting-up bolts. Drive a driftpin through each hole to clear and smooth it and to line up the parts before driving the ribbed bolt. Drive each ribbed bolt with a pneumatic nail driver (fig. 58) or a maul to a solid bearing on the head. Then run on the nut and tighten it to a snug fit with the impact wrench (fig. 56) (stock number 40–9823.5) or with a

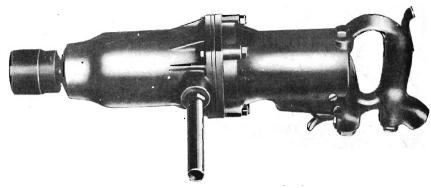


Figure 56. Pneumatic impact wrench.

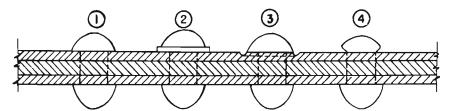


Figure 57. Rivet heads formed with correct and incorrect lengths of stock.

hand wrench. Tap the head of the bolt with a hammer as the nut is turned to assist in getting a tight fit. Do not force the nut too much as there is danger of stripping the threads.

- (c) After all open holes in each joint are filled with ribbed bolts, driftpins and fitting-up bolts are successively removed and replaced with ribbed bolts. Each hole is cleared with a driftpin before driving the ribbed bolt.
- (d) Discard all ribbed bolts that have been driven and removed. Do not reuse them.
- (4) Performance. A bolting crew of 3 men equipped with pneumatic tools can drive and tighten 25 to 40 bolts per hour. A crew of 2 men equipped with hand tools can drive and tighten 20 to 30 bolts per hour.
- 123. RIVETING. a. Rivets. Rivets used in semipermanent bridge construction are $\frac{7}{8}$ -inch buttonhead rivets driven while hot in 15/16-inch holes.
- b. Length of rivets. (1) The length of the rivet is the thickness of the part being connected (the grip) plus the length needed to form a head and fill out the rivet hole. Length of stock needed to fill out the hole and to form the buttonhead is given in table XLV. Grips are measured to the nearest ½ inch, and the stock needed for head and rivet swell is added to determine the length rivet needed. Lengths of all rivets are shown on the detail drawings.
- (2) Excessive rivet stock produces capped heads. Inadequate stock does not permit the forming of full heads. Examples of rivet heads formed by using correct and incorrect lengths of rivet stock are shown in figure 57.

TABLE XLV. Length of %-inch rivet stock required to fill 15/16-inch hole and form full buttonhead.

Grip	Added stock	Grip	Added stock
(inches)	(inches)	(inches)	(inches)
½ to 1¼	1½	13/4 to 3	1 ³ / ₄
1¾ to 15%	15/8	31/8 to 37/8	1 ⁷ / ₈

- (1) Correctly formed head.
- (2) Excess stock used.
- (3) Inadequate stock used.
- (4) Inadequate stock used.
- c. Fitting up. (1) Tight rivets depend largely on adequate bolting and pinning. Unless bolts are drawn tight before riveting, some rivets will be loose in their holes after they cool.
- (2) Before riveting, parts being connected are securely bolted and pinned together with either a bolt or a driftpin in every second hole. The number of bolts used should be about twice the number of pins.
- d. Equipment and tools. (1) Hammer. The pneumatic nail driver (fig. 58) furnished engineer troops with the 105-cfm compressor or the pneumatic riveting hammer available in class IV supplies is used for driving rivets. Rivet sets for 7/8-inch buttonhead rivets are not a standard accessory for this hammer and must be requisitioned separately.

- (2) Holder-on. The pneumatic holder-on (stock number 40-5950.06) with set for 7/8-inch buttonhead rivets is desirable if many rivets are to be driven. The tool is used for bucking up rivets in positions where the holder-on can be backed by adequate support.
- (3) Hand tools. Hand tools used in riveting are shown and listed in figure 59.
- e. Order of driving. Rivets are driven first in holes not filled with bolts or driftpins. Riveting should start at the center of the connection and proceed outward. After open holes have been filled, bolts and driftpins are removed two or three at a time and replaced with rivets.
- f. Riveting crew. (1) The riveting crew consists of four men as follows:
- (a) The heater, who heats the rivets and passes them to the sticker.
- (b) The sticker, who receives the rivets from the heater and puts them in the hole.

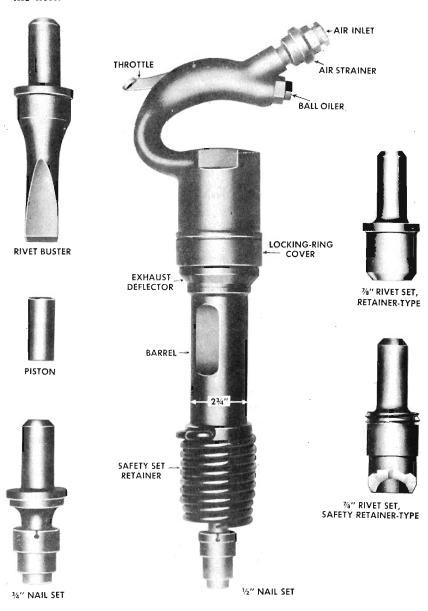
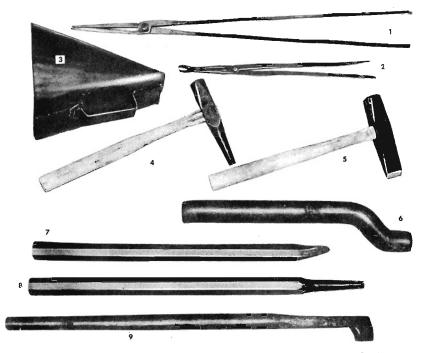


Figure 58. Pneumatic nail driver with accessories. Rivet set for 1/8-inch buttonhead rivets is not a standard accessory.



- Tongs, rivet-heating and pitching
- Tongs, rivet-sticking.
- Can, rivet-catching.
- Punch, backing-out, handled, 3-inch.
- Rivet buster, handled, 12-inch cutting edge
- Bar, dolly, riveting, off set,
- Chisel, rivet-buster, 12-inch
- Punch, backing-out, bar, 3-inch. Bar, dolly, riveting, heel, 3-inch
- Figure 59. Hand tools used in riveting.
- (c) The bucker, who holds the rivets firmly in the hole against the force of the hammer blows.
- (d) The riveter, who forms the rivet head with the pneumatic hammer, causing the rivet to fill its hole.
- (2) The riveter heads the crew. Good riveting depends on fast and efficient work by all members. Ample time for training riveting crews is essential.
- (3) In assembling parts in fabrication, a well-trained riveting crew can drive 30 to 40 rivets per hour.
- g. Heating. Rivets are heated for driving in a coal-burning forge with hand bellows (stock number 41-3604.11-18).
- (1) The needs of the work are anticipated by placing several rivets of the length required for the connection in the fire at a time. These are heated before being withdrawn singly, as required for driving.
- (2) The shank of a properly heated rivet is a uniformed light cherry red; the head remains a dull red.
- (3) Rivets should not be heated beyond a light cherry red nor left in the fire for long periods, since they may become burned and pitted through excessive heat and are then unfit for use.
- h. Sticking. (1) As the rivets are needed, they are taken from the forge and passed to the sticker. If the forge is some distance from the work, rivets are tossed to the sticker, who catches them in a catching can.
- (2) After catching a rivet, the sticker takes it in his tongs, strikes the head sharply against the metal to remove all cinders and scale, and enters it in the hole.

Caution: A 15/16-inch driftpin should be driven through each hole before the rivet is entered to insure a clean well-aligned hole.

- i. Bucking. For most riveting, the pneumatic holder-on is best for bucking rivets. In positions where the holder-on cannot be used, bucking is done with hand tools called dolly bars. (See figs. 59 and 60.)
- (1) Holder-on. The pneumatic holder-on is best suited to bucking rivets in flanges of beams. Blocking is used under the holder-on to raise it high enough.
 - (2) Hand dollies. Hand dollies are of two types.
- (a) Dolly bar. The dolly bar (fig. 59) is a heavy steel bar with ends cupped to fit the buttonheads of \(\frac{7}{8}\)-inch rivets. One end is offset to permit bucking rivets in beam flanges close to the web of the beam.
- (b) Heel dollies. The heel dolly is adapted to bucking in close clearances. It is used like a lever with blocking providing the fulcrum.
- j. Driving. In driving rivets, the hammer must be held against the rivet with considerable pressure and should be rotated or rolled slightly (fig. 61) to aid in forming the head. Clearances required for driving are shown in figure 62.
- (1) Care is used not to ring the metal being riveted by rolling the hammer too much.
- (2) The hammer must line up closely with the rivet or the head will not be concentric with the rivet.
- (3) No attempt should be made to drive a rivet that has cooled below a dull red heat.
- (4) Full air pressure must be maintained on the hammer or the force of its blow is reduced and rivets will be poorly driven.
- k. Testing. An inspector tests rivets for soundness after they have cooled. The officer in charge is responsible for the quality of work and should assure himself that all rivets are tested and are satisfactory.
- (1) Testing is done by holding the finger or a small piece of metal against one side of the preformed head and striking the opposite side of the same head with a light hammer. If the rivet is loose, the jar of the hammer blow is transmitted to the opposite side. If the rivet is tight, no jar or vibration is noticeable.

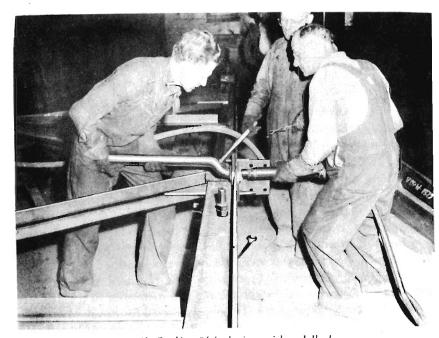


Figure 60. Bucking 1/8-inch rivet with a dolly bar.

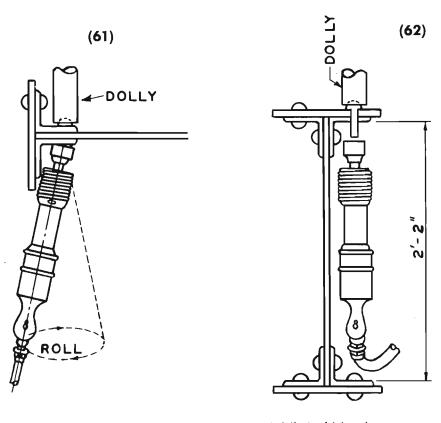


Figure 61. Positions of pneumatic hammer and dolly in driving rivets.

Figure 62. Clearance required for riveting.

- (2) If only a slight jar is felt, the rivet should be left in place if one of a group of several rivets, since in removing it other rivets in the group may be loosened and the rivet hole enlarged. Loose rivets and rivets with inadequate or burnt heads should be removed and replaced. (See fig. 63.)
- I. Removal of rivets. (1) An unsatisfactory rivet is driven out of its hole with a backing-out punch after the head has been removed.
- (2) The head is broken off with a rivet buster set in the pneumatic driving hammer or with hand tools, a maul and a handled rivet buster or a bar buster. The rivet buster is a standard accessory with the pneumatic nail driver.
- (3) If rivets are in thin metal or cannot be reached with a rivet buster, heads are burned off with an oxyacetylene torch. While burning heads off, care must be taken not to burn the metal around the rivet.

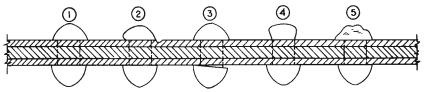


Figure 63. Examples of poorly formed rivet heads.

- (1) Head not concentric with rivet.
- (2) Riveting hammer not held in line with rivet.
- (3) Dolly bar not held in line with rivet.
- (4) Rivet allowed to cool before driving.
- (5) Rivet too hot when driven.

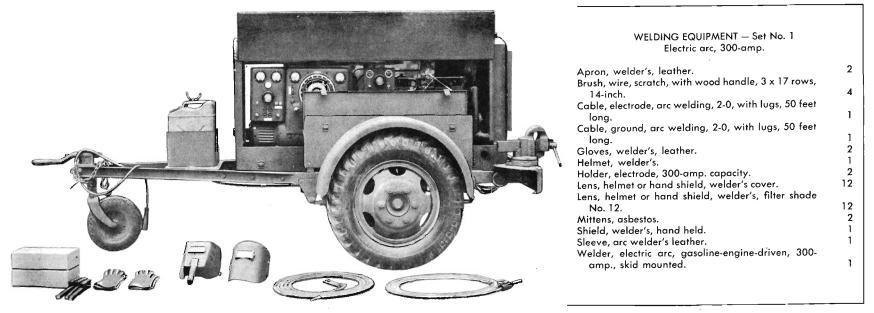


Figure 64. Electric arc-welding equipment, set No. 1, 300-ampere, trailer-mounted.

124. WELDING. a. **Processes.** The two principal welding processes used in structural work are:

- (1) The oxyacetylene process in which welding heat is obtained by burning acetylene gases as they mix with oxygen discharged under pressure from a torch designed for the purpose. This process is preferred for butt welds of heavy metal. Oxyacetylene welding and cutting equipment (fig. 45) is described in TM 5-4100.
- (2) The electric-arc process, in which the welding heat is developed in the electric arc formed between a suitable electrode and the base metal. This process is generally preferred for structural welding. The 300-ampere gasoline-engine-driven electric-arc welder (fig. 64) is suitable for structural welding. It is available as class IV equipment.
- b. Types of welds. The principal types and positions of welds used in structural work are illustrated in figure 65. Nomenclature of welds is shown in figure 66. Ease of welding is determined largely by position, in the following order.
- (1) Flat.
- (2) Vertical,
- (3) Horizontal.
- (4) Overhead.

Whenever possible, work should be turned so welding can be done flat.

- c. Welders. (1) General. Welding of steel for semipermanent bridges requires experienced structural welders. The quality and strength of the weld depends more on the skill of the welder than on any other single factor. The skill of a welder can be determined only by knowledge of his past performance or by testing sample welds made on the job.
- (2) Qualification tests. The two tests described below qualify structural welders. They can be performed in the field without elaborate equipment. If after testing one or more sample welds by each method, the officer in charge is not satisfied with the skill of a candidate, additional training should be given before the tests are repeated.
- (a) Guided-bend test. The guided-bend test is used to determine the quality

of the weld metal at the face and root of the welded joint, the degree of penetration, and the fusion to the base metal. Tests are made both with the face and root of the weld in tension. (See fig. 68.)

- 1. The test is made in a die and plunger which can be made in the field as illustrated in figure 67.
- 2. Test specimens are flame-cut from sample butt weld of plates 3% of an inch thick.
- 3. The test specimen is placed across the die and forced into it by the plunger. Force is applied to the plunger with a hydraulic press such as the 10-ton press furnished with the motorized general-purpose shop.
- 4. To fulfill the requirements of the test, the specimen must bend through 180° without developing cracks greater than ½ inch in any dimension. Satisfactory guided-bend test samples are illustrated in figure 68.
- (b) Nick-break test. The nick-break test determines the internal quality of the weld metal and reveals any internal defects, such as slag inclusion, gas

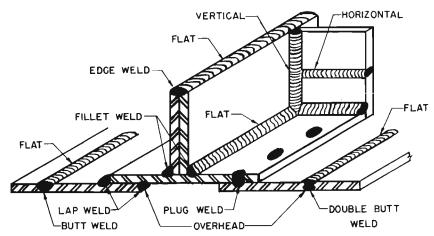


Figure 65. Types and positions of welds. Positions of welds are flat, borizontal, vertical, and overhead.

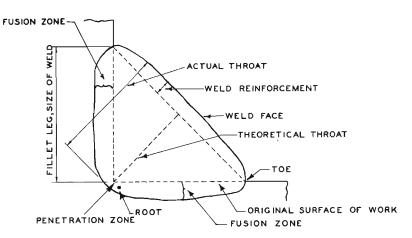


Figure 66. Nomenclature of fillet welds.

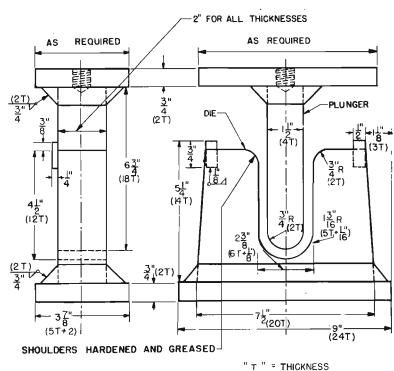


Figure 67. Die and plunger for guided-bend test of butt welds.

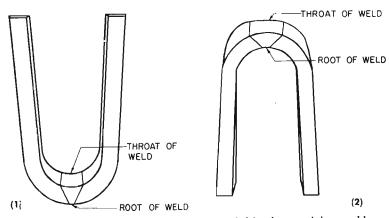


Figure 68. Examples of satisfactory guided-bend tests of butt welds.

pockets, lack of fusion, and oxidized or burned metal.

- 1. Test specimens are flame-cut from a sample weld as for the guided-bend test.
- 2. A saw cut is made at each edge through the center of the weld. Depth of cut is one-eighth the width of the test specimen.
- 3. The saw-nicked specimen is placed on two steel blocks as shown in figure 69 and broken by repeated blows with a heavy hammer.
- 4. Weld metal exposed in the break should be completely fused, free from slag inclusions, and contain no gas pockets greater than 1/16 of an inch across their greatest dimension. There should not be over six pores or gas pockets per square inch of exposed weld.
- d. Preparation of metal for welding. Strength of a welded joint depends largely on correct preparation of the metal edges being welded.
- (1) Edges should be dry and if welded in temperatures below 32° F should be heated until warm to the hand.
- (2) All mill scale, rust, oxide, paint, and other impurities, such as slag particles adhering to flame-cut edges, must be removed.
- (3) Edges must be regular in contour and without nicks or notches.
- (4) Before butt-welding, edges to be joined are separated 1/16 to ½ inch, depending on the type weld and the thickness of parts being joined.
- (5) Plates are beveled 30° on one side for butt welds of plates up to ½-inch thick and on both sides for heavier plates.
- e. Oxyacetylene welding. Good welds require the proper tip and welding rod, correct flame adjustment, and manipulation of torch and welding rod. Satisfactory welds are produced by manipulating the torch and welding rod either forehand or backhand. Backhand welding is preferred on structural work since it uses less metal, requires less puddling of the molten metal, and uses less welding rod than other methods. Backhand welding is illustrated in figure 70.
- (1) Procedure. (a) The welding tip precedes the rod in the direction of the weld with the flame pointed back to the molten puddle. The rod is held between the welding tip and the molten puddle.
- (b) With the heat carefully balanced to melt the end of the rod and the

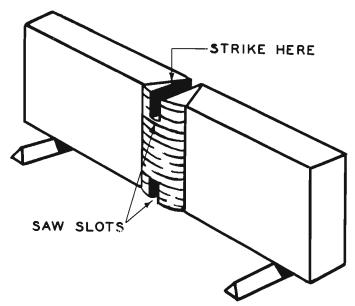


Figure 69. Nick-break testing of sample butt welds.

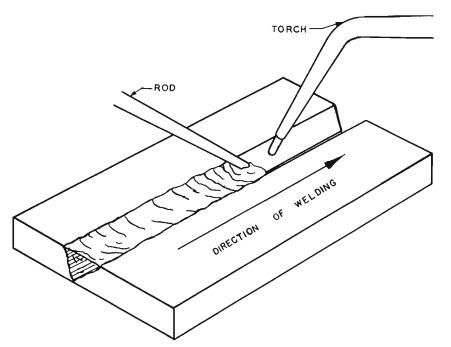


Figure 70, Position of rod and tip in backhand welding.

side walls of the plate being welded, the rod and the tip are moved in opposite semicircular paths across the line of the weld while being advanced slowly and uniformly in the direction of the weld.

- (c) As the flame passes the end of the rod in each motion, a short length of rod is melted and deposited in the weld. The rod is rolled or rotated so it melts off evenly.
- (2) Performance data. Oxyacetylene welding performance data for butt welds is given in table XLVI.

TABLE XLVI. Oxyacetylene welding performance data for butt welds.

Thickness of steel—inches	3/8	1/2	3/4
Joint preparation	90°V	60°V	60°V
Diameter of rod—inches	3/16	3/16	3/16
Speeds—feet per hour	4-5	5-6	2.5-3.5
Oxygen consumption cu. ft. per hour	46	58	92
cu. ft. per ft. of weld	11-9	12-10	37-26
Acetylene consumption cu. ft. per hour	44	56	88
cu. ft. per ft. of weld	11-9	11-9	35-25
Rod consumption—lb. per hour	2.4-3.0	2.9-3.5	3.3-4.6
lb. per ft, of weld	.60	.64	1.31

- f. Electric-arc welding. Several operating variables, such as current, voltage, polarity, arc length, position of electrode, weaving motion, and speed of weld, control the quality of arc welds. Good welds cannot be produced unless all of these conditions are carefully controlled. Weld metal must be deposited uniformly and good penetration of the weld into the base metal must be secured.
- (1) Procedure. (a) The welding arc is started by striking or brushing the electrode against the plates being welded and short-circuiting the welding current. The resulting surge of high current causes both the end of the electrode and a small spot on the plate beneath to melt instantly.

- (b) As contact is made, the electrode is raised to establish an arc. After the arc is established, particles of metal melt off the end of the electrode and are deposited in the molten crater on the plate surface.
- (c) As the electrode melts, it is fed down to the plate to maintain a uniform arc and is moved in a weaving motion along the weld, depositing the weld bead and fusing the side walls of the weld.
- (2) Performance data. Arc-welding performance data for fillet welds is given in table XLVII.

TABLE XLVII. Arc-welding performance data for fillet welds.

Size of fillet—inches Size of electrode—inches Electrode consumption including		5/16 3/16	3/8 7/32	1/2 7/32
waste-lb. per foot of weld	0.20	0.30	0.45	0.80
	8	6	4.5	2.5

g. Multiple-layer welding. In making welds larger than 5/16 inch, the weld metal is deposited in two or more passes. This avoids using a large rod or electrode, and carrying a large puddle of molten metal in the weld. It also secures good fusion with the side walls. By depositing the weld in multiple layers, the welder can concentrate on good penetration at the root of the weld on the first pass and on good fusion with the side walls of the weld on succeeding passes.

Caution: Before the following weld metal is deposited, initial layers must be cleaned of all scale, oxide, and slag by scraping or brushing with a wire brush.

- h. Distortion. (1) Metal added in welding is essentially cast metal. As this metal cools, it shrinks and produces stresses in and near the weld which may cause warping or buckling. If the welded parts are restrained, these stresses may break the weld.
 - (2) Welding stresses can be reduced by proper spacing of parts being

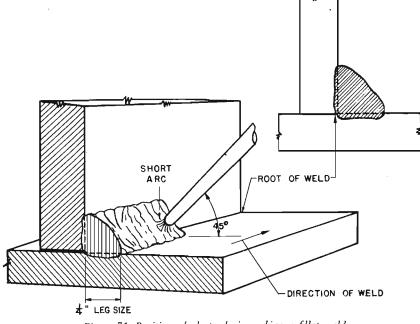


Figure 71. Position of electrode in making a fillet weld.

welded, correct welding sequence, and control of the welding heat.

- (a) Clamps, jigs, or fixtures employed to hold the parts in place during welding permit enough movement to allow for weld shrinkage.
- (b) Tack welds used to hold parts during welding should be spaced to permit welded parts to contract and be located where they will become part of the completed weld. They should be less than 1 inch long and at least 12 inches apart in long seams. Broken tack welds must be removed before final welding.
- (c) The back-step method of welding illustrated in figure 72 is often used to counteract contraction in long welds.
- (d) Where multiple-layer welds are made from both sides of a plate, layers are alternated, the initial pass being made on one side of the joint followed by a pass from the other side.
- (e) Intermittent welds of fillet-welded T-joints are staggered to reduce warp and distortion, a short weld being made on one side of the joint followed by a weld on the other side. (See fig. 73.)
- (3) Welding stresses can be relieved somewhat by lightly peening the finished weld. Excessive or severe peening, however, may cause brittleness or hardening of the finished weld and contribute to its failure.
- i. Inspection. Finished welds should be inspected visually for undercut, overlap, surface checks, cracks, and other defects. Properly welded joints should be uniform in appearance with evenly deposited weld metal. Fusion of the side walls is most important and should be complete in a good joint. Desirable and defective weld profiles are shown in figure 74.
- 125. BLACKSMITHING. a. Work done in the blacksmith shop is of two principal types. (1) Making of small parts requiring bending, forging, welding, or grinding. These parts are:

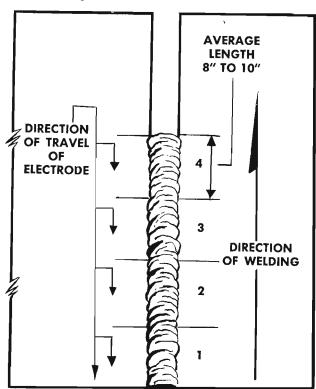


Figure 72. Back-step welding to counteract contraction.

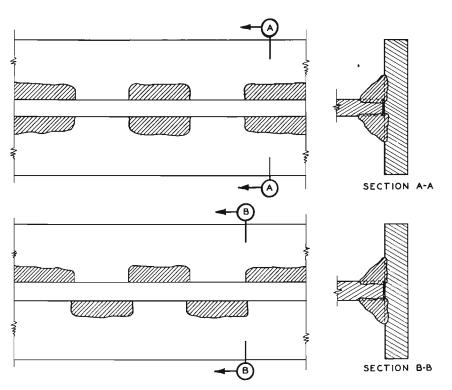
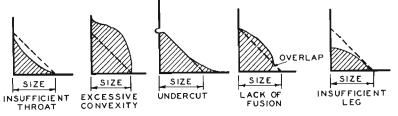


Figure 73. Fillet welds spaced intermittently to counteract assortion.

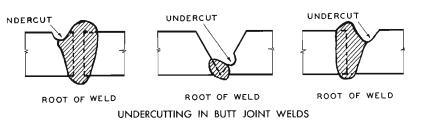
- (a) Plates connecting horizontal tower bracing to tower columns. These are bent and drilled as shown on the drawings.
- (b) Diagonal bracing rods which are cut to length and welded to threaded stub ends and loop rods.
- (c) End stiffener angles of beams when grinding to exact fit is required.
- (d) Hook bolts and driftbolts when not supplied from depot.
- (2) Making of small fabrication and erection tools, straight shank center punches, parts for erection equipment such as that described in chapter 16, and sharpening cutting tools.
- **b.** Tools and equipment in the blacksmith sets furnished engineer troops and their care and use are described in TM 5-225.
- 124 MATCH MARKING. Before separating parts assembled in the fabrication yard, they are all match-marked so they can be erected in the same relative positions. Each joint of two or more members is given a distinguishing number which is painted at the end of each member entering the joint.
- 127. STORING COMPLETED MEMBERS. After match marking, the assembled parts of the structure are separated into individual members or sub-assemblies. These are placed in the storage yard to await erection. Parts are stored so they can be reached as they are needed, without moving other members. Timber dunnage is used to keep steel parts off the ground.
- 128. INSPECTION OF COMPLETED PARTS. Parts should be followed through fabrication by an inspector trained in all requirements of the work. Principal dimensions and connections of all completed members should be checked against the detail drawings. Bolted connections should be checked for tightness. Rivets should be tested as described in paragraph 123. Welds should be inspected as described in paragraph 124.

Section II. TIMBER FRAMING

- 129. SCOPE. a. This manual assumes that the construction forces are experienced with woodworking tools and with the methods of working with timber described in FM 5–10 and TM 5–226. It covers only special framing requirements and operations applying to construction of semipermanent bridges.
- **b.** The term "framing" as used here applies to the cutting, shaping, and boring of timbers for their use in structures, and to related operations performed in the framing yard.
- 130. WORKMANSHIP. Structures required to carry heavy moving loads must be accurately framed. No blocking or shimming of improperly fitting parts can be permitted.
- a. Columns must be cut to exact length and bevel.
- **b.** Ties must be dapped and stringers sized to correct depth so that all loads will be properly distributed.
- c. Cuts must be straight and even to secure full bearing.
- 131. PROPERTIES OF WOOD. a. Unlike other structural materials, wood does not have the same physical properties in all directions. In compression, tension, and bending, it is stronger in the direction of the grain. In shear, it



DEFECTIVE FILLET-WELD PROFILES



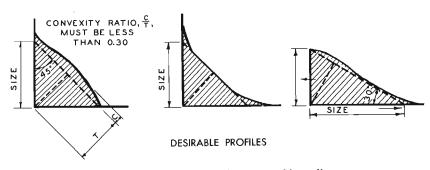


Figure 74. Desirable and defective weld profiles.

is stronger across the grain. Wood splits easily along the grain but not across it. In drying, wood shrinks more across the grain than along the grain. These characteristics must always be kept in mind.

b. Strength of wood depends on its species and speed of growth, position in the log from which it was cut, and the manner and amount of its curing. Green or poorly seasoned wood is not as strong as well-seasoned timber and shrinks more in aging. Timbers which are used together should be of the same kind and should be equally seasoned. Green timber should not be mixed indiscriminately with well-seasoned wood.

- 132. FRAMING YARD. a. Timber is ordinarily framed on firm, level ground close to the bridge site and immediately adjacent to the timber storage.
- **b.** If the size of the work justifies, one or more framing platforms are built. Platforms are made of planking later to be used in some other part of the work. They are loosely nailed to joists laid on the ground and are carefully leveled. Platforms must be large enough to permit assembling a complete bent or a story of a bent.
- 133. TOOLS AND EQUIPMENT. a. Tools and equipment needed for framing semipermanent bridges are listed in table XXXIA. The listing does not include hand tools regularly issued to all squad units.
- b. Principal power tools used in the framing yard are:
- (1) The portable pneumatic tool accessories with the 105-cfm truck-mounted compressor including the following:
- (a) Chain saw with 24-inch blade.
- (b) Circular saw with 12-inch blade.
- (c) Wood-boring reversible drill with 7/16-, 3/4-, and 1-inch wood augers, 12, 18 and 36 inches long.
- (d) Nail driver for driving large nails and spikes.
- (2) Gasoline-engine-driven chain saw (stock number 40-8029.36) with 36-inch blade.
- **c.** Timber can be manhandled but it is better to have a small truck-mounted crane available for moving heavier pieces.
- 134. RECEIVING AND STORAGE. As timber is received on the job, it is checked against the requisition and inspected for damage or natural defects.
- a. Pieces of timber of the same species and grade differ widely in quality. Clear, straight-grained pieces free from large knots or other defects are chosen for members such as stringers, columns, caps, and flooring. Less perfect pieces are set aside to be used for blocking, bracing, curb, and handrails, and are stacked separately.
- **b.** Timbers are stacked close to the framing yard, those of the same kind, length, and use being stacked together. Timbers are blocked up off the ground and layers are separated with plank stripping.
- 135. LAY-OUT. a. Posts of bents and towers. Posts of bents and towers must be cut to exact length and bevel. Careful workmanship is necessary in their framing. Lengths of pieces and bevels of end cuts are given on the detail drawings.
- (1) When framing on a platform, the outline of each bent is drawn on the platform. Timbers are laid down and marked for cutting from the outline of the bent for which they are intended.
- (2) When no platform is used, each post is marked for cutting by careful measurement. To eliminate variations between measurements, a 2- by 1-inch

measuring stick the length of the longest post is marked with the controlling dimensions. This stick is used in all measurements instead of a tape or rule.

- b. Caps, sills, and bracing. Caps, sills, and bracing need not be cut exact length. They are marked for cutting by direct measurement with tape or rule. Length of all pieces is shown on the detail drawings.
- c. Stringers, flooring, and railing. Stringers, floor plank, and railing are not ordinarily framed on the ground, but are squared and cut to length during erection as described in chapter 15.
- d. Scabs, blocking, and handrail posts. Miscellaneous small parts such as scabs, blocking, and handrail posts are usually cut to length by marking from a pattern. One such piece is made to the dimensions shown on the detail drawings and is used for marking all other pieces.
- 136. SAWING. a. Portable, power-driven saws are ordinarily used for rough cuts of all heavy timbers. Circular saws can be used for cutting timbers up to 4 inches thick.
- **b.** Two-man crosscut saws are preferred for making accurate finish cuts and for small framing jobs. Unless a power saw is rigged and immediately available, occasional cuts can be made more efficiently by hand.

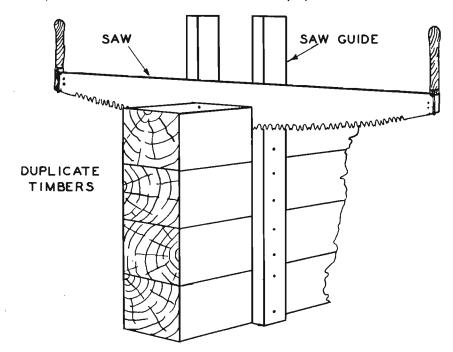


Figure 75. Saw guide used in sawing duplicate timbers.

- c. If the amount of duplication justifies, timbers to be cut to the same dimension may be stacked as shown in figure 75 and all accurately cut in one operation. Strips are lightly nailed on each side at the cut to hold the timbers in place and to guide the saw.
- 137. SIZING AND DAPPING. a. Sizing. Caps, sills, and stringers of rough sawn lumber must be sized to exact depth at all points of bearing. Surfaced timbers do not ordinarily require sizing. Sizing is done with an adz. Even cuts to connect depth are made to provide full bearing.
- b. Dapping. Ties are dapped (notched) over splices in beam flanges to the thickness of the splice plate.

- (1) A saw cut is made each side of the dap and the wood between cuts removed with an adz
- (2) No allowance is made for projecting heads of rivets nor are ties countersunk for rivet heads. The first few trains over the bridge will force ties down to a full bearing on the girders.
- 138. BORING. a. Timber bents. Bents are assembled for boring on a framing platform or on carefully leveled blocking.
- (1) Diagonal bracing of one face is laid down first, followed by the caps, sills, and posts, and the diagonal bracing of the opposite face.
- (2) Bracing is lightly nailed to hold all pieces in position and holes are bored.
- (3) If the bent is not to be erected as a unit, all parts are match-marked before the bent is taken apart. Each connection is designated by a numeral painted at the end of each member making up the joint.
- (4) If it is planned to erect the bents assembled, bolts are driven and the bents stacked in orderly fashion to await erection.
- **b.** Nailer strips. When bolted to steel stringers, nailer strips are cut, bored, and bolted before erection. Each nailer strip is marked for boring from the holes previously drilled in the flanges of the beam to which it is attached.
- c. Other parts. To permit adjusting differences in makeup, other parts such as longitudinal bracing of towers and bents, stringers, caps, deck timbers, and railing posts ordinarily are not bored until in place.
- 139. MACHINE BOLTS. a. Bolts used in semipermanent bridges for bolting timber parts are $\frac{1}{2}$ -, $\frac{3}{4}$ and 1-inch machine bolts having square unfinished heads and nuts. Bolts must be fitted with round steel washers under head and nut. Washers are not supplied with bolts and must be requisitioned separately.
- **b.** Holes for bolts are bored the same diameter as the bolt. When bolts are in place, nuts should be tightened until the washers bite into the wood. This compensates for shrinkage as the wood ages and dries.
- c. When a bolt is not driven at right angles to the face of a timber, the timber must be beveled under the washer to provide full, even bearing. Curved faces are flattened for the washer by a shallow adz cut.
- d. Bolts should not be closer to the edge of a timber than one and one-half times the diameter of the bolt. Bolts should not be closer together than two and one-half times the bolt diameter nor closer to the end of a timber than seven times the bolt diameter.
- 140. DRIFTBOLTS. a. Driftbolts used in semipermanent bridges are ½-and ¾-inch diameter. They are available in class IV supplies with square heads and cone points, or they can be cut from round rods and driven without head or point. Where drawings show flush driftbolts either of the following may be used: (1) a standard driftbolt with head sheared off, (2) a plain driftbolt cut from round bar stock. Driftbolts are driven in prebored holes and are used only for shear connections. They are never used to resist tension.
- **b.** Holes for driftbolts are drilled the same size as the bolts. For bolts parallel with the grain of the wood, the holes are 3 inches shallower than the length of the bolt.
- 141. NAILS AND SPIKES. Nails and spikes are used in the framing yard to make temporary connections during marking, sawing, and bolting.
- a. Types of nails and spikes used in the structures are listed in table III.

b. When one piece of timber is spiked to another, the nail or spike should penetrate the second timber at least one-half of the length of the nail or spike. Use of nails to resist direct pull is to be avoided; where so used, nails should be driven through and clinched.

CHAPTER 12

PILES AND PILE DRIVING

Section I. PILES

- **142. SCOPE.** Pile and pile-driving information in this chapter deals with the detailed work processes. Construction of pile foundations and abutments of semipermanent bridges is described in chapter 13.
- 143. USE. a. Where the ground near the surface cannot support bridge loads on spread footings, bearing piles carry loads in the following ways:
- (1) As a *point-bearing pile* by point resistance on a hard underlying layer of compacted sand, gravel, or rock.
- (2) As a friction pile by frictional resistance of penetrated soil.
- b. Bearing piles are also used on solid ground in the following cases:
- (1) Where spread footings may be undercut by stream scour.
- (2) Where water is too deep or stream current too fast to permit constructing spread footings.
- c. The uses of sheet piling are discussed in paragraph 146.
- 144. TIMBER BEARING PILES. a. General. Straight tree trunks cut above ground swell with branches closely trimmed and bark removed are used as timber bearing piles. A good pile has the following characteristics:
- (1) Free of sharp bends, large or loose knots, shakes, splits, and decay.
- (2) A straight line between centers of butt and tip lies within body of pile.
- (3) A uniform taper from butt to tip.
- b. Size. Limiting cross section dimensions of piles are:
- (1) Piles shorter than 40 feet, 8- to 11-inch tip (small end) diameters and 12- to 18-inch butt (large end) diameters.
- (2) Piles longer than 40 feet, 6- to 8-inch tip diameter and 13- to 20-inch butt diameter. The butt diameter must not exceed the clearance between pile driver leads.
- c. Source of piles. (1) Piles are usually obtained locally from stock or standing timber and are untreated.
- (2) Creosoted piles 16, 30, 40, 50, 60, 70, 80, and 90 feet long are available as class IV supplies.
- d. American timber. Piles can be made of any sound wood that will stand driving. Recommended American timber that will stand driving and has high durability is listed below:
- (1) Red or white oak.
- (2) Pine.
- (3) Douglas fir.
- (4) Larch.
- (5) Cypress.
- (6) Cedar.
- (7) Spruce.

- e. Foreign timber. The following foreign timber may be used for piling as indicated:
- (1) Teak—Southeast Asia, high strength, high durability.
- (2) Sal—India, high strength.
- (3) Jarul—India.
- (4) White siris—India.
- (5) Doedar-India, medium strength.
- (6) Chir—India, medium strength.
- (7) Poon—India, medium strength.
- (8) Eucalyptus:

Iron bark or Jarrah—Australia, medium strength, high durability. White or red gum—Australia, medium strength, high durability.

- (9) Mahogany—Central America, high strength, high durability.
- (10) Palmetto-Tropics, low strength, borer resistant.
- (11) Norway pine—Europe, medium strength.
- (12) White deal—Europe, low strength.
- (13) Kail—Europe, low strength.
- f. Pile life. Life of a pile depends on the specie and condition of the wood, pretreatment, its position with respect to water, and its exposure to borers and rotting. In general, the life of creosoted and untreated piles is as follows:
- (1) Creosoted piles. Creosoted piles last from 5 to 10 years in water infested by marine borers; 10 to 20 years when alternately wet and dry; and indefinitely when continually submerged in water.
- (2) Untreated piles. Untreated piles usually last 3 to 6 months in water infested by marine borers; 5 to 10 years when alternately wet and dry; and indefinitely when continually submerged in water.

Note: Some tropical hardwoods such as cypress, teak, and mahogany last 3 to 4 years in water infested by marine borers. Palmetto is also borer-resistant but will not stand hard driving.

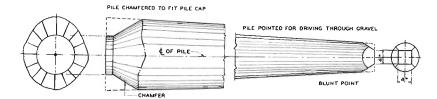
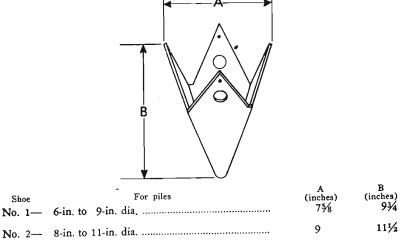


Figure 76. Preparation of timber pile. The butt end is chamfered and the tip is pointed for hard driving.

- g. Preparation for driving. Before piles are driven, they are trimmed, the butt shaped to fit the pile cap, and the tip pointed or squared off. If pile caps are not used or if crushing and splitting occur, the top end of the pile is wrapped with steel wire or banded. Steel shoes are sometimes used to protect the pile tip when driving through gravel or soil containing boulders.
- (1) Butt preparation. The butt is cut square and chamfered (fig. 76) to fit into the recessed pile cap. When driving with a steam hammer, which does not use a recessed cap, the chamfering concentrates the hammer blow on the central area of the butt and helps prevent splitting.
- (2) Pointing. When driving through hard clay and coarse gravel, the tip is trimmed as shown in figure 76. In silts, and soft clays, the tip may be cut square and left unpointed.
- (3) Pile shoes. Steel pile shoes (fig. 77) in two sizes are normally available in depots. The dimensions of these shoes are given in table XLVIII.

TABLE XLVIII. Steel pile-shoe dimensions.



- h. Splicing. Piles can be spliced if single piles of required length are not available or if long piles cannot be handled in the driver. Splices are also used to restore upper sections of burned or damaged trestle piles. Splices are of two types:
- (1) Sleeve joints (fig. 78) made of 8- or 10-inch steel line pipe cut in 3-foot lengths. Contact ends must be carefully cut to give full contact. Pile ends are trimmed to fit snugly in the pipe. A flat transverse bar through the sleeve between the abutting pile ends keeps the sleeve in place during driving.
 - (2) Bolted timber or steel splice pieces as shown in figure 79.

145. STEEL BEARING PILES. a. General. Steel piles are best suited for:

- (1) Driving to rock or other hard bearing surface below the reach of timber piles.
 - (2) Penetrating layers of gravel through which timber piles cannot be driven.
- (3) Driving in rock-bedded and swiftly flowing streams where timber piles cannot be driven deep enough for stability.
- b. Form and size. The preferred steel-pile section is the 12- by 12-inch, 53-pound, H-section. The sections used must:
 - (1) Be heavy enough to withstand hard driving.
 - (2) Be rigid enough to be handled and serve as a column.
 - (3) Provide suitable surface to attach pile-bent bracing. However, steel piles

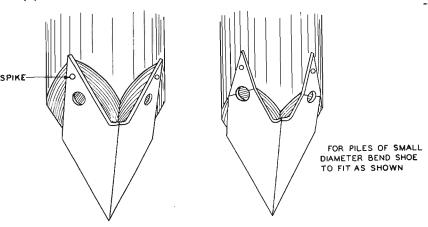


Figure 77. Steel pile shoe used to protect tips of timber piles in hard driving.

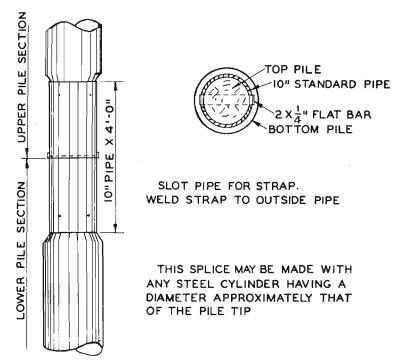


Figure 78. Timber-pile splice using steel line-pipe for a sleeve joint.

under concrete pedestals may be of any shape since bracing is not used.

c. Splicing. Steel piles can be spliced using welded, bolted, or riveted splice plates. (See fig. 80.) Unless butt-welded, ends of spliced sections must be in contact over their full area.

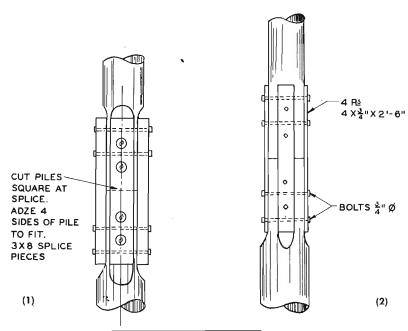


Figure 79. Timber-pile splice using timber or steel splice pieces:

- (1) Timber splice pieces.
- (2) Steel splice pieces.

- 146. SHEET PILING. a. General. Sheet piling is used to resist horizontal pressure of water or soil in the following operations:
- (1) Excavating for abutments and foundations in soft soils. It is used to keep banks and trenches from caving in and must be securely braced with struts and rangers or wales.
- (2) Foundation construction and repair in water. The sheet piling is driven into the stream bottom around the working area so it can be pumped dry.
- b. Timber sheet piling. (1) Types. (a) Single-row sheet piling is normally used in dry earth. (See fig. 81 (1).)
- (b) Double-row overlapping plank is normally used in saturated earth. (See fig. 81 (2).) The two planks are usually bolted together in shiplap form before driving.
- (c) Wakefield sheet piling is used in water or under hard driving conditions. (See fig. 81 (3).) It is made of three thicknesses of equal-width plank nailed

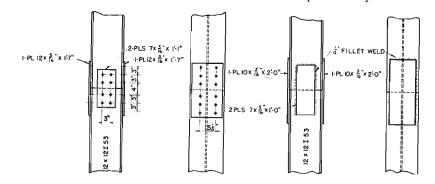


Figure 80. Steel-pile splices using bolted or welded splice plates.

and bolted together. Three 2- or 3- by 12-inch planks are used. All planks should be finished lumber.

- 1. Two-inch planks are bolted together with two ½-inch bolts at 6-foot centers. Three-inch planks are bolted with two ½-inch bolts at 6-foot centers. Spikes are driven at about 18-inch centers in two rows between bolts.
- 2. If bolts are not used, spacing of spikes is reduced to 12 inches and the rows are offset.
- (2) Preparation for driving. The head of the sheet pile is chamfered to concentrate hammer blows on the center of the pile. The foot of the pile is cut at a 6 to 12 slope (fig. 81) to force piles together during driving.
- c. Steel sheet piling. (1) Interlocking steel sheet-piling sections have the following advantages:
- (a) Lug-and-groove interlock on each edge guides the pile during driving and can transfer tension from pile to pile.
 - (b) Strong and easy to drive and align in hard driving.
 - (c) Interlocking lug-and-groove shape reduces leakage in cofferdams.
- (d) Can be pulled easily and used repeatedly.
- (2) The following steel sheet piles are available in class IV supplies:
- (a) A 5-inch 36- pound deep-arch wall section with an effective width of 16 inches. (See fig. 82 (1).)
- (b) A 30.7-pound curved corner section (fig. 82 (2)).

147. CONCRETE PILES. Concrete piles are not ordinarily used in military bridges. However, there are two general types:

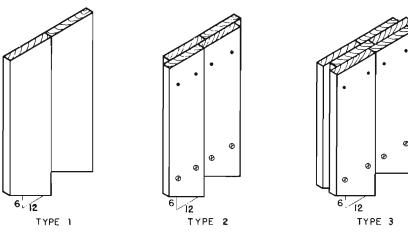


Figure 81. Timber sheet-pile types showing head and point details.

- (1) Single-row plank piling.
- (2) Double-row plank or shiplap piling.
- (3) Wakefield piling.
- a. Precast piles are steel-reinforced members that are cast and thoroughly cured before driving.
- **b.** Cast-in-place piles are columns of unreinforced concrete made by pouring concrete into a hole made with a shell, mandrel, or earth auger. They can be used instead of wood or steel piles to carry foundation loads through firm soil to a subsurface layer of rock. Cast-in-place piles should not be less than 15 inches in diameter.
- (1) Both truck-mounted and skid-mounted engine-driven earth augers are class IV equipment. They will drill up to 22-inch holes, 15 feet deep, in soils not containing boulders over 3 inches in diameter.
- (2) Mandrels can be made of wood, or of steel pipe, if available. Mandrels must not be withdrawn until all holes for the pile group have been driven, or the open holes will be caved by the compression caused in driving mandrels for succeeding holes.
- (3) Piles can be cast in place only in soil that will stand without caving. Holes should be filled with concrete immediately after being made. The soil around the piles must not be disturbed for at least 12 hours after the concrete is poured.
- (4) Commercial cast-in-place piles having a predriven steel shell may be used if available.

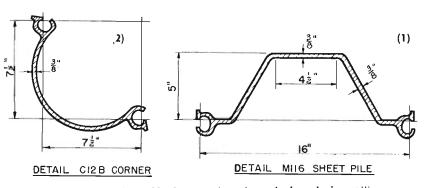
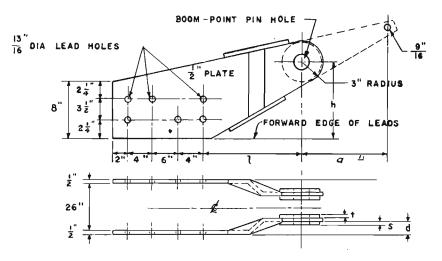


Figure 82. Cross section of standard steel sheet piling.

- (1) 16-inch, 36-pound, 5-inch deep-arch section.
- (2) 30.7-pound corner section.



CRANE MAKE	BOOM-POINT PIN HOLE DIAMETER (INCHES)	l	h	d NCHES	S	t
QUICKWAY 3/8 CU Y.D. TRUCK-MOUNTED CRANE	2	12	9 1/4	4 4	1 4	0
BUCYRUS-ERIE MODEL-15B 1/2-CU-YD. SHOVEL	2 1/2	15	11 3	1 3	1/2	0
OSGOOD MODEL 200 21 1/2-CU YD. SHOVEL	9 16	16	1/2	3 🖁	1/2	0
BUCKEYE 의	3	12 3	8 <u>11</u>	5 	1/2	0
LORAIN MODEL 82	2 9 16	19 3	12	6 4	1/2	٥
NORTHWEST MODEL 78 D	3 <u>1</u> 6	15	12 2	0	1 2	0
25-TON STIFF-LEG DERRICK	2	18	15	6 4	0	ı
30-TON STIFF-LEG DERRICK	2	42	12 3/4	4 5 8	0	ı

- ${
 m II}$ BUCKEY ADAPTORS HELD WITH 1/2 X25 1/2 " BOLT ABOVE BOOM-POINT SHEAVE, ${
 m \it Q}$ = 12 INCHES
- 2 OSGOOD ADAPTORS ATTACHED ABOVE BOOM-POINT SHEAVE, FURNISHED WITH 1 1/2 x 26 INCH THREADED ROD
- 3/ ADAPTORS SUPPLIED WITH SPECIAL BOOM-POINT SHEAVE PIN

Figure 83. Boom-point adapters for standard pile-driving equipment.

Section II. PILE DRIVING

- 148. DEFINITION. Pile driving consists of the following operations:
- a. Hoisting and placing the pile in position for driving.
- **b.** Driving the pile to desired penetration.
- 149. PILE-DRIVING EQUIPMENT. a. General. (1) Pile-driving equipment consists of:
- (a) Pile hammer (steam-pneumatic or drop hammer) to deliver driving blow.
- (b) Pile cap to cushion hammer blow and guide pile butt during driving.
- (c) Leads to guide cap and hammer.
- (d) Hammer line and pile-handling line to raise and lower hammer and to position pile.

- (e) Jets may be used to facilitate driving.
- (2) Newly standardized pile-driving leads and standard 1,200-, 1,800-, and 3,000-pound drop hammers with pile caps, as well as 5,000-, and 7,000-pound pneumatic or steam hammers, are available in class IV supplies. Adapters for standard loads are furnished with the crane booms of recently purchased standard cranes, shovels, and derricks. (See fig. 83.) If necessary, adapters can be made in the field to fit crane-boom pins of available cranes.
- (3) Nonstandard pile-driving equipment with leads, hammers, and pile caps of manufacturer's own design are available as attachments for some truckmounted and crawler-mounted cranes and shovels purchased before standardization.
- b. Pile-driving hammers. (1) Light sheet piling can be driven into soft ground with a heavy hardwood hand maul or with a pneumatic paving breaker. (See fig. 84.)
- (2) Bearing piles and heavy sheet piling must be driven with the heavier hammers listed below. Hammers must be heavy enough to secure the required friction-pile capacity (par. 155) at penetrations of not less than ½-inch per blow.
- (a) Drop hammers. 1. Drop hammers (fig. 85) weighing 1,200-, 1,800-, 2,500-, and 3,000-pounds are issued with some standard shovels or can be obtained from depots.
 - 2. Accessory to the hammer is a cast-steel pile cap or follow block which is recessed to fit over the head of the pile. It also has jaws by which it is guided in the leads. The pile cap transmits the hammer blows to the pile and holds it in position between the leads during driving. The standard pile cap shown in figure 85 is for wood piles; steel bearing piles and steel sheet piles require special pile caps or adapters

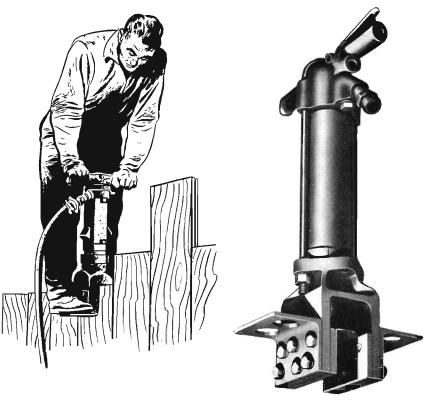


Figure 84. Pneumatic paving breaker with sheet-piling driver head.



Figure 85. Standard drop hammer and pile cap.

- 3. For efficient work, drop hammers should weigh as much as the pile being driven; preferably, they should weigh twice as much.
- (b) Steam hammers. 1. 5,000- and 7,000-pound double-acting steam-pneumatic hammers are available as class IV equipment. The piston in double-acting hammers is lifted up and driven down against the pile cap. In single-acting hammers, no pressure is exerted on the piston during its downward movement. A 10,200-pound single-acting hammer is available with some engineer units. (See fig. 86.)
 - 2. Steam-pneumatic hammers can be run on steam or compressed air. Steam and air requirements as well as dimensions, weights, and performance data are given in table XLIX.
 - 3. The cap of a standard steam-pneumatic hammer is an integral part of the hammer. Cap fittings to position steel sheet and bearing piles are shown in figure 87.
- c. Leads. (1) Pile-driving leads are constructed of wood or steel. Wood leads should be lined with steel to reduce wear and friction.
- (2) Leads are classified according to the method of attachment listed below:
- (a) Fixed leads are rigidly attached to the pile driver; they are used to drive vertical piles only.
- (b) Swinging leads are pivoted and braced at an angle to drive batter piles—piles driven at an angle. (See fig. 15.)

TABLE XLIX. Characteristics of stem-pneumatic hammers.

	Double	e-acting	Single-acting
Weight of hammer, lb	5,000	7,000	10,200
Weight of striking part, lb	800	1,600	5,000
Over-all height, in	73	98	159
Width between leads, in	22	21	20
Stroke of piston, in	9.5	17	36
Steam operation:			
Boiler pressure, psi	100	100	80
Boiler required, hp	35	45	40
Pneumatic operation:			
Air pressure, psi	100	100	80
Volume, cfm	450	600	565

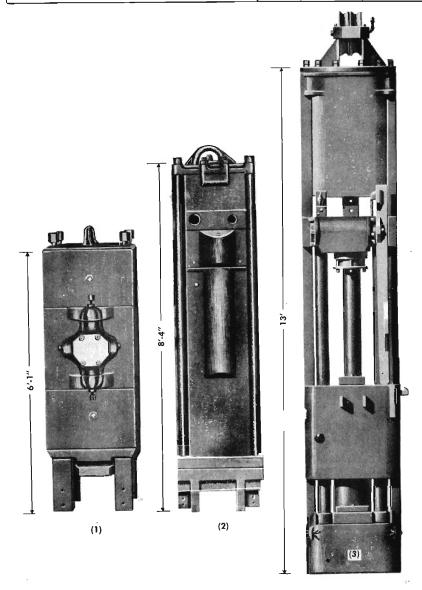


Figure 86. Steam-pneumatic pile hammers:

- (1) 5,000-pound double-acting hammer.
- (2) 7,000-pound double-acting hammer.
- (3) 10,000-pound single-acting hammer.

- (c) Hanging leads are hung from the boompoint with wire rope tackle. They can be used to drive vertical or batter piles, but their use should be avoided since control of their alignment is difficult.
- (3) Leads are normally attached to a crane boom with adapters or brackets on the boom-point pin or shaft. This limits batter to one direction.
- (4) Standard leads of steel are issued in 10-, 15-, and 20- foot sections. The 20-foot section is used as the top section and 10- and 15-foot sections can be added underneath it.
- (5) When leads are used with the standard cranes and shovels, the lead foot is braced with a telescoping catwalk connected to the base of the boom.
- d. Truck-, crawler-, and skid-mounted equipment. (1) Three-eighth- and $\frac{3}{4}$ -cubic-yard truck-mounted cranes with standard pile-driving attachments are available as class IV equipment. (See fig. 88.)
- (2) Crawler-mounted shovels in all sizes available to troops are issued with crane booms and most of them can be fitted with the standard pile-driving attachment. (See fig. 89.)
- (3) The standard skid-mounted pile drivers are of wood or steel construction.
- (a) The steel-frame skid-mounted pile driver is equipped with a 5,000-pound double-acting steam-pneumatic hammer and 55- or 65-foot standard leads. (See fig. 90.) The leads can be inclined in two directions: in line with the skid frame using the forebatter guide; and perpendicular to it, using the moonbeam.
- (b) The wood-frame skid-mounted pile driver is usually equipped with the 5,000-pound hammer and has 66-foot wood leads. These leads are for vertical piles.
- (4) Derricks can be equipped with adapters to handle the standard piledriving attachments.
- e. Jetting equipment. (1) Jetting consists of forcing air, water, or both, around and under a pile to displace, loosen, and lubricate the surrounding soil.
- (2) Air and water jets are used in silt, sand, or gravelly soils to assist pile driving. In sand where jets are most effective, piles can be sunk to within a few feet of full penetration with water-air jets alone; the hammer must rest on the pile to give it sufficient weight to overcome buoyancy.
- (3) One hundred to 250 gpm of water are usually required for effective driving depending on soil and penetration.
- (4) Jetting equipment shown in figure 91 can be requisitioned by parts from class IV equipment and supplies. Jetting pumps may also be furnished

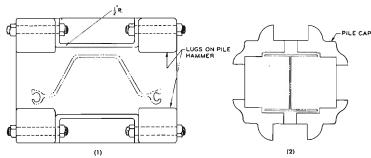


Figure 87. Steam-pneumatic pile-hammer cap fittings:

- (1) Steel-sheet-pile cap fitting.
- (2) Steel-bearing-pile cap fitting.

with jetting pipe assemblies of slightly different dimensions.

- (1) Pump.
- (2) Suction hose.
- (3) Jetting-pipe assembly of class IV material.

150. USE OF EQUIPMENT IN BRIDGE-FOUNDATION CONSTRUCTION. Bridge-foundation piles can be driven with the pile-driving rig on the bridge deck, on the ground, or on floating rafts or barges. Use of standard equipment to drive piles in bents, footing piles, and sheet piling is discussed and illustrated below.

- a. Piles in bents. (1) Driving from bridge deck. Any pile-driving rig can be used from the deck of a bridge if leads can reach the next bent (fig. 92). The limiting reach of truck- and crawler-mounted equipment is given in tables LXXXII and LXXXIII.
- (a) Piles. Timber piles are driven in the normal manner. Steel piles must be driven with their webs parallel to bridge center line. This requires that the leads be rigged as hanging leads and guyed in position, or chamfering of the pile flanges to fit in the cap and a frame at the foot of the leads to guide the pile.



Figure 88. Truck-mounted crane with pile-driving attachment of manufacturer's design.

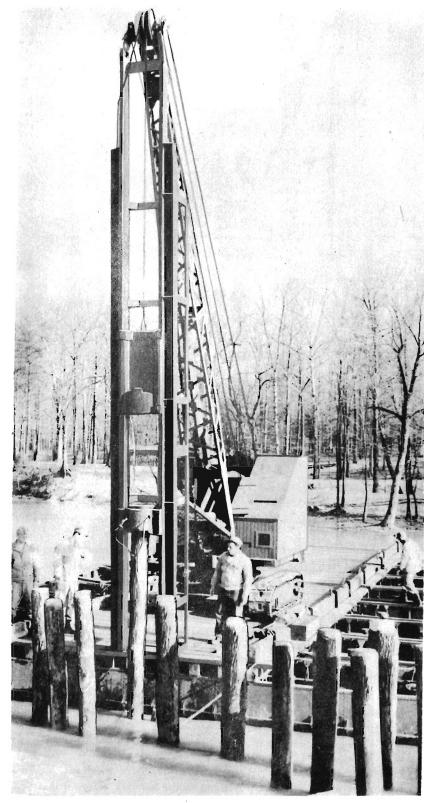


Figure 89. Shovel with crane boom and standard pile-driving attachment driving timber piles.

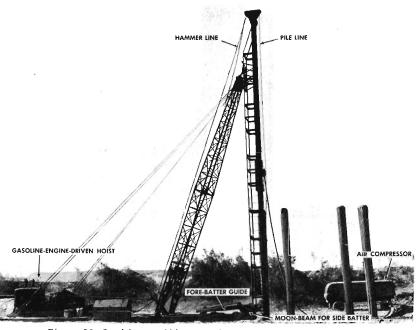
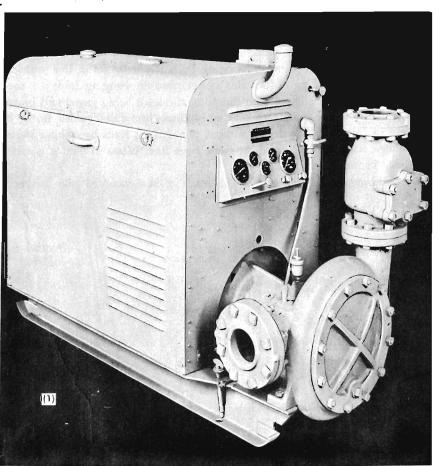


Figure 90. Steel-frame skid-mounted pile driver with swinging leads,

- (b) Batter piles. 1. The outside piles of railway-bridge bents are battered. The inside vertical piles should be driven first to carry a horizontal frame upon which the lower end of the leads can be supported for driving the outside battered piles. Leads may be either of hanging or swinging type. Figure 93 shows arrangement of hanging leads resting on frame in position to drive a batter pile.
 - 2. A steam-pneumatic hammer is required when driving batter piles with hanging leads. With swinging leads a drop hammer can be used to drive batter piles provided leads are well-greased.
 - 3. An expedient adapter can be used to swing leads laterally. (See fig. 94.) The foot of the leads must be securely guyed and supported.
 - (1) Boom-point wire-rope lead suspension.
- (2) Frame fastened to vertical piles to guide foot of leads in driving batter piles.
- (2) Driving from ground and rafts. (a) If site conditions permit, piles should be driven from the ground. When bents with batter piles are constructed, the pile driver should be placed in line with the bent to utilize the batter adjustment of standard leads.
- (\dot{b}) When piles are driven in water, pile drivers can be mounted on rafts or barges. (See figs. 95 and 96.)
- (1) 3/8-cubic-yard crane mounted on a pneumatic M3 raft.
- (2) $\frac{1}{2}$ -cubic-yard shovel equipped with crane-boom and pile-driving attachment mounted on a five-ponton 25-ton ponton raft.



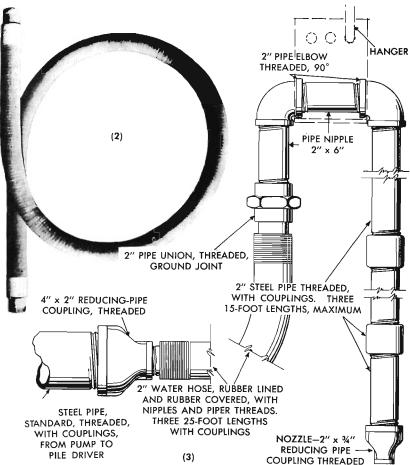


Figure 91. Jetting equipment with 200-gpm, 350-foot head, 150-psi, centrifugal pump.

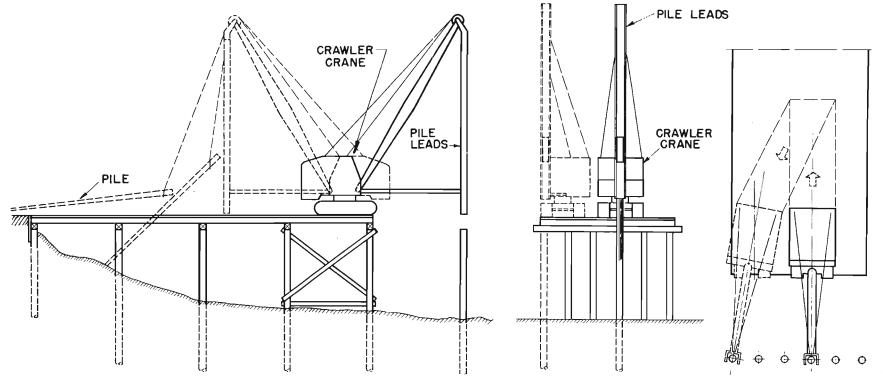


Figure 92. Driving piles from bridge deck. Note equipment reach.

b. Piles in footings. Piles for footings are usually driven from the ground or from rafts or barges. However, if piles are driven from deck level, leads must be lowered to guide pile and hammer. Driving footing piles follows generally the procedure used in driving pile bents; no batter piles are used.

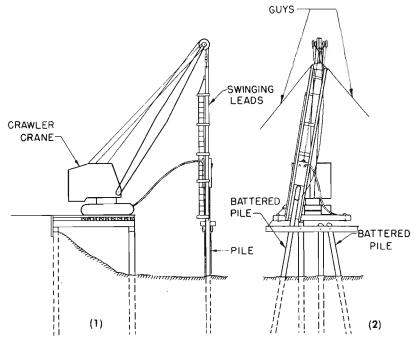


Figure 93. Driving batter piles from bridge deck.

- c. Sheet piling. Sheet piling is normally driven from the ground or from barges or rafts. A driver using swinging leads is usually set in line with the face of the sheet piling. When this is not possible, hanging leads are used because they can be aligned with the piles, the leads being guyed and braced to previously driven piles. Securely interlocked sheet piles guided firmly by cofferdam frames can be driven without pile driving leads by using a steam-pneumatic hammer hung from the crane hoist line. When so used it is called a *flying* hammer.
- d. Skid-mounted pile drivers. The reach of skid-mounted pile drivers is

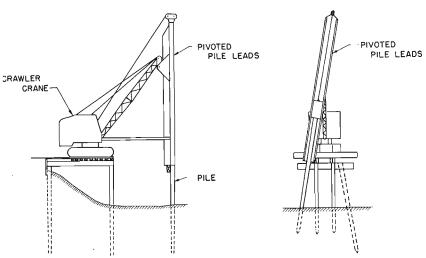


Figure 94. Expedient adapter used to swing leads laterally. The foot of the leads must be securely guyed and supported.

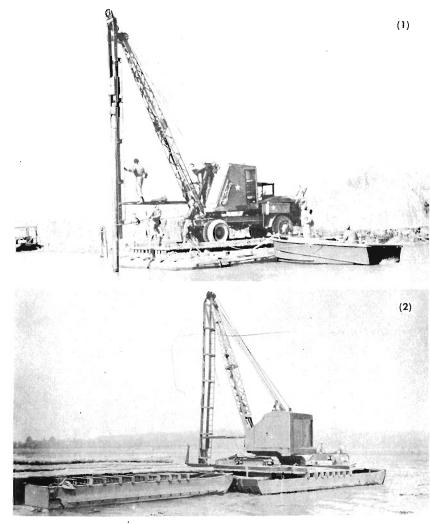


Figure 95. Raft-mounted pile drivers.

limited to about 20 feet, depending on weight of pile and hammer on the overhanging end and weight of hoist at the back end. The distance between bents cannot normally exceed 20 feet when the pile driver is used on the bridge deck. To extend the reach, the back end can be loaded with ballast or lashed down to a pile bent. On single-lane and railway bridges, it may be necessary to use outriggers on the pile bents. They should be used on the deck only when other types of drivers are not available.

151. DRIVING PROCEDURE. a. Bearing piles. (1) Piles are delivered within reach of the handling line. In handling, the pile line is attached near the pile butt, the pile is dragged or floated to the foot of the leads, and the pile is hoisted free of the ground.

Note. In attaching pile line with hook, the open part of the hook should face toward the pile tip. (See fig. 97 (1).)

- (2) The pile hammer is raised and held at the top of the leads. When a drop hammer is used, the pile cap is slung to the hammer before it is raised.
- (3) The pile is pulled up into the leads and the foot of the pile is placed in position. If the pile is driven through water a timber frame may be placed at the foot of the leads to position the lower end of the pile.

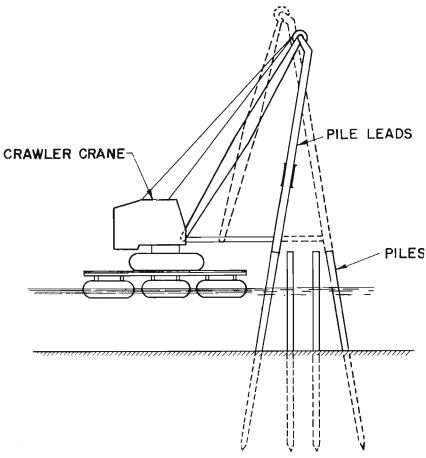


Figure 96. Raft-mounted pile driver with pile driver in line with pile bent. This allows use of swinging leads to obtain pile batter.

- (4) The pile is centered under the pile cap and the pile cap and hammer are lowered to the pile. A method of doing this is shown in figure 97 (1), (2), and (3).
- (5) (a) Drop hammers. With drop hammers, driving is started slowly, the hammer being raised only a few inches until the tip of the pile is firmly set. The height of fall is then increased gradually to a maximum of 10 to 15 feet. Driving blows should be as rapid as possible to keep the pile moving. If an obstruction such as a boulder or sunken log is reached, a few fast heavy blows can be used to displace or break the obstruction. Repeated long drops should be avoided, since they tend to crush and split the pile butt.
- (b) Steam hammers. Pressure on the first few blows of steam hammers is restricted until the pile tip is firmly set; it is then increased to full pressure as indicated in table XLIX.
- (6) (a) During driving the pile is watched for indications of splitting or breaking below ground. If driving is hard and suddenly becomes easier or if the direction of the pile suddenly changes, it is probably broken or split. Broken or split piles must be replaced. This can be done by driving a new pile nearby (offsetting) or pulling the broken pile and driving another pile in its place.
- (b) Springing causes loss of hammer efficiency and pronounced bouncing of the hammer. Springing and bouncing will occur under the following conditions:
 - 1. Using crooked piles.

- 2. When pile butt is not square.
- 3. When pile and leads are out of line.
- 4. When too light a hammer is used.
- 5. When penetration ceases because of obstruction or refusal.
- (7) If the fibers at the head of a pile become crushed or broomed, much of the hammer's energy is lost. A broomed pile should be cut back to sound wood and reshaped.
- (8) Piles driven to rock or other hard strata are often damaged by overadriving with consequent loss of capacity. The effect of overdriving is illustrated in figure 98.

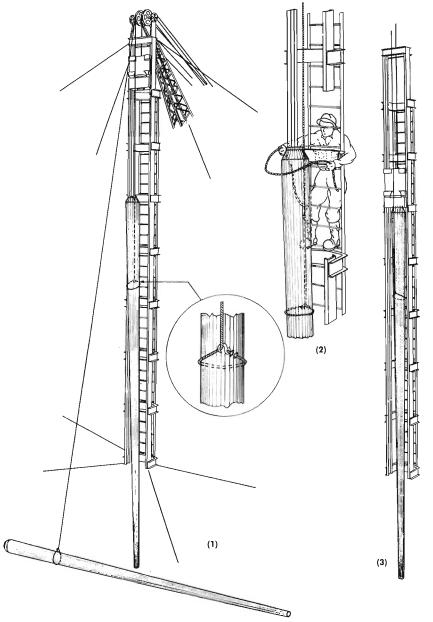


Figure 97. Placing pile in leads.

- (1) Pile hoisted in front of leads. Note pile-line attachment detail.
- (2) Line thrown around pile butt.
- (3) Hammer and cap lowered on pile ready to start driving.

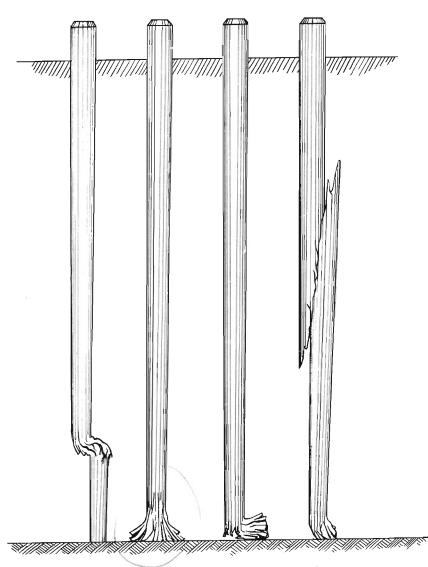


Figure 98. Effect of overdriving on wood piles.

- b. Sheet piling. General procedure in driving sheet piling varies from bearing-pile driving in the following ways:
- (1) The sheet pile heads are bored for handling-line shackles.
- (2) The lower end of the steel-sheet-pile slot should be plugged to keep out dirt and to allow easy driving of succeeding piles.
- (3) The first sheet pile is driven only until the point is firmly set; succeeding sheet piles are driven to the same point; each pile is then driven a few feet at a time to the required penetration.
- (4) The pile tongue should be kept at the free edge so stones will not become wedged in the groove and make it difficult to drive the succeeding pile.
- (5) Timber sheet piles can be held close together by snubbing a line tightly around the group.
- c. Jetting. (1) Jetting aids pile driving.
- (2) Jets are usually not fastened to the pile but are handled separately by a line attached to the top of the jet and carried over a pulley at the top of the leads. They are lowered into the ground by their own weight as the water removes the soil at their points.
 - (3) The jets are manhandled and are kept in motion to prevent coarse

material packing around the pipe and causing it to stick.

- (4) Jets may be used singly or in pairs. If two jets are used, one jet is kept moving slightly ahead of the pile while the other is slowly raised and lowered between the foot of the pile and the ground surface to maintain a flow of water along the pile.
- (5) While being driven a pile will tend to move toward a single jet. This tendency is used to straighten piles. (See fig 101.)
- (6) Jets should be taken up before the pile reaches final penetration and the pile sunk the last few feet with the hammer alone.
- d. Realigning piles. When piles are not driven straight, they can be realigned by using one of the following methods:
- (1) Inclined strut. (See fig. 99.)
- (2) Block and tackle. (See fig. 100.)
- (3) Single water jets. (See fig. 101.)

Note. The greater the penetration the harder realignment becomes. Alignment should be checked during driving and piles should be realigned as soon as misalignment is noticed.

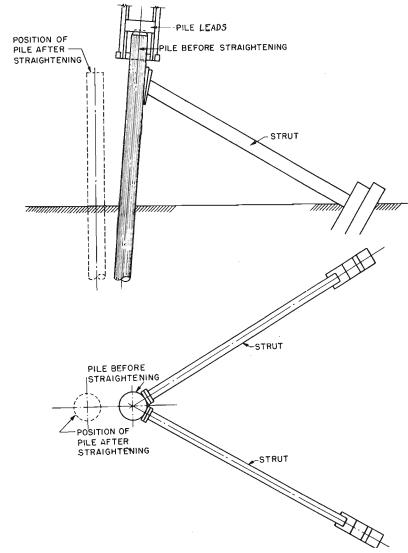


Figure 99. Straightening pile with inclined struts.

- e. Driving sequence. (1) Driving should progress from an area of high resistance to low resistance, toward a stream, or down slopes. This minimizes shoving previously driven piles out of place, when driving succeeding piles.
 - (2) When piles are driven in a group:
- (a) Outer rows are driven first if they derive their principal support by friction. (See par. 154.)
- (b) Inner rows are driven first if the piles derive their support by point bearing.
- 152. PULLING PILES. a. If piles must be removed, they can be pulled with the pile line or by the inverted hammer arrangement shown in figure 102. Pulling damaged piles should begin immediately after the pile has been broken, so the ground around the pile does not consolidate to make pulling more difficult. Jetting can be used to help loosen a pile. A few blows with a hammer may help loosen a pile.
- **b.** Piles can be pulled with tackle suspended from an A-frame or gin pole. A pull of 25 to 75 tons may be required. If a crane is used, the boom must be snubbed to the ground to prevent the crane's upsetting if piles suddenly come loose or the tackle breaks.
- c. The light steam hammer can be inverted and used in pulling piles. A cable sling is passed over the hammer and attached to the pile as shown in figure 102. A steady pull is put on the pile to keep it in motion as it is lifted by the upward blow of the inverted hammer.

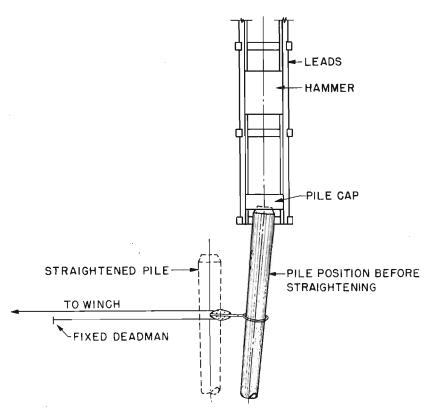


Figure 100. Straightening pile with block and tackle.

- (1) Correcting pile-tip position.
- (2) Correcting pile-butt position.

Section III. ESTIMATION OF PILE CAPACITY

- 153. LOADS ON BEARING PILES. a. Bearing piles in bridge foundations carry vertical loads (the weight of the bridge and vehicles) and horizontal loads from wind, current, and movement of vehicles on the bridge.
- b. The vertical loads determine the required pile resistance; the horizontal loads limit the bent and tower heights in deep swift water. (See par. 10.) Pile sizes should not be smaller than given in paragraph 144.
- c. Pile design loads are shown on the assembly drawings for the different pile foundation designs. The loads given are dead and live loads, or 80 percent of dead and live load in combination with loads from lateral and longitudinal forces whichever is greater. The range of loads is:
- (1) Timber piles—8 to 18 tons.
- (2) Steel piles—10 to 50 tons.
- 154. FACTORS GOVERNING PILE CAPACITY. a. Pile Stress. The portions of piles above the ground (between braces) act as columns. The loads on

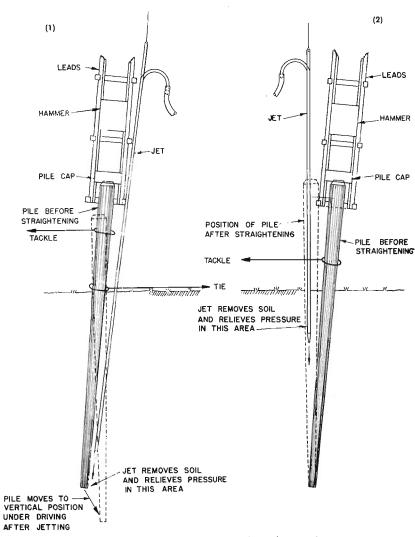


Figure 101. Straightening pile with water jet.

pile bents and on individual piles under towers therefore must not exceed their unbraced column strength. Also the permissible timber stress for compression perpendicular to the grain must not be exceeded for pile-cap bearing on the pile. The timber working stress must not be exceeded by combined compression and bending at a point below ground where the soil is firm enough to give the pile side support. (See par. 156.)

b. Point bearing resistance. The strength of timber piles resting solidly on rock or other hard bearing surface is governed by the timber stresses. In all but the softest soils, point bearing on the soil under the pile provides some of the load resistance. In firm sand and gravel, the point resistance may exceed one-third of the total load resistance of timber piles. The remainder of the penetration load resistance is frictional force on the pile surface.

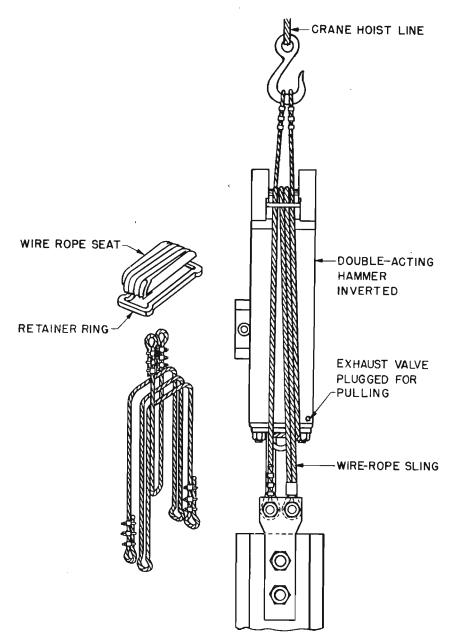


Figure 102. Wire-rope sling stream-pneumatic-hammer assembly used to pull piles.

Exhaust valve must be plugged for pulling.

c. Frictional resistance. The load capacity determined by friction between the soil and the pile surface is proportionate to the circumference of the pile and to its penetration of the ground. The friction increases with increased grain size, good grading, and soil compaction; in fine grained soils, it decreases with increased soil moisture. For short penetrations in fine-grained soils, timber piles have greater frictional capacity than steel piles because of their greater displacement.

155. FRICTION BEARING-PILE CAPACITY. a. General. The capacity of friction bearing piles (defined in par. 143 (2)) is estimated by:

- (1) Static friction based on penetration surface area and frictional resistance in similar soils. (See table XXVI.)
 - (2) Dynamic resistance based on driving energy. (See par. 155 c.)
- b. Preliminary estimates. Before driving begins, the size and length of friction piles required are estimated as described in paragraph 83. The length of point-bearing piles is determined by depth to rock or other firm bearing material.
- c. Estimation of pile capacity using driving data. (1) The following formulas are used to estimate the safe bearing-pile capacity from data obtained during driving. In bridge construction, each pile is driven until the average penetration per blow becomes less than that developing the required bearing capacity.
 - (a) Piles driven by drop hammer.

Timber pile	$P = \frac{2 W d.h}{s + 1.0}$ $3 W d.h$
Steel pile	$P = \frac{3 W d.h}{s + 1.0}$

(c) Pile driven by double-acting pneumatic or steam hammer.

Timber pile	$P = \frac{2E}{s + 0.1}$
Steel pile	$P = \frac{3 E}{s + 0.1}$

Symbols:

b = average height in feet of fall of drop hammer for last six blows.

H = stroke of ram in inches.

P = estimated safe load capacity in pounds per pile.

s = average pile penetration in inches per blow for the last 6 blows of drop hammer or last 20 blows of pneumatic or steam hammer. For small values of s the formula does not give consistent results. In that case, an average may be taken for several adjacent piles driven to approximately the same penetration. See subparagraph 149b(2).

Wd = weight of drop hammer in pounds.

Wr = weight of ram of steam or pneumatic hammer in pounds. (See Table XLIX).

E = driving energy in foot-pounds per blow of double-acting steam or pneumatic hammer, which may be estimated as follows:

	Strokes per minute	Energy foot-pounds per blow
	(225	4,150
5,000-lb. hammer	195	3,720
	170	3,280
	140	8,200
7,000-lb. hammer	130	7,000
	120	5,940

- (2) The formulas are subject to certain limitations and modifications.
- (a) The capacity formulas are reliable for bearing piles which derive their support principally from skin friction in granular non-plastic soils, such as gravel, coarse-grained sand, and dry fine-grained sand. For piles driven into fine-grained silts, clays, and saturated fine sands, the formulas give values which are too conservative.
- (b) Except in rare instances, bearing capacities of friction piles increase after driving. To determine whether or not soil conditions are such that the formulas apply, compare the average penetration per blow during the last six blows with the average penetration per blow after a 24-hour rest. If the penetration per blow after 24 hours is less than two-thirds the penetration when first driven, a soil condition is indicated for which the formulas give unnecessarily conservative values. The increase in bearing capacity after driving may make it possible to avoid splicing piles. If the required bearing capacity does not develop, drive a friction pile to nearly its full depth, allow it to stand 24 hours, and then check its capacity with at least 10 blows with a drop hammer or 30 blows with a steam-pneumatic hammer. Piles need not be spliced and driven deeper if the average penetration per blow on redriving is less than that required by the formula to give the needed bearing capacity.
- (c) When jetting is used to aid driving, the formulas apply only if the pile is rested after jetting and then driven to final position without jetting. Data from the final driving is used in the formulas.
- d. Static-load test. (1) General. Static-load tests can be used to estimate the capacity of piles driven in any type soil by any driving method. This is a reliable method but is slow and cumbersome.
- (2) Soil type limitations. (a) Load testing of piles driven in granular non-plastic soils can begin immediately after driving.
- (b) Piles driven in fine-grained silts, clays, and saturated fine sands must be allowed to rest at least 24 hours after driving before static-load testing is started. When piles are driven in these soils, the skin-friction resistance during driving is much less than the skin-friction resistance after a 24-hour rest, while the point-resistance is greater during driving than after a rest. This is because the compression of the material under the pile point during driving compacts the soil and squeezes water out of it. The water escaping upward along the sides of the pile lubricates it and reduces skin friction. During the rest the water seeps away from the pile into the adjacent soil and the earth settles against the pile, grips it, and develops skin friction.
- (3) Jetted piles. Piles placed by jetting, or by both driving and jetting, are surrounded by a lubricating film of air and water. A 24-hour rest is required to allow the water to seep away from the pile and the earth to settle against it.
- (4) Testing methods. A simple testing method is to build a platform on top of a pile and load it. Beginning with a load somewhat below the predicted safe load, weight is added and left for 48 hours. Meanwhile, careful

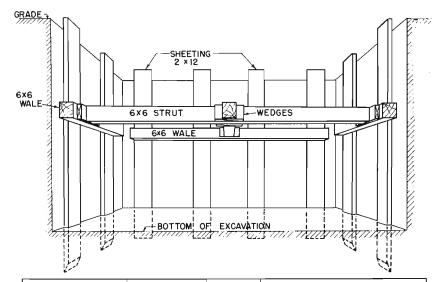
measurements of settlement and time are recorded. The maximum safe load per pile is one-half the total applied load which in 48 hours produces settlement of one-half inch, not including the initial settlement during and immediately after applying the load increment.

156. CAPACITY OF PILES ACTING AS COLUMNS. a. Capacity Formula. The capacity of timber piles acting as columns is determined by the column-

stress formula for piles: 1000
$$\left(1 - \frac{L}{60d}\right)$$
 in which $\frac{L}{d}$ is the length

to diameter ratio for the unbraced length of pile, and 1,000 psi the allowable working stress for continuously wet wood of the grade carried in depot stocks. This stress also governs for combined bending and compression.

- b. Unbraced length. (1) The unbraced length of pile is taken as the longest distance between transverse or longitudinal braces, or from the lowest brace connection to a point slightly below ground where the soil is firm enough to give the pile side support (for well-consolidated soils, up to one-eighth the penetration).
- (2) The maximum column loads for piles of 10-, 13-, and 16-inch diameter acting as columns are:



Exc	avation	Sheeting	Wales		Cross bra	ces or str	uts
Depth in feet	Kind of soil	(2- by 4-inch lumber) Type of construction	(4-foot spacing) Size in inches	For ti	er size in rench wid aced leng 6 feet	th or	Maximum longi- tudinal spacing in feet
5 to 10	Hard, com- pact	Open; spaced not over 8 feet	2 x 10	4 × 4	4 x 6	6 × 6	8
4 to 10	Soft, sandy	Close sheet- ing	4 x 6 ¹	4 × 4	4 × 4	6 x 6	6
4 to 10	Hydrostatic pressure	Tongue-and- groove sheeting	6 x 8 ¹ 1	4 × 6	6 x 6	6 x 6	6

¹Wales placed with larger dimension horizontal.

Figure 103. Bracing and sheeting excavations.

- (1) Typical excavation in firm earth.
- (2) Minimum sizes of timber.

Unbraced length (feet)	Average diameter unbraced length of pile		
	10 in.	13 in.	16 in.
	(tons)	(tons)	(tons)
10	(32)		
20	(24)		
30	16	(35)	
40	8	(25)	(50)
50		15	(37)

Values with parenthesis are higher than used in these designs (par. 46).

- 157. PILE PENETRATION. Bearing piles must be driven at least 8 reet into firm ground and 15 to 20 feet into soft ground. Piles must be driven deeper if scour is probable.
- 158. SHEET PILING. a. Sheet piles are used to resist horizontal forces. Maximum depths are governed by the following: (1) Strength of sheet piles in bending and strength of interlock in cellular construction.
- (2) Strength and spacing of wales in braced trenches and tied or braced cofferdams.
 - (3) Strength of struts between wales of inside-braced cofferdams.
- (4) Strength of tie rods between outside wales in filled cofferdams.
- **b.** The use of timber and steel sheet piles in typical cofferdam construction with safe spacing of supporting wales is shown in appendix II.

CHAPTER 13

FOUNDATIONS AND ABUTMENTS

Section I. GENERAL

- 159. SCOPE. a. This chapter describes methods of constructing the different types of foundations included in this manual. Two general types of foundations are considered:
- (1) Pile foundations: bents, piers, footings, and abutments.
- (2) Spread foundations: grillages, concrete pedestals, and abutments. Timber cribs and concrete or masonry piers are not included.
- **b.** Driving bearing piles for foundations and abutments and sheet piles to protect foundation excavations is discussed in detail in chapter 12. However, bracing and capping of pile bents and piers is discussed in this chapter. General information on construction of foundations is given in FM 5-10.
- c. Designs and construction procedures for foundations described in this manual should not be used in regions where permanently frozen ground (permafrost) exists. In permafrost, it is usually necessary to modify designs and construction normally used under other climatic conditions. (See TB 5-255-3.)
- 160. EXCAVATING. Excavations for footings and abutments of semipermanent bridges are usually shallow. Excavating machines, power shovels, or draglines, can be used to advantage for preliminary grading. Finished excavations are usually made with hand tools.

- a. Dry excavation. (1) In dry or moist soil, excavations to depths of 4 to 5 feet can usually be made without shoring or sheeting. Sides of the excavation are vertical if the ground is firm and has no tendency to cave or slide. In loose earth, sides of the excavation must be sloped.
- (2) Deeper excavations, excavations at the foot of steep slopes, and excavations close to railway tracks or to areas heavily loaded by other foundations, must be shored or sheeted to prevent caving.
- (a) Continuous sheeting need not be used in firm, stable, earth. Plank are set vertically at intervals not greater than 5 feet and are held by horizontal wales and struts. (See fig. 103.)
- (b) In unstable or sandy soils, sheeting must be continuous. It is held by horizontal sets consisting of wales and struts framed to the size of the excavation. Vertical sheeting is driven around the outside of the sets as the excavation is deepened.
- b. Cofferdam excavation. (1) Cofferdams. (a) Excavations through water or in saturated soil are made inside watertight cofferdams. Cofferdams are built by driving closely fitting or interlocking sheet piling or sheeting around timber wales framed to the dimensions of the excavation. Typical cofferdams and data for their design are given in appendix II.
- (b) For cofferdams started on the ground, a shallow hole is dug. The wale frame is set in the excavated area and serves as a guide for driving the sheeting. For cofferdams started in the water, the wale frame is floated in place and guide piles or posts are driven to anchor the frame in position. The frame then serves as a guide for driving the sheeting.
- (c) In shallow excavations, the sheeting may be driven to the full required depth before excavation is started. In deeper excavations, sheeting is driven until driving becomes difficult; the hole is then partially excavated, an additional set is placed if needed, and driving is resumed. The two operations are used alternately until the required depth of excavation is reached.
- (d) Excavation in small cofferdams is usually done with hand tools, and the cofferdam must be unwatered while excavation proceeds. In sand, gravel, or other porous soil, the sheeting must be driven far enough ahead of the excavation to prevent large amounts of water flowing up through the bottom of the excavation. In tight silty soils or clay, the sheeting need be driven only enough to embed it firmly below bottom of excavation.
- (2) Unwatering cofferdams. Cofferdams usually leak appreciably and pumping is necessary to remove the water. Portable low-head centrifugal pumps should be used. A strainer must always be used on the suction end to keep out trash and stones.
- (a) The pneumatic sump pump (stock number 11–7468.5) having a capacity of 175 gpm at 25-foot head is best. Its operation requires 80 cubic feet of air per minute at 80 pounds pressure. This pump is suspended in a sump inside the cofferdam. It will continue to operate even when submerged.
- (b) Gasoline-engine-driven pumps available in class IV supplies include a base-mounted centrifugal pump (stock number 11–4619.28) having a capacity of 166 gpm at 25-foot head, and a portable centrifugal pump (stock number 11–4619.24) having a capacity of 55 gpm at 50-foot head. The larger pump is usually needed, but the small pump will unwater small cofferdams in tight soils.
- (c) Gasoline-engine-driven centrifugal pumps must be set outside the cofferdam to avoid danger from exhaust fumes. To reduce suction lift they

should be set as low as possible. The suction hose should be set in a sump and be kept completely submerged to prevent the pump sucking air and losing its prime.

- (3) Control of leakage. Leaks in walls of cofferdams are caused by poorly fitting, defective, and broken or split sheeting. Large leaks can be stopped by driving additional sheet piles behind the sheeting and by calking openings from inside the cofferdam. Small openings above the bottom can be stopped by sifting sand, cinders, or grain into the water close to the leak where it will be carried into the opening by the flow of water. Rapid unwatering of a cofferdam compacts the surrounding soil, reduces the flow of water through it, and causes small crevices to be filled with silt and sand.
- c. Size of excavation. (1) Excavations in firm soil for concrete foundations having vertical sides can be made the size of the foundation. Sides are cut to line and squared, and the concrete is placed without forms.
- (2) Cofferdams for wet excavations are made with 1-foot or more clearance between concrete forms and sheeting on all sides. Water leaking into the cofferdam can be pumped out of this space before it damages fresh concrete.
- 161. CONCRETE. a. Use. Concrete is used without reinforcing in pedestals and abutments of semipermanent bridges. It is preferably used only where water can be excluded from the forms. Placing of concrete under water should be done only when experienced personnel are available.
- **b. References.** See paragraph 43 for quality of concrete required. See chapter 9, TM 5–226, for detailed information on concrete form construction.

- c. Equipment. (1) The 14-cubic-foot trailer-mounted concrete mixer furnished to construction units mixes from 12 to 15 cubic yards of concrete per hour. This capacity is ample for pouring foundations of semipermanent bridges, the largest of which contains approximately 35 cubic yards of concrete.
- (2) Materials are stock-piled close to the mixer and are delivered to it in wheelbarrows. Five wheelbarrows are needed to handle materials, two for fine aggregate and three for coarse aggregate. Six to eight wheelbarrows should be provided to deliver mixed concrete to the forms.
- (3) Seven to eight gallons of mixing water are required per minute. It can be pumped to the mixer or can be delivered in tanks by truck.
- d. Anchor bolts in concrete. Anchor bolts embedded in concrete must be accurately set with wood templates held by timber frames nailed to the forms. They should be set before concrete is placed and their position checked immediately before and after placing the concrete. Anchor bolts must not be driven into the concrete after it is placed.
- e. Steel reinforcement. The concrete designs in this manual do not require reinforcing steel. However, the advantages of steel reinforcement warrant the use of available scrap material such as wire mesh, fencing, or salvaged Sommerfeld or bar-and-rod type landing mat to strengthen abutment bulkheads and concrete pedestals. In bulkheads, reinforcement should be near the rear face and extending well below the bridge seat. In concrete pedestals on piles, horizontal reinforcement should be placed both ways near the top of piles.
- 162. BACKFILL AND GRADING. a. Footings and grillages must be back-

filled to prevent the ponding of water around the footing and consequent softening of the foundation material.

b. Backfill should be placed in uniform, horizontal layers of not more than 6 to 12 inches, and each layer should be thoroughly compacted with hand or pneumatic tampers (stock number 66–8425.5). After backfilling, the ground surface should be graded so surface water will be carried away from the footing.

Section II. FOUNDATIONS

- 163. PILE BENTS. Pile bents are not usually braced and capped by the pile-driver crew. When the pile-driver rig is advanced over the structure, a crew lays stringers and sufficient flooring for pile-driving equipment.
- a. Timber pile bents (fig. 1). Where piles are not driven to exact position, they must be pulled into place and aligned with tackle and aligning frame (fig. 105) before the bent can be braced and capped.
- (1) After the piles are drawn into position, planks are spiked at the correct elevation to guide the saw in cutting off the piles (fig. 104); the piles are cut off either with a two-man crosscut saw or with a power chain saw; the cap timber is put in place; holes for driftbolts are bored through the cap and into the head of the pile; and the driftbolts are driven.
- (2) After the bent is capped, guides and aligning frame are removed, bracing is nailed into place, holes are bored through bracing and piles, and bolts are inserted to complete the bent. Preboring of piles, cap, and bracing

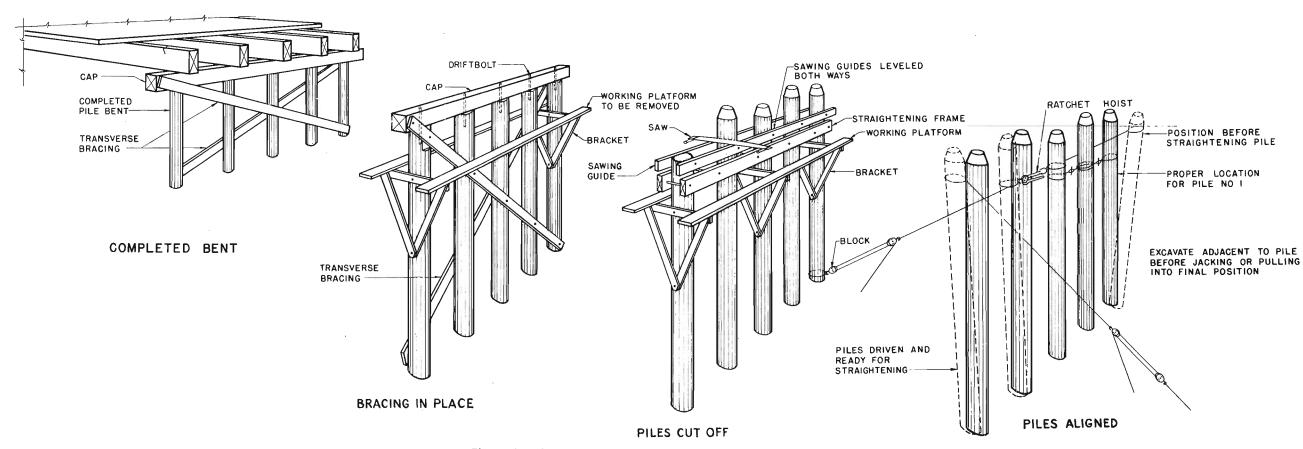
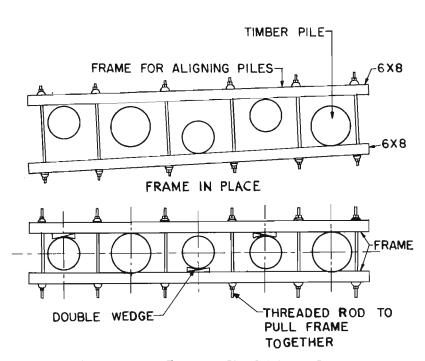


Figure 104. Aligning timber piles and successive steps in completing pile bents.

is not practical because of variations in shape, size, and spacing of piles. Methods of dapping and blocking to compensate for differences in size of piles are shown in figure 106.

- (1) Bracing on face of larger piles, filler blocks used on smaller piles.
- (2) Bracing face of smaller piles, larger piles dapped.
- (3) Bracing pulled against all piles, no blocking or dapping.
- b. Steel pile bents (fig. 3). Steel piles in bents must be driven so their webs are parallel with bridge center line. If not, piles must be rotated as well as aligned before they can be capped and braced. To draw piles into position, tackle, jacks, and timber frames are used as shown in figure 107.
- (1) Capping. Caps are bolted, riveted, or welded to piles. Bolting with standard machine bolts is preferred, since inaccuracies in connections can be best compensated by this method.
- (a) Bolted connections. After caps have been assembled with their diaphragms and drilled for connections, they should be set in place on the piles and held by clamps or on blocking from the straightening frame. Holes are then drilled or burned and reamed. Piles are marked and are cut off with an oxyacetylene torch. Bolts are inserted and tightened.
- (b) Welded connections. These are made with the cap bolted or clamped in place and supported from the straightening frame.
- (2) Bracing. (a) Irregularities in the positioning of piles makes it impractical to prebore holes, either in bracing or in piles. Welded bracing connections are preferred to bolted or riveted connections.
- (b) After caps have been connected, bracing is raised to position and held with clamps. Holes for bolts or rivets are drilled or the connections are welded.
- **164. PILE PIERS** (fig. 5). After individual bents are completed, jacks or tackle are used to draw them to correct spacing and to parallel alignment. Longitudinal corbels and bracing are installed to complete the pier.



FRAME TIGHTENED, PILES IN POSITION

Figure 105. Aligning frame to draw timber piles into position for capping.

165. SILLS ON TIMBER PILES (fig. 8 (1)). In driving piles to carry sills, particular care must be used to drive piles in correct alignment. They usually do not project enough above ground line to permit them to be aligned after driving.

166. STEEL FRAMES ON STEEL PILES (fig. 20 (1)). a. Piles to be capped with steel frames must be accurately driven. For this reason timber guide frames are used. Steel frames are prefabricated but are not assembled for erection.

- **b.** Piles are prepared for frames and frames are set in the following sequence:
- (1) Piles are cut off at correct elevation and flanges are cut (coped) as required for attachment of steel frame.
- (2) Cross beams are set and held in place with clamps while holes for their connection are drilled in piles.
- (3) Fitting-up bolts are inserted and drawn tight.
- (4) Cross diaphragms between beams are set and are bolted with fitting-up polts.
- (5) End angles between piles are set and held in place with clamps while holes for their connection are drilled.
- (6) Final connection of all parts is made with machine bolts, rivets, or structural ribbed bolts.
- c. After all parts of the four tower foundation frames are completed, the center of each tower column is carefully determined. From these centers, holes for anchor bolts are marked and drilled or burned.
- 167. CONCRETE PEDESTALS ON PILES (fig. 9 (1)). The pedestals of pile-supported concrete pedestal footings are normally at ground level. However, when piles are in water the concrete pedestals are built above water.

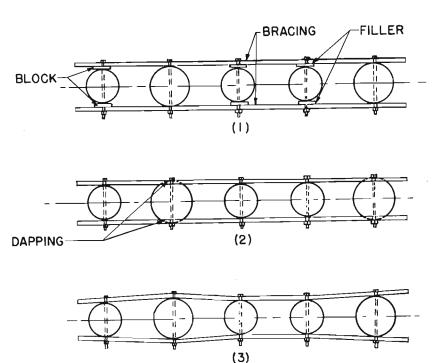


Figure 106. Methods of blocking and dapping piles for bracing to compensate for different size piles.

Butts of piles should be either thoroughly saturated before concrete is placed or should be sealed against water.

- a. Pedestals in soil (fig. 20 (2)). The bottoms of concrete pedestals must be set below the frost line usually from 3 to 5 feet deep, depending on climatic conditions. After piles are driven, the bottom of the pedestal excavation is leveled, piles are cut off at the correct elevation, forms are built, and concrete is poured. If the bottom of the excavation is soft, a bed of sand or gravel is laid before the concrete is placed.
- b. Pedestals over water (fig. 20 (3)). When placing concrete pedestals over water, timber sills are bolted to the piles and a platform somewhat larger than the pedestal is built on them at the level of bottom of pedestal. Piles are then cut off at correct elevation, forms are constructed on the platforms, and concrete is placed.
- 168. BRACING PILES BELOW WATER. Foundation piling should not have unbraced lengths from firm ground up to bottom of sills, pedestals, or transverse bracing greater than given in paragraph 10. Underwater lateral support can be provided by wire-rope bracing or riptap.
- a. Wire-rope bracing. Piles of bents and piers are braced below water with wire-rope guys connected as shown in figures 108 and 109. Guys must be tight to be effective. The section braced with wire rope should not be more than 12 to 15 feet high.
- (1) Guys on wood piles. To install guys on wood piles, two turns in the middle of the guy rope are taken around the outside pile of the bent and are pushed down to the bottom with a pole. One end of the line is looped twice around the pile at the other end of the bent above waterline. A pull-jack or turnbuckle is used to draw the line tight and the two ends of the guy rope

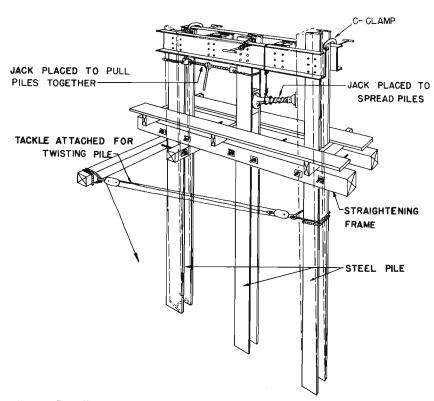


Figure 107. Pulling steel piles into position before drilling to connect cap and bracing.

are connected. Guy ropes are ½-inch galvanized wire rope and are connected with galvanized wire-rope clips.

- (2) Guys on steel piles. Before the pile is completely driven, two wire ropes are connected to the pile through holes drilled or burned in each flange. The wire ropes are lashed to the pile, and the pile is driven to final position, the lower ends of the wire ropes being near stream-bed level. Lashing is removed, and the free end of each guy is threaded through a hole burned or drilled in upper end of the pile at the opposite end of the bent. The guy rope is then drawn tight and wire-rope clips installed. Guys on steel piles are placed in paris connecting into each flange of the pile. Guy ropes are ½-inch galvanized wire-rope clips.
- **b. Riprap.** Riprap placed around foundation piles protects against scour and gives lateral support to the piles. (See fig. 20 (3).) Riprap must be deposited in uniform horizontal layers so piles will not be forced out of position. Side slopes of riprap should not be steeper than 1½ to 1.
- (1) Stone riprap. Stones, concrete, or masonry in pieces weighing 50 to 100 pounds are used if available. Irregular pieces stay in place better than rounded stones. Stones weighing less than 50 pounds should not be used for riprap.
- (2) Sacked concrete riprap. Sacked concrete can also be used as riprap. Cloth cement sacks or burlap bags of 1- to 2-cubic foot capacity are filled about two-thirds full, securely tied, and placed before the concrete sets. A 1-to-6 mix concrete using local sand or sandy soil for aggregate is satisfactory.
- 169. CONCRETE PEDESTALS ON GROUND. a. Concrete pedestals are set at least 3 feet below ground surface. They are set lower if necessary to:
 - (1) Reach firm soil having adequate bearing capacity.
- (2) Protect from frost action in cold climates.
- **b.** If excavation is carried deeper than intended, it must not be filled in with earth. Backfill is made with well tamped, selected, well graded sand and gravel, or concrete is used and the thickness of the pedestal is increased accordingly.
- 170. GRILLAGES. a. Bedding. To avoid uneven settlement, grillages must be carefully bedded and set. They must not be placed on loose, plastic, or non-uniform soil, nor on frost-bearing ground.
- (1) To secure even bedding, grade stakes are set at each corner of the grillage excavation. From these the ground is carefully leveled, using a straightedge and carpenter's level. High points over the area are removed with shallow cuts. Low areas are filled and the soil firmly tamped.
- (2) Tamping is done with a hand tamper; pneumatic tampers should not be used. Water can be used sparingly to aid in compacting loose, dry soil but the bed must not be muddy. Sand or fine gravel can be used to fill low spots in the surface.
- (3) Where soil conditions are unsatisfactory, the ground below the grillage is excavated to uniform, firm soil below frost line, drainage outlets are installed, and excavation is backfilled with select material well-compacted.
- b. Timber grillages. (fig. 10 (1)). Grillage timbers are placed one by one on the prepared bed. Each timber should be firmly bedded and the top surface of the first course leveled before placing the second course. Holes for driftbolts are then drilled and driftbolts driven to hold the two courses together.
- c. Steel grillages (fig. 14). Steel grillages are usually assembled in the

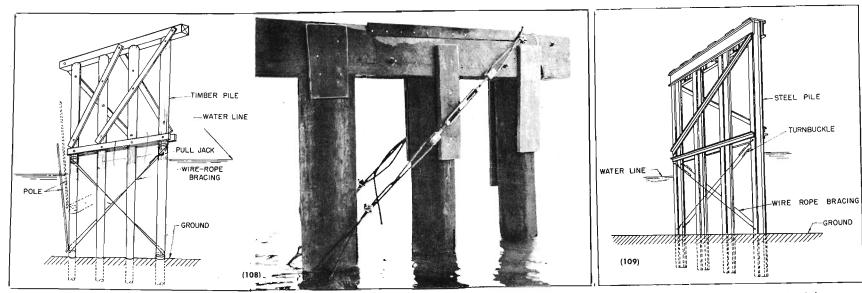


Figure 108. Method of attaching wire-rope guys to brace timber piles below water.

Figure 109. Method of attaching wire-rope guys to brace steel piles below water.

- (1) Arrangement of guys on bent.
- (2) Guys in place, tightened with turnbuckle.

fabrication yard and set as a unit. Because of their weight, they must be handled by a crane. They must be set exactly to permit correct placement of tower columns. Grillages may be set in a concrete bedding to obtain full uniform bearing.

171. FOUNDATIONS ON ROCK. Where foundations are on solid rock, no grillages are required. Column bearing plates are set on the rock after leveling the bearing area with grout or concrete. Anchor bolts are set in drilled holes and are cemented in place with grout.

Section III. ABUTMENTS

- 172. PILE ABUTMENTS. a. Pile abutments consist of one or two rows of timber or steel piles capped to form a seat for stringers of the end span, and a timber and pile bulkhead (end dam) to retain the approach embankment. See sheet 21 for details of a typical pile abutment.
- b. Procedure for construction of pile abutments is as follows:
- (1) Piles are driven and are cut off at correct elevations.
- (2) Bearing piles are capped and posts to support the bulkhead are bolted to the piles.
- (3) Horizontal planks of the bulkhead are nailed to the posts and ends are cut square.
- c. After the bulkhead is built, the approach embankment is extended to the abutment and allowed to spill past the ends of the bulkhead. Fill against the bulkhead must be well compacted.
- 173. TIMBER-GRILLAGE ABUTMENTS. a. Timber-grillage abutments consist of vertical posts set on a timber grillage. These are capped to form a seat for the stringers of the end span. The bulkhead is supported by the posts which are anchored by guy ropes to deadmen under approach fill. For low abutments,

the posts are omitted and the cap supporting the stringers rests directly on the grillage. See sheet 22 for details of a typical timber-grillage abutment.

- b. Procedure for construction of a timber-grillage abutment is as follows:
- (1) The grillage is assembled and set as a unit.
- (2) Posts, cap, and bulkhead timbers are framed, assembled, and set on the grillage.
- (3) Posts and backwall are braced away from the bridge at a slight batter, not over 1 in 12.
- (4) Wire-rope guys are attached to the posts with wire-rope clips, anchored to deadmen under the approach fill, and tightened.
- (5) The approach fill is placed against the backwall in well-tamped layers. When enough fill is placed to keep the backwall from overturning, the temporary bracing is removed. As additional fill is placed, posts and backwall will be forced to correct vertical position.
- 174. CONCRETE ABUTMENTS. a. Principal operations required for construction of concrete abutments are covered in section I. The rules in paragraph 169 for concrete pedestals apply also to abutments. See sheet 27 for details of a typical concrete abutment.
- b. Abutment concrete should be placed without construction joints. Under no condition should a construction joint be made at the top of the bridge seat unless steel dowels are provided to connect the backwall with the concrete below.
- c. Abutments should not be backfilled until the concrete has attained ample strength. At least 5 days should be allowed when using standard Portland cement concrete and 2 days when using high early-strength concrete. The top of the backwall should be protected with timbers during construction of the entire bridge. The wheels of heavily loaded construction vehicles should not be permitted close to the backwall, except on planking heavy enough to carry their load well back on the embankment.

CHAPTER 14

ERECTION PLANNING AND EQUIPMENT

Section I. ERECTION PLANNING

- 175. GENERAL. Erection procedure is determined by the type and size of bridge, the site the skill and experience of personnel, and the capacity of available equipment.
- **176. SELECTION OF PROCEDURE.** a. Step-by-step erection procedure must be developed. The speed of erection depends on the ingenuity of the officer in charge of construction. Larger bridges and difficult erection problems require accurate and detailed planning, including:
 - (1) Sketches of positions of equipment.
- (2) Plotting of reach and lifting capacity of equipment in each position.
- (3) Tabulation of weights of parts to be erected.
- **b.** Sound procedure results in:
- (1) Quick erection with a minimum of special equipment and labor, least chance of delay through accident or mishandling, and least risk to men and equipment.
- (2) Delivery of materials or assemblies within reach of equipment.
- (3) Employment of forces in separate groups not concentrated on one task or at one piece of equipment.
- (4) Firm footing and ample working room for all operations.
- c. Suggested methods of erecting structures of different types, heights, and span lengths under different site conditions, and detailed procedure for erecting typical units are given in chapter 16. Expedient crection of large structures may require combining two or more of the methods described, each being used to erect that part of the structure to which it is best adapted.
- 177. CHARACTERISTICS OF SITE. a. Characteristics of a bridge site are controlling factors in determining general layout, span lengths, and height of supporting towers or bents. These, in turn, are primary factors in determining erection procedure.
- **b.** Condition of approaches and their location with respect to the existing road net determine whether erection can be carried on from one or both ends of the structure and whether materials must be delivered to one or both approaches at deck level or to the ground or water below.
- c. A firm, gently sloping bank permits free use of equipment and free conduct of operations on the ground. Soft or steep banks require erection from overhead or from falsework. A wide waterway may require using floating equipment.
- 178. SKILL OF PERSONNEL. a. General. The skill and experience of available troops must be considered in developing procedure, particularly for difficult erection problems. Ability to handle equipment expertly and safely under maximum loads, knowledge of precautions necessary in handling heavy loads, and ability to anticipate contingencies are gained only through experience.
- **b.** Crane operators. Able crane and machine operators judge the speed with which capacity loads can be raised, lowered, or swung by the feel of their

- equipment; this ability can be gained only through experience. If skilled operators are not available, procedure should be planned to avoid handling erection parts near the capacity or maximum reach of erection equipment.
- **c.** Riggers. If the men are unaccustomed to working above ground, the number of connections to be made during erection should be reduced to a minimum by assembling parts on the ground and erecting them as units.
- **d.** Welders. (1) Highly skilled welders are required for erection welding. They must have passed qualification tests for welds of horizontal and vertical position. (See par. 124 and fig. 65.)
- (2) Welding main-member splices and connections during erection is not recommended. Secondary members, bracing, and fittings, which are less important to the safety of the bridge can be welded in place.
- 179. CAPACITY OF EQUIPMENT. Each principal member and subassembly must be examined to determine whether its erection is within the reach and safe load capacity of available equipment. If not, erection procedure must be modified or special equipment provided. Safe load capacities of standard truck-mounted and crawler-mounted cranes are given in tables LXXXII and LXXXIII. These data are used in determining construction schemes. Before handling loads near the maximum capacities, each crane or rig should be tested at the site since counterweights and construction may vary for equipment of one model.

Section II. EQUIPMENT

180. HAND TOOLS. Tools required to erect typical semipermanent bridge units are listed in table XXXI. This table does not include hand tools regularly issued to engineer squads and platoons. Figure 110 shows special tools required for erecting steel bridges.

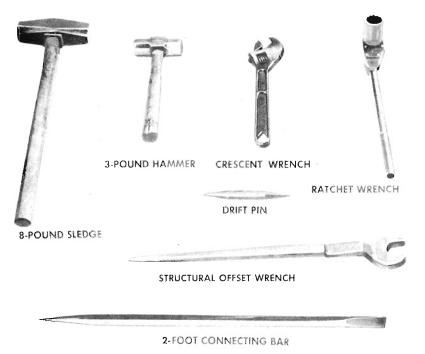


Figure 110. Hand tools used in erecting steel bridges.

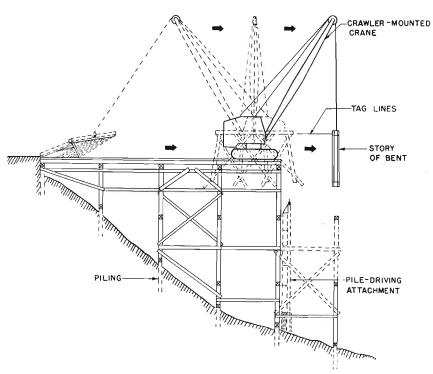


Figure 111. Crawler-mounted crane operating from deck of bridge to drive piles and erect timber towers within reach of crane.

- 181. RIGGING. a. Rigging instructions given in TM 5-225 cover use of lines and tackle and of gin poles and shears.
- b. Capacity of gin poles and shears of moderate height and reach is usually determined by the strength of guys and their anchorage. For the higher lifts and greater reaches often required in bridge erection, the strength of spars becomes the controlling factor in determining capacity.
- c. Stresses in guys and spars for different inclinations of each are shown in table LXXIV. Safe stresses in round and square spars of varying lengths are given in table LXXIII. Safe load capacities of wire rope and cordage are obtained from tables LXII, LXIII, and LXIV.
- 182. CRANES. Truck- and crawler-mounted cranes are preferred for erecting semipermanent bridges. They can be used to extend construction by moving out over the successively completed spans (fig. 111) or, if conditions permit, they can work from the ground. (See fig. 112.) Timber mats can be used to operate cranes over soft ground. For work over water they can be placed on a raft or barge. When operating from floating equipment, the raft or barge must be large enough to support the machine and its load without losing stability. Booms of the standard cranes are sectional and can be extended to raise loads to considerable heights.
- a. Truck-mounted cranes. (1) Truck-mounted cranes are suitable for erecting structures of moderate span; on larger bridges they are used principally to handle parts behind the main erection units and to supplement fixed or less mobile equipment. For details see chapter 16.
- (2) Truck-mounted cranes are highly mobile but require a firm level base for their operation; they should not be used on rough or soft ground.
- (3) Outriggers give stability when handling heavy loads. (See fig. 113.) They may not increase the capacity of the crane to handle end loads but they

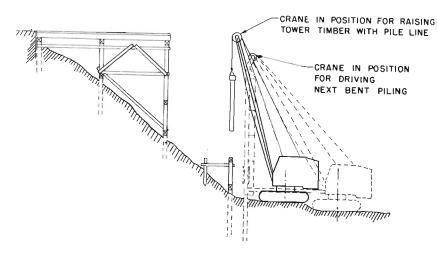


Figure 112. Crawler-mounted crane operating from ground to drive piles and erect timber towers,

always permit handling heavier side loads. Outriggers for the 3/8-cubic yard trucks are obtained from depots.

- b. Crawler-mounted cranes. (1) Crawler-mounted cranes and crawler-mounted shovels with crane-boom attachments are available to engineer troops in capacities from 3/8 to 2 cubic yards. (See table LXXXIII.)
- (2) They are less mobile than truck-mounted cranes but can maneuver easily and are better suited to erection use.
- (3) They can be operated over rough ground, ground too soft to support truck-mounted equipment, and, if the bottom is firm, in water deep enough to cover their crawlers.

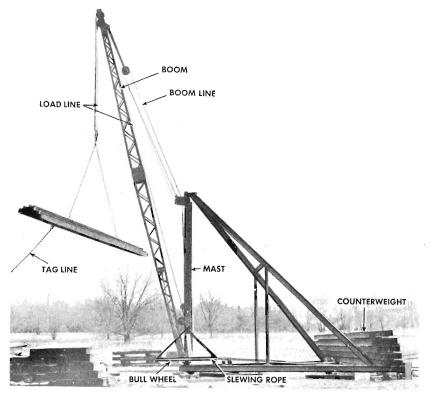
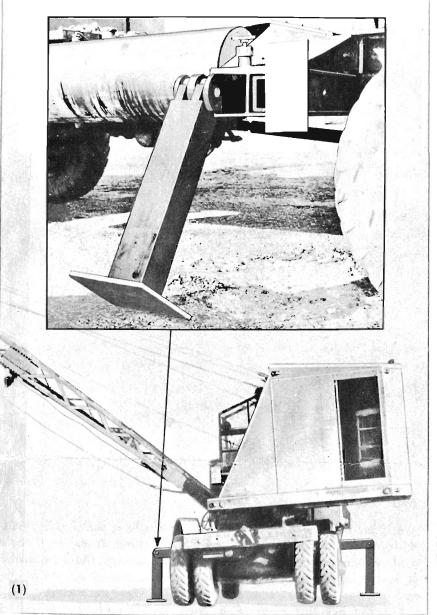


Figure 114. Four-ton stiff-leg derrick. Hoist is not in view.



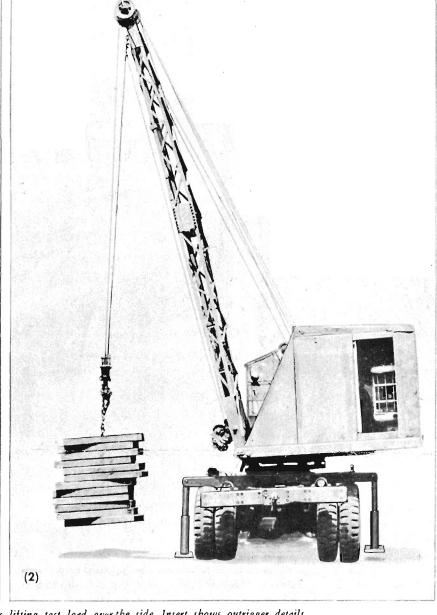


Figure 113. Truck-mounted 3/8-cubic yard crane with outriggers lifting test load over the side. Insert shows outrigger details.

Outriggers are obtained from depots and installed in the field.

(1) Coleman truck-mounted crane.

- 183. DERRICKS. Two types of derricks are ordinarily used in semipermanent bridge construction. Their use is not economical unless continued operations are carried on within reach of their booms.
- a. Guy derrick. (1) A guy derrick consists of a mast, a boom pivoted at the foot of the mast, and guys and tackle. If the guy lines to the top of the mast clear the end of the boom, the boom can be swung through a full circle. Loads are moved by hand hoist or by engine-driven hoist.
- (2) Details of a guy derrick designed for erection of high timber towers are shown on sheets 232 to 234 inclusive. Boom and mast of this derrick can be made of materials used later in the bridge. Special parts can be made in the field.

- (2) Brockway truck-mounted crane.
- b. Stiff-leg derrick. (1) The mast of a stiff-leg derrick (fig. 114) is held in a vertical position by two inclined struts connected to the top of the mast. The struts are spread apart 60° to 90° to provide support in two directions and are attached to sills extended from the bottom of the mast. The mast and boom swing through an arc of about 270°.
- (2) Steel derricks of the stiff-leg type are available to engineer troops in two sizes: 4-ton rated capacity at 28-foot radius, and 30-ton rated capacity at 38-foot radius when properly counterweighted. Both derricks are erected on fixed bases. Their adaptability to bridge construction is limited by their weight, dimensions, and immobility.
 - (a) The 4-ton derrick including a skid-mounted two-drum gasoline-engine-

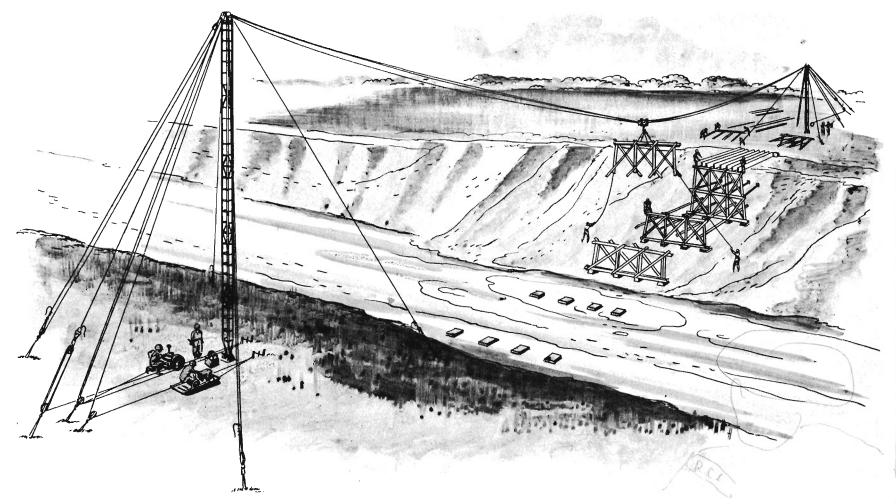


Figure 115. Medium cableway in position over bridge center line for erection of bridge.

driven hoist weighs 7 tons and occupies a space 22 feet square.

(b) The 30-ton derrick including a skid-mounted two-drum hoist weighs approximately 22 tons and occupies a space 29 feet square.

Note. When used on the deck of double-lane bridges, these derricks must be moved on rollers. Derricks on single lane and railway bridges must be supported by outriggers.

- c. Field-constructed derricks. Lashed stiff-leg and guy-mast derricks are described in TM 5-225. These and similar derricks often serve some special use in bridge construction. However, they must be seated on a fixed base or on a skid frame.
- 184. CABLEWAYS. a. The medium cableway (fig. 115), developed for military operations, can be used effectively for erecting timber and steel towers and for launching light stringers. The maximum cableway span is 1,200 feet, the cableway tower height 63 feet, rated capacity 3,000 pounds, and maximum hook load with caution 4,000 pounds. It can be installed in 6 hours by trained engineer troops. It weighs 20,000 pounds and is transported on four trucks.
- b. The cableway should be installed with the base of cableway towers approximately at grade and on the bridge center line. For detailed information, see Technical Manuals on this equipment.
- 185. HOISTS. Hoists are of two principal types, drum hoists, including winches and crab hoists, and chain hoists.

- **a.** Drum hoists. A drum hoist consists essentially of one or more winding drums, a train of reducing gears, and a power source. It may carry one or more winch or capstan heads for handling secondary lines. Hoists are attached to construction equipment of many types either as an essential part of a machine such as a crane or derrick or as an attachment on trucks and tractors.
- (1) The following power-driven drum hoists are available to engineer troops.

Power	Number of drums	Capacity in tons
Diesel	2	6
Gasoline (fig. 116)	2	4
Pneumatic (fig. 117)	1	1

- (2) Single-drum hand winches of 2-, 5- and 15-ton capacities are available as class IV equipment. (See fig. 118.) A winch arranged for attachment to a boom or mast is called a crab hoist. Winches are used principally to operate gin poles, shears, and derricks.
- b. Chain hoists. Chain hoists (fig. 119) are used for raising and holding loads and are particularly useful when accurate placing or adjustment of loads is required. They are of two types: differential chain hoists available in capacities of 1 to 5 tons, and ratchet chain hoists in capacities of $1\frac{1}{2}$ to $4\frac{1}{2}$ tons.

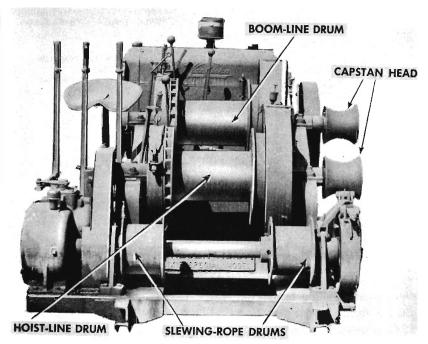


Figure 116. Gasoline-engine-driven hoist, double-drum, 4-ton capacity.

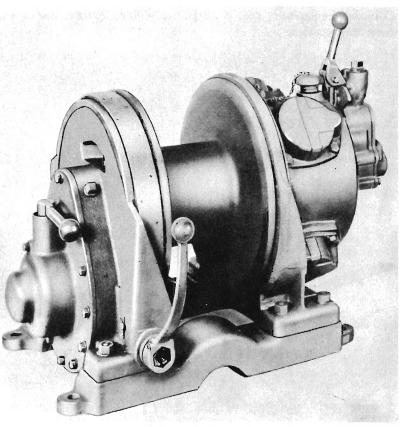


Figure 117. Pneumatic hoist, single-drum, 1-ton capacity.

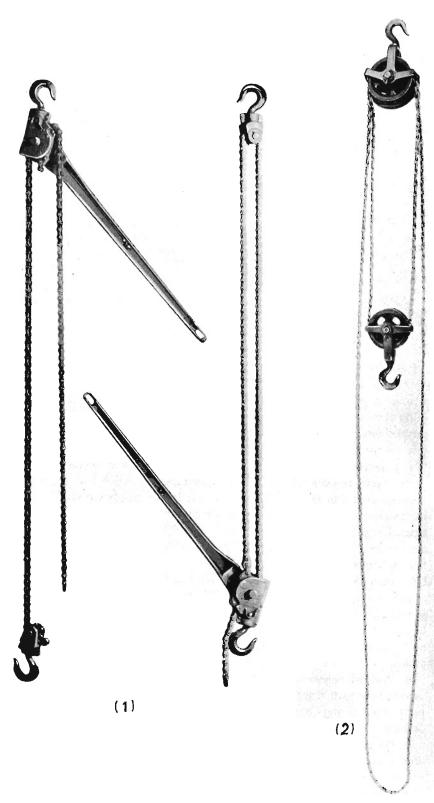


Figure 119. Chain hoists, hand-operated.

- (1) Ratchet chain hoist. View shows standard bridge hoists rigged for 1½-and 3-ton loads.
- (2) Differential chain hoist.

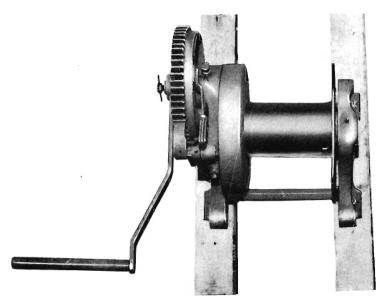


Figure 118. Hand winch, single-drum, 2-ton capacity, mounted on timber frame.

- 186. JACKS. Jacks are used to raise or lower heavy loads short distances. They are available in capacities from 5 to 100 tons. Small-capacity jacks are operated through a rack bar or screw while those of large capacity are usually operated hydraulically. Jacks most used in bridge construction are:
- a. Pushing and pulling jacks. Pushing and pulling jacks (fig. 120(1)) are screw jacks of 10-ton rated capacity with end fittings which permit pulling parts together or pushing them apart. Their principal use in erection is to spread or brace parts and to tighten lines or lashing.
- **b.** Ratchet lever jack. The ratchet lever jack (fig. 120(2)) available to engineer troops as part of panel bridge equipment is a rack-bar jack having a rated capacity of 15 tons and an effective movement of at least 11 inches. It has a foot lift by which loads close to its base can be engaged.
- c. Screw jacks. Screw jacks (fig. 120 (3)) having a rated capacity of 12 tons are supplied with the platoon pioneer set. They are about 13 inches high when closed and have a safe rise of at least 7 inches. This jack can be used for general erection purposes.
- d. Hydraulic jacks. Hydraulic jacks (fig. 120 (4)) are available in class IV supplies in capacities up to 100 tons. Loads normally encountered in semi-permanent bridge construction do not require large-capacity hydraulic jacks.

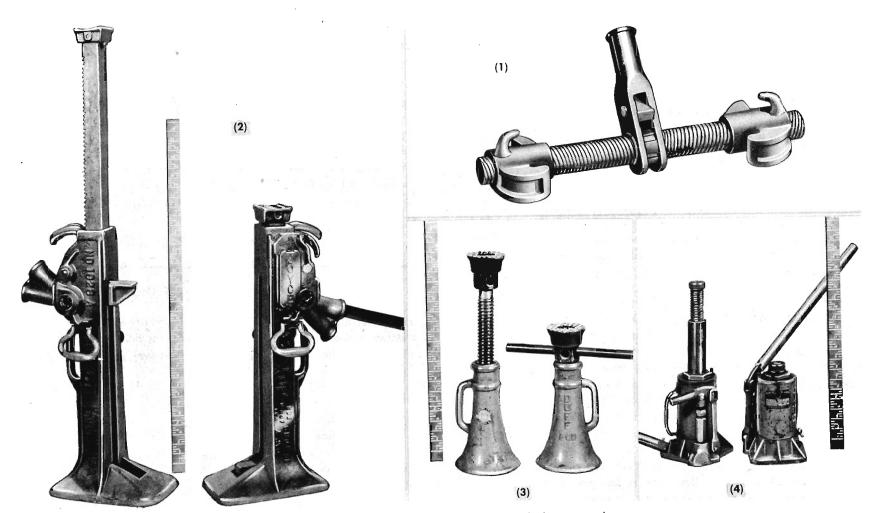


Figure 120. Mechanical jacks used in semipermanent bridge construction.

- (1) Pushing and pulling jack.
- (2) Ratchet lever jack with foot lift.
- (3) Screw jack.
- (4) Hydraulic jack.

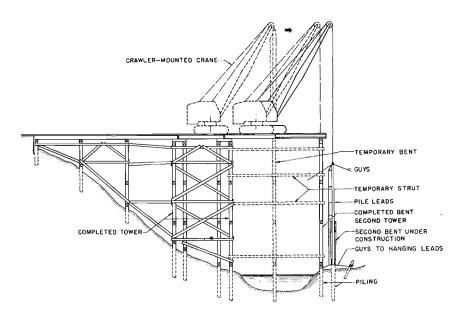


Figure 121. Crawler-mounted crane operating over falsework to drive piling and erect timber tower for long span.

Those supplied with the squad pioneer set have a rated capacity of 12 tons, a rise of at least 51/4 inches, and when closed are 11 inches high. They are large enough for usual construction needs.

Section III. FALSEWORK

187. GENERAL. Falsework is any construction intended for erection use only and then removed or abandoned. It includes temporary towers, bents, or trestles, fixed and floating platforms, staging, runways, and ladders. On major structures, temporary trestles provide quick access to points of construction. Falsework bents provide temporary supports for erection of superstructure spans. Staging is used to provide working platforms. Ladders should be provided for all towers. Safety should be given full consideration in locating and designing falsework. Whenever practicable, falsework should be built of local materials or materials that can be used in the permanent structure after they have served their temporary purpose.

188. FALSEWORK BENTS. Falsework bents can be used to support long spans when they are erected in sections before splicing, or when they are erected before the permanent tower or bent supporting their outer end has been built. Their use makes it possible to drive piling and erect superstructure with light mobile cranes. Falsework bents must be well-built, securely braced or guyed, and must be adequate to support all loads placed on them. Typical applications are shown in figures 121 and 122 and are described in detail in paragraph 209.

189. FALSEWORK TRESTLE. Foundations, towers, and bents of long-span bridges can be built over shallow water or soft ground by first constructing a low trestle to support erection equipment. The trestle is usually built alongside the line of the towers to be erected. (See fig. 122.) It is made as light as equipment and erection loads will permit and only wide enough for the equipment used.

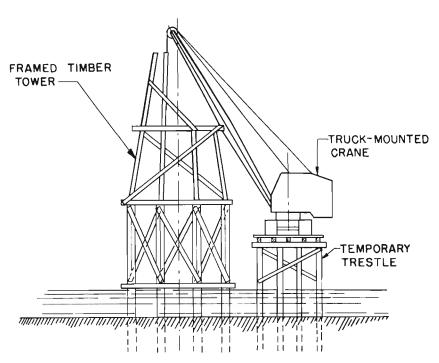


Figure 122. End view of crawler-mounted crane operating over temporary trestle built alongside bridge as a platform from which to drive piling and erect timber towers.

190. PLATFORMS AND SCAFFOLDING. a. Drilling, bolting, and nailing of timber towers is ordinarily done from scaffolds (fig. 123) carried up from story to story as erection advances.

b. Operations such as fitting up, bolting, riveting, and welding require the use of hanging scaffolds called floating platforms. These are easily moved from connection to connection by two men. Two such platforms are usually needed at each connection being made.

CHAPTER 15

STEEL AND TIMBER ERECTION

Section I. STEEL ERECTION

191. GENERAL. a. All parts and subassemblies of parts are prepared for erection in the fabrication yard, where holes for bolts and rivets are drilled and subassemblies are match-marked. Prefabricated parts are erected in the following sequence:

- (1) Raising and entering.
- (2) Plumbing and aligning.
- (3) Fitting up.
- (4) Connecting.

b. Since piles cannot be driven to exact position and alignment, parts for steel pile bents cannot be completely fabricated until in place. Special features of their erection are discussed in paragraph 163.

192. RAISING AND ENTERING. a. Riveted and bolted connections.

(1) Members or subassemblies are raised into position with slings. Slings are

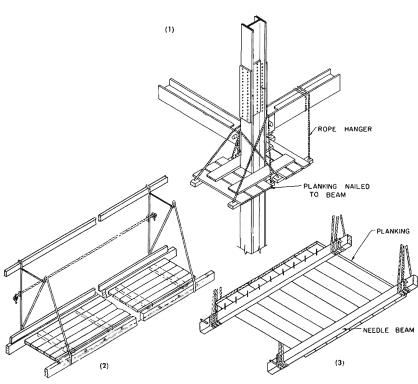


Figure 123. Examples of hanging scaffolds used in bolting and riveting steel bridges.

attached to column sections near the upper end so the column will hang vertically; they are attached to horizontal members, bracing, struts, and girders so they balance. While being raised, all parts must be guided with tag lines by men on the ground.

- (2) As the part is drawn near the connecting point, it is caught by a rigger on the previously erected work. The rigger uses an erection bar as a lever to draw the part into position. When any hole in the part being raised matches its corresponding hole in the previously erected work, the rigger inserts the tapered end of a structural or spud wrench through the holes to hold the connection. The member is then shifted as necessary to bring other holes into line. When the other holes match, driftpins are inserted, erection or fitting-up bolts are added and drawn tight, and slings are released.
- (3) When splices are made with tightly fitting parts, it is occasionally necessary to wedge or jack splice plates apart so the connecting part can enter between splice plates. Connections must not be forced by heavy pounding with a sledge as the metal will be injured, rivets and bolts loosened, and welds broken.
- b. Welded connections. If parts are welded in place, erection bolts are used to hold parts together while they are being welded. Procedure for raising parts and entering connections is similar to that for riveted or bolted connections.
- c. Pin connections. Horizontal struts and diagonal bracing rods of steel towers are connected to the tower columns with pins. (See fig. 124.)
- (1) In connecting horizontal struts and diagonal bracing rods to tower columns, the strut is first lifted into position and rested on erection bolts in the tower column. The connecting pin is then driven, passing in order through: one flange of the tower column, one flange of the strut, the first eye of the bracing rod, the pipe separator, the second eye of the bracing rod, the second

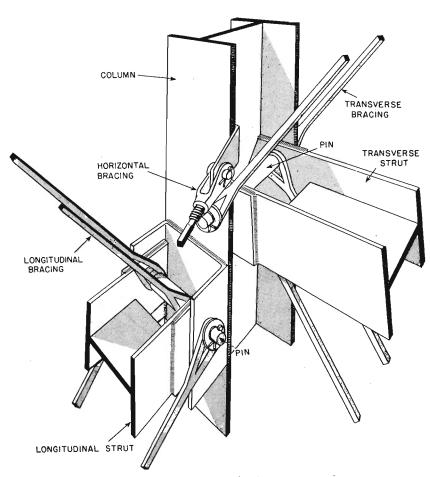


Figure 124. Pin connections of bracing to tower column.

flange of the strut, and the second flange of the column. The two outer diagonals are threaded over the pin, washers are added, and cotter pins are driven through the holes at the ends of the pin.

- (a) If the bracing rods are from the panel below, they are already connected at their lower end to the opposite column and considerable force is required to pull them into position. This force can be supplied with tackle attached to the column and to the turnbuckle which joins the two sections of the bracing rod. The rod is lengthened with the turnbuckle so it can be pulled into position without too much effort.
- (b) If the bracing rods are diagonals for the panel above, they are lowered into position, either singly or together, for insertion of the pin. After the pin is inserted, the free ends of the rods are lashed to the horizontal strut until they are needed to complete the connection above.
- (2) The horizontal diagonal bracing rods are connected by a clevice and pin to a plate attached to the tower column. After the rods are attached, turn-buckles must be carefully tightened to take the sag out of the bracing rods and to square the tower.
- 193. PLUMBING AND ALIGNING. After their erection, towers and bents must be plumbed to bring all parts of the structure into correct position and alignment. If parts have been accurately fabricated, little adjustment will be required.
- a. Riveted and bolied construction. Riveted or bolted towers and bents are not plumbed until all parts have been erected. Plumbing should begin

with the bottom panel and progress upward.

- (1) Erection bolts are first loosened in splices at which correction is required. At joints requiring major correction, it may be necessary to loosen driftpins also. Bolts and driftpins must not be removed, but only loosened enough to permit the joint to rotate.
- (2) Columns are plumbed by adjusting the length of diagonal bracing rods with the turnbuckle in each rod.
- (3) After correction is made, bolts are tightened and driftpins redriven to prevent the joint slipping.
- b. Welded construction. In welded construction, splices in tower columns are made as each section is erected. Bracing connections are usually not welded until all parts of the tower or bent have been erected.
- (1) As each column splice is made, it is carefully aligned to make sure that the column will be straight from bottom to top.
- (2) If after all parts have been erected, it is found that the tower or bent is not plumb, the condition is corrected in the following manner.
- (a) Temporary diagonals of wire rope are run from the base of one column to the top of the adjacent column. A pushing and pulling jack is linked with each of these false diagonals to adjust its length.
 - (b) Connections of the diagonal bracing are loosened.
- (c) The position of the tower or bent is corrected by adjusting the length of the false diagonals.
 - (d) Connections for the bracing are tightened and false diagonals removed.
- 194. FITTING UP. a. Riveted construction. Fitting up of joints to be riveted consists of reaming all mismatched holes, adding erection bolts and driftpins, and pulling parts securely together for riveting. For details see chapter 11. Fitting up is ordinarily done by a two-man crew working on floating scaffolds.
- (1) Driftpins should not be forced into holes by hard driving. Holes that do not match should be reamed.
- (2) Erection bolts should draw parts firmly together. Tight erection bolts are necessary to get good connections with rivets or structural ribbed bolts.
- b. Bolted construction. When connections are made with machine bolts, fitting up is not ordinarily a separate operation. The crew that fits up the joint completes the permanent connection.
- c. Welded construction. No bolts other than those used in raising and entering parts are driven at joints to be welded. Secondary members may be clamped in place, if they support no load during erection and the safety of the welding crew is not jeopardized. Fitting of minor connections made after erection is complete is done by the welder and his assistant.
- 195. CONNECTING. Connections are made by riveting, bolting, or welding, or with pins.
- a. Riveting. Riveted connections are made by a four-man crew in a manner similar to that described in paragraph 123 for riveting in fabrication.
- (1) The heater's forge is set up on a solidly supported platform of 2- by 12-inch planking. It should be erected as near the work as possible and on the same level. If riveting is being done on more than one level, the heater's forge should be placed where it can serve all points most efficiently. Others of the riveting crew, the sticker, bucker, and riveter, work from floating scaffolds hung at the joint being riveted.
 - (2) The riveting crew first makes sure that erection bolts are tight and

that open holes match and are clean. Rivets are driven first in open holes near the center of the joint. Erection bolts and driftpins are removed as riveting progresses outward.

- (3) Connections cannot be riveted in place as readily as on the ground, since movements of the men are restrained by the relative insecurity of the floating scaffold and much time is lost in moving equipment from one scaffold to another. An efficient four-man crew can average about 25 rivets per hour.
- **b.** Bolting. Connections made with machine bolts are completed by the bolting crew. Connections are bolted in the manner described in paragraph 122.
- c. Welding. (1) Welding during erection is used extensively to connect bracing members, diaphragms, and fittings. Splicing main girders by welding after erection is not recommended; the welded splices shown on drawings necessitate overhead welding of important fillet welds unless the stringers can be turned during welding.
- (2) Tower column splices can be welded after erection by highly skilled welders. When column splices are welded, erection proceeds slowly as erection of each main member must await completion of welds connecting previously erected members.
- d. Pin connections. Pin connections are made as parts are lifted into place as described in paragraph 192.
- 196. ADJUSTING OF BRACING. After all parts of the structure are in place and connections made, rod bracing must be adjusted and tightened with the turnbuckles. Intersecting diagonals in any panel should be equally tight. No slack in these diagonals is permitted but they must not be drawn so tight that they are under heavy stress. After adjusting, the turnbuckles are wired or blocked so they will not loosen by vibration.
- 197. PAINTING. Semipermanent bridges are not ordinarily painted. However, in locations where rapid corrosion is expected, painting is advisable if the bridge is to serve more than 1 year.
- a. Painting is preferably done in the yard. It may be done after all steel is erected and connections made but before timber deck is placed. Before painting, steel must be cleaned of all oil, scale, loose rust, and dirt. Standard paints should not be applied on moist surfaces or when the temperature is below 40° F. Crevices between parts should be carefully sealed with paint to exclude moisture.
- **b.** Painting may be with brush or spray gun. Paint should be used as prepared by the manufacturer and should be thinned only if necessary for spraying. Average coverage of 1 gallon of paint on steel surfaces is:

Brush painting	200	to	40	00	
Spray painting	400	to	60	00	
Average labor for applying 1 gallon of paint on steel, not uired to clean surfaces, is:	includ	inį	g ti	me	16
		1	Нои	irs	
Brush painting		3	to	5	
Spray painting		1	to	2	

Section II. TIMBER ERECTION

198. TOWERS AND FRAMED BENTS. a. Members for towers and framed bents are prepared for erection in the framing yard as described in chapter 11.

Square feet

They are erected either singly or as assemblies of several members, usually a complete bent or a story of a bent as the capacity of erection equipment permits. (See figs. 115 and 125.) Match-marking of members provides for their erection in the position for which they were framed.

- (1) Slings are attached to members or subassemblies of members and they are raised to position. Sling attachment points must be carefully chosen in erecting subassemblies so they will not be wracked, pulled apart, or broken when lifted.
- (2) When in position, members or subassemblies are guyed or braced temporarily until permanent bracing can be erected and connections made. Columns are toenailed to sills and caps, and bracing is nailed in place. Holes for bolts are drilled, bolts are driven, and nuts tightened.
- **b.** It is important that columns have full bearing over their entire cross section against caps and sills.
- (1) Thin shims or wedges should not be used to correct errors in framing. Thin pieces of wood warp and split and soon work out of a connection. Steel plates or shims can be used but they must be single pieces wide enough to provide contact over the full face of the column.
- (2) If a column is not cut square or to correct bevel, it can be recut short enough to be filled-in with a hardwood block not less than 4 inches thick. The block must be long enough to extend 1 foot beyond the column on each side and must be securely bolted to the cap.
- c. Splices in bracing members, diagonals, and struts should be carefully made; they should always be bolted. Nailed splices of timbers are inadequate in semipermanent bridges.
- 199. STRINGERS. a. The short span of timber stringers either in pile trestles or in framed bent construction permits placing them by hand (fig. 126) or with a truck- or crawler-mounted crane operating from the deck of previously completed work. The centerline of the bridge is projected onto the cap of the bent as it is completed, and the position of stringers is marked on the cap by measurement from the centerline.

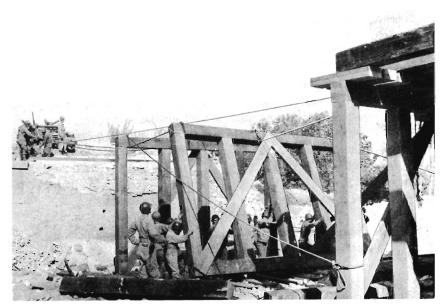


Figure 125. Raising framed bents into position with truck winch.

Bridge details are not standard.

- (1) Interior stringers of highway bridges overlap the cap, and it is not necessary to cut them to exact length. They must be long enough to have full bearing on the cap, however.
- (2) Stringers of railway bridges and the outside stringers of highway bridges are butt-spliced over the cap. It is imperative that these stringers be cut in place to exact length. One end of the stringer is cut square and butted against the stringer of the preceding span; the cut for the opposite end is marked and squared with the stringer in position and the cut made on the line marked
- **b.** Stringers are toenailed to the cap, preferably with one 40d nail on each side of each end of the stringer. Holes are bored for driftbolts and bolts are driven. Scabs splicing stringers over bents are nailed in place, holes are bored and bolts are tightened.



Figure 126. Bringing up timbers to be set in place with erection equipment.

Heavy timbers are being manhandled with peavies.

- 200. RAILWAY DECK. a. Ties for railway deck are landed on the stringers with the erection equipment and are manhandled into position. The preframed tie-spacing timbers insure correct spacing of ties. Ties are fastened to steel stringers with hook bolts (fig. 127) and to timber stringers with drift-bolts through every third tie.
- b. Laying of track is described in FM 5-10.
- 201. HIGHWAY DECK. It is ordinarily more efficient to manhandle deck planks than to place them with erection equipment. On steel stringers, nailers are attached to top flanges of stringers either with welded clips or bolts as shown on sheet 128. Deck planks are nailed directly to timber stringers or to the nailers on steel stringers. About 1-inch space is allowed between all planking, except laminated planking, to allow drainage and easy maintenance. Typical deck-laying procedures are illustrated in figures 128 to 130 inclusive.
- **202.** WALKWAYS AND HANDRAILS. So far as practicable, curbs and handrails are framed before erection. Brackets for walkways are ordinarily assembled in advance.

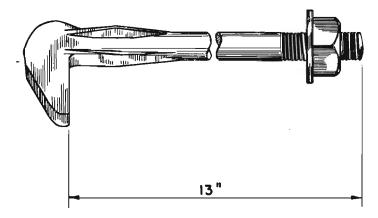


Figure 127. Hook bolt for fastening ties to steel stringers.

Section III. SAFETY RULES

- **203.** HANDLING OF LOADS. a. Before swinging heavy loads, equipment and rigging are both checked under load.
- b. Heavy loads are moved slowly and kept under control at all times. They are moved in only one direction at a time. The critical moment in the lowering of a heavy load is when the load is checked; at that moment the equipment must withstand the inertia of the load as well as its weight.
- c. Loads are guided and prevented from swinging sidewise with tag lines tied to the load and held by one or more men on the ground.
- d. Loads should not be lifted during strong or gusty winds.
- e. Loads should not be swung over the heads of working men.
- **f.** While hoisting equipment is in operation, the operator should not be permitted to perform any other work.
- g. An operator should not be permitted to leave his position at the controls while a load is suspended from a crane or derrick.
- h. Only one person in each crew should give signals to an equipment operator.
- **204.** TACKLE. a. Slings and tackle should be inspected frequently and frayed or worn equipment replaced.
- **b.** Wire rope should be removed from service when 4 percent of the total number of wires in the rope are found broken or when:
- (1) Three broken wires are found in one strand of 6-by-7 wire rope.
- (2) Six broken wires are found in one strand of 6-by-19 wire rope.
- (3) Nine broken wires are found in one strand of 6-by-37 wire rope.
- c. Wire ropes should not be used on sheaves or blocks having a diameter less than those specified in table LXVII.
- d. Wire-rope slings are preferred to chain slings for handling loads.
- **e.** Wood blocking should be placed under slings lifting heavy steel members to prevent slings being cut.
- f. Shackles are preferred to hooks for attaching blocks. Hooks, if used, must be moused.
- g. Blocking or cribbing should always be used to secure necessary height under jacks. Jacks should not be set on a post or strut where they might kick sideways under strain.
- h. Loose lines should not be permitted to hang from the structure or from equipment.



Figure 128. Nailing deck plank to timber stringers. The timber stringers shown are substitute-size shallow stringers.

205. SCAFFOLDS. a. Scaffolding should be of ample strength and secure against slipping or overturning.

- b. Loose boards should not be allowed to project beyond their supports.
- c. Nails should not be used in tension to hold scaffolding or falsework. They should always be driven all the way in.
- d. Scaffold horses should be supported evenly and should be nailed to the platform on which they are supported.
- e. Ladders should be blocked at foot or tied at top to prevent slipping. Scaffolds over 6 feet high should have a guardrail on the back side.

206. INDIVIDUALS. Individuals must:

- a. Stand clear of loads suspended in the air.
- b. Stand away from and out of line with rope lines under heavy strain.
- c. Not ride a load being lifted or lowered into place.
- d. Not stand in the line of movement of a load.
- e. Not stand within the angle formed by a line carried over a block.
- f. Not feel for matching holes with fingers or hand.
- g. Not work beneath other operations where falling tools, bolts, and erection parts are a hazard.
- h. Use all prescribed personal protective equipment, such as goggles and safety belts.

CHAPTER 16

ERECTION METHODS

207. GENERAL. a. The procedures described in this chapter give methods for quick and safe erection under normal conditions of any of the structures described in the manual. Other equally satisfactory procedures can be developed. Combinations of these procedures and adaptations of other procedures may be necessary where site conditions are unusual.

- **b.** Single-span bridges are erected by launching stringers from the shore, following methods described in TM 5–285. Where stringers can be launched from previously completed spans, similar methods are used to erect long spans of multiple-span bridges.
- c. Multiple-span trestle bridges can be erected in the following ways:
- (1) From deck level by advancing construction as successive spans are completed:
- (a) Spans short enough so supports one span away can be reached with erection equipment; no falsework required.
- (b) Spans so long that supports one span away cannot be reached; falsework required for erecting towers.
- (c) Spans so long that equipment cannot lift one stringer at a reach of one-half span; falsework or special rig required for erection of spans.
- (2) From ground level:
- (a) Height of bridge within lifting height of equipment; no special erection equipment required.
 - (b) Height of bridge beyond lifting height of equipment.
 - 1. Bridge carried on steel towers; gin poles required.
 - 2. Bridge carried on timber towers; guy derrick required.

- (2) The first pile bent is constructed with the crane on the abutment.
- (3) Stringers for the first span are set in place on the abutment and the first bent.
- (4) Deck planks, or ties for railway bridges, are laid. Stringers on railway spans are spread apart and cross ties staggered to obtain a temporary deck wide enough for the crane.
- (5) The crane is moved out over the deck to the first bent. The second bent is driven and the second span erected. This procedure is repeated until the far abutment is reached.
- (6) As the crane is moved off each span, stringers are set in final position, the deck is nailed, tread planks and curbs are placed, and walkway and handrails are constructed to complete the span.
- b. Spans on pile piers. Procedure for erecting bridges with short steel-stringer spans on timber pile piers is similar to that for bridges on pile bents. It is necessary to reach and construct only the nearest bent of the forward pile pier before an intervening span can be placed temporarily and the crane moved out on the structure.
- (1) The second bent of the pile pier is constructed and the pile pier completed.

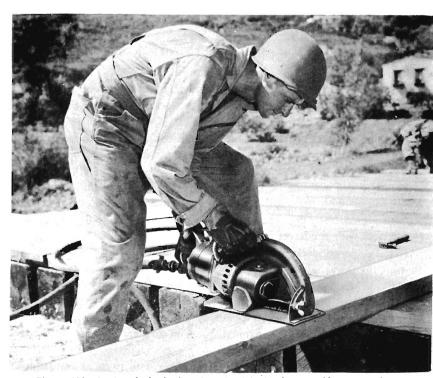


Figure 129. Cutting deck plank to length with circular portable pneumatic saw.

- 208. ERECTION FROM BRIDGE DECK WITHOUT FALSEWORK. Bridges built of a succession of relatively short spans can be erected from deck level without falsework. Erection equipment preferred is a 3/4-cubic-yard truckmounted crane.
- a. Spans supported on pile bents (fig. 92). Erection of short spans on pile bents proceeds in the following manner.
- (1) Materials and fabricated parts from the fabricating yard are delivered to the bridge within reach of handling equipment.



Figure 130. Drilling curb with pneumatic wood borer.

- (2) The stringers can be set in final position on corbels after the crane has moved forward off the span.
- c. Spans on framed timber towers. Foundations for framed towers are usually constructed in advance. Erection of timber towers proceeds as follows:
- (1) Sills on foundation, although framed with the bents, are set separately and anchored to piles with scabs or driftbolts or to footings with anchor bolts.
- (2) The first tower bent is delivered to the crane assembled. (It may be assembled on the ground immediately behind the crane.) The crane then places the bent over the previously placed sill. (See fig. 111.) The bent is carefully guided with tag lines. Bents more than one story high are set one story at a time.
- (3) The bent is braced with final struts or temporary bracing or is guyed, and anchor bolts are tightened.
 - (4) Stringers are set and deck is laid.
- (5) The crane is moved out on the structure. The remaining bents of the tower are erected and longitudinal tower bracing is installed.
- (6) Guys and temporary bracing holding the first bents are removed.
- (7) Stringers of the tower span are set in place and deck is laid. The crane is then ready to move forward.
- (8) When towers are carried on timber piles, piles are usually driven while erection of superstructure proceeds. If the crane is used to drive piles and erect the bridge, pile hammer and leads are set aside so the full capacity of the crane is available for handling tower bents and stringers while piles are being cut off and capped.
- 209. ERECTION FROM BRIDGE DECK USING FALSEWORK. a. Falsework is used to advantage in erecting moderately high bridges over water or ground too soft to support erection equipment. It is not usually justified for structures over 40 feet high. Falsework bents can be pile bents or well-braced timber bents. Allowance should be made for 1 to 2 feet of blocking between caps and bottom of stringers when in position.
- b. The following procedure is outlined for erecting a 90-foot highway span having its outer end supported on a timber tower. (See fig. 131.) The same procedure can be used to erect other structures. Stringers are erected in sections and are spliced in place.
- (1) The crane moves into position at the end of the gap, and the first falsework bent is constructed approximately 20 feet beyond the end bent of the completed span.
- (2) The first sections of all stringers are set in place with their outer ends resting on the falsework bent. These stringer sections are 25 feet long.
- (3) To prevent stringers overturning they are blocked over the falsework bent.
- (4) Temporary decking is laid and the crane moves out on the span to but not beyond the falsework bent. A second bent is constructed approximately 20 feet beyond the first.
- (5) The middle section of each stringer except the center stringer is set in place and held by the crane while it is spliced to the previously erected section. These sections are 40 feet long. The splices are bolted and pinned but final connections are not made. After the splices are made, the stringers are seated on the outer falsework bent, carefully leveled, and blocked for lateral support.
 - (6) Temporary decking is laid and the crane moves out to the second false-

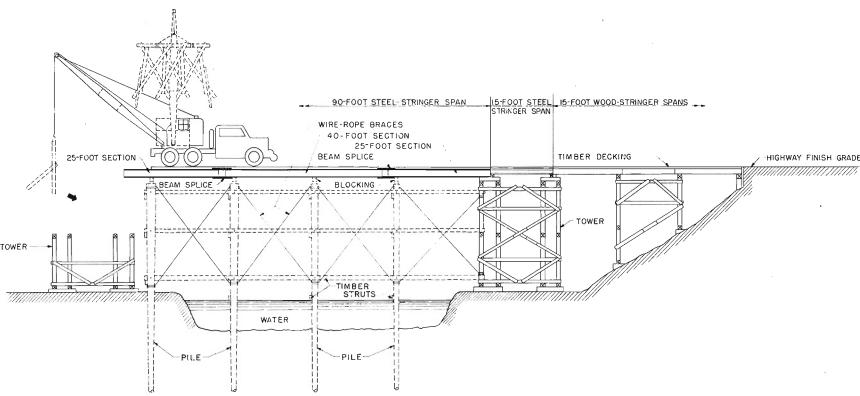


Figure 131. Ninety-foot steel-stringer span on timber towers erected on falsework.

Crane is shown erecting far tower from span supported on falsework.

work bent. A third bent is placed approximately 20 feet beyond the second to support the outer end of the middle stringer section. Piles for this falsework bent must be driven between the steel stringers.

- (7) The stringers are wedged up for even support and temporary decking is laid out to the third bent. The crane moves out and a fourth bent is erected approximately 20 feet beyond the third.
- (8) The end sections of the girders are lifted into place, spliced to the center section with bolts and pins, and are seated on the fourth bent. These sections are 25 feet long. The stringers must be wedged up slightly so as not to interfere with the tower construction.
- (9) Temporary decking is laid on the end section, and the crane moves out to erect the tower which supports the ends of the stringers.
- (10) When the tower is completed and stringers lowered to final position the crane moves off the span and the temporary decking is removed.
- (11) Stringers are jacked at points of temporary bearing to correct alignment in both vertical and horizontal direction and are then set on their end bearing plates.
- (12) Permanent girder splices are made either with rivets or with structural ribbed bolts. Bracing and diaphragms are installed.
- (13) Blocking over the falsework bents is removed, leaving the stringers supported only on end bearings. Falsework bents are dismantled.
- (14) Bridge floor, curb, and handrail are added to complete the span.

210. ERECTION FROM GROUND WITH CRANES. a. Where ground and site conditions permit, long-span bridges of moderate height can be erected more easily from ground level or from rafts. A 3/4-cubic-yard crawler-mounted crane is the equipment preferred. It is more maneuverable than truck-

mounted cranes and can be operated over rougher and softer ground. Erection of superstructure from the ground proceeds in the following manner:

- (1) The first tower is erected (fig. 132), the tower plumbed, and permanent connections are made between members. The crane also raises stringers of the tower span to place.
- (2) If two cranes are not available, a gin pole is erected at the abutment in position to raise one end of one of the outside stringers. The crane is moved into position to handle the other end of the same stringer, delivered below

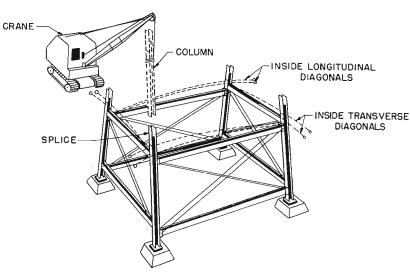


Figure 132. Crawler-mounted crane erecting steel tower from ground.

the span. Lines are attached from the gin pole and from the crane, and the stringer is raised to position.

Caution: The crane must be on firm, level footing when stringers are raised. Where necessary, the ground should be leveled and mats laid.

- (3) The gin pole and crane are moved laterally and successive stringers are raised until all stringers of the span are in place.
- (4) Diaphragms and bracing are erected and connections made. Deck is laid to the far end of the tower span.
- (5) The gin pole is moved to the completed tower for erection of the second span, while the crane places the next tower.
- 211. ERECTING HIGH STEEL TOWERS WITH STEEL GIN POLES. High steel towers cannot be erected with standard truck- or crawler-mounted cranes. Special equipment must be used. Suggested procedure for erecting towers is illustrated in figure 133. Use of the same equipment parts in launching spans is shown in figures 134 and 135.
- **a.** Equipment. The erecting equipment consists of four gin poles, one for each column of the tower.
- (1) Gin poles are made of the 10-inch 42-pound beam section used for tower struts. Accessories and fittings, except tackle and hoists, can be made in the field. Details of gin poles and fittings are shown on sheets 228 and 229.
- (2) Hoists for raising members are described in chapter 14. Single-drum pneumatic hoists are preferred, one for each of the four gin poles. Hand winches are used for holdback lines and can be used for hoisting lines if pneumatic hoists are not available.
- (3) Holes for bolts connecting gin poles to columns are shown on column details.
- **b.** Tower erection procedure. Construction of a two-story tower is described below. Similar procedure is followed in erecting higher towers.
- (1) The gin poles are set on blocking next to the column foundations. (See fig. 133 (1).) The bottom section of each tower column is set on its foundation. Anchor-bolt nuts are run on and tightened. The anchor bolts hold the columns erect while bracing is added.
- (2) Transverse tower bracing of the bottom story is erected. (See fig. 133 (2)): first the bottom strut, then the diagonal rod-bracing with loops between the flanges of struts (inside diagonals), then the top strut and inside diagonal of the second story. Bracing connections are made with pins as described in chapter 14. Struts must be raised at an angle to enter between flanges of tower columns. The high end is rested on a temporary 14-inch bolt immediately below its connection; the other end is raised and the temporary bolt under that end is inserted.
- (3) Longitudinal bracing of the bottom story is erected as shown in figures 133 (3) and 133 (4): first the bottom strut, then the inside diagonal of the bottom story, then the top strut and the inside diagonals of the second story, and finally the outside diagonal rod bracing of the bottom story.
- (4) Gin poles are raised with tackle to new positions for erecting the second story as shown in figure 133 (5) and sheet 228. Above ground, the gin pole is held as follows:
- (a) Supporting brackets are pinned to the base of the gin pole and are bolted to the column at each level.
- (b) Temporary straps are attached to each column to guide the gin poles while being raised.
- (c) Tackle is attached to the top of the tower and to the bottom of the gin

pole, and the gin pole is lifted into position.

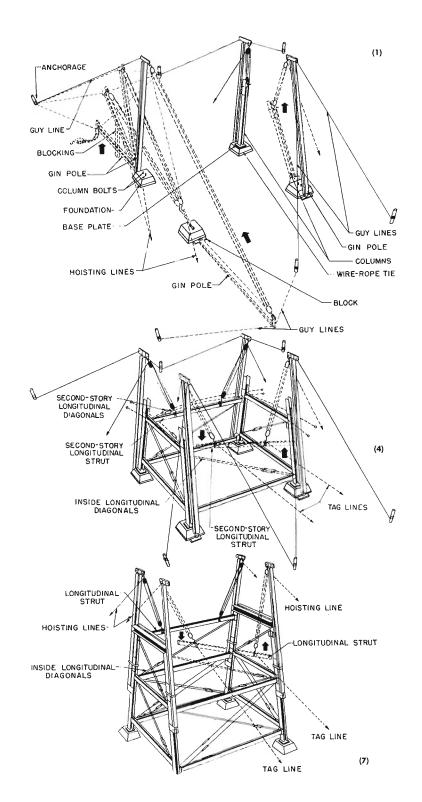
- (5) The second section of each tower column is erected and splices are bolted and pinned.
- (6) Column caps are erected and are connected with bolts and driftpins. Gin poles must be leaned away from tower columns during erection of caps. (See fig. 133 (6).) Inside transverse diagonals of the second story are raised between flanges of the column sections before the column cap is connected but are not connected at the top until after the cap is connected.
- (7) Longitudinal struts and bracing are erected and connected. (See fig. 133 (7).) The inside diagonals are leaned against the column below the connection; the top struts are lifted into place and they and the inside diagonals are connected; the outside diagonals are raised and connected last.
- (8) Stringers of the tower span are erected as shown in figure 133 (8), using all four hoist lines on one stringer.
- (9) After all stringers are in place, horizontal tower bracing is erected and the tower is squared and plumbed. Riveting of column splices or bolting with structural ribbed bolts can then proceed.
- (10) Gin poles are lowered to the ground with tackle attached near the top of the tower column and to the bottom of the gin pole. (See fig. 133 (9).)
- 212. ERECTING LONG SPANS WITH STEEL OUTRIGGERS. Equipment for launching the stringers consists of the four gin poles used in erecting the towers and the outrigger accessories detailed on sheets 230 and 231. Assembly of the gin poles and outriggers is shown on sheet 228.
- a. Outriggers are assembled on the towers at center line of bridge (see fig. 134) as follows:
- (1) Outrigger accessories and supporting beams are attached to the gin poles to make the two outrigger assemblies.
- (2) Rods to support outriggers are connected at their upper ends to the tower columns. Their lower ends are connected to the outrigger support beams later after the beams have been raised.
- (3) Tackle is attached to the top of each tower column and to the outriggers. Assemblies are raised, supporting rods connected, and outriggers tied back to towers.
- (4) Tackle is attached to outer ends of outriggers and outriggers are pivoted forward to position.
- b. Stringers are delivered to the end of the completed spans and are placed on pipe rollers for launching. Beveled plates are welded to stringer bottom flanges at splices (fig. 135) so stringers will be lifted at outriggèr rollers and will clear splice plates and rivet heads. Outside stringers are launched first.

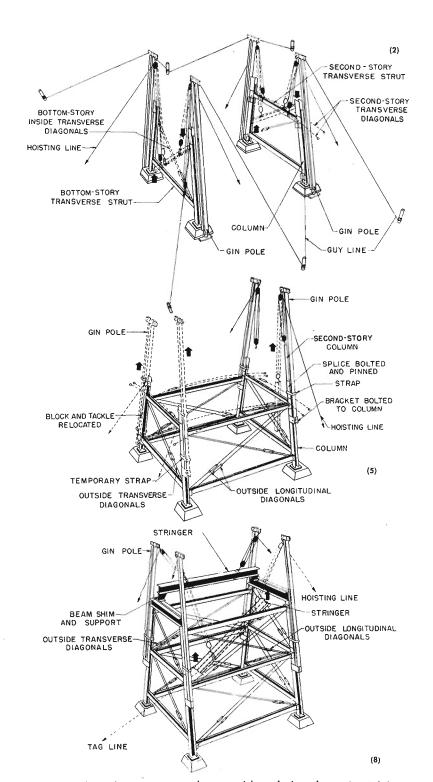
Cantion: Long beams have little lateral stiffness; every care must be taken to prevent their twisting or overturning.

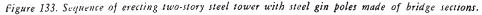
- c. Tackle is attached from the far tower to the stringer and the stringer is pulled across the gap. (See fig. 135 (2).) As the forward end of the stringer reaches each outrigger, the height of that outrigger is adjusted with tackle so it supports the end of the stringer.
- d. When the stringer is centered over the span, it is lowered onto the column cap (fig. 135 (3)) by slacking both outriggers together while keeping the stringer carefully centered and securely held with tackle at each end. Stringers are seated on timber skids on top of the tower and are braced to prevent their overturning. (See fig. 136.) When a stringer is seated, outriggers are lowered far enough to clear the stringer.

Note. Bottom member of timber skid must be a continuous piece dapped over bearing plates and rivet heads.

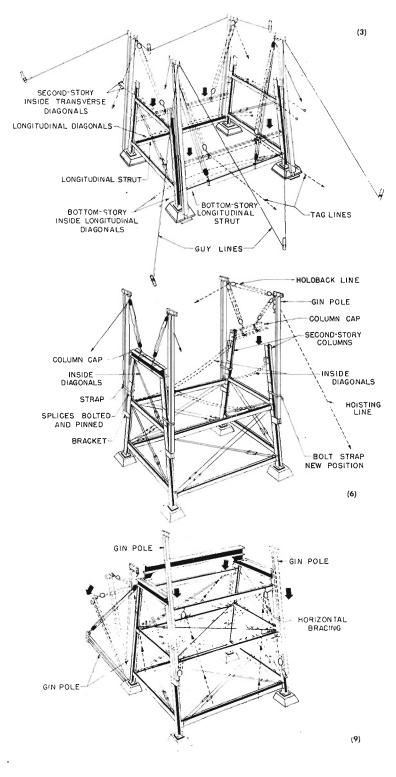
- e. The stringer is jacked laterally to position as shown in figure 136. Jacking must be carefully controlled so stringers are moved slowly without jerking. Sliding surfaces of timber skid should be smooth and well-oiled.
- f. When all stringers of the span have been launched, seated on blocking, and jacked to position, outriggers are lowered and removed from the towers.
- g. Diaphragms and bracing between stringers are installed, and sections of the timber skid are then sawed out to permit seating jacks on the tower cap beam under end diaphragms. (See fig. 137.) The span is raised slightly on jacks, blocking is removed, and the span seated in its final position.
- 213. ERECTING HIGH TIMBER TOWERS. Special equipment must be used to erect high timber towers beyond the lifting height of standard equipment. Suggested procedure for erecting these structures is shown in figures 138 and 139.
- a. Equipment. The guy derrick, detailed on sheets 232 to 234 inclusive, is used. Mast, boom, and sill of the derrick are of bridge-timber sizes.
- (1) All derrick parts can be made in the field; tackle and winches are class IV or organic equipment.
- (2) Hand winches (stock number 66–9450.050–000) can be used for hoisting on load lines and boom lines.
- (3) Swing of the boom is controlled with tackle attached to the boom and to the tower bracing or columns. The derrick rests on timbers laid longitudinally on the tower sills or caps.
- b. Tower erection. Procedure for erecting a two-story tower is given below. Procedure for erecting a higher tower is similar.
 - (1) Sills of all bents are laid and bolted to foundations.
- (2) The derrick (fig. 139 (1)) is set up. Guys to the mast are anchored to extreme corners of the tower. The derrick sill is anchored to prevent the foot of the derrick sliding.
- (3) Tower bents are delivered by units close to the tower. Each unit includes posts, cap, and transverse bracing for one story. Bracing is spread away from the base of the posts slightly so it will not interfere with sills when set in place. If necessary, temporary filler blocks are put on bolts connecting bracing at top of posts.
- (4) The first-story section of one end bent is lifted and set in place. (See fig. 138 (1).) Longitudinal bracing members are connected temporarily to hold the section upright.
- (5) Forward guys of the derrick are moved one at a time, so they do not interfere with the inside bent to be set next.
- (6) The first-story section of the next bent is lifted and set on its sill. Longitudinal bracing connecting the two bents is bolted in place. (See fig. 138 (2).)
- (7) The derrick boom is swung through 180° to set the bents at the opposite end of the tower. As the boom is swung, the guy line in its path must be released, thrown over the boom, and again connected near the corner of the tower. Never release more than one guy at a time.
- (8) First-story sections of the remaining two bents are erected, the end bent first then the inner bent (fig. 138 (3)) as described above.
- (9) Longitudinal tower bracing of the first story is completed.
- (10) The derrick is raised as described in subparagraph 213c onto the caps of the first story.
- (11) Second-story sections of each bent are raised in the same sequence as the first story (figs. 138 (4), 138 (5), and 138 (6)).







- (1) Setting gin poles on ground to erect first story; tower columns being erected.
- (2) Transverse struts raised to position while diagonal bracing rods connecting between flanges (inside diagonals) are tied in position. It is difficult to enter diagonals into the corner between the column and the strut after the strut is in place.
- (3) Erecting bottom longitudinal struts and inside diagonals of first story.
- (4) Erecting upper longitudinal struts of first story. Inside diagonal braces of second story are connected at lower ends.
- (5) First story. Gin poles being raised to position for erecting second story. View shows second-story inside bracing connected at lower ends.
- (6) Second story. Lower columns in place. Column caps being erected.



- (7) Erecting longitudinal strut with inside diagonal bracing tied into position at upper end. The pin is threaded through the holes in the strut and the loops of inside diagonals at one time.
- (8) Tower erected. Setting tower stringer in place.
- (9) Gin poles lowered to ground after erecting tower. Only one tower stringer is shown.

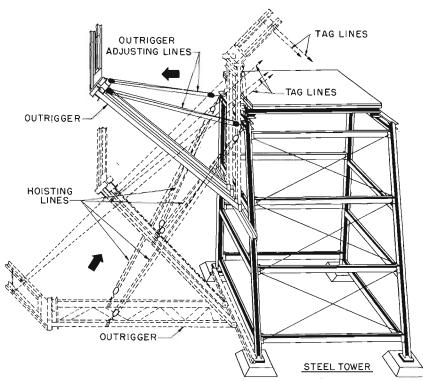


Figure 134. Two gin poles connected with bracing, rollers, and guide frame serve as outriggers used to launch long steel stringers from bridge deck. Successive steps in raising outriggers are shown.

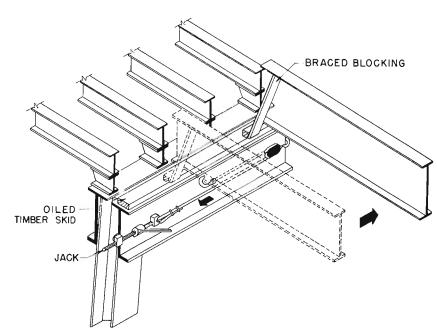


Figure 136. Jacking stringer into position using timber skid, tackle, and pushing-and-pulling jack.

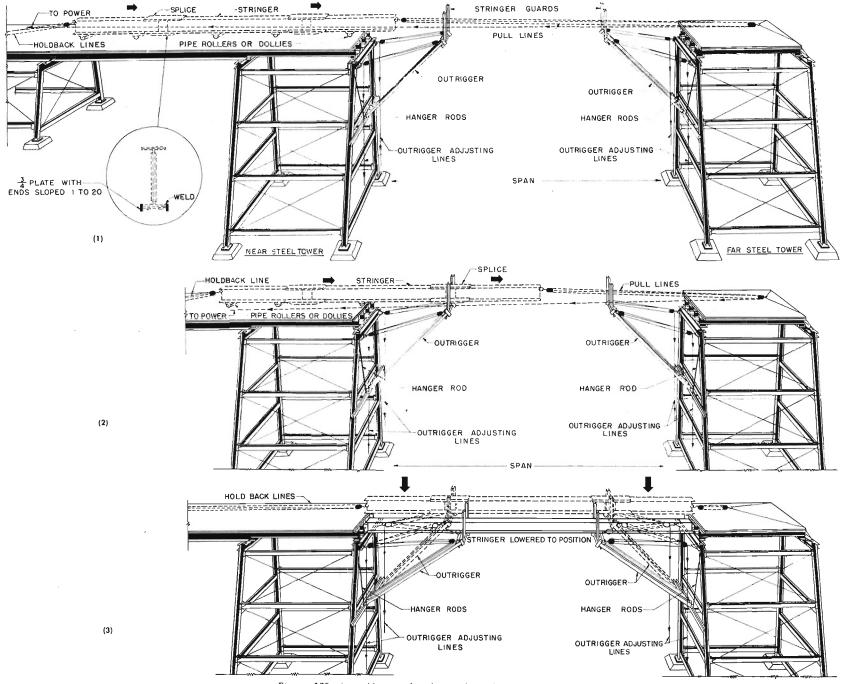


Figure 135. Launching steel stringers from bridge deck with outriggers.

- (1) Outriggers and stringer in position for launching; tackle attached, stringer on pipe rollers.
- (2) Stringer supported on outrigger being drawn across gap.
- (3) Launching completed, stringer lowered to column cap beam by paying out outrigger adjusting lines.

- (12) Longitudinal bracing is raised and connected. Corbels are set in place, drilled, and bolted.
- (13) Stringers are raised from ground over the side of the tower and swung between the derrick guys into position. Stringers on one side of the derrick are raised first, the derrick boom is swung around, and then the stringers on the other side are set. (See fig. 138 (7).)
- c. Elevating derrick to higher level. Assembly of the guy derrick is shown in figure 139 (1). It is raised from one level to the next in the following manner.
- (1) Tackle guys are attached to the boom point. The boom is raised as close to the mast as possible, and guys to the boom point are secured.
- (2) The boom tackle is released from the point of the boom and is lashed near its base. (See fig. 139 (2).)
- (3) Using the mast as a gin pole, the boom is lowered and seated on timbers either on the ground or at the base of the derrick. (See fig. 139 (3).)
- (4) The boom tackle is released from the boom and the hoisting tackle is connected to the mast with lashing far enough down for a 13-foot lift. (See fig. 139 (4).)
- (5) Guys on the mast are slacked and with the boom as a gin pole the mast and sill are raised to the second level and seated on its timbering. (See figs. 139 (5) and 139 (6).)
- (6) The hoisting tackle is released from the mast and the boom tackle is lashed to the boom near its basc. (See fig. 139 (7).)
- (7) The boom is raised with the mast as a gin pole and connected at the higher level. (See fig. 139 (8).) Guys guide the boom as it is raised.
- (8) Tackle is again connected as shown in figure 139 (1) and guys to the boom point are released.
- 214. LAUNCHING LONG SPANS WITH GIN POLES. Stringers are launched from the deck of completed spans as shown in figure 140, using gin

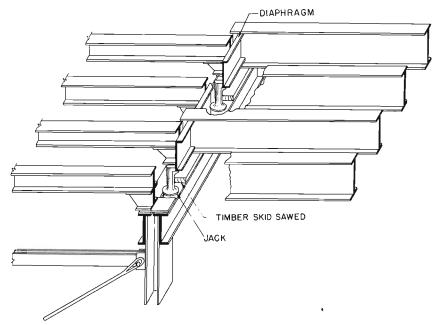


Figure 137. Lowering stringers to final position on bearings. Two or more stringers are lowered as a unit after diaphragms have been connected. Timber skids are sawed free from jacks.

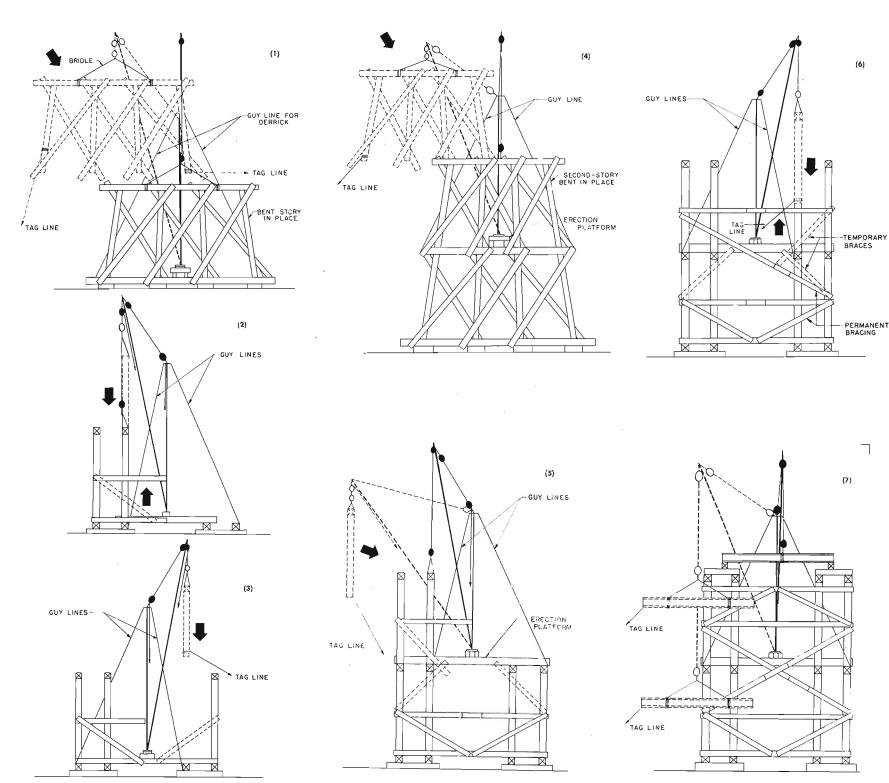


Figure 138. Sequence of erecting two-story timber tower with guy derrick made of bridge timbers

- (1) Guy derrick placed on erection platform of timbers between tower bents. First-story outside bent being erected.
- (2) First-story inside bent being erected. Temporary longitudinal bracing placed.
- (3) Last first-story bent being lifted into place. Guv lines have been shifted to clear he bent.
- (4) Derrick raised and erecting second-story end bent.
- (5) Guy lines shifted for setting inside bent. Temporary bracing for second story; permanent longitudinal bracing in first story.
- (6) Erection proceeds from the outside toward the center of the tower at each level.
- (7) Tower erected. Derrick placing steel stringers of tower span.

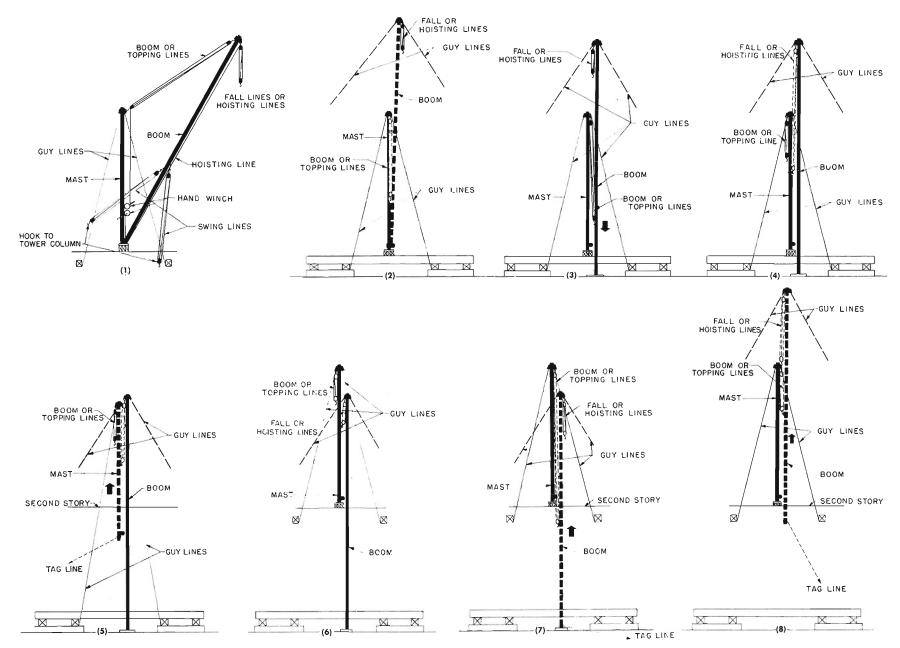


Figure 139. Steps in raising guy derrick to higher level for erection of multi-story timber towers.

- (1) Guy derrick in working position.
- (2) Boom raised to mast before shifting beom line. Temporary boom from mast step.
- (3) Boom lowered and standing on timber platform.
- (4) Boom guyed as gin pole to raise mast.
- (5) Mast and sill raised by boom to higher level.
- (6) Mast and sill seated and guyed at higher level. Sill must be securely anchored to prevent its sliding.
- (7) Mast acting as gin pole to raise boom.
- (8) Guyed mast and boom line used to raise boom to mast step.

poles. TM 5–285 contains detailed information on this launching procedure. The steel gin poles or the mast and boom used in erecting towers can be rigged as gin poles for this launching.

- a. The shortest gin pole or the mast of the derrick is rigged on the far tower and the longest gin pole or boom of the derrick is set up on the near tower. Both are guyed to anchorages at ground level.
- b. A fully assembled stringer is set on pipe rollers or on dollies on the bridge deck. A timber frame to guide the stringer and hold it upright during launching (fig. 141) is made and bolted at the end of the completed spans.
- c. Tackle is attached from each gin pole to the forward end of the stringer with wire-rope lashing. A snubbing line is attached to the rear end of the stringer.
- (1) Tackle must be attached so the beam has no tendency to twist or overturn.
- (2) Each tackle must be strong enough to support the full weight of the stringer.
- d. The stringer is launched across the gap by hauling in on the far tackle while paying out the near tackle. The snubbing line should be only tight enough to control the rate of movement. The tackle must be controlled during launching so the stringer bears on the forward roller at all times.
- e. When the forward end of the stringer nears the far support, tackle from the gin pole on the near tower is connected with lashing to the near end of the stringer, the stringer is centered over the gap, and is lowered onto its bearings. The stringer is blocked in place.
- f. Gin poles are shifted and succeeding stringers are launched in the same manner. Diaphragms are connected as soon as two stringers are seated. When all stringers of the span are in place, deck is laid to complete the span.

PART THREE

MAINTENANCE AND REPAIR

CHAPTER 17

MAINTENANCE AND REPAIR

- 215. GENERAL. General information on maintenance and repair of bridges is given in FM 5-10.
- a. Inspection. Maintenance and repair required on these bridges are determined by periodic inspection. The frequency of inspections depends on:
 - (1) Importance of bridge.
 - (2) General condition and workmanship.
 - (3) Character and amount of traffic.
- (4) Type of structure (timber or steel).

Ordinarily, a general monthly inspection is made by an officer experienced in bridge maintenance. Additional inspections should be made after each high water or whenever the bridge has been damaged in any way.

b. Repairs. Continual, properly directed maintenance will largely eliminate the need for extensive repairs and will keep the bridge open to traffic at all times.

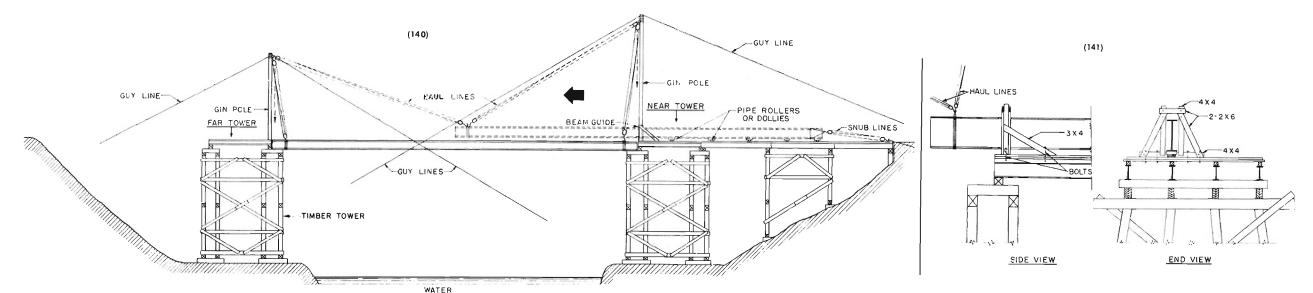


Figure 140. Launching steel stringers with gin poles. Gin poles on timber towers must be guyed to ground.

- 216. BRIDGE FLOOR. a. Highway bridges. (1) Nails in floor planks should be redriven as they work loose. Damaged or worn longitudinal tread plank forming the wearing surface should be replaced when 10 to 15% of the original thickness has worn away. Splintering and rapid wear can be prevented by a tar or asphalt coating over which coarse sand or fine gravel is spread.
- (2) Curbs and handrails should be checked regularly for loose connections. Replacement is usually necessary only when members have been damaged by accidents.
- b. Railway bridges. Burned or damaged ties should be replaced promptly. Rail fastenings, hook bolts, and tie-spacer connections should be kept tight.
- 217. BEARINGS. a. Wherever steel work rests on masonry or timber supports its tendency to rust increases. As dirt and debris at these points accelerates rusting, these areas should be kept clean.
- **b.** Expansion bearings must be clean to function properly. Slotted holes must be free of dirt and rust.
- c. Any obstruction to free movement of stringers at expansion joints must be removed promptly.
- 218. CONNECTIONS. a. Timber. Unless thoroughly seasoned, timber shrinks during the early life of the structure. Frequent checks should be made and all bolted and nailed connections tightened when loose.
- b. Steel. Properly made riveted or welded joints require no maintenance. Structural ribbed bolts have little tendency to loosen, but they should be examined and nuts drawn tight if loose. Rivets and bolts are tested for looseness by striking with a light hammer as explained in paragraph 123.
- **219. TIMBER MEMBERS.** a. Failure of structural timbers may be caused by decay, rot, excessive load, structural defect, fire, or explosives.
- **b.** Untreated timbers in contact with the ground often deteriorate rapidly. Timbers continuously below water do not decay but may be attacked by marine borers. In some localities, insects may cause serious damage to timber structures. Piling and timbers in footings and abutment bulkheads should be checked carefully, and damaged timbers should be replaced. Damage by insects can be

arrested or retarded by painting with creosote. Piling may be repaired by splicing in new sections above the ground line. (See par. 144.)

- 220. STEEL MEMBERS. a. Rusting. (1) Rusting is rarely rapid enough to require special attention on semipermanent bridges. However in locations subject to salt-water spray and in moist, warm climates, serious rusting of steel parts in contact with timber members may occur. Dirt and trash should not be permitted to accumulate in pockets and crevices between members since it retains moisture and promotes rusting.
- (2) Rust flakes are five to eight times as thick as the metal from which they are formed. Loose rust is not serious; only deep pitting needs to be checked. Areas subject to severe rusting should be painted or coated with tar or asphalt. For painting of steel bridges, see paragraph 197.
- b. Bracing. Turnbuckles permit adjusting the rod diagonals of framed steel towers. Shake the rods to see that none are loose and that none are under undue tension. Rods should be tight but not heavily stressed. Uniform adjustment should be maintained.
- c. Replacement. Replacement of steel members in semipermanent bridges is usually necessary only when they have been damaged by accident or explosives.
- 221. FOUNDATIONS. a. Scour. Foundations should be inspected after each high water. Soundings should be made around bridge foundations in water if there is any indication of scour.
- (1) Where scour has occurred, the original contour of the stream bed should be restored by filling with stone, and the foundation should be protected with riprap.
- (2) Where spread footings have been partly undermined, concrete or tightly packed stone should be used to restore the original bearing area. The surrounding area must be thoroughly protected with riprap so the new supporting material will remain in place.
- (3) If repair must be made in deep water, a cofferdam of either type shown in appendix II, figures 152 or 154, can be used.

Figure 141. Timber frame used to guide stringer during launching. The beam should be launched directly over a stringer of the completed bridge.

- **b.** Settlement. Foundation settlement can be caused by overload or by softening or shrinkage of the foundation material.
- (1) Minor settlement can be corrected by jacking up the supported structure and inserting shims between it and the settled foundations. Shims should be placed between stringers and pile caps of pile bents and piers, and between bearing plates and pedestals. Steel shims should be used under steel members and steel or hardwood shims under timber members.
- (2) Wherever possible, conditions causing settlement should be corrected before major damage occurs and it becomes necessary to replace the foundation.
- (a) Areas close to spread footings on earth should be graded so they drain properly.
- (b) If foundations are threatened by scour or caving of stream banks, banks should be protected with timber and brush mats, riprap, dumped stone, or pile and timber retaining walls. (See par. 225, FM 5-10.)
- c. Drift. Drift should not be allowed to collect against bridge supports. Masses of drift may destroy the bridge during flood; during low stream stages they are a fire hazard. When large amounts of drift are carried by the stream, constant attention may be required to keep it from massing against supports. Small pieces of drift can be cleared with poles and hooks; large pieces can be pulled clear by a crane working from the bank or from the bridge deck.
- d. Ice. Moving sheet ice and ice jams against the bridge must be broken, by blasting when necessary. Piling may be worn and cut by thin floating ice. Where such damage becomes severe, piles can be protected with sheet metal bands.
- **222.** APPROACHES. Approaches at abutments should be well maintained. Settlement of the approaches back of the abutments should be corrected immediately.
- a. Highway bridges. Grade line of unpaved approaches of highway bridges should be about 1 inch above the grade line of the bridge. The grade line of paved approaches should be the same as that of the bridge.
- **b.** Railway bridges. To prevent a dip in the track, ballast should be added to track back of bridge abutments as settlement occurs.

PART FOUR

DESIGNS

CHAPTER 18

DESIGNS

223. STANDARD DESIGNS. a. Arrangement of drawings.

- (1) The design drawings are arranged in the following groups:
- Group 1: Sheets 1-43, Highway, class 50, single-lane.
- Group 2: Sheets 44-90, Highway, class 50, double-lane.
- Group 3: Sheets 91-127, Highway, class 25, double-lane.
- Group 4: Sheets 128-155, Drawing common to all highway bridges.
- Group 5: Sheets 156-225, Railway, E-45.
- Group 6: Sheets 226-227, Alternative welded details for steel towers.
- Group 7: Sheets 228-234, Special erection equipment.
- Group 8: Sheets 235-245, Adaptations to prefabricated standard bridges.
- (2) The design drawings for each unit of construction make up a drawing set. The drawings comprising each set are listed on:
 - Sheet 1, Highway, class 50, single-lane.
 - Sheet 44, Highway, class 50, double-lane.
 - Sheet 91, Highway, class 25, double-lane.
 - Sheet 156, Railway, E-45.

For example, sheets required for a framed steel tower for a railway bridge are listed on sheet 156, set RR-5.

- (3) In each set there is a basic drawing showing assembled views. Companion sheets show fabrication details, bills of materials, symbols used on drawings and general notes. The general note sheet 154 and symbol sheet 155 are included in all drawing sets.
- (4) All pieces of each unit are given mark numbers. The mark number distinguishes each piece as to size, length, and fabrication details. Mark numbers carrying designation R (right) and L (left) have the same details but in reverse positions. Where pieces are marked with "X end," the piece must be set with the "X end" in position as shown on the assembly plan. Stock numbers are shown for requisitioning from supply depots. Complete stock numbers are given where full length pieces are required. For short pieces or random-length pieces the subdecimal of the stock number indicating length has been omitted.
- (5) Pieces such as floor planking and handrails are specified as to length in bill of materials. Random lengths may be used as indicated on the drawings and for short pieces.

- (6) Span lengths are fixed by the stringer lengths which remain the same for end, intermediate, and single spans.
- (a) Timber spans. No space is left between ends of stringers on intermediate supports nor between stringers and end dam on abutments. Stringers in highway spans have lapped ends on intermediate supports; stringers on railway spans have butted ends. Timber span dimensions are measured as follows:

	At intermediate	At abutment,
	support, to:	to:
Highway span, 11-, 13-, 15-foot	Center of cap	Center of cap
Railway span, 12-, 14-, 16-foot	Center of cap	Face of end dam

- (b) Steel spans. Designs are prepared for:
- Highway spans, 15-foot length and 20- to 90-foot length by even 10-foot intervals.

Railway spans, 15- to 50-foot length by even 5-foot intervals; also 30-foot length of two continuous 15-foot spans with center support.

The over-all length of steel stringers is 1½ inches less than the designated span. On intermediate supports, the 1½-inch space allows for expansion of the stringers and variation in position of the support. On abutments, 2-inch clearance is figured between ends of stringers and face of bulkhead posts, except railway pile bent abutments for 25-foot maximum span and timber grillage abutments for 15-foot span on which the stringers extend 1¼ and 2¼ inches respectively beyond the face of the bulkhead posts. Steel-span dimensions with respect to the different types of support are measured as follows:

1. Highway spans on intermediate supports.

The state of the s	
Timber pile piers	
Steel pile bents	To center of bent
Steel pile piers	To center of pier
Timber towers, span to tower	2'-5" beyond center of end
	bent
15-foot tower span	1'-7" beyond center of inside
-	bent
Steel towers, span to tower	To center of bent
30-foot tower span	To center of bent
2. Highway spans on abutments.	
Timber grillage, class 25, all spans	33/4" beyond center of cap
class 50, 15-to 40-foot span	33/4" beyond center of cap
	43/4" beyond center of cap
Timber pile bent, all spans	43/4" beyond center of cap
Steel pile bent, all spans	
Concrete, all spans	
3. Railway spans on intermediate support	
Braced timber pile piers, span to pier	2'-5" beyond center of end
- " - <u>-</u>	bent
15- foot span between piers	1'-7" beyond center of bent
Braced steel pile bents, 15- to 30- foot spans	
Braced steel pile piers, 35- to 50- foot span	
to pier, and 15-foot span between piers	To center of piers
Timber tower, span to tower	
•	bent
Double 15-foot tower span	1'-10" beyond center of in-
•	side bent

	Steel tower, span to tower		
•	Timber grillage, 15-foot span only	8"	beyond center of cap
	Timber pile bent, 15- to 25-foot span		
	Timber pile pier, 30- to 45-foot span		
	50-foot span	43/4"	beyond center of cap
,	Steel pile bent, all spans	43/4"	beyond center of cap
	Concrete, all spans	11/4"	from face of backwall

- 5. Riveted spliced stringers. For riveted spliced stringers exceeding 40 feet in length bills of materials are shown assuming exact length for 40 foot sections. All other sections are shown in bills of materials ½-inch less in length than dimensioned on the fabrication drawings in order to provide cutting tolerance of minus 0 to plus ½-inch. Where 40 foot sections overrun or underrun lengths of adjacent sections must be adjusted accordingly.
- 6. Welded spliced stringers. For welded spliced stringers exceeding 40 feet in length bills of materials are shown assuming exact lengths of all pieces as dimensioned on the fabrication drawings. Spliced ends must be fitted, beveled and trimmed to exact length with allowances of 1/8-inch gap for butt welding.
- 7. Bills of materials. These are complete for all standard designs. When modifying standard designs, adjustments must be made for other material needed. The drawings show details of timber and steel stringer spans meeting on a common support, and unequal depth steel stringers meeting at a common support. The drawings from which bills of materials and details for shims, blocking, bearing plates, and anchor bolts can be obtained are shown on sheet 154. Anchor bolts for anchoring framed towers to footings are shown in bill of materials for footings.
- b. Use of drawings. After the bridge lay-out has been determined and the types of units of construction selected, the complete list of drawings required for assembly of parts, bills of materials, and fabrication details can be made by combining the lists of drawings for all units used in the bridge.
- c. Variation in tower heights. (1) Framed steel towers. Complete plans for framed steel towers varying in height from 15 to 77 feet by 2-foot increments are included in the manual. In the lay-out, footing elevations are adjusted so towers of odd height are not used.
- (2) Framed timber towers. (a) Complete plans including bills of materials are given for timber towers varying in height from 13 feet 4 inches to 75 feet 10 inches. If dressed-size timber is used for caps and sills the column lengths shown on sheets 148 and 183 should be increased to compensate for the smaller size.
- (b) Towers 13 feet 4 inches, 25 feet 10 inches, 38 feet 4 inches, 50 feet 10 inches, 63 feet 4 inches, or 75 feet 10 inches high are built of full 12-foot 6-inch stories. Towers of intermediate heights are built of one or more full 12-foot 6-inch stories and a short bottom story. In preparing bills of materials for towers containing a short bottom story, the bottom story is counted as a full story and members for it are cut in the field to fit. Footing locations are shown for heights varying by 2-foot intervals. (See sheets 37, 82, 121, and 214.)
- d. Longitudinal bracing. (1) Timber pile bents. In trestle bridges of timber stringers on timber pile bents more than 17 feet high, longitudinal brac-

ing is required between bents in every third span. Where longitudinal bracing is two panels high, longitudinal struts are added in unbraced spans. Bents less than 17 feet high require no longitudinal bracing.

- (2) Steel pile bents. Steel pile bents for highway spans are not braced longitudinally. For railway bridges, longitudinal bracing is required in alternate spans.
- e. Combinations of spans. Combinations of spans and supporting units, bents, piers, and towers are shown in the selection diagrams, tables XVII to XXIV inclusive. Details of junctions of steel and timber spans on a common support are shown on the drawings.

Caution: The combined length of the two spans on a common support must never exceed the lengths shown below. (Height of support is measured from grade to ground.)

co st cc	laximum ombined length of two pans on common support
-777 -77 -78	Feet
Highway, all classes, on timber pile bent up to 30 feet high	30
on timber pile pier up to 18 feet high	180
on steel pile bent up to 23 feet high	100
23 to 30 feet high	70
on steel pile pier up to 35 feet high	180
Highway, class 50 on timber pile pier 18 to 30 feet high	100
Highway, class 25 on timber pile pier 18 to 30 feet high	120
Railway, on timber pile bent up to 30 feet high	32
	50+15
	30+15
• · · · · · · · · · · · · · · · · · · ·	50+15

- f. Construction in water. Limitations of construction in water are given in paragraph 10.
- g. Expansion and contraction. (1) No provision is necessary in timber bridges for expansion and contraction of stringers.
- (2) Bearings at one end of all steel stringers have slotted bolt holes permitting expansion and contraction of stringers with temperature changes.
- (a) Steel stringers should be arranged at intermediate supports so there is one expansion and one fixed bearing at each support.
- (b) Timber decks of highway structures on steel-stringer bridges must be broken over all expansion joints. Timbers must not extend across the joint but must be cut at the ends of the stringers as shown on sheet 128. Nailers should be placed on end diaphragms of steel spans for full width of roadway to provide additional support for roadway planking.
- h. Riprap. Where foundations are built in water and protection must be made against scour around piles, riprap (par. 168b) can be placed as indicated on the drawings. Extreme amounts of riprap are shown. The amount necessary depends on stream characteristics. (See par. 221a.) Enough riprap should be used to:
- (1) Protect the bottom effectively against scour.
- (2) Keep the unbraced pile length within limits given in paragraph 10. No riprap should be used around piles if the stipulated maximum water depth

(par. 10) is unlikely to be exceeded after scour. Riprap unwisely placed may restrict the flow of the stream and cause scour which otherwise would not have occurred.

- i. Walkways and refuge bays. Walkways may be provided on highway bridges (sheet 130) and refuge bays or walkways may be provided on railway bridges (sheet 174) if the bridge is long and a safety zone is desired. If a sidewalk is added when the bridge is constructed, its design can be simplified by using extended deck plank as walkways, or by using extra long cross ties at intervals.
- j. Tower bracing for steel towers. The standard designs for either riveted, bolted, or welded construction provide longitudinal, transverse, and horizontal bracing of round rod sections with pin and connections. Each diagonal of longitudinal or transverse bracing consists of two loop rods threaded at the straight end and a turnbuckle. Each rod of the horizontal bracing consists of two clevises, two rods threaded at both ends, and a turnbuckle requisitioned as one unit from the supply depot. After the length of the diagonal is determined one of the threaded rods or loop rods is cut in two and a length of additional rod is spliced in to give correct length. Pipe sleeves, washers, and cotter pins complete the assembly in erected position.
- k. Splices. Splices shown for steel stringers are designed on the basis of actual shears and moments at the point of splice. A change in the location of a splice on the beam should be made only on the recommendation of experienced designers.
- **224.** ALTERNATIVES. a. Connections. The manual shows details of riveted, bolted, and welded connections of steel parts. Structural ribbed bolts may be used instead of rivets; nominal size (but not length) and number of bolts is the same as for rivets.
- (1) If $\frac{7}{8}$ -inch machine bolts are substituted for rivets, the bridge capacities must be adjusted as shown in the following paragraphs.
- (a) Capacity must be reduced 20 percent for the following steel construction units using machine bolts:

0	
Construction will	Machine bolts used in
All spans over 40 feet long	Stringer splices.
Pile piers under highway spans of over 140-foot	
combined length	Corbels and cap beams.
Towers supporting class 50 highway	Cap beam, column splices.
Two-story, over 70-foot span.	
Three-story, over 60-foot span.	
Four-story, over 50-foot span.	
Pile bents under railway spans of 40-and 45-foot	
combined length	Cap beam.
Pile piers under railway spans of 50-, 55-, and	
60-foot combined length	Corbel and cap beam.
Pile abutment under 50-foot railway span	Cap beam.
Towers and steel pile frames supporting railway	•
span	Cap beam, column splices,
•	steel-frame connections.

Three-story, for 50-foot span.

Four-story, over 40-foot span.

(b) No reduction in capacity is required for steel construction units with __machine bolts in:

Stiffeners, diaphragms, bracing for spans, bents, and piers.

Highway pile bents, abutments, steel pile frames under towers.

Pile piers under highway spans up to 140-foot combined length.

Towers, class 25, any height and span.

Towers, class 50, two-story up to 70-foot span.

three-story up to 60-foot span. four-story up to 50-foot span.

Pile bents under railway spans of 30- and 35-foot combined length.

Pile piers under 50-foot railway span (65-foot combined length). Pile abutments under railway spans up to 45-foot length.

TABLE L. Moments and shears for steel stringers for standard designs.

Span (feet)	Max moment (ft, kips)	SM required (inch³)	Max shear (kips)	Web area required (sq. in.)
	CLASS 50, SINGLE-LAI	NE HIGHWAY (EAC	CH OF 4 STRING	ERS)
15	112.6	50.1	35.0	2.12
20	174.1	78.9	40.3	2.45
30	305.6	138.3	47.5	2.88
40	446.6	202.2	51.9	3.15
50	593.8	268.8	55.5	3.37
60	763.7	345.9	59.2	3.59
70	925.8	419.3	61.9	3.75
80	1127.9	501.5	65.6	3.98
90	1340.6	596.0	68.9	4.18
	CLASS 50. DOUBLE-LAN	VE HIGHWAY (EA	CH OF 6 STRING	GERS)
15	138.8	61.7	35.2	2.13
20	213.2	94.8	40.6	2.46
30	374.5	166.4	47.8	2.90
40	550.9	245.0	52.8	3.20
50	735.0	326.7	56.8	3,44
60	931.8	414.2	60.2	3.65
70	1144.1	508.5	63.4	3.84
80	1383.2	615.0	67.2	4.07
90	1663.5	739.0	72.0	4.36
	CLASS 25, DOUBLE-LAN	NE HIGHWAY (EAC	CH OF 6 STRING	ERS)
15	79.1	35.2	20.1	1.22
20	120.2	53.4	22.8	1.38
30	210.6	93.6	26.8	1.62
- •	210.6 305.0	93.6 135.6		1.62 1.77
30			29.3	1.77
30 40	305.0	135.6	29.3 31.2	1.77 1.89
30 40 50	305.0 408.2	135.6 181.4	29.3	1.77 1.89 2.02
30 40 50 60	305.0 408.2 516.7	135.6 181.4 229.8	29.3 31.2 33.3 35.5	1.77 1.89 2.02 2.15
30 40 50 60 70	305.0 408.2 516.7 641.6	135.6 181.4 229.8 285.2	29.3 31.2 33.3	1.77 1.89 2.02
30 40 50 60 70 80	305.0 408.2 516.7 641.6 773.6 924.2	135.6 181.4 229.8 285.2 343.8	29.3 31.2 33.3 35.5 37.6 40.0	1.77 1.89 2.02 2.15 2.28
30 40 50 60 70 80	305.0 408.2 516.7 641.6 773.6 924.2	135.6 181.4 229.8 285.2 343.8 410.8	29.3 31.2 33.3 35.5 37.6 40.0	1.77 1.89 2.02 2.15 2.28
30 40 50 60 70 80 90	305.0 408.2 516.7 641.6 773.6 924.2	135.6 181.4 229.8 285.2 343.8 410.8	29.3 31.2 33.3 35.5 37.6 40.0	1.77 1.89 2.02 2.15 2.28 2.42
30 40 50 60 70 80 90	305.0 408.2 516.7 641.6 773.6 924.2 RAILW.	135.6 181.4 229.8 285.2 343.8 410.8 AY, E-45 (FOR EAC	29.3 31.2 33.3 35.5 37.6 40.0 H RAIL) 88.1	1.77 1.89 2.02 2.15 2.28 2.42
30 40 50 60 70 80 90	305.0 408.2 516.7 641.6 773.6 924.2 RAILW.	135.6 181.4 229.8 285.2 343.8 410.8 AY, E-45 (FOR EAC 129.5 210.3	29.3 31.2 33.3 35.5 37.6 40.0 H RAIL) 88.1 108.9	1.77 1.89 2.02 2.15 2.28 2.42
30 40 50 60 70 80 90	305.0 408.2 516.7 641.6 773.6 924.2 RAILW. 277.4 452.2 661.2	135.6 181.4 229.8 285.2 343.8 410.8 AY, E-45 (FOR EAC 129.5 210.3 306.0	29.3 31.2 33.3 35.5 37.6 40.0 H RAIL) 88.1 108.9 122.4	1.77 1.89 2.02 2.15 2.28 2.42 5.34 6.60 7.42
30 40 50 60 70 80 90 15 20 25 30	305.0 408.2 516.7 641.6 773.6 924.2 RAILW. 277.4 452.2 661.2 883.2	135.6 181.4 229.8 285.2 343.8 410.8 AY, E-45 (FOR EAC 129.5 210.3 306.0 404.6	29.3 31.2 33.3 35.5 37.6 40.0 H RAIL) 88.1 108.9 122.4 134.6	1.77 1.89 2.02 2.15 2.28 2.42 5.34 6.60 7.42 8.16
30 40 50 60 70 80 90 15 20 25 30 35	305.0 408.2 516.7 641.6 773.6 924.2 RAILW. 277.4 452.2 661.2 883.2 1119.0	135.6 181.4 229.8 285.2 343.8 410.8 AY, E-45 (FOR EAC 129.5 210.3 306.0 404.6 519.0	29.3 31.2 33.3 35.5 37.6 40.0 H RAIL) 88.1 108.9 122.4 134.6 146.7	1.77 1.89 2.02 2.15 2.28 2.42 5.34 6.60 7.42 8.16 8.90

1 Kip = 1,000 lb.

Towers and steel pile frames supporting railway spans.

Three-story up to 45-foot span.

Four-story up to 40-foot span.

- (c) Machine bolts used for final connections must have shanks (unthreaded length) not shorter than the thickness of the joined steel sections. Washers are used and nuts must be tight.
- b. Roadway decks. An alternative to the standard double-layer plank roadway is the laminated floor with longitudinal tread plank. The two types are shown on sheet 128. Use of laminated floor is recommended where plank for the standard floor is not available and the smaller dimension timber required for it can be obtained.
- c. Stringer sections. (1) Standard designs. For each class of traffic and each standard span length, there is one standard stringer design. Standard sections should be used for all new structures if the required sections are available. Moments and shears are listed in table L. Where possible standard designs should also be used in reconstructing existing or damaged structures. Any deviation from standard span lengths or standard number or sections of stringers requires adjusting details and bills of materials.
- (2) Nonstandard designs. Nonstandard spans should be used only where standard stringer sections are not available or where existing bridge supports fix span lengths for new superstructures. Design data for selecting stringer sections for spans not of standard length and stringer sections not used in the standard designs are given in figures 142 to 144 inclusive and table LI.
- (3) Use of design data. The following examples illustrate the use of this design data.
- (a) Highway bridges—steel stringers. The tables (figs. 142(2), 142(4) or 143(2)) are used when span lengths are standard but standard stringer

TABLE LI. Required total width of timber stringers in inches for different bighway and railway spans.

Span		Stringer depth (surf	aced dimension lumber))
(feet)	12-inch	14-inch	16-inch	18-inch
	HIGHWAY S	SPANS, CLASS 50, S	INGLE-LANE	
11	62	55	49	44
13	74	56	50	45
15	88	67	52	46
	Highway si	PANS, CLASS 50, DO	OUBLE-LANE	
11	114	100	89	79
13	138	103	91	81
15	164	124	94	84
	Highway si	PANS, CLASS 25, DO	DUBLE-LANE	
11	71	58	52	47
13	90	66	53	48
15	108	75	62	51
	RAILWAY SPA	ns, E–45 loading	, TWO RAILS	
12	44	36	32	28
14	60	44	36	32
16	76	56	42	38

sections are not available. The graphs (figs. 142(3), 142(5) or 143(3)) are used when span lengths are not standard.

- 1. Example A: Required: 40-foot span, class 50, single-lane highway. Condition: 24-inch 87-pound I-beam required for standard design not available. From the table (fig. 143(2)) there are two substitutes:
 - 5 stringers, 24-inch I 74-pound
 - 6 stringers, 21-inch I 63-pound

Details such as diaphragms must be modified accordingly.

- 2. Example B: Required: 68-foot span, class 50, single-lane highway. Enter lower edge of graph (fig. 143(3)) with 68-foot span; follow vertically to intersection with curve marked "4 stringers—standard design"; read at left side of graph—"33-in. I 132-lb."; or for "5 stringer alternate No. 1," read at left side of graph "33-in. I 125-lb."; or for "6 stringer alternate No. 2", read at left side of graph "30-in. I 108-lb."
- (b) Highway bridges—timber stringers. Table LI is used for standard length spans. No data are given for odd-length timber spans.

Example C: Required: 15-foot timber span, class 25, double-lane highway. Condition: Stringers deeper than 14 inches are not available. From table LI, the net width of 14-inch stringer required is 75 inches. Hence, 14-inch net-dimension stringers can be used as follows:

$$19 - 4 \times 14$$
 W = $19 \times 4 = 76$ inches
 $13 - 6 \times 14$ W = $13 \times 6 = 78$ inches
 $10 - 8 \times 14$ W = $10 \times 8 = 80$ inches

- (c) Railway bridges—steel stringers. For standard span length, no alternative sections are given. For special span lengths, figure 144 is used, the procedure being as outlined in example B above.
- (d) Railway bridges—timber stringers. For special span lengths, no design data are given. For standard span lengths, table LI is used, the procedure being as outlined in example C above.
- (e) Plate girders. If rolled beams are not available but plates and angles can be obtained, plate girders can be fabricated in the field and used instead of rolled sections. The design of riveted and welded plate girders equivalent to standard rolled beams is given in appendix I.
- 225. MODIFICATIONS. a. Towers on sloping banks. (1) Standard tower designs have the base plates of all four columns of the same elevation. Footings should be at different levels only where the bank is very steep or where the excavation necessary to place footings at a uniform level would be difficult.
- (2) Where footings must be at different levels, bracing is divided into stories to fit the highest column of the tower. Material is requisitioned to construct a standard tower of height of highest column. Bracing and the short column in the bottom story are modified in the field to fit the conditions. The footing under the short column is pleaced nearer to the bridge center line so the column batter is maintained. Modification of column lengths and bracing to fit footings at different levels is shown in figure 145.
- b. Curved alignment. (1) General. For long bridges on sharp curves, bents, piers, or towers are set on radial lines. However, bents in each individual pier or tower should be parallel to avoid special longitudinal bracing. Span lengths are measured on roadway center line. Where supports are on radial lines, the outer stringers are longer than the inner stringers. Where possible this adjustment is made in the slotted-hole locations only, the actual stringer length remaining unchanged.

(2) Railway bridges. (a) For curved track alignment on a straight bridge, the maximum length of straight bridge for any given curve is given by the formula:

$$L = \sqrt{\frac{2RM}{3}}$$

Symbols:

L = total length of straight bridge in feet.

$$R = \text{radius of curve in feet} = \frac{5730}{\text{degree of curve}}$$

M =Length in inches of middle ordinate of curve taken over total length of straight bridge.

(M must not exceed 8 inches.)

(b) For a given length of bridge, the sharpest curve (fig. 146) that can be used is given by the formula:

$$R = \frac{3L^2}{2M}$$

(c) The following speed restrictions should be enforced on railroad bridges built on a curve.

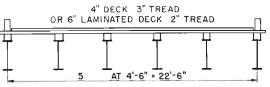
Degree of curve	Permissible speed in m.p.h.	
0° to 1° 30′	40	
1° 30′ to 2° 30′	30	
2° 30′ to 6° 30′	20	

With speeds restricted as shown above, no superelevation of track is necessary.

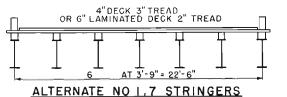
- (d) No provision is necessary for strengthening railway bridges for centrifugal forces resulting from curved alignment.
- (3) Highway bridges. No speed reduction or superelevation is proposed on highway bridges built on curve.
- c. Grades. All designs given in the manual are for bridges with level roadway or deck. For bridges on grade, blocking or shims are used between stringers and supports. Shims must be beveled to conform with the roadway slope.
- **226.** ADAPTATIONS. a. Highway bridges. Bents, piers, and abutments of class 50 single-lane highway bridges can be adapted to standard steel highway spans described in other manuals.
- (1) Semipermanent highway steel bridges, 30-, 60-, and 90-foot spans. These semipermanent prefabricated highway bridges are described in TM 5-285. They are referred to as prefabricated semipermanent highway or 1943 design bridges. Modification of standard supporting structures for use with these spans is shown on sheets 235 to 243.

	S	Sheet number	
Support	30-foot	60-foot	90-foot
Framed timber tower	235	238	241
Steel pile pier	236	239	242
Timber pile pier	236	239	242
Timber grillage abutment	236	239	242
Concrete abutment	237	240	243
Steel pile abutment	237	240	243
Timber pile abutment	237	240	243

DOUBLE-LANE HIGHWAY



STANDARD DESIGN 6 STRINGERS



OR 6" LAMINATED DECK 2" TREAD

11

AT 3'-2%"=22'-6"

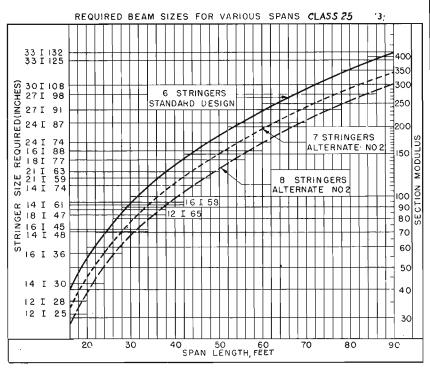
ALTERNATE NO 2,8 STRINGERS

CLASS 25

SPAN	STANDARD DESIGN	ALTERNATE NO I	ALTERNATE NO 2	
LENGTH (FEET)	6 STRINGERS SIZE(INCHES)	7 STRINGERS SIZE(INCHES)	8 STRINGERS SIZE(INCHES)	(2)
1.5			12 I 25	
1.5	14 I 30	12 I 25	12 1 2 3	
2 0	16 I 36	16 I 36	14 I 30	
30	21 I 59	18 I 47	16 I 45	
4 0	21 I 63	2 I 59	21 I 59	
5 0	24 I 87	24 I 74	21 I 63	
60	27 I 91	241 87	24 I 74	
7.0	30 I 108	271 98	24 I 87	
8.0	33 I 125	30 I 108	30 I 108	
9 0	33 I 132	30 I 108	30 I 108	

CLASS 50

	SPAN	STANDARD DESIGN	ALTERNATE NO I	ALTERNATE NO 2
4)	LENGTH	6 STRINGERS	7 STRINGERS	8 STRINGERS
	(FEET)	SIZE(INCHES)	SIZE(INCHES)	SIZE(INCHES)
	15	18 I 47	16 I 36	14 I 30
	20	21 I 59	18 I 47	16 I 45
	30	24 I 74	24 I 74	21 I 59
	40	27 I 9i	24 I 87	24 I 74
	50	33 I 125	30 I 108	27 I 91
	€0	33 I 132	33 I 125	30 I 108
	70	36 I 150	33 I 132	33 I 125
	80	36 I 182	36 I 150	36 I 150
	90	36 I 230	36 I 182	36 I 82



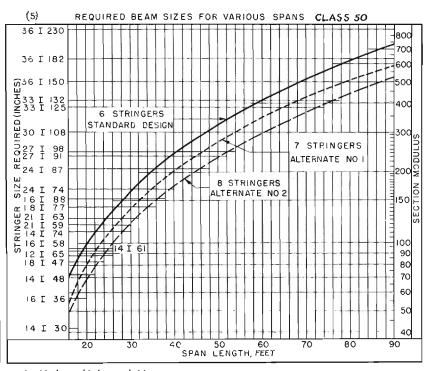
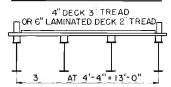


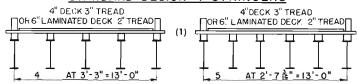
Figure 142. Alternative stringers for double-lane highway bridges.

- (1) Stringer spacing and arrangement.
- (2) Table of standard and alternative stringer sections, class 25 highway bridges.
- (3) Graph of required stringer sizes for different spans, class 25 highway bridges.
- (4) Table of standard and alternative stringer sections, class 50 highway bridges.
- (5) Graph of required stringer sizes for different spans, class 50 highway bridges.

SINGLE-LANE HIGHWAY



STANDARD DESIGN 4 STRINGERS



ALTERNATE NO 1.5 STRINGERS ALTERNATE NO 2.6 STRINGERS

CLASS 50

·			
SPAN	STANDARD DESIGN	ALTERNATE NO I	ALTERNATE NO 2
LENGTH	4 STRINGERS	5 STRINGERS	~6 STRINGERS
(FEET)	SIZE (INCHES)	SIZE(INCHES)	SIZE(INCHES)
1.5	16 I 33	14 I 30	12 I 25
20	18 I 47	I6 I 45	16 I 36
30	24 I 74	21 I 59	2 I 59
40	24 I 87	24 I 74	21 I 63
50	30 I 108	27 I 91	24 I 87
60	33 I 25	30 I 108	27 I 91
7 0	331132	33 I 125	30 I 108
80	36 I 150	33 I 132	33 I 125
9 0	36 I 182	36 I 150	33 I 132

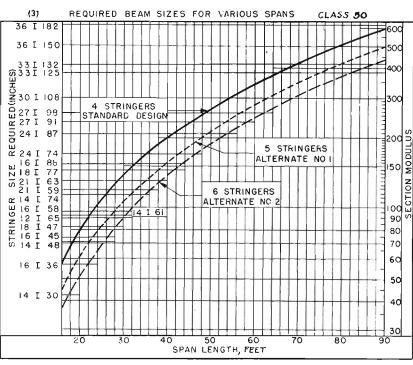


Figure 143. Alternative stringers for single-lane highway bridges.

- (1) Stringer spacing and arrangement,
- (2) Table of standard and alternative stringer sections.
- (3) Graph of required stringer sizes for different spans.

- (2) Fixed steel panel bridge, Bailey type. Bailey bridges are described in TM 5–277. They may be used with timber pile bents, piers, and abutments, steel pile bents and abutments, or with concrete abutments of this manual. Necessary modifications are shown on sheet 244.
- (3) Portable steel highway bridge H-10 and H-20. These bridges are described in TM 5-274. They may be used with steel or timber pile piers or abutments or with concrete abutments of this manual. Necessary modifications are shown on sheet 245.
- **b.** I-beam railway bridges. I-beam spans are described in TM 5-371. By modifying the end bearings, they may be used with any of the railway supports given in this manual except timber pile bents.

PART FIVE

APPENDIX I

PLATE GIRDER DESIGN

1. GENERAL. Typical details of riveted and welded plate girders are given on figures 150 and 151 respectively. These girders can be used instead of the

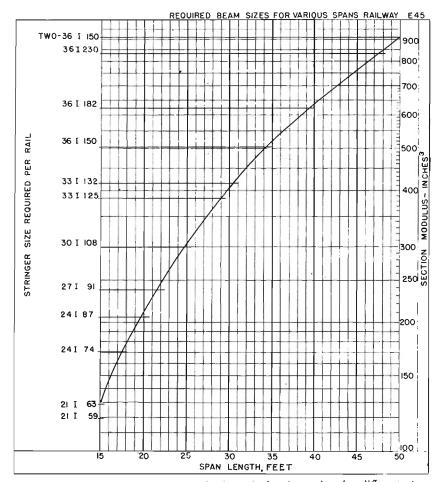


Figure 144. E-45 railway bridges. Graph of required stringer sizes to different spans.

21- and 24-inch beams used in the standard designs. Examples of the method used in designing the 24-inch girders are given in the following paragraphs. The examples will guide trained designers in proportioning plate girders to be used instead of standard rolled beams and in checking and repairing plate girders found in the field.

2. PROBLEM. The problem is to design a plate girder to be used instead of the 21-inch 63-pound rolled beam used in the standard 40-foot span of the class 25, double-lane highway bridge. From table L, the moments and shears to which the girder will be subjected are:

Maximum moment (M) = 305.0 foot kips. Maximum shear (V) = 29.3 kips.

- 3. RIVETED DESIGN. Use 24-inch plate girder with 3/8-inch web (class IV material) as shown in figure 147.
- a. Determine flange section. Approximate distance between the centers of gravity of flanges: 241/2''-2''=221/2''

Less one-eighth of web area effective as flange

$$\frac{1}{8} \times 24 \times \frac{3}{8} = \frac{1.12}{4.00}$$
 sq. in.

Additional net area required in flange = 4.90 sq. in. Use two angles, 5- by $3\frac{1}{2}$ - by $3\frac{1}{2}$ - inch.

Gross area $2 \times 3.05 = 6.10$ sq. in. Deduct two holes for rivets $2 \times 15/16 \times \frac{3}{8} = 0.70$ sq. in. Net area provided 5.40 sq. in.

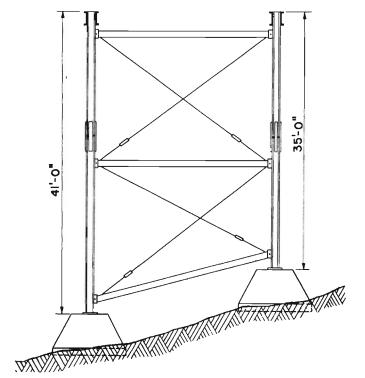


Figure 145. Bracing of framed steel tower modified to suit footings set at different levels.

b. Check flange stress for actual distance between centers of gravity of anges.

anges.		
Center-to-center flanges24.5" — $(2 \times .86")$	=	22.78"
One-eighth area of web	=	1.12 sq. in.
Net area, two angles	=	5.40 sq. in.
Total net area		6.52 sq. in.
Stress in flange	=	24,600 psi.
Allowable stress	=	27,000 psi.
c. Check shear stress in web.		
Maximum shear	=	29.3 kips.
Area of web24 $ imes$ $ imes$ 8	=	9.0 sq. in.
Shear stress in web	=	3,260 psi.
Allowable stress	=	16,500 psi.

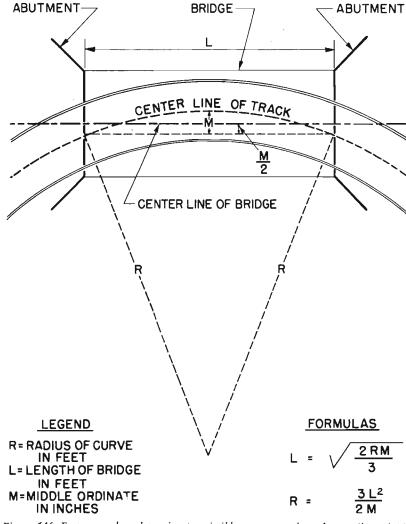


Figure 146. Factors used to determine permissible curvature of track on railway bridges.

d. Determine stiffener spacing. No intermediate web stiffeners are required because $\frac{d}{t} = \frac{17.5}{375} = 46.7$ (fig. 147), which is less than 70. Generally, when $\frac{d}{d}$ is greater than 70, intermediate stiffeners are provided. Their spacing must not exceed 72 inches or that given by the formula:

$$d = \frac{10,500}{\sqrt{S}}$$

Symbols:

d = clear distance between stiffeners in inches.

t = thickness of web in inches.

S = unit shearing stress (psi) of gross section of web at point considered.

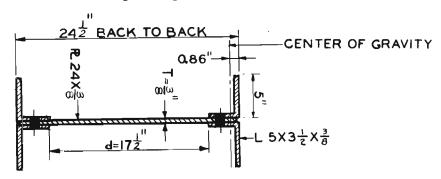


Figure 147. Cross section through riveted plate girder equivalent to 21-inch 63-pound rolled beam.

e. Determine spacing of flange rivets.

Value of \(\gamma_8\)-inch rivet in bearing on \(\gamma_8\)-inch plate:

$$30,000 \times .875 \times .375 = 9,840 \text{ lb/rivet}$$

Value of %-inch rivet in double shear:

$$\frac{2 \times \pi \times .875^2 \times 15,000}{4} = 18,050 \text{ lb/rivet}$$

Bearing value governs since it is less than value in double shear.

Flange rivet stress $\frac{29,300}{22.78} = 1,290 \text{ lb./in.}$ Wheel concentration (assumed longitudinal distribution of wheel load Resultant stress $\sqrt{1,290^2 + 665^2} = 1,450 \text{ lb./in.}$ Required rivet spacing $\frac{9,840}{1.450} = 6.8 \text{ in.}$ Maximum 5-inch spacing has been used (6-inch could have been used).

f. Select end-bearing stiffeners.

Use two angles, 4- by 6- by 3/8-inch to fit diaphragm connection.

g. Design web splice. (See fig. 148.) The sheer used in this example is the maximum that can occur in the girder, and actually governs only for a splice near the supports.

(1) For moment carried by web.

Web area carrying moment
$$\frac{1}{8} \times 24 \times \frac{3}{8} = 1.12$$
 sq. in. Use two flat bars $2\frac{1}{2} \times \frac{3}{8} = 1.875$ sq. in. Net area with two rivet holes deducted $= 1.175$ sq. in. Rivets required $= \frac{1.12 \times 27,000}{9,840} = 3.07$ rivets

Space rivets at 3-inch centers. Rivet spacing required for normal flange stress is 6.8 inches. Therefore, number of rivets required through flange angles

stress is 6.8 inches. Therefore, number of rivets required through flange angles and
$$2\frac{1}{2}$$
- by $\frac{3}{8}$ -inch bar is
$$\frac{3.07}{1 - \frac{3.0}{6.8}} = 5.5 \text{ rivets.}$$

Use five rivets.

(2) For shear carried by web. See fig. 148. Use two plates 13 inches by 3/8 inches by 1 foot 5 inches.

Maximum shear
$$= 29.3 \text{ kips}$$

Section modulus of rivets $= \frac{4(3.5^2 + 7^2)}{7} = 35 \text{ in.}^3$

Moment on rivet group $= 29,300 \times 3.5 = 105,500 \text{ in./lb.}$

Rivet stress (resultant of shear and moment stresses)

$$\sqrt{\left(\frac{102,500}{35}\right)^2 + \left(\frac{29,300}{10}\right)^2} = 4,100 \text{ lb./rivet}$$

The resulting stresses in the web splice rivets are well under the allowable stress. However, a minimum of two vertical rows of rivets should be provided on each side of center line of splice.

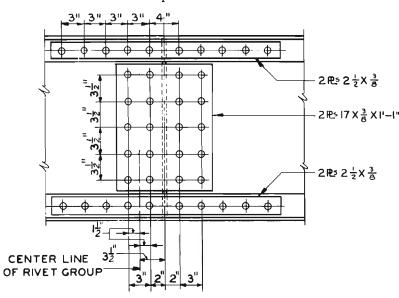


Figure 148. Riveted web splice of plate girder equivalent to 21-inch 63-pound rolled beam.

h. Design flange splice. The moment used is the maximum that can occur in the girder and actually governs only for a splice near the center of the span. Net area of 5- by 3½- by 3½-inch angle with two rivet holes out (one through horizontal and one through vertical leg) is

$$3.05 - 2 \times 15/16 \times \frac{3}{8} = 2.35$$
 sq. in.

Use 5- by 3½- by 3%-inch splice angles. Rivets required in single shear at

9,025 pounds, each to develop 5- by 3½- by 3½-inch angles, are

$$\frac{2.35 \times 27,000}{9,025} = 7.05 \text{ rivets}$$

Use four rivets in each leg of angle.

i. Detail. For complete detail of girder, see figure 150.

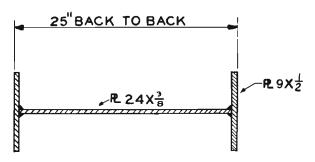


Figure 149. Cross section through welded plate girder equivalent to 21-inch 63-pound rolled beam.

4. WELDED DESIGN. See figure 149. Use 24-inch plate girder with 3/8-

a. Determine flange section.

Distance between centers of gravity of flanges = 241/2" Area of flange required. $\frac{305.0 \times 12}{27.0 \times 24.5} = 5.54 \text{ sq. in.}$ Additional area required = 4.04 sq. in. Use 9- by $\frac{1}{2}$ -inch plate, area = 4.5 sq. in.

b. Check shear stress in web.

•	Maximum shear			
	Unit stress in web	29,300	= 3,260 p	si.
	Allowable			
	No intermediate stiffeners will be required, because	se $\frac{d}{}$ of	web plate -	<u> 24</u>
	1 ,	t	•	.38

- = 64, under 70. For further explanation, see paragraph 3d.
- c. Determine flange plate connection to web.

- d. Select end bearing stiffeners. As stated in paragraph 3, only nominal material is required for bearing stiffeners. Use two 4- by 3/8-inch plates. Weld stiffener plates to web with continuous 1/4-inch fillet weld.
- e. Design of web splice. The shear used in this example is the maximum that can occur in the girder. (See par. 3g.)

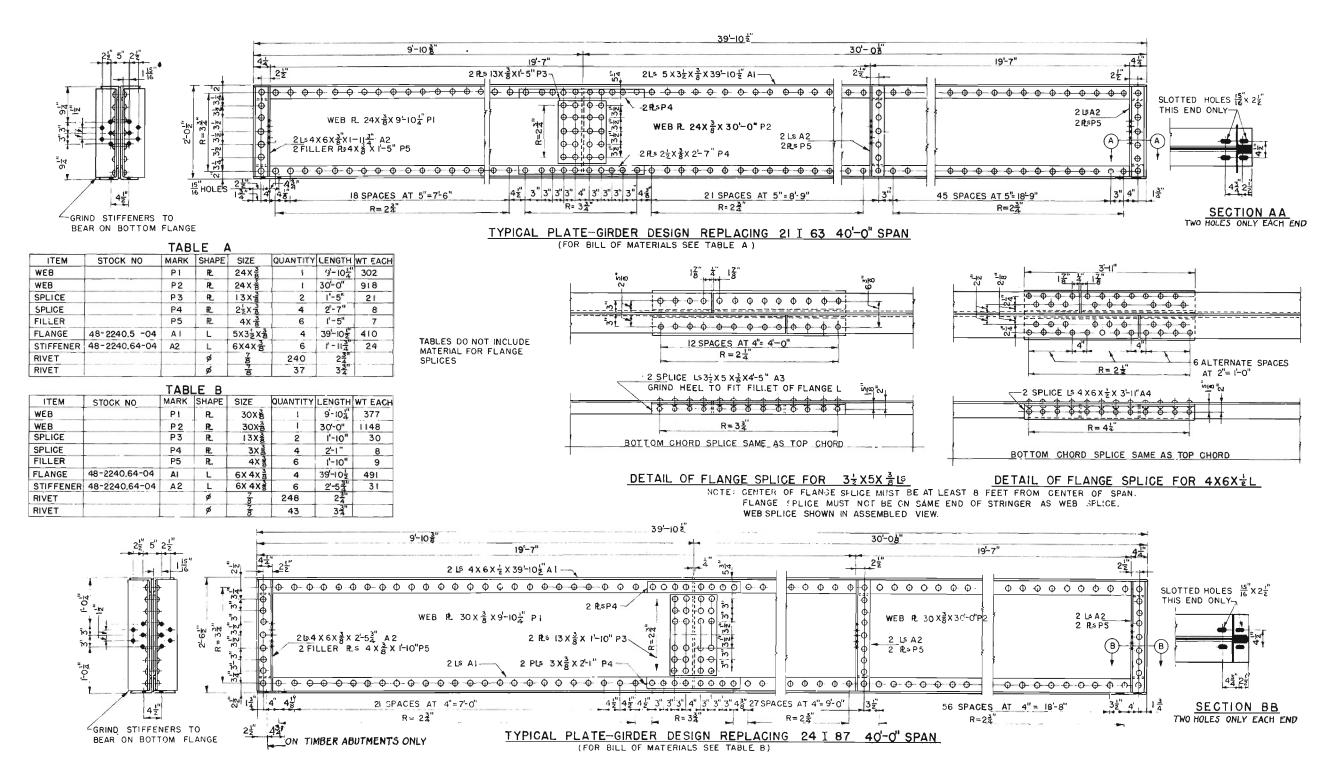


Figure 150. Riveted plate girders.

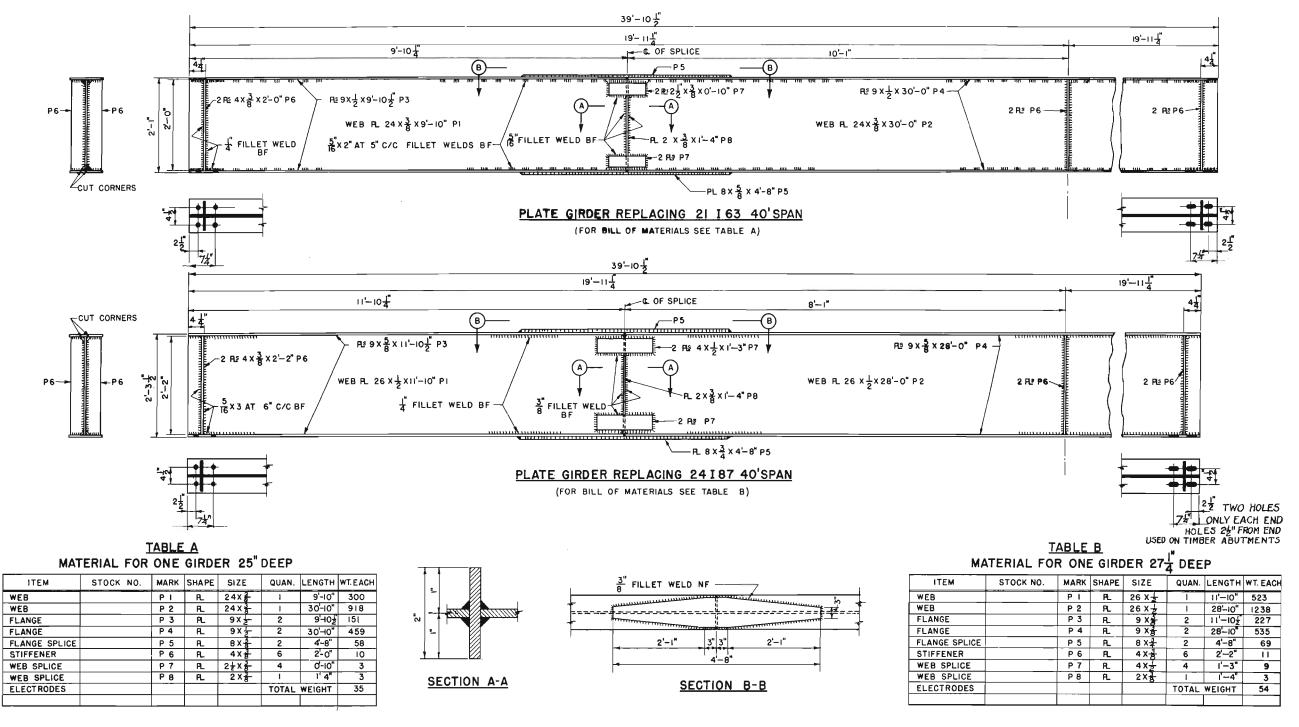


Figure 151. Welded plate girders.

Use two $2\frac{1}{2}$ by $\frac{3}{8}$ by 10-inch plates—area = 1.875 sq. in. Develop each plate for $1.50 \times 27,000 \dots = 20,200 \text{ lb.}$ Capacity of 5/16-inch fillet weld 5 \times 425 = 2,125 lb./in. Length of weld required $\frac{20,200}{2.125} = 9.5$ in.

(2) Develop web splice for maximum shear of 29.3 kips. In this example, a 2- by 3/8-inch by 1-foot 4-inch plate inserted between ends of web plates has been used as a convenient butt-joint detail.

Length of 5/16-inch weld required
$$\frac{29,300}{2125}$$
 = 13.9 in.
Length of 5/16-inch weld provided $\frac{29,300}{2125}$ = 32 in.

f. Design flange splice. The moment used in this example is the maximum that can occur in the girder (see par. 3h). (In this example with no butt joint between ends of flange plates, all flange stress is carried by splice plate.)

Use 8-inch by 5/8-inch by 4-foot 8-inch splice plate, area = 5.0 sq. in.Length of 3/8-inch fillet weld required.

$$\frac{4.5 \times 27,000}{6 \times 425} = 48 \text{ inch}$$

Length of $\frac{3}{6}$ -inch fillet weld provided = 4 ft. 8 in. = 56 in. (In standard stringer splices, butt welds are used between the ends of the beam flanges and are effective for compressive stress transfer of

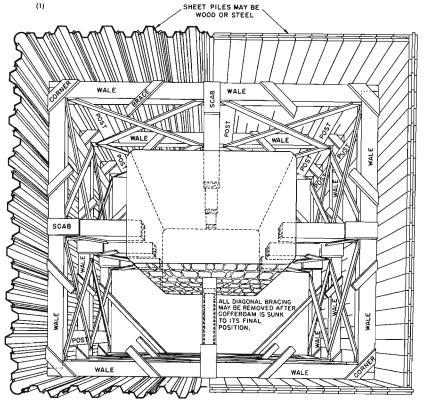
Taper ends of flange splice plates as shown on figure 151.

q. Drawing. For complete details of welded girder, see figure 151.

APPENDIX II

COFFERDAMS

- 1. GENERAL. a. This appendix shows the arrangement of wales, posts, and bracing in sheet pile cofferdams (figs. 152 to 154) and gives tables (tables LII to LVI inclusive) for the selection of timber sizes and spacing of wales.
- b. The cofferdams are intended for use in repairing partly demolished masonry piers for use as foundations for semipermanent trestle bridges. They should not be used in water over 10 feet deep. They can also be used in constructing concrete pedestal and grillage foundations in water. (See par. 221.)
- 2. EXAMPLE. The following example illustrates the use of the data in designing a cofferdam 30 feet long by 10 feet wide.
- a. From table LIV, for 10-foot depth, use three-wale cofferdam with wales spaced 4 feet apart in the bottom panel and 6 feet apart in the top panel.



VIEW LOOKING DOWN ON COFFERDAM BRACING FROM ABOVE

ALL BRACES, WALES, STRUTS, POSTS, AND SCABS IN PLACE READY TO BEGIN SINKING OPERATIONS

EITHER WOOD OR STEEL SHEET PILES MAY BE USED WITH ANY ONE SET OF BRACING. SHEET PILES ARE NOT TO BE ATTACHED TO BRACING. BRACING FRAMEWORK TO BE SECURELY FASTENED TOGETHER WITH SCABS, SPIKES.

REMOVE HORIZONTAL
DIAGONAL BRACING AFTER SHEET
PILES ARE DRIVEN 5 FEET INTO THE
EARTH

(2)

CUT AWAY VIEW SHOWING COFFERDAM BRACING THROUGH BOLTS, AND DRIFT BOLTS. FOR SIZES OF WALES, STRUTS, A:1D SHEETING, SEE FIGURE 153 AND TABLES LII TO LVI. SIZE OF POSTS SAME AS WALES. ALL DIAGONAL BRACING 2 x 6 PLANKS.

SHEET PILES MAY BE

Figure 152. Rectangular cofferdams.

- (1) Top view.
- (2) Cut away view.

Use two transverse struts at each wale level, making the wale span 10 feet and the strut length 10 feet.

- b. From table LV, for 10-foot strut spacing and h₁ of 6 feet, 10-by 10-inch wales are selected.
- c. From table LVI for 10-foot strut spacing and h₁ of 6 feet, 6- by 6-inch struts are selected.
- d. Posts will be the same size as the wales, 10- by 10-inch.
- e. Sheet piling may be 4-inch shiplap, 6-inch Wakefield, or steel sheet piling.

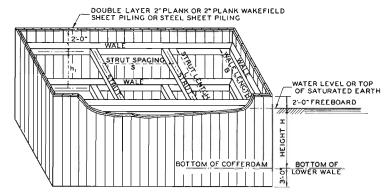
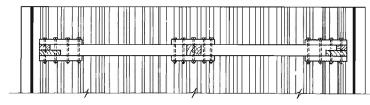


Figure 153. Cofferdam dimensions.



SECTION A-A

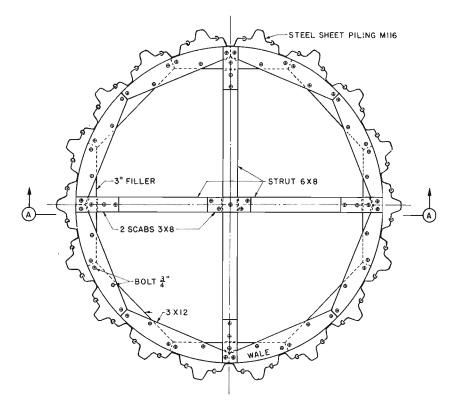


Figure 154. Circular cofferdam.

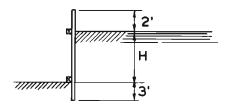


Table LII. Minimum wale size-2-wale cofferdam

		Strut spacing S or unsupported length of wale b in feet—See fig. 153											
Н	5	6	7	8	9	10	11	12	13	14	15	16	17
	SIZE OF WALE												
5 6 7	6 x 6 6 x 6 6 x 6	6 x 6 6 x 6 8 x 8	6 x 6 8 x 8 8 x 8	6 x 6 8 x 8 8 x 8	8 x 8 8 x 8 8 x 8	8 x 8 8 x 8 10 x 10	8 x 8 10 x 10 10 x 10	8 x 8 10 x 10 10 x 10	10 x 10 10 x 10 10 x 10	10 x 10 10 x 10 12 x 12	10 x 10 10 x 10 12 x 12	10 x 10 12 x 12 12 x 12	10 x 10 12 x 12 12 x 12

Table LIII. Minimum size and maximum length of struts-2-wale cofferdam

						:	Strut spacing S in f	eet					
н	5	6	7	8	9	10	11	12	13	14	15	. 16	17
		SIZE AND LENGTH OF STRUTS—SEE FIG. 153											
5 6 7	6 x 6 19'-0" 6 x 6 18'-6" 6 x 6 17'-6"	6 x 6 19'-0" 6 x 6 18'-0" 6 x 6 16'-6"	6 x 6 18'-6" 6 x 6 17'-6" 6 x 6 16'-0"	6 x 6 18'-0" 6 x 6 17'-0" 6 x 6 15'-6"	6 x 6 17'-6" 6 x 6 16'-6" 6 x 6 15'-0"	6 x 6 17'-6" 6 x 6 16'-0" 6 x 6 14'-6"	6 x 6 17'-0" 6 x 6 15'-6" 6 x 6 14'-0"	6 x 6 16'-6" 6 x 6 15'-0" 6 x 6 13'-6"	6 x 6 16'-0" 6 x 6 14'-6" 6 x 6 13'-0"	6 x 6 16'-6" 6 x 6 14'-0" 6 x 8 14'-6"	6 x 6 15'-0" 6 x 8 16'-0" 8 x 8 20'-0"	6 x 8 17'-6" 6 x 8 16'-0" 8 x 8 20'-0"	6 x 8 17'-0" 8 x 8 20'-0" 8 x 6 19'-6"

Tai	Table LIV.		Wale spacing—3-wale cofferdam					
ч	85		10.0	11.5	13.5			

|--|

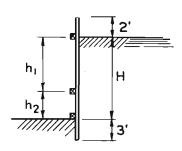


Table LV. Minimum wale size-3-wale cofferdam

					1 aut Ly	. IVLITITITUM W	uie size j-wai	e cojjeraam					
	Strut spacing S or unsupported length of wale B in feet-See fig. 153												
h ₁	5	6	7	8	9	10	11	12	13	14	- 15	16	17
			·	·	<u> </u>			<u>'</u>	<u> </u>			<u> </u>	
	SIZE OF WALE												
5	8 x 8	8 x 8	8 x 8	10 x 10	10 x 10	10 x 10	10 x 10	10 x 10	12 x 12	12 x 12	12 x 12	12 x 12	
6	8 x 8	8 x 8	10 x 10	10 x 10	10 x 10	10 x 10	12 x 12	12 x 12	12 x 12				*********
7	10 x 10	10 x 10	10 x 10	12 x 12	12 x 12	12 x 12	12 x 12						
8	10 x 10	12 x 12	12 x 12	12 x 12		**********							
	l	l			l	1	<u> </u>	<u> </u>					

APPENDIX III

TABLES OF USEFUL DATA

(Tables LVII through LXXXVI)

TABLE LVII. Weights of common materials.

Material	Wt. in lb. per cu. ft.	Material	Wt. in lb. per cu. ft.
Aluminum:		Ice	56
Cast	160		
Wire	168	Iron:	
		Grey cast	439-445
Asphalt	60–80	Wrought	487–492
Brass	510-542	Lead	710
Brick	110-130	Lime	53-75
		Masonry:	
Bronze	545-555	Mortar rubble	155
Coal:		Dry rubble	125
Anthracite	97		
Bituminous	84	Rock solid:	
		Granite	125-187
Concrete:		Shale	162
Reinforced	150	Soapstone	
Plain	140-150	Trap	187–190
Copper, cast	549-558	Salt	129–131
Earth:		Snow:	
Clay:		Fresh, fallen	
Dry, compacted	100	Wet, compact	15-20
Damp, plastic	110		
• • • • • • • • • • • • • • • • • • • •		Steel	474–494
Common:			
Dry, loose	65-88	Tar	75
Moist, compacted	95-135		
		Tin	455
Mud, wet:			
Fluid		Water:	(2.4
Compacted	110-130	Fresh Sea	62.4 64.0
		Sea	04.0
Sand:	110	Zinc	438
Dry, compacted		ZIIIC	-1/0
Damp, loose	94		
Gravel, crushed rock:			
Damp, loose	82–125		

Dry, compacted 90-145

Table LVI. Minimum size and maximum length of struts-3-wale cofferdam

	Strut spacing S in feet												
b ₁	5	6	7	8	9	10	11	12	13	14	15	16	17
	SIZE AND LENGTE OF STRUTS—SEE FIG. 153												
5	{6 x 6 17′-0″	6 x 6 16'-0"	6 x 6 15'-6"	6 x 6 15'-0"	6 x 6 14'-6"	6 x 6 14'-0"	6 x 6 13'-6"	6 x 6 13'-0"	6 x 8 14'-6"	6 x 8 14'-0"	8 x 8 19'-6"	8 x 8 19'-0"	
6	6 x 6 15'-6"	6 x 6 14'-6"	6 x 6 14'-0"	6 x 6 13'-6"	6 x 6 12'-6"	6 x 6 12′-0″	6 x 6 11'-6"	6 x 8 13'-0"	8 x 8 18'-0"				
7	6 x 6 14'-0"	6 x 6 13'-0"	6 x 6 12'-6"	6 x 6 12'-0"	6 x 6 11'-0"	6 x 6 10'-6"	6 x 8 12'-0"						
8	6 x 6 13'-0"	6 x 6 12'-0"	6 x 6 11'-0"	6 x 6 10'-6"						***********			

TABLE LVIII. Structural timber-allowable stresses. U. S: structural timber.

Variety and grade of wood		Average uni	Allowable w	orking stresses fo	r military bridge	es¹ (psi).	Modulus of
Species and grade description	Stress grade ² (lb.)	weight ³ (lb. per cu. ft	Extreme fiber	Horizontal shear	Compression perpendicular to grain	Compression parallel to grain'5	elasticity (psi)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Douglas fir	************	35		••		•••••	1,600,000
Dense select structural	1,800		2,700	180	500	1,950	
	∫ 1,600	***************************************	2,400	180	500	1,800	
Select structural	1,400		2,100	150	450	1,650	
Yellow pine (long leaf, or dense short leaf)		40					1,600,000
Select structural	2,000		3,000	150	500	2,200	
Prime structural	1,800		2,700	150	500	1,950	
Merchantable structural; and structural square edge							
and sound	1,600		2,400	150	500	1,800	***************************************
No. 1 structural	1,400		2,100	150	500	1,500	
Larch		36		***************************************	******		1,300,000
Select structural	1,800		2,700	200	500	1,950	*,
Structural	1,600		2,400	150	470	1,800	
Common structural	1,200		1,800	135	430	1,650	
Redwood (structural)		30	**********	***************************************	***************************************	******	1,200,000
Dense select all heart	1,400		2,100	135	350	1,800	
Select all heart	1,200		1,800	120	350	1,650	
Bulkhead and heart	1,100		1,650	120	350	1,650	******
Southern cypress		32				•••••	1,200,000
Select structural	1,400		2,100	180	400	1,800	
Structural	1,100	*	1,650	150	400	1,500	************
Eastern hemlock		30					1,100,000
Select structural	1,100	•	1,650	105	400	1,050	
	F	oreign Woods	3				
Group I		45					1,600,000
Teak, sal, white siris, jarul, lendia, oak, ash, Philippine							-,,-
mahogany			1,800-2,700	200	360-500	1,680-2,000	********
Group II		35	,,,,,,,,,,	**************			1,250,000
Doodar, chir, poon, gumhar, Norway (northern) pine			1,500-2,250	150	300-450	1,340-1,800	
Group III		30					1,000,000
White deal, kail			1,340-2,000	100	260–390	1,110-1,500	
, , , , , , , , , , , , , , , , , , , ,			,,			_,	***************************************

¹ Reduce all stresses to 70 percent of tabular values for greenwood and for design of parts of bridge structure continuously wet. Reduce all stress values to 75 percent of tabular values for design of structures carrying long-continued live load.

² Grade designations of structural timber adopted by United States lumber industry.

³ At about 15 percent moisture content.

Working stress in tension same as for bending.

⁵ Working stresses for compression parallel to grain apply to posts, columns, and struts the unsupported length of which does not exceed 11 times least dimension of cross section. For working stresses for unsupported lengths from 11 to 50 times least dimension of cross section, see chapter 4.

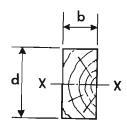


TABLE LIX. Properties of dressed timber (S4S).

Nominal size b (inches) d	American standard dressed size (S4S) b in inches d	Area of section A = bd (sq. in.)	Section modulus $S = bd^2$ 6 (in.3)	Board feet per linear foot of piece	weight o	t of piece	when er cubic
2 x 4	15/8 x 35/8	5.89	3.56	2/3	1.6	1.8	2.0
2 x 6	15/8 x 55/8	9.14	8.57	1	2.5	2.9	3.2
2 x 8	15/8 x 7½	12.19	15.23	11/3	3.4	3.8	4.2
2 x 10	15/8 x 91/2	15.44	24.44	12/3	4.3	4.8	5.4
2 x 12	15/8 x 11½	18.69	35.82	2	5.2	5.8	6.5
2 x 14	15/8 x 13½	21.94	49.36	21/3	6.1	6.9	7.6
3 x 6	25/8 x 55/8	14.77	13.84	11/2	4.1	4.6	5.1
3 x 8	25/8 x 71/2	19.69	24.61	2	5.5	6.2	6.8
3 x 10	25/8 x 91/2	24.94	39.48	21/2	6.9	7.8	8.7
3 x 12	25/8 x 111/2	30.19	57.86	3	8.4	9.4	10.5
3 x 14	25/8 x 131/2	35.44	79.73	31/2	9.8	11.1	12.3
4 x 4	35/8 x 35/8	13.14	7.94	1 1/3	3.7	4.1	4.6
4 x 6	35/8 x 55/8	20.39	19.12	2	5.7	6.4	7.1
4 x 8	35⁄8 x 71∕2	27.19	33.98	23/3	7.6	8.5	9.4
4 x 10	35/8 x 91/2	34.44	54.53	31/3	9.6	10.8	12.0
4 x 12	35⁄8 x 11½	41.69	79.90	4	11.6	13.0	14.5
6 x 6	$5\frac{1}{2} \times 5\frac{1}{2}$	30.25	27.73	3	8.4	9.5	10.5
6 x 8	$5\frac{1}{2} \times 7\frac{1}{2}$	41.25	51.56	4	11.5	12.9	14.3
6 x 10	$5\frac{1}{2} \times 9\frac{1}{2}$	52.25	82.73	5	14.5	16.3	18.1
6 x 12	$5\frac{1}{2} \times 11\frac{1}{2}$	63.25	121.23	6	17.6	19.8	22.0
6 x 14	$5\frac{1}{2} \times 13\frac{1}{2}$	74.25	167.06	7	20.6	23.2	25.8
6 x 16	$5\frac{1}{2} \times 15\frac{1}{2}$	85.25	220.23	8	23.7	26.6	29.6
6 x 18	$5\frac{1}{2} \times 17\frac{1}{2}$	96.25	280.73	9	26.7	30.1	33.4
8 x 8	$7\frac{1}{2} \times 7\frac{1}{2}$	56.25	70.31	51/3	15.6	17.6	19.5
8 x 10	$7\frac{1}{2} \times 9\frac{1}{2}$	71.25	112.81	62/3	19.8	22.3	24.7
8 x 12	$7\frac{1}{2} \times 11\frac{1}{2}$	86.25	165.31	8	24.0	27.0	29.9
8 x 14	$7\frac{1}{2} \times 13\frac{1}{2}$	101.25	227.81	91/3	28.1	31.6	35.2
8 x 16	$7\frac{1}{2} \times 15\frac{1}{2}$	116.25	300.31	$10\frac{2}{3}$	32.3	36.3	40.4
8 x 18	$7\frac{1}{2} \times 17\frac{1}{2}$	131.25	382.81	12	36.5	41.0	45.6
10 x 10	$9\frac{1}{2} \times 9\frac{1}{2}$	90.25	142.90	81/3	25.1	28.2	31.3
10 x 12	9½ x 11½	109.25	209.40	10	30.3	34.1	37.9
10 x 14	$9\frac{1}{2} \times 13\frac{1}{2}$	128.25	288.56	112/3	35.6	40.1	44.5
10 x 16	9½ x 15½	147.25	380.40	131/3	40.9	46.0	51.1
10 x 18	9½ x 17½	166.25	484.90	15	46.2	52.0	57.7
12 x 12	11½ x 11½	132.25	253.48	12	36.7	41.3	45.9
12 x 14	11½ x 13½	155.25	349.31	14	43.1	48.5	53.9
12 x 16	11½ x 15½	178.25	460.48	16	49.5	55.7	61.9
12 x 18	$11\frac{1}{2} \times 17\frac{1}{2}$	201.25	586.98	18	55.9	62.9	69.9

TABLE LX. Properties of full-sawn timber.

		Nominal size b (inches) d	Area of section A = bd	Section modulus $S = \frac{bd^2}{6}$	Board feet per linear foot of	line whe	ght in poun ear foot of j n weight of cubic foot e	f piece of wood equals	
		b (menes) d	(sq. in.)	(in.3)	piece	40 lb.	45 lb.	50 lb.	
1	x	2	2	.67	1/6	.56	.63	.70	
1	x	3	3	1.50	1/4	.83	.94	1.04	
1	x	4	4	2.67	1/3	1.11	1.25	1.39	
1	x	6	6	6.00	1/2	1.67	1.88	2.08	
1	x	8	8	10.67	2/3	2.22	2.50	2.78	
1	x	10	10	16.67	5%	2.78	3.12	3.47	
1	x	12	12	24.00	1	3.33	3.75	4.17	
1	x	14	14	32.67	11/6	3.89	4.38	4.85	
1	x	16	16	42.67	1 1/3	4.44	5.00	5.55	
1	x	18	18	54.00	11/2	5.00	5.62	6.25	
					• -				

All properties shown are directly proportional to width b.

To obtain properties for timbers other than 1 inch wide, multiply properties in table by actual width.

TABLE LXII. Breaking strength of 6 x 19 wire rope.

Size (inches) 1/4	3/8	1/2	5/8	3⁄4	7/8	1	11/8	11/4	11/2
Approximate weight per 100 feet (pounds)	23	40	63	90	123	160	203	250	360
GRADE		BREA	KING	STRE	NGTH	(U. S.	TONS)	1	
Iron	2.1	3.6	5.5	7.9	10.6	13.7	17.2	21.0	29.7
Traction steel	4.0	6.8	10.4	14.8	20.0	26.0	32.7	40.6	56.6
Cast steel 2.1	4.5	7.7	11.8	16.8	22.8	29.5	37.0	46.0	65.0
Mild plow steel	5.0	8.5	13.1	18.7	25.4	33.0	41.5	51.0	72.5
Plow steel 2.5	5.5	9.4	14.4	20.6	28.0	36.5	46.0	56.5	80.5
Improved plow steel 2.9	6.3	10.8	16.6	23.7	32.2	42.0	53.0	65.0	92.5

6 x 19 wire rope means 6 strands of 19 wires each.

The strength varies slightly with the strand construction and number of strands.

The maximum allowable working load is the breaking strength divided by the appropriate factor of safety. (See table LXIII.)

TABLE LXIII. Wire-rope safety factors.

Type of service	Minimum safety factor	Type of service	Minimum safety factor
Track cables	3.0	Haulage ropes	6.0
Guys	3.5	Derricks	6.0
Miscellaneous hoisting equipment	5.0	Slings	8.0

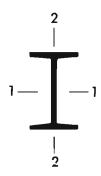


TABLE LX1. Properties of steel beams.

		AME	RICAN WID	E-FLANGE	BEAMS.		
Depth of	Weight per	Area of	Fla	nge	Web	Section	modulus
section (in.)	foot (lb.)	section (sq. in.)	Width (in.)	Thickness (in.)	thickness (in.)	Axis 1-1 (in.3)	Axis 2-2 (in.*)
36.72	300	88.17	16.655	1.680	.945	1105.1	147.1
35.88	230	67.73	16.475	1.260	.765	835.5	105.7
35.84	150	44.16	11.972	.940	.625	502.9	41.8
33.00	200	58.79	15.750	1.150	.715	669.6	87.8
33.15	132	38.84	11.510	.880	.580	413.7	36.1
33.00	125	36.78	11.500	.805	.570	385.1	32.7
29.82	108	31.77	10.484	.760	.548	299.2	25.8
27.00	98	28.82	10.000	.792	.500	255.3	24.6
26.84	91	26.77	9.983	.712	.483	233.2	21.8
24.16	87	25.58	9.025	.807	.480	204.3	20.6
23.87	74	21.77	8.975	.662	.430	170.4	16.5
21.00	63	18.52	8.25	.620	.410	128.0	13.0
20.91	59	17.36	8.230	.575	.390	119.3	12.0
18.16	77	22.63	8.787	.831	.475	141.7	20.2
17.90	47	13.81	7.492	.520	.350	82.3	9.0
16.16	88	25.87	11.502	.795	.504	151.3	32.2
15.86	58	17.04	8.464	.645	.407	94.1	14.3
16.12	45	13.24	7.039	.563	.346	72.4	8.7
15.85	36	10.59	6.992	.428	.299	56.3	6.3
14.19	74	21.76	10.072	.783	.450	112.3	26.5
13.91	61	17.94	10.000	.643	.378	92.2	21.5
13.81	48	14.11	8.031	.593	.339	70.2	12.8
13.86	30	8.81	6.733	.383	.270	41.8	5.2
12.12	65	19.11	12.000	.606	.390	88.0	29.1
12.00	28	8.23	6.500	.420	.240	35.6	5.4
11.87	25	7.39	6.500	.355	.240	30.9	4.5
11.78	5 3	15.59	12.046	.437	.436	67.0	21.2
10.00	49	14.40	10.000	.558	.340	54.6	18.6
10.12	45	13.24	8.022	.618	.350	49.1	13.3
9.90	21	6.19	5.750	.340	.240	21.5	3.4
7.93	24	7.06	6.500	.398	.245	20.8	5.6
6.00	15.5	4.59	6.000	.269	.240	10.0	3.06
	BRITIS	H BEAMS	(EQUIVAL	ENT TO A	MERICAN	BEAMS)	
24	95	27.94	7.5	1.011	.57	211.09	16.68
18	- 75	22.09	7.0	.928	.55	127.91	13.30
20	65	19.12	6.5	.820	.45	122.62	10.02
18	55	16.18	6.0	.757	.42	93.53	7.88
15	42	12.36	5.0	.647	.42	57.13	4.72
12	32	9.40	5.0	.550	.35	36.84	3.88

TABLE LXIV. Properties of commercial sisal cordage.

Diameter (inches)	Circumference (inches)	Weight per 100 feet (pounds)	Minimum breaking strength tons	Safe load capacity tons
1/4	3/4	1.71	0.22	0.06
3/8	11/8	3.45	0.51	0.13
1/2	11/2	7.36	1.06	0.26
5/8	2	13.10	1.76	0.44
3/4	21/4	16.40	2.16	0.54
7/8	23/4	22.00	3.08	0.77
1	3	26.50	3.60	0.90
1 1/8	31/2	35.20	4.80	1.20
1 1/4	33⁄4	40.80	5.40	1.35
11/2	41/2	58.80	7.40	1.85
13/4	51/2	87.70	10.60	2.65
2	6	105.00	12.40	3.10
21/2	71/2	163.00	18.60	4.65
3	9	237.00	25.60	6.40

For quality manila, the factors for minimum breaking strength and safe load capacity may be increased 25 percent. Safe-load-capacity factors are based on a factor of safety of 4.

LABLE LAV. Properties of chains.

wormal	Approx. wt.		Safe working lo		
size ¹ (inches)	per 100 feet (pounds)	Common iron	High grade iron	Soft steel	Special steel
3/8	160	2,700	2,980	3,300	6,400
7/16	210	3,460	3,800	4,360	8,300
1/2	280	4,500	4,960	5,260	*
5/8	430	6,940	7,620	8,460	10,500
3/4	630	10,140	11,160	12,000	15,200
7/8	840	14,000	15,400	16,500	21,000
1	1,100	18,600	20,460	21,200	28,660 36,400

¹ Normal size means diameter of the bar from which the chain is formed.

TABLE LXVII. Relation of sheaves and wire-rope diameter.

Type of wire rope (strands by wires)	Recommended sheave and drum diameter	Minimum sheave and drum diameter
6 by 7	72 x rope diameter	42 x rope diameter.
6 by 19	45 x rope diameter	30 x rope diameter.
6 by 37	27 x rope diameter	18 x rope diameter.
8 by 19	31 x rope diameter	21 x rope diameter.

 $\it Note.$ These limits do not apply to blocks for wire rope tackle with loads in accordance with table LXX.

TABLE LXVIII. Lead-line pull factors and efficiencies for hoist or fall wire rope.

Number of parts of rope 2	3	4	5	6	7	8	9	10
Efficiency, percent96.1	92.4	88.9	86.5	82.2	79.0	76.0	73.0	70.3
Lead-line pull factor0.52	0.36	0.28	0.23	0.20	0.18	0.165	0.15	0.14

Note. The stress in the lead line equals the load to be lifted multiplied by the lead-line pull factor.



TABLE LXVI. Safe loads on hooks.

Diameter of metal	Inside diamete of eye		Safe load
A (inches)	B (inches)	C (inches)	(pounds)
5⁄8	3⁄4	1	1,000
1½16	7/8	11/16	1,200
3/4	1	11/8	1,400
7⁄8	11/8	11/4	2,400
1	11/4	13/8	3,400
1 1/8	13/8	11/2	4,200
11/4	11/2	111/16	5,000
13/8	15/8	17/8	6,000
11/2	13/4	2½ ₁₆	8,000
1.5/8	2	21/4	9,400
17/8	23/8	21/2	11,000
21/4	23/4	3	13,600
25/8	31/8	33/8	17,000
3	31/2	4	24,000
SINGLE	DOUBLE	DOUBLE	TRIPLE
1/1	. /1/1		$\sqrt{2}\left \int_{-1}^{1}\right 3$
SINGLE	SINGLE D	DOUBLE DOUBLE	TRIPLE D

TABLE LXIX. Simple block-and-tackle rigging for manila rope (factor of safety 3)

Load to be lifted (tons)	Total number of sheaves in blocks	2 (2-single blocks)	3 (1-single 1-double)		5 (1-double 1-triple)	
1/2	Smallest permissible rope diameter (inch)	1/2	⅓ 16	3⁄8	3/8	3/8
	Lead-line pull (lb.)	540	380	300	250	220
1	Rope(inch)	3/4	5⁄8	1/2	1/2	1/2
	Pull	1,100	760	600	500	440
11/2	Rope(inch)	7/8	3⁄4	5/8	5/8	1/2
	Pull	1,600	1,100	900	750	660
2	Rope(inches)	11/8	7/8	3/4	5/8	5∕8
	Pull	2,200	1,500	1,200	1,000	880
3	Rope(inches)	15/16	11/8	1	7/8	3/4
	Pull	3,300	2,300	1,800	1,500	1,300
4	Rope(inches)	11/2	11/4	11/8	1	1
	Pull	4,400	3,000	2,400	2,000	1,800
6	Rope(inches)	•	11/2	15/16	11/4	1 1/8
	Puli		4,500	3,600	3,000	2,600
8	Rope(inches)			15/8	11/2	15/16
	Pull			4,800	4,000	3,500

TABLE LXX. Simple block and tackle rigging for plow-steel wire rope (factor of safety 6)

Load to be lifted (tons)	Total number of sheaves in blocks	2 (2-single blocks)	3 (1-single 1-double)	4 (2-double blocks)	5 (1-double 1-triple)	6 (2-triple blocks)
1	Smallest permissible rope diam-					
	eter (inch)	3/8	3/8	3/8	3/8	3/8
	Lead-line pull (lbs.)	1,000	720	560	460	400
2	Rope(inch)	1/2	3/8	3/8	3/8	3/8
	Pull	2,100	1,400	1,100	920	800
4	Rope(inch)	5/8	1/2	1/2	3/8	3/8
	Pull	4,200	2,900	2,200	1,800	1,600
6	Rope(inch)	3/4	5/8	5/8	1/2	1/2
	Pull	6,200	4,300	3,400	2,800	2,400
8	Rope(inch)	7/8	3/4	5/8	5/8	5/8
	Pull	8,300	5,800	4,500	3,700	3,200
10	Rope(inch)	1	7/8	3/4	5/8	5/8
	Pull	10,400	7,200	5,600	4,600	4,000
15	Rope(inch)	11/8	1	7/8	3/4	3/4
	Pull	15,600	10,800	8,400	6,900	6,000
20	Rope(inches)	11/2	11/8	1	7∕8	7/8
	Pull	20,800	14,400	11,200	9,200	8,000

Table LXXI. Sling load chart

Load chart of sling stress at various angles of inclination with a load of 1,000 pounds	Total sling stress (lb)	Angle (degrees)
		0
5	11,473	5
10	5,759	10
15°	3,863	15
25°	2,924	20
30	2,366	25
35°	2,000	30
45°	1,743	35
55.50	1,555	40
70 65 60 60	1,414	45
90° 85° 80 75 70	1,305	50
	1,220	55
	1,154	60
	1,103	65
	1,064	70
	1,035	75
	1,015	80
	1,003	85
	1,000	90

Stress in each leg of a sling assembly is found by dividing the total sling stress by the number of legs. If the load is over or under 1,000 pounds, divide the load by 1,000 and multiply by the total sling stress found in the table for the corresponding angle.

TABLE LXXII. Holding power of deadmen in ordinary earth.

Mean depth of	Inc	lination of pull safe resistance i	(vertical to bor n pounds per squ	izontal) and are foot.	
anchorage (feet)	Vertical	1/1	1/2	1/3	1/4
3	600	950	1,300	1,450	1,500
4	1,050	1,750	2,200	2,600	2,700
5	1,700	2,800	3,600	4,000	4,100
6	2,400	3,800	5,100	5,800	6,000
7	3,200	5,100	7,000	8,000	8,400

Formula for dimensioning deadmen:

$$T = \frac{2667 \text{bh}^2}{L} \text{for a rectangular timber}$$

or

$$T = \frac{1600 \mathrm{d}^3}{L}$$
 for a round timber.....where

Symbols:

T = Maximum allowable cable pull in pounds

b = Width of the contact face of the deadman in inches

h = depth of deadman in direction of pull in inches

d = diameter of round timber in inches

L = Length of deadman in inches

TABLE LXXIII. Safe capacity of spruce timbers as gin poles in normal operations.

Size of timber (inches)			-	ity (pounds) h in feet		
(inches)	20	25	30	40	50	60
6 diameter	5,000	3,000	2,000			
8 diameter		11,000	8,000	5,000	3,000	
10 diameter	31,000	24,000	16,000	9,000	6,000	
12 diameter			31,000	19,000	12,000	9,000
6 x 6	6,000	4,000	3,000		•••••	
8 x 8		14,000	10,000	6,000	4,000	
10 x 10	40,000	30,000	20,000	12,000	. 8,000	
12 x 12			40,000	24,000	16,000	12,000

Safe capacity of each leg of shears or tripod is seven-eighths of value given.

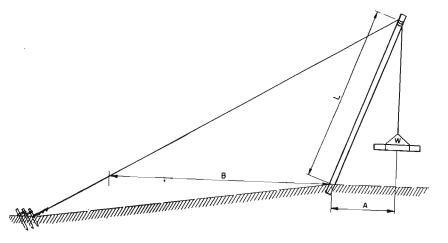


TABLE LXXIV. Stresses in guys and spars used as gin poles.

W = Weight to be lifted. (Include ample allowance for jars and jerks)

A = Drift

B = Horizontal distance from base of pole to guy.

L = Length of gin pole

Stress in guy for W = 1000 lb.

Stress in spar for W = 1000 lb.

0 1 L 10 1 L	1 L 0 230	3 L 0 180	L 0 150	$1\frac{1}{2}L$ 0 130	2 L 0 · 120	B 1 L A 2 0 1,000 1 L 1,210 10 1 L 1,260	,	L 1,000 1,100	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 L 1,000 1,050
8 1 L 6 1 L	400 630	300 480	260 410	220 350	200 320	8 1 L 1,350			1,130 1,210	1,100 1,160
4 1 L 3	890	680	580	480	440	4 1 L 1,770 3	1,530	1,420	1,300	1,240

Table LXXV. Standard bolt dimensions.

	A	rea			-	Heads					Nuts		
Diameter Total D			Number of threads	Hex	agon		Squ	ıare	Hex	agon		Sq	uare
Inches	Gross Dia. D. Sq. in.	Net Dia. K. Sq. In.	per inch	Diamer	er (in.)	Height (inches)	Diamet	er (in.)	Diamet	er (in.)	Height (inches)	Diame	ter (in.)
	3q. m.	5q. 1u.		Long	Short		Long	Short	Long	Short		Long	Short
1/4 3/8 1/2 5/8 3/4 7/8 1 1/8 1/4	.049 .110 .196 .307 .442 .601 .785 .994 1.227	.027 .068 .126 .202 .302 .419 .551 .693	20 16 13 11 10 9 8 7	76 58 78 176 156 156 1176 218	3/8 9/16 3/4 13/16 11/8 11/2 11/16 17/8	%6 4 6 6 7 6 8 7 6 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8 8 7 6 8	1/2 3/4 1 15/16 19/16 11/3/16 21/16 25/16 29/16	3/8 9/16 3/4 13/16 11/8 11/6 11/6 11/6	1/2 11/6 15/6 1/8 1/8 1/9 11/2 111/6 115/6	7/6 5/8 13/6 1 11/8 15/6 11/2 111/6	14 5/6 1/6 9/6 11/16 3/4 1/8	5/8 7/8 11/8 13/6 19/6 11/3/6 22/6 25/6	7/6 5/8 13/6 1 11/8 15/6 11/2 111/6 17/8

TABLE LXXVI. Weights of bolts with square heads and nuts-pounds per 100 bolts.

Length of bolt under head				Diamet	er of bolts	s in inches	;		
(inches)	1/4	3/8	1/2	5/8	3⁄4	3∕8	1	1 1/8	1 3/4
2	4.3	10.8	21.8	38	57	86	122	165	221
2½	5.0	12.3	24.6	42	63	95	133	179	238
3	5.7	13.9	27.4	46	70	103	144	194	255
3½	6.4	15.5	30.2	51	76	112	155	208	273
4	7.1	17.0	33.0	55	82	120	166	222	290
4½	7.8	18.6	35.8	59	88	129	177	236	307
5	8.5	20.2	38.5	64	95	137	188	250	325
6	9.9	23.3	44.1	72	107	154	211	278	360
7	11.3	26.4	49.7	81	120	171	233	306	394
8	12.7	29.6	55.2	90	132	188	255	334	429
10		35.8	66.4	107	157	222	300	391	499
12	*******	42.1	77.5	125	182	256	344	447	568
14			88.6	142	207	290	389	503	638
16			99.8	159	232	325	433	560	707
18			111.0	176	257	359	477	616	777
20	•		122.2	194	282	393	522	672	847
Per inch addi-									
tional	1.4	3.1	5.6	8.7	12.5	17.0	22.3	28.2	34.8

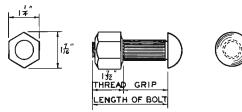
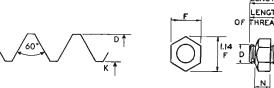


Table LXXVII. Principal dimensions and weights of 1/8-inch structural ribbed bolts

Grij	,	Length of	Weight	Total thickness
No.	G (inches)	L (inches)	with nut (pounds)	of work (inches)
1	15/22 21/22 21/22 21/22 11/22 11/25 11/25 11/25 12/22 21/22 21/22 22/23/22	111/6 17/8 21/16 21/4 22/6 20/8 218/6 33/16 33/16 33/16 33/16	0.88 .91 .94 .97 1.00 1.03 1.06 1.09 1.12 1.15 1.18	38 to 1/2 9/6 to 1/6 34 to 7/8 15/6 to 1/6 11/6 to 1/4 11/6 to 1/4 11/6 to 1/5/6 11/6 to 1/3/6 11/6 to 23/6 21/4 to 23/6 21/4 to 23/6 25/6 to 23/6
14	$\frac{2^{29}_{32}}{2^{29}_{32}}$ $\frac{3^{8}_{32}}{3^{8}_{32}}$	41/8 45/6	1.27 1.30	2 ¹³ / ₁₆ to 2 ¹⁵ / ₁₆ 3 to 3 ¹ / ₈





Grip—inches	1/2	3/4	1	11/4	11/2	15/8	13/4	2	21/4	21/2	23/4	3
Undriven length—inches	2	21/4	21/2	23/4	3	31/4	31/2	33/4	4	41/4	41/2	5
Weight per 100 pounds	58	62	67	71	75	79	84	88	92	96	101	109

TABLE LXXIX. Sizes of wire nails and spikes.

TABLE LXXX. Allowable compressive stresses for masonry.

	Size	Length (inches)	Number per pound	Size	Length (inches)	Number per pound	Material	Allowable compressive
2-d 3-d 4-d 5-d 6-d 7-d 8-d 9-d		1 1½ 1½ 1½ 1¾ 2 2¼ 2½ 2¾ 2½ 2¾	900 615 322 250 200 154 106 85	12-d	3½ 3½ 4 4½ 5 5½ 6	57 46 29 23 17 13½ 10½	Coursed rubble—Portland-cement mortar Ordinary rubble—Portland-cement mortar Coursed rubble—Lime mortar Ordinary rubble—Lime mortar First-class granite masonry—Portland-cement mortar First-class Limestone masonry—Portland-cement mortar First-class sandstone masonry—Portland-cement mortar Selected, hard, common brick masonry—Portland-cement mortar	250 200 150 60 800 500
10-d		3	74	¾"	10	3	Common brick masonry—Lime mortar Common brick masonry—Portland-cement mortar Paving brick masonry—Portland-cement mortar	100

TABLE LXXXI. Properties of pneumatic tools.

Tool	Weight (lb.)	Air consumption (cfm)	Remarks											
Backfill tamper	. 32	30	•											
Clay digger	. 19	35												
Chipping hammer		29	3-inch stroke, heavy duty.			•	TABLE L	XXXIV.	Metri	c conver	sion tabl	es.		
Concrete vibrator	. 24	28												
Drill, steel	. 35	93						METI	ERS TO	FEET				
Drill, rock		86	55-pound class.	Meters	0	1	2	3	4	5	6	7	8	9
Grinder	. 17	58	Rotary portable.			3.28	6.56	9.84	13.12	16,40	19.68	22.97	26.25	29.53
Hammer, pneumatic or				10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.77	59.06	62.34
steam, pile-driver	5.000	450		20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.86	95.14
Hammer, pneumatic or	- ,,			30	98.42 131.23	101.71	104.99	108.27	111.55	114.83	118,11	121.39	124.67	127.95
steam, pile-driver	7.000	600		40 50	164.04	134.51 167.32	137.80 170.60	141.08 173.88	144.36	147.64	150.92	154.20	157.48	160.76
		160	1-ton single-drum, at 80 feet per minute lift	60	196.85	200.13	203.41	206.69	177.16 209.97	180.45 213.25	183.73 216.54	187.01 219.82	190.29 223.10	193.57 226.38
Hoist	. 310	100		70	229.66	232.94	236.22	239.50	242.78	246.06	249.34	252.62	255.90	259.19
TT-13		27.1	(should be run at lower speed).	80	262.47	265.75	269.03	272.31	275.59	278.87	282.15	285.43	288.71	291.99
Holder-on		Nil	Rivet set.	90	295.28	298.56	301.84	305.12	308.40	311.68	314.96	318.24	321.52	324.80
Nail driver		30												
Paving breaker	. 80	60	Provided with sheet-pile driving cap.					FEET	TO ME	TERS				
Pump, sump	. 29	80	2½-inch discharge, 175 gpm at 25-foot head.	Feet	0	1 0.305	2 0.610	3 0,914	4 1.219	5 1.524	6 1,829	7 2.134	8 2.438	9 2.743
Pump, sump	. 51	140	2½-inch discharge, 150 gpm at 100-foot	10	3.048	3.353	3.658	3.962	4.267	4.572	4.877	5.182	5.486	5.791
1, 1			head.	20	6.096	6.401	6.706	7.010	7.315	7.620	7.925	8.230	8.534	8.839
Riveting hammer	. 18	30	18-pound class.	30	9.144	9.449	9.754	10.058	10.363	10.668	10.973	11.278	11.582	11.887
Saw, chain		90	24-inch capacity.	40	12.192	12.497	12.802	13.106	13.411	13.716	14.021	14.326	14.630	14.935
Saw, circular		36	12-inch portable, 4-inch capacity.	50 60	15.240 18.288	15.545 18.593	15.850 18.898	16.154 19.202	16.459 19.507	16.764 19.812	17.069	17.374	17.678	17.983
Wood borer				70	21.336	21.641	21.946	22.250	22.555	22.860	20.117 23.165	20.422 23.470	20.726 23.774	21.031 24.079
	-	63	2-inch capacity.	80	24.384	24.689	24.994	25.298	25.603	25.908	26.213	26.518	26.822	27.127
Wrench, impact	. 27	38	3/4-inch to 11/4-inch capacity reversible.	90	27.432	27.737	28.042	28.346	28.651	28.956	29.261	29.566	29.870	30.175

Weight of tool and air consumption are approximate and will vary with make and model of tool. All tools operate at 80 to 90 psi.

														stics of truck-mounted cranes.				100					
IDENTIFICATION TRUCK-MOUNTED CRAN WITH ATTACHMENTS			HC		œ F	ENSI		Z	CAP CAP EXGE OF TI	RANE ACITY, EDING PPING		55 50 45 45 35 30 25 J	2/ 3/3/3/4/3/3/3/4/3/3/3/4/3/3/3/4/3/3/3/4/3	ATTACH DRAGLIN 20° CLAMSHE	E			AND DI	ROP H		SHC SHOVEL RATE	DVEL ED AT 45° I G A5° I	
SPECIFICATION TYPE	RATING	BASE FO	RADIUS TOO	TAIL- SWING	HEIGHT M		RIGGER S IR SIDE		P STANDARD MAX CENTER H15009	HOOK HEI	DWIT BOOM ANGLE XAM	W SINGLE	USE OF OUTRIGGERS	AT CLEAR DISTAN END OR SIDE S	CEKFROM UPPORT	EMPTY CLEAR WEIGHT WEIGHT WEIGHT WEIGHT	T. ~	X PILE LEADS CONTRACT	EIGHT OF L	MAXIMUM REACH 2000 LB PILE LENGTH GO A LAMAX A HAMMER GO CAT WALK CAT WALK	DIPPER MAXIMUM	DUMPING BANK	T DITCH S S S S S S S S S S S S S S S S S S S
1 2	3 4	5 6	7 8	9	10	11 12	13		15 16				21	2 23 24 25 26 27 28		31 32 33	34	35 36	37				47 48 49
	YD TON	IN FT F	T FT	FT					FT FT		0.		N	TON FT TON FT TON	FT TON TO	ON FT TO	l FT	FT LB	TON	FT FT FT F	T YD FT FT	FT FT	FT FT TON
SPECIFICATION T-1137A	*	196 8.5		8.0		(3) (4)	+	16.8	35.2AT			½ 3,0)	ND 5.5 10 12 3.25 17 2.39 DE 3.35 10 11 2.35 16 1.6	21 1.15 0	.4	+	20+10 1200	1.8	15 31 6 2	3 8 13.0	0 16.5	3.5 10.5
QUICKWAY E	1/8 5½	147 8.0 I	.8 4.7	8.2	11.2	2.3	1	13	35 2AT	5 36	77	½ 3.		ND 6.0 10 13 4.4 23 2.6	33 1.4 0	.5 8.3 .8	6.8	264 1200	1.4		3 3 20.0 13.	0 16.8 16.5	3.5 10.9 13.5
TRUCK SHOVEL ON COLEMAN TRUCK			+	+	- 4	1.0	2						DO OUTRIGGER	DE 2.5 10 11 2.5 21 1.0 ND 6.0 10 13 4.4 23 2.6	33 14		+ +		+	7 20	8	+	
OIT OCCUMENT THOUSE							5.0						DO	DE 6.0 10 9 4.5 19 2.0						16			
QUICKWAY E	8 62	198 8.4 1.	.8 5.2	8.2		3.4 4.0		17	35 2AT	36.5	77	₹ 3.	NO OUTRIGGE DO	ND 6.5 10 11 4.7 21 3.6 DE 4.2 10 11 3.0 21 1.5	31 1.5 0.	5 8.3 .8	6.8	264 1200	1.4		है 20.0 13.	0 16.8 17	2.9 11.5 17.5
TRUCK SHOVEL ON BROCKWAY TRUCK						4.5	5						OUTRIGGER	DE 4.2 10 11 3.0 21 1.5 ND 6.5 10 11 4.1 21 3.5	31 1.5	-+-	+ +		+	24		+	+
	, ,						6.0	_						DE 6.0 10 9 4.0 19 2.4	1					19			
MICHIGAN T-6-K	8 4 ₂	130 8.0 2	.3 5.0	5.8		4.0	+	11	30 5	32	75	ž 3.	NO OUTRIGGER	ND 4.5 10 10 3.1 16 2.0 DE 3.8 10 10 2.4 16 1.5		5 8.0 .8	6.8 2	20+10 1200	1.8	9	8 20.416.0	0 17.2 18.4	2.2 13.1 11.0
FOWER SHOVEL						5.0				-			OUTRIGGER	ND 8.8 10 9 5.0 15 3.0	25 1.8					16			1.
THEM CHOUSE MOT	3 10	175 8.0 2	2 = =	0.6	00.	5.0	(6.0)		40 10	43	0.7	5	DO NO OUTBIGGE	DE 7.3 10 8 4.2 14 2.5	19 1.8	0 100		37 2000	105	12	3 040 5	100000	5.0 15.5 00
THEW SHOVEL MC3	4 10	175 8.0 2	.5 5.5	0.8		4.0	+	<u> </u>	40 (10	42	0.3	8	D O	ND 10.3 10 10 5.8 20 3.0 DE 9.3 10 11 5.3 21 2.6		9 10.0	++	31 2000	2.5	17	4 24.2 15.4	20.8 21.2	5.2 15.5 22.0
							(7.0			1			OUTRIGGER	VD						20	1 1		
THEW SHOVEL MC4	3 10	175 8.0 2	3 6 5	9 9	0 9 1		(1.0		40 10	41	83	<u>ş</u>		D 12.2 10 10 8 7.0 18 3.9			1	20+15 1800	2.4	24	3 242 15 4	20 8 21 2	5.2 15.5 22.0
LORAIN	4 12	175 0.0 2.	.5 5.5	0.0		4.0			70 10	+	33	-	DO	DE 11.0 10 11 6.5 21 3.4			+ '	20.101000	2.7	19	4 272 13.4	20.021.2	5.2 15.5 22.0
							(7.0						OUTRIGGER	ID 15.5 10 8 10.1 18 5.9						33			
HARNISCHFEGER 255A	3 12	184 80 2	5 60	89	119 5			1 1	40 10	40	81		5 NO OUTRIGGE			9 10 8 1 5	982	20+15 1800	24	14 36.6 7.7 14	£ 262 15 5	217 215	60 47 260
HARNISUNFEGER 200A	4 12	104 0.0 2	0.0	0.3		4.0		1 7	. 0 .0	1,0	J.	3 7.	DO	E 10.0 10 11 7.2 21 3.6	36 2.0	10.0 1.0	3.0 2	.0.10 1000	2.7	22	4 202 10.0	21.1 21.0	0.0 14.7 20.0
						7.0	7.0						OUTRIGGER	D 18.0 10 8 12.2 18 5.8	3 3 3.2					31			
BAY CITY SHOVEL 18	3 137	194 8.0 2	.5 5.8	9.3 1	12.3	1	+		40 10	40	82	§ 5.	NO OUTRIGGER	ID 13.8 0 8 8.2 18 4.3	3 3 2 2 3 1	1 10.0 1.5	9.0 2	0+15 1800	2.4	23	£ 244 173	213 213	5.0 14.4 23.1
	4	0.0				1.0						0 3	DO	DE 10.0 10 11 5.2 21 2.5	36 1.4	1.5.5				16	4 27.7 17.3	21.3	0.0 14.4 25.1
						8.	o (7.0)						OUTRIGGER	D 16.5 10 7 13.0 17 5.9	32 3.4					32			
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NOTES

⁽⁾ LIFTING CAPACITIES INCLUDE WEIGHT OF HOOKS, BLOCKS, SLINGS, AND CHAINS; THEIR WEIGHT MUST BE ADDED TO LOAD HANDLED.

(2) WEIGHT OF DRAGLINE AND CLAMSHELL BUCKETS AND PILEDRIVING RIGS MUST BE CHECKED IN OPERATION.

(3) PILEDRIVING 10-AND 15-FOOT LEAD SECTIONS ARE USED INTERCHANGEABLY. SINGLE-LENGTH LEADS ARE NONSTANDARD, OF MANUFACTURERS' OWN DESIGN.

(4) ADAPTERS TO STANDARD PILEDRIVING LEADS ARE FURNISHED FOR QUICKWAY CRANES.

(5) OUTRIGGER DIMENSIONS MUST BE CHECKED IN THE FIELD.

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			CRAWLE	R BOOM	CL	.EARAI	NGE	\ -		воом	LIFTING			CRANE	LIF"	TING	CAPAC	TY I	FOR		AGLINE	CLA	MSHELL		AIN 3	S CAP	ACH LB PIL	RIG		RA	DIUS	HEIGHT	ᆜ ᇉ
	MODEL			FOOT	PiN			AR AC LAI	⊢ L8	ENGTHS	HEIGHT	RO	PE F	RATING							UCKET		CKET	DIMEN	ISIONS	ADS D C	E E	DIMENSI	SNC	CUTTI	NG	CUTTING	
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SPECIFICATION			LENG	AAE	ᄝᄼ	모	S R S		R R	SEN SEN	ĭ∑ ĕ	₹ ≯ ĕ	SIN	씸~~						AP.	DO EM	OL!	EMP.	LEADS	HAMMER	MME	A H	SE	CAT _	Z Z	되 의	8 E	2 X
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		SIZELOAD			R S	N	0 P	SIZE	1			DIAM					LOAD K			AD SIZE			≯ ⊺	X	SIZE	> I	К	YT			C D		E
1	2	3 4	5 6		8 9	10	11 12		14 1		17 18		20				26 27				32 3			37	38	39				4 45 4	6 47	48 49	50
₹YD SHOVE	1.6	YD TON	FILE	T FT 1	FT FT	FT	IN FT	WAII	TON F	: F t	[IN	TON	ON FT	FILIO	NIFI	TON F	TON	FILE	טאן אוכ	TON F	T YD	TON FT	FT	LB	TON	FΤ	FT FT	FT Y	D FT F	TIFT	FT FT F	T TON
SPEC T-1443	LS	1 3 0				105	13	750	T 7 7	^ E			1	ه جاری ما						1 5		3		OF TO 75	1000				1 1 9		100		51 . 75
AUSTIN - WESTERN	BADGER	8 2½ 3 3		3.0 I.0 3	7 FIXED	10.5		750	3 11 3	0 5	34.0 72	p 1	50	2.5 12.0 3.4 10.0	11 2	2.3 16	1.7 21	13	26 I	1 3	.4 8	3.0 §	.8 7.0	25 TO 35 0 20+10	1200	1.8	9			20.0	16.0	20.4 4.2	11.5 10
BAY CITY	20	3 4 ½		7.7 20 3	.8 7.0	9.8	13 2.3	750	10 3	0 5	31.0 75		6.6	4.5 10.0	10 2	.5 15	1.6 20	1.2	25 .	9 🖁		3.2 3	.8 8.0	25	1000	-1.0		26.0 5.0		20.5	4.5 17.3	8.8 4.0	13.3 11
LINK-BELT SPEEDER		à 4 ½	9.7		1.2 7.5						28.0 73	o 1/2		4.5 10.0	7 3	.4 10	2.5 15		21 1.	l š	.5 9	9.5 ਤੋਂ	.8 8.		1125	1.2	12		į			18.8 4.0	
½ YD SHOVE	LS																																
SPEC T-1443	п	½ 5	7.5			10.5		750	3	5 10				5.0 2.0						2	.9	1 2	1.2	25 TO 30					1	21.5	18.5	1	2.5 12.5-16
BUCYRUS - ERIE 4	15 B	1 6½		3.0 3.1 4	1.3 7.5	10.0	11 2.5	800	13 3		34.0 77			6.8 10.0		7 15	2.5 2.0	1.9	30 1.).0 ½	1.2 8.5		1800			31.0 8.0	2			20.0 5.7	
UNK-BELT SPEEDER OSGOOD (4)		½ 5½5 7 5	9.8 8		1.2 7.7 1.2 7.8		12 3.0 11 3.3						5.2 4.2	5.5 10.0 6.9 10.0	7 4	.1 10) 1.5	30 I.			3.7	1.2 75		1800	2.2	12	2.5 4.0	18 3			9.2 4.0 I 9.5 4.0 I	
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SPEC T-1061		3 7		30		11.0	12	1000	7	5 10		7	6.0	7.0 12.0			, , , , , , , , , , , , , , , , , , ,			3	12	3	15	25 TO 35	2500		$ \top$		3	24.0		Π.	14.0 18-20
	CLIPPER70	3 7	11.7 8	3.7 2.3 4	1.7 8.5		12 2.8				342 77	o 5		7.3 10.0	6 7	0 9	5.0 19	2.5	29 1.	8 3	.9 9	5 3	1.5 8.5		2000	-	3	3.5 7.0	18 3		5.1 20.3	21.1 5.9 1	15.3 17
KOEHRING	304-A	3 9		0.6 2.7 5	5.3 9.0		13 3.6	1000	19 3	5 5-10	350 80	o §	5.8	9,0 12.0	9 6	.6 14	4.5, 19	3.3	29 2.	2 3	1.0 io.		1.4 10.5	30	2200		15		3	27.3 1	7.8 23.1 2	2.9 6.9 1	16.6 21
HARNISCHFEGER P&H		3 82		9.8 2.5 4			10 3.0			0 10		0 5		8.5 12.0		.8 14	43 24	2.7	34 1.		.9 10.	0 1	1.5 9.0		2300			6.5 6.8	14		5.5 2 3.2 2		4.8 19
LIMA LOCOMOTIVE					1.0 9.2	10.4	13 3.0	1500	19 3	5 5	39.5 80	Ĭ 	5.9	2.6 10.0	p 10	0.0 14	4.6 19	1 3.4	[29] 2.	1 1	1.1 10.	.ɔ []	1.5 9.5	KO + 10	2500	2.5	18		4	: 27.5	04 24.4	21.6 7.1 1	<u>5.U 21</u>
SHOVELS I						1 1 2 1 1		T ===		ماد		<u> </u>	1001	20 :00		ا من ام	45 5	70	24 6		1 4 1 11	<u> </u>	101	200110	0500	0.5	07			loor!	7 07 01 3	4077	07 00
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												Т. П										.5 1½	2.2 12.0	20+15	2500			J. J					
KOEHRING	604-B	1 1 1		2.7 4.0		1 1								9.4 12.0		.2 18			ll		1.7 11.			. 10		Į.	33	\Box		33.0 2			9.9 47
THEW SHOVEL 4		2 30	14.1 1	4 3.1 5	5.5 12.0	12.1	10 2.9	1500	45 7	0 20	65.0 78	2 2	12.0 2	1.0 15.0	13 14	.0 23	8.0 43	4.0	63 2.	4 2	2.2 13	6 2	3.2 12.7		3000			5.5 8.7	23.0 2	33.1 22	28.0 2	7.1 8.3 1	7.5
NORTHWEST (4)	802 78 D	2 40		.4 3.6 5		12.3	9 3.5	1500	75 6	0 10~20	58 82	4	12.0 4	u9 12.0	13 14	5 23	10.7 38 8.5 43	5.8	63 2	D 2	2.4 13	6 2	3.4 12.7	20+15 <i>)</i> +10+10)	3000 3000		41 38 56	50 0 7				7.8 9.5 18 5.5 7.4 1	
BUCYRUS -ERIE		2 21					3.7	1500	63 8	0 20	80.0 78) 1	13.5 4	4.5 12.0	13 20	8 33	8.4 53	4.8	68 3.	5 22	2.8	2 2	3.5	· · · · (3000		50	0.5				8.8 9.0 1	
SPEC A S 1629		2 21						1500		0 20-30				1.0 15.0		1				2		2								32.0	28.0		6.0 56
																									_	_							_

- 1. LIFTING CAPACITIES INCLUDE WEIGHT OF HOOKS, BLOCKS, SLINGS AND CHAINS; THEIR WEIGHT MUST BE ADDED TO LOAD HANDLED.
 2. WEIGHT OF DRAGLINE-AND CLAMSHELL BUCKETS AND PILE-DRIVING RIGS MUST BE CHECKED IN OPERATION.
 3. PILE-DRIVING IO-AND 15-FOOT LEAD SECTIONS ARE USED INTERCHANGEABLY. SHORTER LEADS AND LIGHTER DROPHAMMERS MAY BE USED TO EXTEND REACH. SINGLE-LENGTH LEADS ARE NON-STANDARD, OF MANUFACTURERS OWN DESIGN.
- 4. ADAPTORS TO STANDARD PILE-DRIVING LEADS ARE FURNISHED FOR THIS SHOVEL.

 5. CAPACITIES FOR CRANE FURNISHED WITH EXTRA COUNTERWEIGHT; 1500 LB LS-50; 1100 LB OSGOOD; 4000 LB PAYMASTER 34.

				
LABLE	LXXXV.	Meiric	conversion	tables.

		K	ILOGRA	MS TO	POUNI	OS AVO	IRDUPO	IS			
Kg.	0	1	2	3	4	5	6	7	8	9	
		2.20	4.41	6.61	8.82	11.02	13.23	15.43	17.64	19.84	
10	22.05	24.25	26.46	28.66	30.86	33.07	35.27	37.48	39.68	41.89	
20	44.09	46.30	48.50	50.71	52.91	55.12	57.32	59.52	61.73	63.93	
30	66.14	68.34	70.55	72.75	74.96	77.16	79.37	81.57	83.78	85.98	
40	88.18	90.39	92.59	94.80	97.00	99.21	101.41	103.62	105.82	108.03	
50	110.23	112,44	114.64	116.84	119.05	121.25	123.46	125.66	127.87	130.07	
60	132.28	134.48	136.69	138.89	141.10	143.30	145.51	147.71	149.91	152.12	
70	154.32	156.53	158.73	160.94	163.35	165.35	167.55	169.76	171.96	174.17	
80	176.37	178.57	180.78	182.98	185.19	187.39	189.60	191.80	194.01	196,21	
90	198.42	200.62	202.83	205.03	207.23	209.44	211.64	213.85	216.05	218.26	
				*							
]	POUNDS	AVOIR	DUPOIS	то ки	LOGRAM	S			
Lbs.	0	1	2	3	4	5	6	7	8	9	
- •		0.4536	0.9072	1.361	1.814	2.268	2.722	3.175	3.629	4.082	
10	4.536	4.990	5.443	5.897	6.350	6:804	7.257	7.711	8.165	8.618	
20	9.072	9.525	9.979	10.433	10.886	11.340	11.793	12.247	12.701	13.154	
30	13.608	14.061	14.515	14.969	15.422	15.876	16.329	16.783	17.237	17.690	
40	18.144	18.597	19.051	19.504	19.958	20.412	20.865	21.319	21.772	22.226	
50	22,680	23.133	23.587	24.040	24.494	24.948	25,401	25.855	26.308	26.762	
60	27,216	27.669	28.123	28.576	29.030	29.484	29.937	30.391	30.844	31.298	
70	31.751	32.205	32.659	33.112	33.566	34.019	34.473	34.927	35.380	35.834	
80	36.287	36.741	37.195	37.648	38.102	38.555	39.009	39.463	39.916	40.370	
90	40.823	41.277	41.731	42.184	42.638	43.091	43.545	43.998	44.452	44.906	

Unit A			Unit B	Unit A			Unit B
Measure	to unit B	To convert to unit A multiply by:	Measure	Measure	To convert to unit B	to unit A	Measure
Length:					multiply by:	multiply by:	
Miles	5280	.0001894	Feet.	Foot-pound	.0000003766	2655403	Kilowatt hours.
Feet	.167	6	Fathoms.	Foot-pound	.13826	7.23300	Kilogram meters.
Feet	.0606	16.5	Rods.	Power:			
Feet	.0151	66	Chain.	Horsepower	550	.001818	Foot-pounds per second.
Feet	.0015	660	Furlongs.	Horsepower	.746	1.341	Kilowatts.
Fathoms	.0083	120	Cable lengths.	Horsepower U. S	1.0139	.98632	Horsepower, metric.
Miles	1.609	.6214	Kilometers.	Horsepower metric	75	.01333	Kilogram meters
Yards	.9144	1.0936	Meters.				per second.
Feet	.3048	3281	Meters.	Angles:			
Feet	.0003048	3281.0	Kilometers.	Degrees, angle	.01745	57.29578	Radians.
Inches	2.54	.3937	Centimeters.	Mils (circular)	.0562	17.78	Degrees, angular.
Miles	.868	1.1515	Nautical miles.	Mils (circular)	.008982	1.019	Radians.
Surface:	.008	1.1717	ivadicai iimes.	Shipping:			
Square miles	640	.001563	Acres.	Cubic feet	.010	100.0	Register tons.
· · · · · · · · · · · · · · · · · · ·	4840	.001303	Square yards.	Cubic feet	.0250	40.0	U. S. shipping tons.
Acres		.000207	Square feet.	Cubic feet	.0238	42.0	British shipping tons.
Acres			Square kilometers.	Weights-Avoirdupois or com	mercial weigh	t unless othe	
Square mile	2.59	.3861	Hectares.	Pounds	7000	.0001429	Grains.
Acres	.4047	2471		Ounce	437.5	.002286	Grains.
Acres	4046.9	.0002471	Square meter.	Ounce (Troy or	23112	.002200	O1411101
Square yard	.8361	1.1960	Square meter.	apothecaries' weight)	480	.002083	Grains.
Square yard	.008361	1196	Acres.	Pounds		2240	Long tons or gross tons.
Square feet	.0929	10.764	Square meter.	Net tons or short tons	POPPOOL	2240	Long tons of gross tons.
Square inch	6.452	.155	Square centimeter.	ton (U. S.)	.89286	1 12	Tong tong or group tong
Volume:				ton (0. 3.)	.89280	1.12	Long tons or gross tons.
Cubic feet	1728	.000579	Cubic inches.	Danie Ja	152/	2 205	(Br)
Cubic feet	7.481	.1337	U. S. gallons.	Pounds		2.205	Kilograms.
Cubic feet	6.229	.1605	Imperial gallons.	Ounce	28.35	.03527	Grams.
Cubic feet	.8036	1.2445	U. S. bushels.	Ounce (Troy or	24 402	02045	•
Cubic feet	12.	.0833	Board feet.	apothecaries' weight)	31.103	.03215	Grams.
Cubic feet	.007813	128	Cords of wood.	Grain		15.432	Grams.
Cubic inches	.5541	1.805	Fluid ounces (U. S.)	Tons, short		1.1023	Tons, metric.
U. S. gallons	.83251	1.2009	Imperial gallons.	Tons, short		.0011023	Kilograms.
U. S. gallons	.03175	31.5	Barrels.	Tons, long		.9842	Tons, metric.
Cubic yard	.7645	1.308	Cubic meters.	Pennyweight (Troy)			Grains.
Cubic feet	.02832	35.314	Cubic meters.	Hundredweight (long)			Pounds.
Cubic feet	28.317	.03531	Liters.	Stone			Pounds.
U. S. gallons	3.785	.2642	Liters.	Carat for diamonds	3.086	.3240	Grains (Troy).
U. S. quart	.946	1.0567	Liters.	Linear Weights:			
Cubic inch	16.38716	.061	Cubic centimeters.	Pounds per foot		.672	Kilograms per meter.
Pounds per cubic yard	.0593	16.856	Kilograms per hectoliter.	Pounds per yard	.496	2.016	Kilograms per meter.
Velocities:				Pressure:			
Miles per hour	1.467	.6818	Feet per second.	Atmospheres (mean)		.02950	Feet of water.
Feet per second	.3048	3.281	Meters per second.	Atmospheres (mean)		.0680	Pounds per square inch.
Miles per hour	.4470	2.237	Meters per second.	Atmospheres (mean)	29.92	.03342	Inches of mercury.
Miles per hour	1.609	.6214	Kilometers per hour.	Pounds per square inch		.4912	Inches of mercury.
Miles per hour	.8684	1.1516	Knots.	Feet of water	62.42	.01602	Pounds per square foot.
Flowing water:	.000 1	1.1710	ithous.	Kilograms per square			
Cubic feet per second				centimeter	14.22	.0703	Pounds per square inch.
(second feet)	60.0	01667	Cubic feet per minute.	Kilograms per square			A 4
	60.0	.01667	Cubic feet per minute.	meter	.2048	4.8824	Pounds per square foot.
Cubic feet per second	440.0	002222	II C sellene was esternis	Density	510		For odame took
(second feet)	448.8	.002228	U. S. gallons per minute.	Pounds per cubic foot	.0160	62.428	Grams per cubic
Cubic feet per minute	7.481	.1337	U. S. gallons per minute.	por value rootiii	.0100	04.140	centimeter (specific
Energy:	00		TO 1.11 PMI - TT 1.				gravity for solids).
Foot-pound	.001285	778.1 3087.77	British Thermal Unit. Kilogram calories.	Pounds per cubic foot	16.0184	.0624	Kilograms per cubic

TECHNICAL MANUAL 5-286 SEMIPERMANENT HIGHWAY AND RAILWAY TRESTLE BRIDGES

PART SIX — DRAWINGS

	TECHNICAL MAN	UAL 5-286	SHEET	UNIT OF CONSTRUCTION	IN ORMATION GIVEN	SFIEEI	UNIT OF CONSTRUCTION	IN ORMATION GIVEN
	SEMIPERMANENT HIGHWAY AND		26	Abutments for steel spans	Fabrication details and bill of materials for steel pile abutments	55	Steel towers for steel spans For double-lane class 50 and class 25 (15 to 76 feet high)	General views of 69- to 77-foot towers
	PART SIX — I	DRAWINGS	27	do	General views and bill of materials for concrete abutments	56	do	General views of 15- to 67-foot towers
	LIST OF DRA	WINGS	28	Timber pile bents for timber spans.	Bill of materials; general views of 1-	57	do	Bill of materials common to all towers
Grav	up 1. LIST OF DRAWINGS FOR SINGLE-LA	ANE CLASS 50 HIGHWAY BRIDGES	29	(1 to 28 feet high)	to 16-foot bents General views of 17- to 28-foot bents	58	do	Bill of materials which vary with tower height
Gioc	1) 1. LIST OF DEATHIROS TOX SITTOLE 1.		. 27	do	Ceneral views of 17- to 20-tool being			
SHEET	UNIT OF CONSTRUCTION	INFORMATION GIVEN	30	Timber pile piers for steel spans (1 to 13 feet high)	General views	59	do	Riveted construction: fabrication of cap beam, strut, and pin
1	All units	Index: Sets of drawings for units of construction	31	do	Bill of materials; details of piers sup- porting one steel and one timber span	60	do	Riveted construction: fabrication of columns
. 2	Timber spans (11 to 15 feet long)	General views	32	Steel pile bents and piers for steel	Riveted construction: general views	61	do	Riveted construction: fabrication of
3	do	Bill of materials		spans (1 to 20 feet high)				columns and struts
4	Steel spans (15 to 90 feet long)	General views	33	do	Riveted construction: bill of materials	62	do .	Fabrication of rod bracing
5	do	Bill of materials: steel for riveted con- struction; lumber and hardware for	34	do	Welded construction: general views	63	Steel towers, bents, and piers for steel spans	Details and bill of materials for shims under stringers of different depths;
		standard plank floor	35	do	Welded construction: bill of materials			superstructure anchor bolts
6	do	Bill of material: steel for welded con- struction; lumber and hardware for alternate laminated floor	36	Timber sill and pile foundations for timber towers	General views	64	Timber abutments for timber spans	General views of pile abutments; bill of materials for pile and grillage abut- ments
7	Timber towers for timber spans	General views	37	Concrete pedestals for timber towers	General views and bill of materials	65	do	General views of grillage abutments
	(15 to 76 feet high)		38	Concrete pedestals for steel towers	General views and bill of materials			
8	do	Bill of materials			for pedestals on ground	66	Abutments for steel spans	General views of timber pile abut- ments
9	Timber towers for steel spans (15 to 76 feet high)	Details and bill of materials for con- nection of spans to towers	39	do	General views and bill of materials for pedestals on piles	67	do	General views of timber grillage abutments
10	do	General views	40	Steel frame on steel pile foundations for steel towers	General views and bill of materials	68	do	Bill of materials for timber pile and grillage abutments
11	do	Bill of materials	41	Steel grillage foundations for steel towers	Bolted construction: general views and bill of materials	69	do	General views of steel pile abutments
12	Steel towers for steel spans (15 to 77 feet high)	General views of 69- to 77-foot towers	42	do	Welded construction: general views and bill of materials	70	do	Fabrication details and bill of mater-
13	do	General views of 15- to 67-foot towers	40	The second secon	General views and bill of materials	71	do	ials for steel pile abutments
14 .	do	Bill of materials common to all towers	43	Timber grillage foundations for timber towers	General views and bill of materials	71	do	General views and bill of materials for concrete abutments
15	do	Bill of materials which vary with tower height		Group 2. DOUBLE-LANE CLASS (Used also for class 80 si		72	Timber pile bents for timber spans (1 to 28 feet high)	Bill of materials; general views of 1- to 16-foot bents
16	do	Riveted construction: fabrication of	4.4	All	lades are of demoters for solve of	73	do	General views of 17- to 28-foot bents
		cap beam, strut, and pin Riveted construction: fabrication of	44	All units	Index: sets of drawings for units of construction	74	Timber pile piers for steel spans	General views
17	do	columns and struts	45	Timber spans (11 to 15 feet long)	General views		(1 to 13 feet high)	
18	do	Riveted construction: fabrication of columns	46	do	Bill of materials	75	do	Bill of materials; details of piers sup- porting one steel and one timber span
10	do	Fabrication of rod bracing	47	Steel spans (15 to 90 feet long)	General views	76	Steel pile bents and piers for	Riveted construction: general views of
19	ao	•	48	do	Bill of materials: steel for riveted con-		steel spans (1 to 20 feet high)	bents
20	Steel towers, bents and piers for steel spans	Details and bill of materials for shims under stringers of different depths; superstructure anchor bolts			struction; lumber and hardware for standard plank floor	77	do	Riveted construction: general views of piers
63	Timber abutments for timber spans	General views of pile abutments; bill	49	do	Bill of materials: steel for welded con- struction; lumber and hardware for	78	do	Riveted and welded construction: bill
21	timper appliments for timper spans	of materials for pile and grillage abut- ments			alternate laminated floor	79	do	of materials Welded construction: general views of
			50	Timber towers for timber spans	General views	,,	40	bents
22	do	General views of grillage abutments	51	(15 to 76 feet high)	Bill of materials	80	do	Welded construction: general views of piers
23	Abutments for steel spans	General views of timber pile abut- ments; bill of materials for timber pile	51			81	Timbor cill and pile foundations	•
		and timber grillage abutments	52	timber towers for steel spans (15 to 76 feet high)	Details and bill of materials for con- nection of spans to towers	01	Timber sill and pile foundations for timber towers	General views
24	do	General views of timber grillage abut- ments	53	do	General views	82	do	Additional views and bill of materials
25	do	General views of steel pile abutments	54	do	Bill of materials	83	Concrete pedestals for timber towers	General views and bill of materials

UNIT OF CONSTRUCTION

SHEET

INFORMATION GIVEN

SHEET

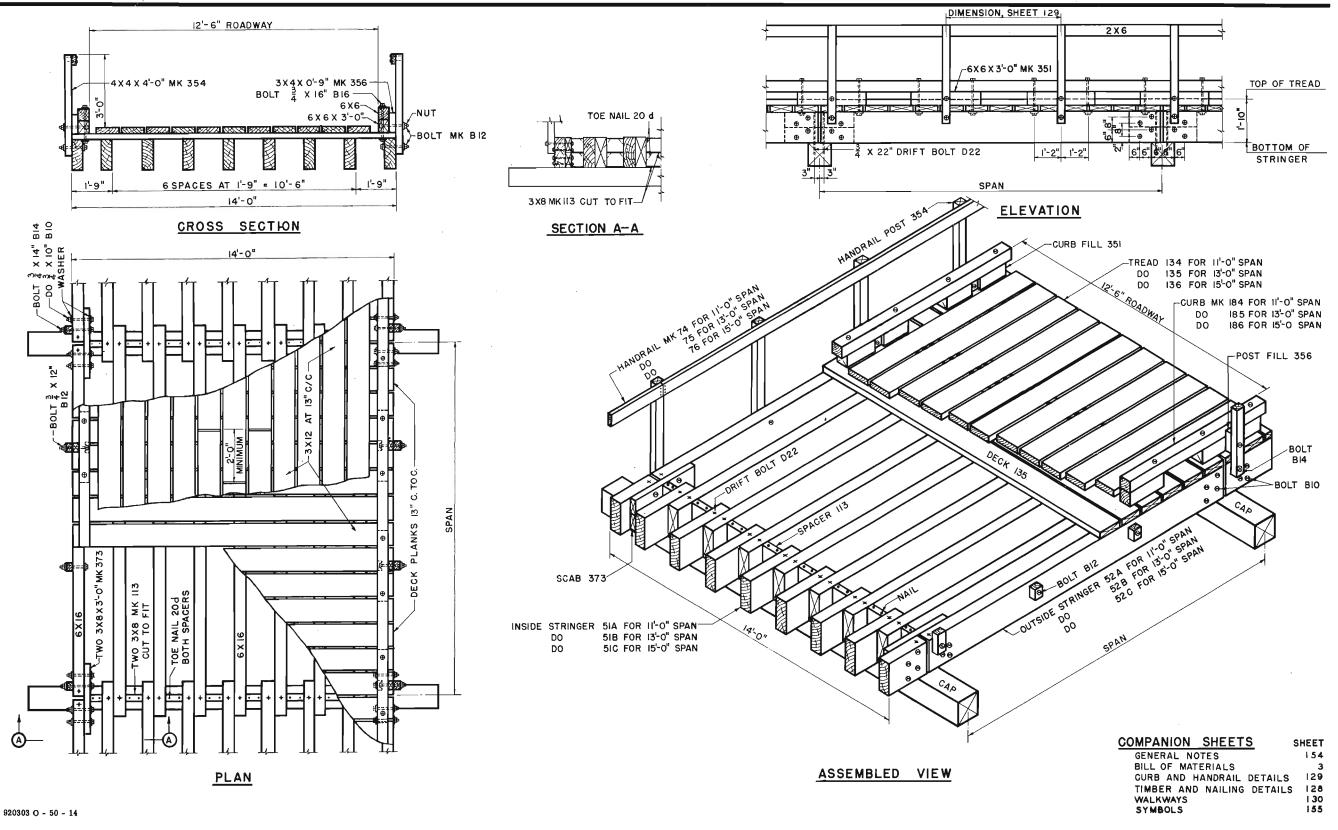
UNIT OF CONSTRUCTION

INFORMATION GIVEN

			CHEET	LINUT OF CONSTRUCTION	INFORMATION ONES	SHEET	UNIT OF CONSTRUCTION	INFORMATION GIVEN
SHEET	UNIT OF CONSTRUCTION	INFORMATION GIVEN	SHEET 108	UNIT OF CONSTRUCTION Abutments for steel spans	INFORMATION GIVEN General views of timber grillage abutments for 6-foot maximum fill	134	Steel spans	Riveted construction: fabrication of stringers 519 and 526
84	Concrete pedestals for steel towers	General views and bill of materials for pedestals on timber piles	109	do	General views of steel pile abutments	135	do	Riveted construction: fabrication of stringers 515 and 522
85	do	General views and bill of materials for pedestals on ground and on steel piles	110	do	Fabrication details and bill of materials for steel pile abutments	136	do	Riveted construction: fabrication of stringers 512 and 525
86	Steel frame on steel pile foundations for steel towers	General views and bill of materials	111	do	General views and bill of materials for concrete abutments	137	do	Riveted construction: fabrication of stringers 514, 517, and 518
87	Steel grillage foundations for steel towers	Bolted construction: general views and bill of materials	112	Timber pile bents for timber spans (1 to 28 feet high)	Bill of materials; general views of 1- to 16-foot bents	138	do	Riveted construction: fabrication of stringers 520 and 524
88	do	Welded construction: general views	113	do	General views of 17- to 28-foot bents	100	do	Welded construction: fabrication of
89	Timber grillage foundations for	and bill of materials General views	114	Timber pile piers for steel spans (1 to 13 feet high)	General views	139	do	stringers 501W to 511W and of dia- phragms C3 and C4
	timber towers	General views	115	do	Bill of materials; details of piers sup-	140	do	Welded construction: fabrication of stringers 512W and 525W
90	do	Additional views and bill of materials			porting one steel and one timber span			
			116	Steel pile bents and piers for steel spans (1 to 20 feet high)	Riveted construction: general views of bents	141	do	Welded construction: fabrication of stringers 513W, 522W, and 523W
	Group 3. DOUBLE LANE CLASS (See also sheets 55		117	do	Riveted construction: general views of piers	142	do	Welded construction: fabrication of stringers 514W, 515W, and 516W
91	All units	Index; sets of drawings for units of construction	118	do	Riveted and welded construction: bill of materials	143	do	Welded construction: fabrication of stringers 520W and 521W
92	Timber spans (11 to 15 feet long)	General views	119	do	Welded construction: general views of bents	144	do	Welded construction: fabrication of stringers 517W and 526W
93	do	Bill of materials	120	do	Welded construction: general views	145	do	Welded construction: fabrication of
94	Steel spans (15 to 90 feet long)	General views			of piers			stringers 518W, 519W, and 524W
95	do	Bill of materials: steel for riveted con- struction; lumber and hardware for	121	Timber sill and pile foundations for timber towers	General views	146	All timber towers	Details of bracing connections
		standard plank floor	122	Concrete pedestals for timber	General views and bill of materials	147	do	Details of bracing connections
96	do	Bill of materials: steel for welded con- struction; lumber and hardware for		towers		148	do	Details of bracing connections and of columns; column dimensions
		alternate laminated floor	123	Concrete pedestals for steel towers	General views and bill of materials	149	Timber towers for steel spans	Details of towers supporting both timber and steel spans
97	Timber towers for timber spans (15 to 76 feet high)	General views	124	Steel frame on steel pile foundations for steel towers	General views and bill of materials	150	Steel pile bents and piers for	Riveted construction: fabrication of
98	do	Bill of materials	125	Steel grillage foundations for	Bolted construction: general views and bill of materials		steel spans	cap beams, corbels, bracing, and con- nections
99	Timber towers for steel spans (15 to 76 feet high)	Details and bill of materials for con- nection of spans to towers	126	steel towers do	Welded construction: general views	151	do	Welded construction: fabrication of cap beams, corbels, and bearing
100	do	General views	. ~ 0		and bill of materials			plates
101	do	Bill of materials	127	Timber grillage foundations for timber towers	General views and bill of materials	152	Steel grillage foundations for steel towers	Bolted construction: fabrication of grillage beams
	Co. Live and for short among	Riveted construction: fabrication of				153	do	Welded construction: fabrication of
102	Steel towers for steel spans (15 to 77 feet high)	cap beam	Gro		LL CLASSES OF HIGHWAY BRIDGES			grillage beams
		to steel towers for double-lane class 25		(Sheets 154 and 155 also app	oly to railway bridges)	154	All units	General notes
	and class 50 steel spans.)		128	All spans	Details of floor construction and at- tachment of nailers to steel stringers	155	All units	Structural symbols
103	Steel towers, bents, and piers for steel spans	Details and bill of materials for shims under stringers of different depths; superstructure anchor bolts	129	do	Details of handrail and curb		Group 5. E-45 RAIL	WAY BRIDGES
104	Timber abutments for timber spans	General views of pile abutments; bill	130	do	General views and bill of materials for walkway	156	All units	Index: sets of drawings for units of construction
		of materials for pile and grillage abutments	131	Steel spans	Riveted construction: fabrication of	157	Timber spans (12 to 16 feet long)	General views and bill of materials
105	do	General views of grillage abutments			stringers 501 to 511 and of dia- phragms 527 and 528	158	Steel spans (15 to 50 feet long)	General views of 15- to 45-foot spans; assembly diagrams for riveted con-
106	Abutments for steel spans	General views of timber pile abut-	132	do	Riveted construction: fabrication of		(.5 10 00 100. 5119)	struction
		ments; bill of materials for timber pile and timber grillage abutments			stringers 516 and 521 and of bearing plates 3500 and 3501	159	do	General views of 50-foot span
107	ор	General views of timber grillage abutments for 3-foot maximum fill	133	do	Riveted construction: fabrication of stringers 513 and 523	160	do	Bill of materials: structural steel for riveted construction

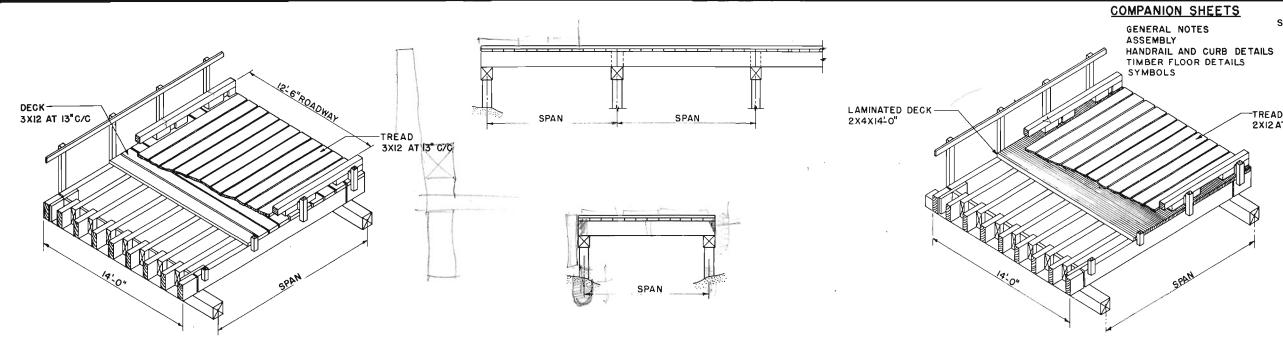
SHEET	unit of construction	INFORMATION GIVEN	SHEET 192	UNIT OF CONSTRUCTION Steel towers for steel spans (15 to 77 feet high)	INFORMATION GIVEN Details and bill of materials for shims under stringers of different depths;	SHEET 223	UNIT OF CONSTRUCTION Timber grillage foundations for timber towers	INFORMATION GIVEN General views
161	Steel spans (15 to 50 feet long)	Bill of materials: structural steel for welded construction, lumber, and deck hardware	193	Timber abutments for timber spans	superstructure anchor bolts General views of pile abutments; bill of materials for pile and grillage	224	do	Additional views and bill of materials
162	do	Riveted construction: fabrication of lateral braces	194	do	abutments General views of grillage abutments	225	Timber grillage foundations for timber towers	Additional views
163	do	Riveted construction: fabrication of stringers 401, 402, 403, and 420, and	195	Abutments for steel spans	General views of timber pile abut- ments		Group 6. ALTERNATIVE WELDED DE	TAILS FOR ALL STEEL TOWERS
164	do	of diaphragms Riveted construction: fabrication of stringers 404, 405, 406, and 407	196	do	Bill of materials for timber abutments; general views of timber grillage abut-	226	Steel towers for steel spans	Welded construction with rod bracing: cap beams and column splices welded in fabrication and erection
165	do	Riveted construction: fabrication of stringers 408, 409, 410, and 411	197	do	ments General views of steel pile abutments	227	do .	Welded construction with welded
166	do	Riveted construction: fabrication of stringers 412, 413, 418, and 419	198	do	Fabrication details and bill of materials for steel pile abutments			angle bracing: cap beams and column splices welded in fabrication and erec- tion
167	do	Riveted construction: fabrication of stringers 414, 415, 416, and 417	199	do	General views and bill of materials for concrete abutments		Group 7. SPECIAL EREC	TION FOLIPMENT
168	do	Welded construction: assembly dia- grams and fabrication of lateral braces	200	Timber pile bents for timber spans (1 to 28 feet high)	General views	228	Steel gin pole and outrigger for	General views
169	do	Welded construction: fabrication of	201	do	Additional views and bill of materials	•	erecting steel towers and stringers	
109	do	stringers 401W, 402W, 403W, and 420W, and of diaphragms	202	Timber pile piers for steel spans (1 to 11 feet high)	General views	229	do	Fabrication of gin pole
170	do	Welded construction: fabrication of	202	do	Bill of materials	230	do	Fabrication of outrigger
		stringers 404W, 405W, 406W, and 407W	203	do	bill of materials	231	do	Bill of materials; fabrication of outrig-
171	do	Welded construction: fabrication of	204	Steel pile bents and piers for steel spans (1 to 20 feet high)	Riveted construction: general views of bents	232	Timber derrick for erecting timber	ger General views
	,	stringers 408W, 409W, 410W, and 411W	205	do	Riveted construction: general views of piers	232	towers and steel stringers	ocheral views
172	do	Welded construction: fabrication of stringers 412W, 413W, 414W, and 415W	206	do	Riveted construction: fabrication of cap beams, corbels, and bracing con- nections	233	do	Bill of materials; stresses when mast and boom are used as gin poles for placing stringers
173	do	Welded construction: fabrication of stringers 416W, 417W, 418W, and 419W	207	do	Riveted construction: bill of materials	234	do	Fabrication of steel parts
174	Timber and steel spans	General views and bill of materials	208	do	Welded construction: bill of materials			
	·	for refuge bay and walkway General views	209	do	Welded construction: general views of bents	'	 ADAPTATION OF SUPPORTS TO S Supports for class 50 single-lane 	STANDARD PREFABRICATED BRIDGES Adaptation of timber towers to 30-
175	Timber towers for timber spans (15 to 76 feet high) do	Bill of materials	210	, do	Welded construction: general views of piers	235	semipermanent highway bridges (TM 5-285)	foot I-beam spans
176		Details for connection of spans to	211	do	Welded construction: fabrication of		,	Adaptation of pile piers and timber
177	Timber towers for steel spans (15 to 76 feet high)	towers			cap beams, corbels, and bracing connections	236	do	grillage abutments to 30-foot 1-beam
178	do	Details and bill of materials for con- nection of spans to towers	212	Timber sill and pile foundations for timber towers	General views and bill of materials	237	do	Adaptation of pile and concrete abut- ments to 30-foot 1-beam span
179	do	General views	213	do	General views			•
180	do	Bill of materials	214	Concrete pedestals for timber	General views and bill of materials	238	do	Adaptation of timber towers to 60- foot I-beam spans
181	All timber towers	Details of bracing connections		towers				·
182 183	do do	Details of bracing connections Details of bracing connections and of	215	Concrete pedestals for steel towers	General views and bill of materials for pedestals on timber piles	239	do	Adaptation of pile piers and timber grillage abutments to 60-foot I-beam span
184	Steel towers for steel spans	columns; column dimensions General views of 69- to 77-foot towers	216	do	General views and bill of materials for pedestals on ground and on steel piles	240	do	Adaptation of pile and concrete abut- ments to 60-foot I-beam span
	(15 to 77 feet high)		217	Steel frame on steel pile	General views and bill of materials			ments to oo-tool t-beam span
185	do	General views of 15- to 67-foot towers		foundations for steel towers		241•	do	Adaptation of timber towers to 90- foot truss span
186	do	Bill of materials common to all towers	218	Steel grillage foundations for	Bolted construction: general views			·
187	do	Bill of materials which vary with tower height		steel towers	and bill of materials for grillages \$101 and \$102	242	do	Adaptation of pile and concrete abut- ments to 90-foot truss span
188	do	Riveted construction: fabrication of cap beam, strut, and pin	219	do	Bolted construction: general views and bill of materials for grillage \$103	243	do	Adaptation of pile piers and timber grillage abutments to 90-foot truss
189	do	Riveted construction: fabrication of columns	220	do	Welded construction: general views			span
190	do	Riveted construction: fabrication of columns and struts	224		and bill of materials for grillage \$103 (\$101 and \$102 are similar)	244	Supports for Bailey-bridge spans up to 90 feet long (TM 5-277)	Adaptation of pile and concrete abut- ments, pile bents, and pile piers
191	do	Fabrication of rod bracing	221	do	Bolted construction: fabrication	245	Supports for H-10 and H-20 spans	Adaptation of pile and concrete abut-
171	ao	, application of four bracing	222	do	Welded construction: fabrication	~-0	up to 99 feet long	ments, pile bents, and pile piers

	SET NUMBER 50S-1		SET NUMBER 50S-5		SET NUMBER 50S-10
	TIMBER SPANS		STEEL TOWERS FOR STEEL SPANS		STEEL PILE BENTS AND PIERS FOR STEEL SPANS
SHEET	(11 to 15 feet long)	SHEET	(15 to 77 feet high)	SHEET	(1 to 20 feet high)
2	General views	12	General views of 69- to 77-foot towers	32	Riveted construction: general views
3	Bill of materials	13	General views of 15- to 67-foot towers	33	Riveted construction: bill of materials
128	Details of floor construction and attachment of nailers to steel stringers	14 15	Bill of materials common to all towers Bill of materials which vary with tower height	34 35	Welded construction: general viewa Welded construction: bill of materials
129	Details of handrail and curb	16	Riveted construction: fabrication of cap beam, strut, and pin	150	Riveted construction: fabrication of cap beams, corbels, bracing, and connec-
130 154	General views and bill of materials for walkway General notes	17	Riveted construction: fabrication of columns and struts		tions
155	Structural symbols	18	Riveted construction: fabrication of columns	151	Welded construction: fabrication of cap beams, corbels, and bearing plates
	,	19 20	Fabrication of rod bracing Details and bill of materials for shims under stringers of different depths; sup-	154 155	General notes Structural symbols
	SET NUMBER 50S-2	20	erstructure anchor bolts	133	
	3E1 140MBER 303-2	226	Welded construction with rod bracing: cap beams and column splices welded		SET NUMBER 50S-11
	STEEL SPANS	007	in fabrication and erection		TIMBER SILL AND PILE FOUNDATIONS FOR TIMBER TOWERS
	(15 to 90 feet long)	227	Welded construction with welded angle bracing: cap beams and column splices welded in fabrication and erection		THE POST OF THE PO
		154	General notes	36	General views
4	General views	155	Structural symbols	154	General notes
5	Bill of materials: steel for riveted construction; lumber and hardware for standard plank floor		NOTE: When welded construction is used in accordance with sheets 226	155	Structural symbols
6	Bill of materials: steel for welded construction; lumber and hardware for alter-		or 227, bills of materials on sheets 14 and 15 and fabrication details on sheets 16, 17, and 18 must be adjusted in the field.		SET NUMBER 50S-12
	nate laminated floor		When sheet 227 is used, sheet 19 does not apply.		SET NOMBER 303-12
128 129	Details of floor construction and attachment of nailers to steel stringers Details of handrail and curb				CONCRETE PEDESTALS FOR TIMBER TOWERS
130	General views and bill of materials for walkway		SET NUMBER 50S-6	37	General views and bill of materials
131	Riveted construction: fabrication of stringers 501 to 511 and of diaphragms		3E1 140/MBER 303-0	154	General notes
100	527 and 528 Riveted construction: fabrication of stringers 516 and 521 and of bearing plates		TIMBER ABUTMENTS FOR TIMBER SPANS	155	Structural symbols
132	3500 and 3501				SET NUMBER 50S-13
133	Riveted construction: fabrication of stringers 513 and 523	21	General views of pile abutments; bill of materials for pile and grillage abut-		
134	Riveted construction: fabrication of stringers 519 and 526	2.	ments		CONCRETE PEDESTALS FOR STEEL TOWERS
135	Riveted construction: fabrication of stringers 515 and 522 Riveted construction: fabrication of stringers 512 and 525	22	General views of grillage abutments		
136 137	Riveted construction: fabrication of stringers 512 and 523	154	General notes Structural symbols	38 39	General views and bill of materials for pedestals on ground General views and bill of materials for pedestals on piles
139	Welded construction: fabrication of stringers 501W to 511W, and of diaphragms	155	Structural symbols	12	General views and bill of indierials for peaestals on piles General views of 69- to 77-foot towers
1.40	C3 and C4			13	General views of 1,5- to 67-foot towers
140 141	Welded construction: fabrication of stringers 512W and 525W Welded construction: fabrication of stringers 513W, 522W, and 523W		SET NUMBER 50S-7	154	General notes
142	Welded construction: fabrication of stringers 514W, 515W, and 516W		ABUTMENTS FOR STEEL SPANS	155	Structural symbols
143	Welded construction: fabrication of stringers 520W and 521W		ABOTHER TO FOR OTELE OF ARO		
145 154	Welded construction: fabrication of stringers 518W, 519W, and 524W General notes	23	General views of timber pile abutments; bill of materials for timber pile and		SET NUMBER 50S-14
155	Structural symbols		timber grillage abutments		STEEL FRAME ON STEEL PILE FOUNDATIONS FOR STEEL TOWERS
	,	24	General views of timber grillage abutments		OTELL TRANSLE ON OTELL THE TOURDANDING FOR STELL TOWARD
	OFT NUMBER COC O	25 26	General views of steel pile abutments Fabrication details and bill of materials for steel pile abutments	40	General views and bill of materials
	SET NUMBER 50S-3	27	General views and bill of materials for concrete abutments	12	General views of 69- to 77-foot towers
	TIMBER TOWERS FOR TIMBER SPANS	154	General notes	13	General views of 15- to 67-foot towers
	(15 to 76 feet high)	155	Structural symbols	154 155	General notes
				133	Structural symbols
7	General views			•	
8	Bill of materials		SET NUMBER 50S-8		SET NUMBER 50S-15
146 147	Details of bracing connections Details of bracing connections		TIMBER PILE BENTS FOR TIMBER SPANS		STEEL GRILLAGE FOUNDATIONS FOR STEEL TOWERS
148	Details of bracing connections and of columns; column dimensions		(1 to 28 feet high)		OFFICE CONTENTS OF STEEL TO WERE
154	General notes		(41	Bolted construction: general views and bill of materials
155	Structural symbols	28	Bill of materials; general views of 1- to 16-foot bents	42	Welded construction: general views and bill of materials
	CET NUMBER FOR 4	29	General views of 17- to 28-foot bents	152	Bolted construction: fabrication of grillage beams
	SET NUMBER 50S-4	154	General notes	153 12	Welded construction: fabrication of grillage beams General views of 69- to 77-foot towers
	TIMBER TOWERS FOR STEEL SPANS	155	Structural symbols	13	General views of 15- to 67-foot towers
	(15 to 76 feet high)			154	General notes
			SET NUMBER 50S-9	155	Structural symbols
9	Details and bill of materials for connection of spans to towers General views		TIMBER PILE PIERS FOR STEEL SPANS		
10 11	General views Bill of materials		(1 to 13 feet high)		SET NUMBER 50S-16
146	Details of bracing connections	SHEET			TIMBER GRILLAGE FOUNDATIONS FOR TIMBER TOWERS
147	Details of bracing connections	20	Ganara viaws		SALES CALLET CONTONIONO FOR TIMBER TOTTERS
148 149	Details of bracing connections and of columns; column dimensions Details of towers supporting both timber and steel spans	30 31	General views Bill of materials; details of piers supporting one steel and one timber span	43	General views and bill of materials
154	General notes	154	General notes	154	General notes
155	Structural symbols	155	Structural symbols	155	Structural symbols



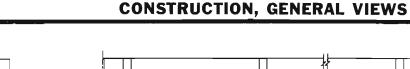
SHEET

TREAD 2XI2ATI3"C/C



					 		11'-0" 5	PAN	13'- 0" SPAN		15'-0"	SPAN
LINE	DESCRIPTION	STOCK NUMBER	SIZE (INCHES)	LENGTH	MARK	WE IGHT (PUUNOS)	QUANTITY	F.8.K.	QUANTITY	F.B.M.	QUANTITY	F.B.M.
_	LLIMBER SOFTWOXO						*******				1	
ı	STRINGER		6X16	16'0"	510	480					7	⊌96
. 2	DO		6X1ö	16'0"	52C	480					2	∠ 56
3	DO .		óΧΙό	14'0"	518	42C			7	784		
4	po		6X16	14.0	528	420			2	224		
5	DO:		6X16	12'6"	51A	360	7	572				
ó	DO		6X16	12'0"	52A	360	2 .	192				ĺ
7	SPACER	39-3330,00-1	3X8	16'0"	113	75	2	40	2	40	2	40
8	SCA8	35-3330-08	3x8	3'0"	373	.23	4	24	4	24	4	24
9	TREAD AND DECK	39-3330,12	3X12	14'0"	135	158	J 10	420	^ш 23	966	IJ <u>1</u> 4	588
10	TREAD	35-3330,12-16	3X12	16'0"	136	180					11	528
11	00	39-3952 12-12	3X12	12'0"	134	135	11	396				
12	CUR8	39-3360.06-16	6X6	16'0"	186	180					2	96
13	DO	39-3360.00-14	6x6	14'0"	185	158			2	84		
14	. 20	39-3360.06-12	6x6	12'0"	184	135	2	72				
15	CURB FILL	39-3560.06	6X6	3'0"	351	34	4	36	4	36	6	54
16	HANDRAIL POST	39-3340.04	4×4	4'0"	354	20	4	22	4	22	6	32
17	POST FILL	06-05روز-وو	3X4	015"	356	3	4	3	4	3	6	5
18.	HANDRA I L	880.06-16 880 عود	2x6	16'0"	76	60					2	32
19	DO	39-3880-06-14	2x6	14'0"	75	52			2	28	1	
20	no.	39-3880-06-12	2X6	12'0"	74	45	2	24			T	
	STEEL HARDWARE, BLACK							POULDS		PCUNDS		PUUNDS
-21	MACHINE BOLF WITH SQUARE NUT AND 2 WASHERS	45-2325-07-16	- 3/4	16*	B16	2.52	8	20	8	20	12	30
22	DO	43-2325.07-144	3/4	14"	814	2.27	2	5	2	5	2	5
23	DO	43-2525-07-124	3/4	12"	812	2.02	6	12	6	12	10	20
24	00	43-2325-07-1	3/4	10"	B10	1.77	14	25	14	25	14	25
25	DRIFT BOLT	43-1636 07-22	3/4	22"	022	3.00	18	54	18	54	18	54
26	WIRE SHIKE	42-6488-035-07	5/16	7^		. 15	90	23	108	27	126	52
27	WIRE NAME	42-6026, 3-5	50d			.10	150	19	180	23	215	27
	WIRE NAIL	42-6028 3-2	20 d			.05	24	1	24	1	32	1

							11,0, 2	JP4N	1310=	SPAN	15.0	SPAN
LINE	DESCRIPTION	STOCK NUMBER	SIZE (INCHES)	LENGTH	MARK	WEIGHT (POUNDS)	QUANTITY	F.B.M.	QUANTITY	F.B.M.	QUANTITY.	F.B.M.
	LUMBER, SOFTWOOD											
1	STRINGER		6X16	16'0"	51C	486					7	895
2	υc		6X16	16'0"	52C	480					2	256
٠.	DO:		6X16	14'0"	.51B	420			7	784		
4	DO		6X16	14'0"	52B	420			2	224		
5	DC		óX16	12'0"	51A	360	7	672				
6	DO		6X16	1210*	52A	360	2	192				
7	SPACEH (STRINGER)	39-3330, 08-1	3x8	10'0-	113	75	2	40	2	40	.2	40
8	SCAB	39-3330.68	3X8	3'0"	575	23	4	29	4	.24	4	24
9	DECK	59-5886.04-14	2x4	14'0"		35	82	765	96	895	1111	1037
10	TREAD	39-3228, 12-12	2x12	12'0"		90	11	396				
11	OC	39-3228. 12-14	2X12	14'0"		105			11	462		
14	DO	39-3228, 12-16	2X12	16'0"		120						
13	CURB	39-3300.06-12	6X6	15,0.	184	135	2	72			l n	526
14	00	39-3360, 06-14	6X6	1410=	185	158			-2	84		
15	1)0	39-3360, 06-16	δXċ	16'0"	186	180					2	96
16	CURB FILL	39-3360,06	6x6	3'0'	351		4	36	4	36	6	.54
17	HANDRAHL POST	39-3340,04-08	4X4	4'0"	354	20	4	22	4	22	6	32
18	POST FILL	08 ٥٥ درد -ود	3X4	0'0"	356	3	4	3	4	3	6	5
15	HANDRAIL	39-3880, 06-12	2X6	12'0"	74	45	.2	24				
20	00	35-3660.06-14	2X6	14'0"	75	52			.2	.28		
21	DO .	39-3880.06-16	2X6	16'0"	76	50					2	32
	STEEL HARDWARE, BLACK		-	'			•	POUNDS		POUNDS		POUND
22	MACHINE BOLT WITH SQUARE MIT AND 2 WASHERS	43-2325, 07-16	3/4	16"	B16	2.52	8	20	8	.20	12	30
23	DO DO	43-2325, 07-144	3/4	14"	814	2.27	2	5	2_	5	.2	5
24	00	45-2325-07-124	3/4	12"	B12	2.02	6	12	6	12	10	20
25	000	42-2325.07-1	3/4	10*	610	1.77	14	25	14	25	14	25
26	DRIFT BULF	43-1636-07-22	3/4	22"	DZZ	3.00	18	54	18	54	18	54
27	HIRE HAIL	42-6028. 3-2	20 d			.05	24		24		32	
28	WIRE NATE	42-6028.3-5	504			.10	143		165		187	



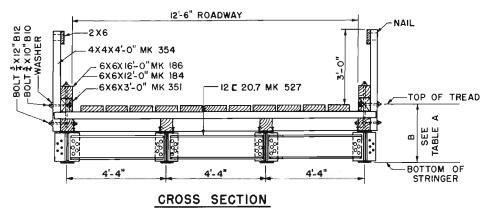
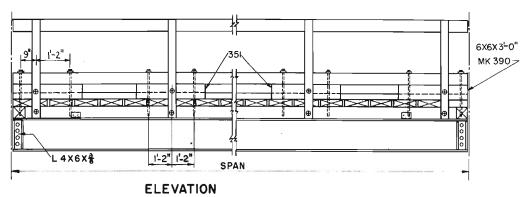
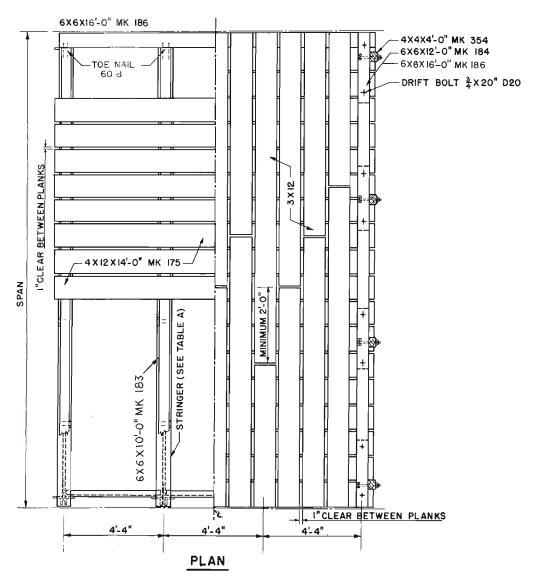
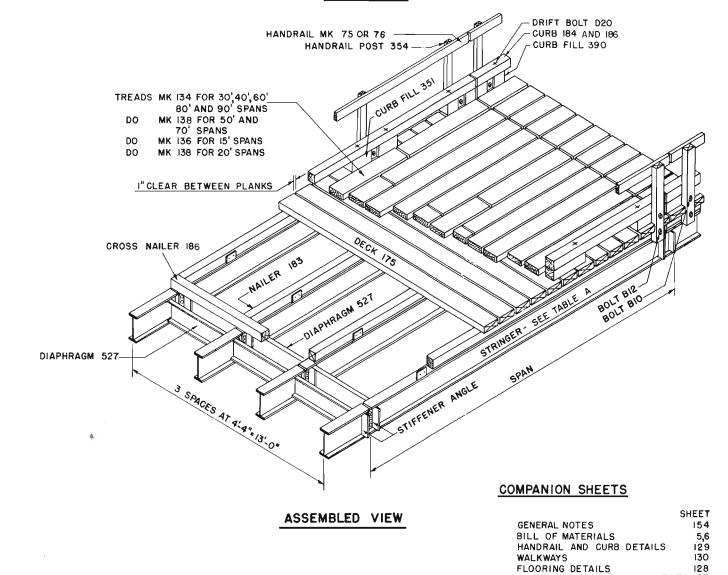


	TABLE A										
SPAN	STRINGER SIZE	МК	В								
15'-0"	16 I 36	502	2'-47"								
20'-0"	18 I 47	505	2'-67"								
30'-0"	24 1 74	510	3'-07"								
40'-0"	24 I 87	511	3'- 1"								
50'-0"	30 I 108	514	3'- 6 ⁷ / ₈ "								
60'-0"	33 I 125	517	3'-10"								
70'-0"	33 I 132	519	3'- 10 1 "								
80'-0"	36 I 150	523	4'-07"								
9ď-ď	36 I 182	525	4'-13"								







131 TO 145 155

WALKWAYS

SYMBOLS

FLOORING DETAILS

FABRICATION DRAWING

SUPERSTRUCTURE, 15- TO 90-FOOT STEEL SPANS

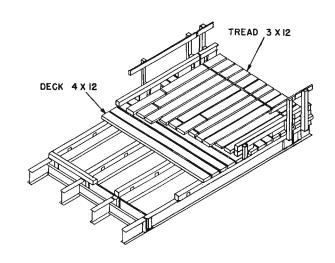
RIVETED CONSTRUCTION, SPANS, STANDARD PLANK FLOOR BILL OF MATERIALS

SHEET 5

				0000 L CMC																					
				SPAN LENG				5' I 36	20°		3C 24 I		24]		5C'		33.1	125	_	I 135	80		90	0' I 182	
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	1	UNIT WEIGHT (POUNDS)	QUANTITY		QUANTITY	FBM	QUANTITY	FBM	QUANTITY	i Bin	QUANTITY	_	QUANTITY	FBM	QUANTITY		QUANTITY	E 15,0 FBM	QUANTITY	FBM	LINE
	LUMBER, SOFT WOOD					T OUNDS A																			\vdash
1	FLOOR, TREAD	39-5330.12-2	138	3 X 12	20'-0"	225			11	660					28	1680	-	_	39	2340					1
2	00	39-3330.12-16	136	3 X 12	16'-0"	180	11	528			28	1008	37	1332			55	1980			74				2
3. 4	DO FLOOR, DECK	39-3952.12-12 39-3340.12-14	175	3 X 12 4 X 12	14'-0"	135 210	14	784	19	1064	28	1568	37	2072	46	2576	55	3080	65	3640	74	2664	83 83	2988 4648	3 4
5	NAILER	39-3360.06-16	186	6 × 6	16'-0"	180	2	96	2	\$6	2	96	2	96	2	96	2	96	2	96	2	96	2	96	5
6	DO	39-3360.06-1	185	6 X 6	10'-0"	112	6	180	8	240	12	360	16	480	20	600	24	720	28	840	32	960	36	1080	6
7	CURB	39-3360.06-16	186	6 X 6	16'-0"	180	2	96	3	144	1	48	6	288	4	192	9	432	11	528	12	576	14	672	7
8	DO	39-3360.06-12	184	6 X 6	3'-0"	155 34	4	36	4	36	4	144 36	4	36	4	144 36	4		4	,,	.				8
. <u>9</u>	CURB FILL DO	39-3360.06 39-3360.06	390 351	6 X 6	3'-0"	34	2	18	4	36	8	72	10	90	14	126	16	36 144	20	36 180	22	36 198	26	36 234	10
11	HANDRAIL POST	39-3340.04	354	4 X 4	41-01	20	6	32	8	4.3	12	64	14	75	18	96	50	107	24	128	26	139	30	160	11
12	HANDRAIL	35-3880.06-16	76	2 X 6	16'-0"	60	2	32							_										12
13	DC	39-3880.06-14	75	2 X 6	14'-0"	53			3	42	5	70	6	84	8	112	۶	126	11	154	12	168	14	196	13
14	STEEL STRUCTURAL STRINGER		525	36 I 182	40'-0"	7280	ı		1										I				4		14
15	DO		525		24'-10 3/4"	4530			1						_					_			8		15
16	DO	48-2900.36-15	523	36 I 150	40'-C"	6600															4				16
17	DO	48-2900.36-15	523		191-10 3/4*	2985											<u> </u>	_			8				17
18	DO	48-2900.33-132	519	33 I 132	14'-10 3/4"	5280 1970	-												8						18
19 20	DO DO	48-2900.33-132 48-2900.33-125	519 517	33 I 132		5000	1			-	+ +						4		- •						20
21	00	48-2900.33-125	517	33 I 125		2480											4					·		_	21
22	00	48-2900.3-108	514	30 I 108	40'-0"	4320									4			_							22
23	00	48-2900.3-108	514	30 I 108		1060							ļ .		4										23
24	00	48-2900.24-087	511		39'-10#"	3470			1		4		4								-		_		24
25	DQ DQ	48-2900.24-074 48-2900.18-047	510 505	24 I 74 18 I 47	101-104*	2110 935				+	1					_									25 26
26 27	90 .	48-2900.16-036	502	16 I 36	14'-10#	535	4																		27
28	DIAPHRAGM	48-3790-12-21		12 [20.7	41-2"	87	6		6		9		9		9		12		12		15		15		28
29	ANGLE	48-2240.64-04		L6X4X3/8	2'-3"	28							J				32		32		40		40		29
30	DO	48-2240-64-04		L6X4X3/8	1'-9*	22	-		16		24		24		24			<u> </u>							30
31	DO DO	48-2240.64-04		L6X4X3/8 L6X4X3/8	1'-3"	15	16		10							-							_		31
32	WEB SPLICE PLATE	47-7844.04		PL 14X3/8	2'-3"	42	1.						6				8		16		16		16		33
34	00	47-7844.04		PL 14X3/8	1'-9"	33									8										34
35	FLANGE SPLICE PLATE			PL12±X7/8	41-31	158							1										16		35
56	00	47-7844.06		PL 12X5/8	3'-1"	74 63	-				-	ļ <u>-</u>	+			ļ	-		16		16				36
37 38	<u>DO</u>	47-7844.05 47-7844.06		PL 12X1/2 PL 12X5/8	4'-6"	115					-	-	#				8		10		1				37 38
39	00	47-7844-06		PL 11X5/8	3'-1"	72					9				8										39
40	00	47-7844-98		PL5 1/2X7/8	41-31	72									ļ.				<u> </u>				32		40
41	00	47-7844.08		PL 5X7/8	2'-11"	44	1					-							<u> </u>		32				41
82		47-7844.06		PL 4 3/405/8	31-11	31 55	1					-	+ +		 		16		32				_		42
43	DO RIVET	47-7844-07 43-6353-08		PL 4 3/40/3/4 7/8	4'-6" 5"	1.04					 						10						768		43
45	DO	43-6353.08		7/8	4 1/4*	.91	Ĭ														512				45
46	DO	43-6353.08		7/8	ų.	-87	ı										320				56				46
47	DO	43-6353.08		7/8	3 3/4"	.83			-				ii .			_	-		448						47
48	00	43-6353.08		7/8 7/8	3 1/4"	.74	 						 -		456		224				252		364		48
49 50	DO DO	43-6353.08-3		7/8	2 3/4"	.66	32		32		72		72		450		224		336		232				50
51	00	43-6353.08-25		7/8	2 1/4*	. 57	60		60		90		90		90		120		120		150		150		51
52	NATUER ATTACHMENT PLATE	47-7844.03		2 X 1/4	0'-4"	.6	16		20		28		36		44		52		60		68		76		52
53	WELDING ROD	46-3772.2-7		3/16*	-		1.2 LB		1.5 LB		2.0 LB		2.6 LB		3.2 LB		3.8 LB		4.4 L8		5.6 LB		5.6 LB		53
\vdash	STEEL HARDWARE, BLA	L K		_				L		<u> </u>	Ш		U				IL.			Ll					
54	MACHINE BOLT WITH SOURCE	43-2325.07-124	B12	3/4	12*	2.1	. 6		8	T	12		14		16		20		24		∠6		30		54
55	200	43-2325.07-1	B10	3/4	10*	1.86	6		8		12		14		18		20		24		26		30		55
56	DRIFT BOLT WITH SQUARE	43-1636.07-2	D20	5/4	20*	3.0	12		16	-	24		28		36		40		48		52		60	$\overline{}$	56
57	STEEL WIRE SPIKE	42-8488.035-7		5/16 X7		. 15	112	-	152		16	3122 125-1	296 16		368 16		448		520 16		592		664		57
58 59	STEEL WIRE NAIL	42-6028.3-6		60đ 50đ		. 10	16		16 242	_	392		518		590		770		832		16 1036		16		58
60	DC	42-6028-3-3		304		.05	32		40		56		72		88		164		120		136		152		60
61	00_	42-6028.3-2		204		,04	28		38		58		68		<u> </u>		98		118		128		148		61

COMPANION SHEETS

-	
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STEEL SPANS, 15-TO 90-FOOT	4
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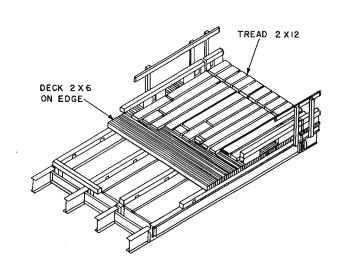


BILL OF MATERIALS FOR FLOOR AND STRINGER COMBINATIONS

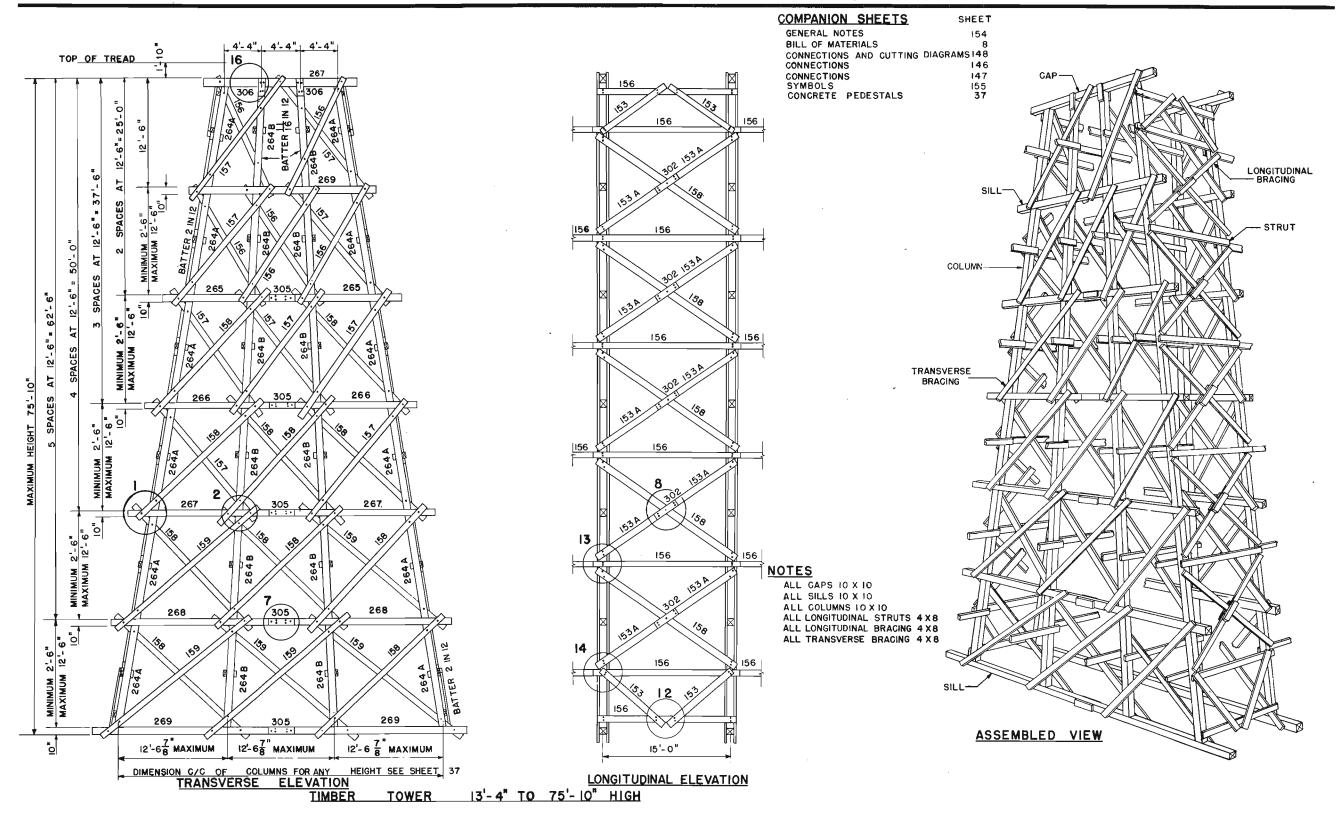
I STANDARD PLANK FLOOR RIVETED STEEL DETAILS HARDWARE	SHEE 5 5 5
2.STANDARD PLANK FLOOR	5
WELDED STEEL DETAILS	6
HARDWARE	5
3. ALTERNATE LAMINATED FLOOR	6
RIVETED STEEL DETAILS	5
HARDWARE	6
4. ALTERNATE LAMINATED FLOOR	6
WELDED STEEL DETAILS	6
HARDWARE	6

	BILL OF MATERIALS F	OR ALTERNATE LA	MINA FED	FLOOR AND	WELDED ST	TEEL DET.	AILS																		
					SPAN LENG	TH	12		20		30		40		50			0'	70		+	0'	·	901	
			ı		STRINGER	SIZE	16 I	36	18 I	47	24]	74	24 1	87	30 I	108	35	I 125	33]	132	36	I 150	36 1	I 182	
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH		QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE
	LUMBER, SOFT WOOD			0 4 6	14'-0"	1.5		3 8 8 9	1 100	2072	221	3094	295	4130	369	5166	443	6202	516	7224	590	8260	664	9296	
2	FLOOR, DECK FLOOR, TREAD	39-3880.06-14 59-3380.12-2	75 108	2 X 6	20'-0"	35 150	111	1554	148	440	221	3094	293	4130	209	2100	443	0202	210	1224	290	8200	004	<u> </u>	2
3	DO TREAD	39-3880, 12-16	106	2 X 12	16'-0"	120	11	352																	3
4	DO	39-3880.12-14	105	2 X 12	14'-0"	105									40	1120			55	1540					4
5	DÓ	39-3228.12-12	104	2 X 12	12'-0"	90					28	672	37	888			55	1320			74	1776	83	1992	5
6	NAILER	39-3360.06-16	186	6 X 6	16'-0"	180	6	96 180	8	96 240	12	96 360	2 16	95 480	20	96 600	2 24	96 720	28	96 840	2	96	2	96	6
8	DO CURB	39-3360,06-1 39-3360,06-16	183	6 X 6	16'-0"	180	2	96	3	144	12	48	6	288	4	192	9	432	11	528	32 12	960 576	36 14	1080 672	7 8
9	00	39-3360.06-12	184	6 X 6	12'-0"	135				-	4	144			4	144									9
10	CURB FILL	39-3360.06	390	6 X 6	3'-0"	34	4	36	Tt.	36	4	36	4	36	4	36	4	36	4	36	4	36	4	36	10
11	DO	39-3360.06	351	6 X 6	3'-0"	34	2	18	4	35	8	72	10	90	14	126	16	144	20	180	22	198	26	234	
12	HANDRAIL POST	39-3340.04	354	4 X 4	16'-0"	20 60	6	32	8	43	12	64	14	75	18	96	20	107	24	128	26	139	30	160	12
13	HANDRAIL DO	39-3880.06-16 39-3880.05-14	76 75	2 X 6	14'~0"	53	2	32	3	42	5	70	6	84	8	112	9	126	11	154	12	168	14	196	13
_ 14	STEEL, STRUCTURAL							-	,														1		
15	STRINGER		525W	36 I 182	40'-0"	7280																	8		15
16	DO		525W	36 I 182	9'-10 1/2"	1797									-								4		16
17	DO DO	48-2900.36-15 48-2900.36-15	523W	36 I 150 36 I 150	40 '-0 " 30'-10:1/2"	5981			 												4				17
18	00	48-2900.33-132		33 I 132	40'-0"	5280													4		1				19
20	DO	48-2900, 33-132		33 I 132		3944													4.						20
21	.00	43-2900.35-125		33 I 125	40'-0"	5000								•			4								21
22	00	48-2900.33-125		33 I 125	19'-10 1/2"	2484						-		-	 		4								22
23	00	48-2900.3-108 48-2900.3-108	514W	30 I 108	9'-10 1/2"	1067					 	-			4										23
24	DO DO	48-2900.3-108		24 I 87	39'-10 1/2°					_			4		+										25
26	00	48-2900.24-074		24 I 74	20"-10 1/2"	2110					4														26
27	DO	48-2900.18-047	50 5W	16 I 47	19"-10 1/2"	935			4																27
28	DO	48-2900.16-036		16 1 36	141-10 1/2*	535	4																		28
29	DIAPHRAGM	48-3790.12-21	C3	12 [20.7		81	6		6		9		9		9		12		12		15 40		15 40		30
30	STIFFENER PLATE	47-7844.04	P15	4 X 3/8	2'-6"	10	Ì								24		32		32		40		40		31
31 32	DO	47-7844.04	P4	4 X 3/8	1'-9"	9					24		24				- /2		- 72		-				32
33	00	47-7844.04	P3	4 X 3/8	1'-4"	1			16																33
34	00	47-7844.04	P2	4 X 3/8	1'-2"	6	16																		34
35	WEB SPLICE PLATE	47-7844.04	P14	12 X 3/8		27									8		8		8		8		16		35 36
36 37	DO FLANGE SPLICE PLATE	47-7844.04	P9 P7	12 X 3/8	1'-6"	122									# *		4		<u> </u>						37
18	DO PERMISE SPEICE PIXIE	47-7844.05	P8	7 × 1/2		22											7		4						38
39	00	47-7844.08	P16	9 x 7/8	3'-7"	96														_			8		39
40	00	47-7844.06	P24	10 x 5/8		115									-						4				40
41	DO	47-7844.1	P25	10 X 1	3'-8"	125			 						1 .						4				41
42	DO	47-7844.04	P28	9 X 3/8 8 X 1/2	1	19 32	-			<u>-</u> -	-				4				\parallel		4		+ -		42
44	00	47-7844.05	P33	9 X 1/2		61									4						<u> </u>				44
45	po	47-7844.08	P35	10 1/2 x 7/8	71-6"	234			I												1		8		45
46	00	47-7844.06	P36	10 X 5/8		106					<u> </u>	ļ			-				₩		1		8		46
47	DO	47-7844.1	P43	9 X 1 9 X 1/2	4'-0"	122					-				+		4		4		1				47
48	DO DO	47-7844.05	P 38	9 X 1/2		66 29											4		4						48 49
50	NAILER ATTACHENT PLATE	47-7844.03		2 X 1/4		0.6	16		20		28		36		44		52		60		68		76		50
51	WELDING ELECTRODE			7/32											36 LB		64 LB		80 LB		87 LB		884 LB		51
52	00	46-3772.2-7		3/16			15 LB		17 LB		29 LB		30 LB		35 LB		45 LB		60 LB		74 LB		91 LB		52
\vdash	STEEL HARDWARE, BLA	ick I	I			1	1		I	_	1		II				1		П		п		11		Т
53	MACHINE BOLT, SQUARE HEAD AND TWO MASHERS	43-2325.07-124	B12	3/4	12*	2.52	6		8		12		14		18		20		3.5				.,		
54		43-2325.07-124	B10	3/4	10"	1.77	6		8		12		14		18		20		24		26 26		30 30		53 54
52	DO DRIFT BOLT STUDE	43-1636,07-2	D20	3/4	20 •	3.0	12		16		24		28		36		40		48		52		60		55
26	STEEL HIRE NAIL	42-6028.3-6		604		,10	8		8		8		8		88		8		8		8		8		56
57	DO	42-6028,3-5		50d		.08	187		242		392		518		590		770		832		1036		1152	—	57
58	00	42-6028.3-3		30 <i>d</i> 20d		.05	1255 24		1668 36		2498 56		3328 64		4158 84		4988 96	<u> </u>	5818 116		124		7478		58
59	1 00	42-6028.3-2	1	200	ــــــــــــــــــــــــــــــــــــــ	.04			J 20		20		J 04		11 04) y0		110		124		144		59

COMPANION SHEETS STEEL SPANS, 15-TO 90-FOOT 4 BILL OF MATERIALS 5 TIMBER FLOOR DETAILS 129 WALKWAYS FOR HIGHWAY BRIDGES 131 TO 145 JUNCTION TIMBER AND STEEL-STRINGER SPANS 159 SYMBOLS SHEETS 155

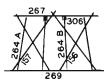


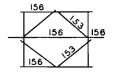
1	BILL OF MATERIALS FOR FLOOR AND STRINGER	COMBINATIONS
\mathbf{I}		SHEET
	I STANDARD PLANK FLOOR RIVETED STEEL DETAILS HARDWARE	5 5 5
	2.STANDARD PLANK FLOOR WELDED STEEL DETAILS HARDWARE	5 6 5
	3. ALTERNATE LAMINATED FLOOR RIVETED STEEL DETAILS HARDWARE	6 5 6
	4- ALTERNATE LAMINATED FLOOR WELDED STEEL DETAILS HARDWARE	6 6 6



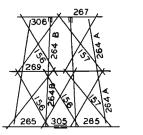
154 148 146

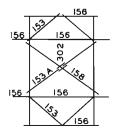
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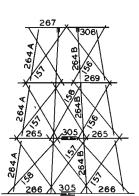


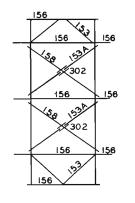
I-STORY TOWER



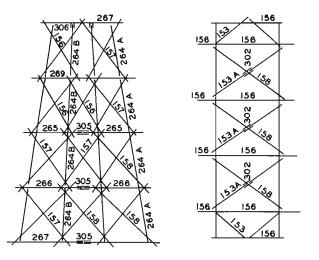


2-STORY TOWER

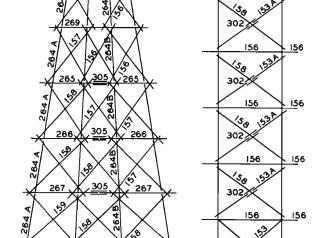




3-STORY TOWER



4-STORY TOWER



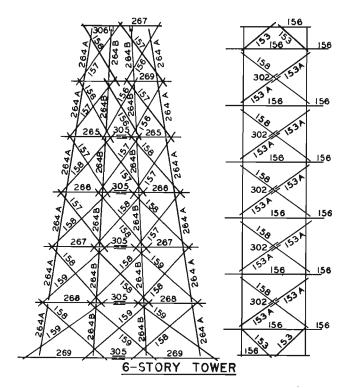
GENERAL NOTES
ASSEMBLY AND PIECE MARKS
CONNECTIONS AND CUTTING DIAGRAMS
CONNECTIONS
CONNECTIONS

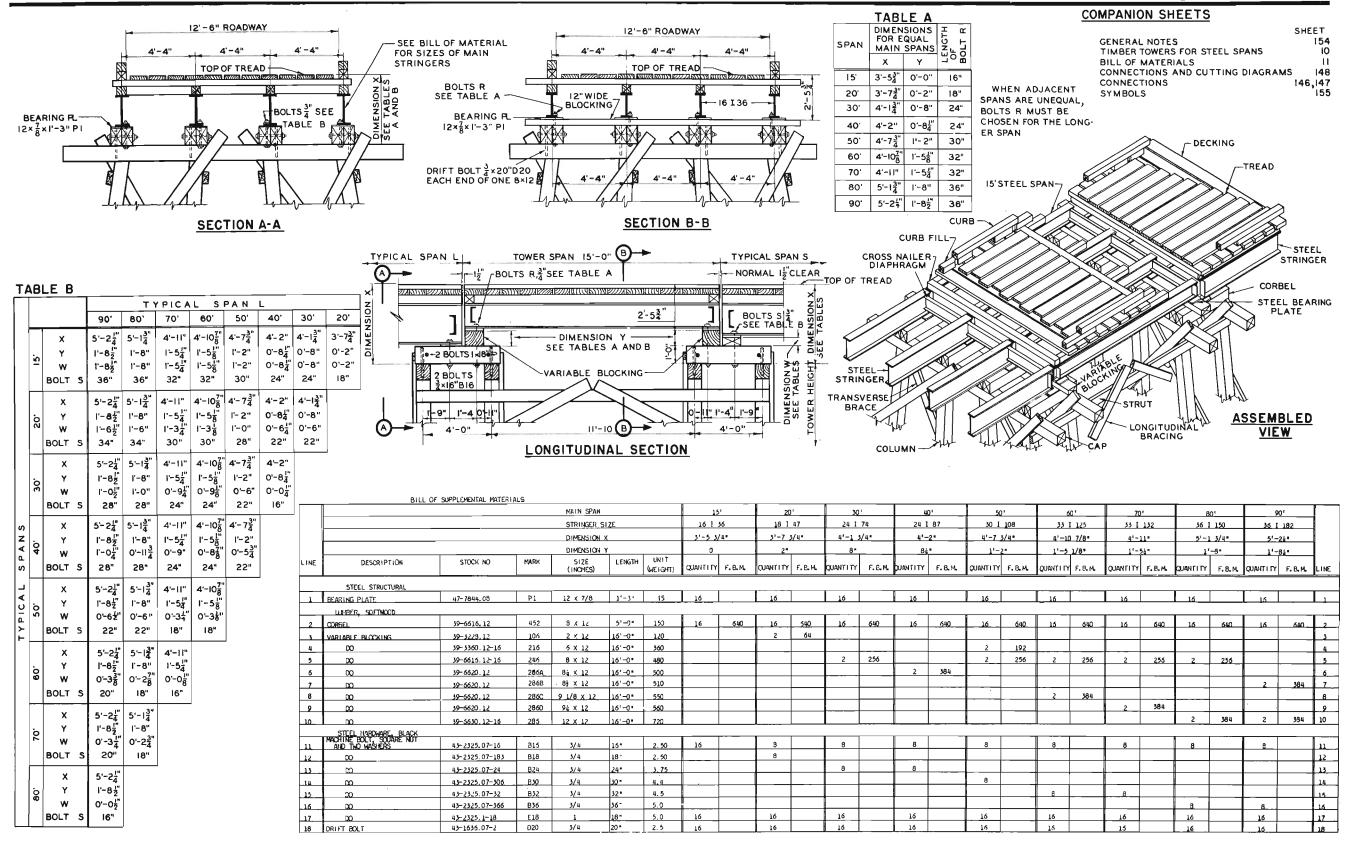
COMPANION SHEETS

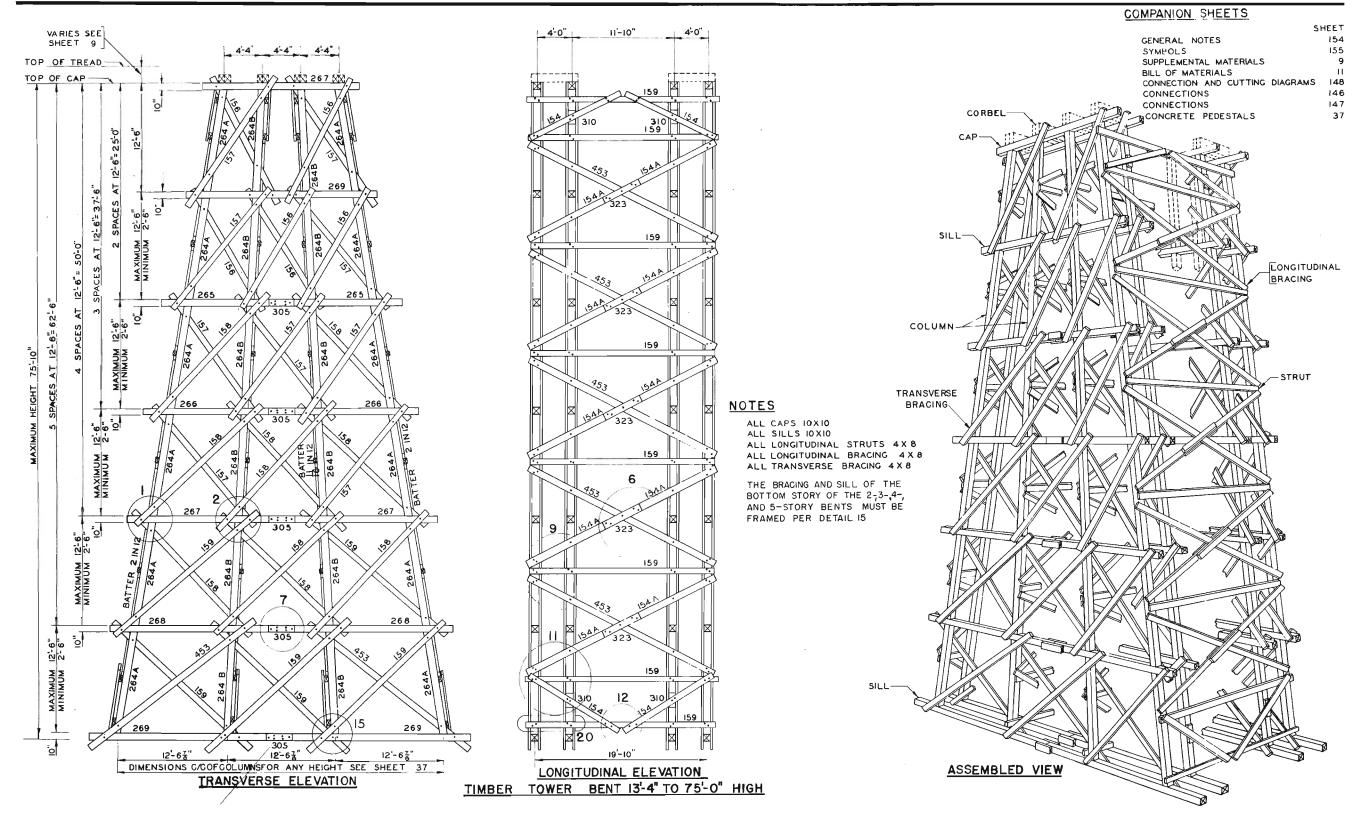
SYMBOLS

5-STORY TOWER

			NUMB	R OF STORIES	3		6-51		5 _. ST	ORY	4-\$1	ORY	3~ST	ORY	2-81	OR Y	1-S	TORY
			10	WER HEIGHT			75 ' - 1	1 0"	63'-	4"	50'-	-10"	38'-	4 "	25'-	10"	13'	-4"
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (THCHES)	LENGTH	WEIGHT WEIGHT (POUNDS	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM
LUM	BER, SOFT WOOD																	
1	CAP	39-6620.1-18	267	10 × 10	18'-0*	563	2	500	2	300	2	300	2	300	2	300	2	300
2	SILL	39-6620.1-22	269	10 x 10	22'-0"	688	6	1100	2	367	2	367	2	367	2	367	2	367
3	DO	39-6620.1-2	268	10 X 10	201-01	625	4	667	4	667								
4	DO	39-6620, 1-18	267	10 X 10	18'-0"	563	4	500	4	600	ų	600						
5	DO	39.6620.1-16	266	10 X 10	16"-0"	500	4	533	4	533	4	533	4	533				
6	00	39-6620.1-14	265	10 × 10	14'-0"	438	4	467	4	467	4	467	ц	467	4	467		
7	COLUMN	39-6620.1-12	2644	10 x 10	12'-0"	375	24	2400	.20	2000	16	1600	12	1200	8	800	4	400
8	DO	39-6620.1-12	264B	10 × 10	1.21-0	375	24	2400	20	2000	16	1660	12	1200	ð	800	4	400
9	STRUT	39-3340.08-16	156	4 x 8	16'-0"	160	52	2219	44	1877	36	1536	28	1195	20	853	12	512
10	BRADING	39-3340.08-22	159	4 X 8	22'-0"	220	12	704	4	235								
11	DQ	39-3340.08-2	158	4 X 8	20'-0"	200	34	1813	28	1493	18	960	8	427	2	107		
12	DG	39-3340.08-18	157	4 X 8	18'-0"	180	20	960	20	960	20	960	16	768	8	384	4	192
13	DO	39-3340.08-16	156	4 X 8	16'-0"	160	12	512	12	512	12	512_	12	512	12	512	4	171
14	DO	39-3340.08-1	153	4 X 8	10'-0"	100	8	213	8	213	8	213	ь	213	8	213	8	213
15	DC	39-3340.08-1	153A	4 X 8	10'-0"	100	20	533	16	427	12	320	8	213	4	107		
16	SCAB	39-3340.1	305	4 X 10	31-01	38	20	200	16	160	12	120	8	80	4	40		
17	DO	39-3330.1	306	3 X 10	2'-0"	19	8	40	8	40	8	40	8	40	8	40	8	40
18	DO	39-3228.08	302	2 X 8	31-4"	17	50	89	16	71	12	53	â	36	4	18		
	STEEL HARDWARE, BLACK																	
19	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.1-24	E24	1	24*	ő. 5	16		16		16		15		16		8	
20	oc .	43-2325.1-2	E20	1	20 -	5.6	238		190		142		94		46		10	
21	DC	43-2325-1-18	E18	1	18"	5.1	16		16		16		16		16		16	
22	DC	43-2525-1-164	£16	1	16"	4.7	172		148		124		100		76		52	
23	DC	43-2325.1-104	E10	1	10*	3.4	66		56		46		36		26		16	
24	DRIFT BOLT, PLAIN	43-1656.07-2	D20	3/4	20"	2.5	144		120		96		72		48		24	



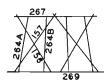


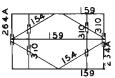


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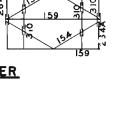
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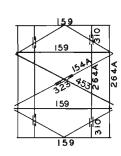
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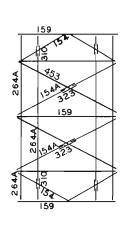


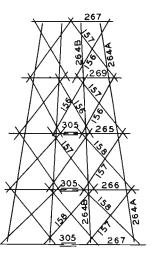


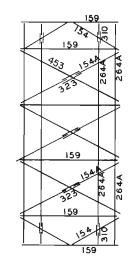
-STORY TOWER

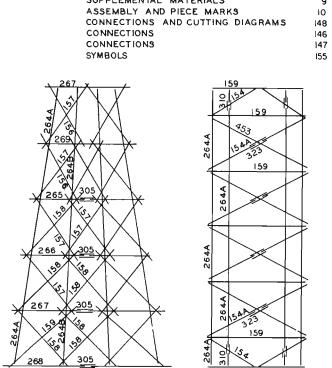












COMPANION SHEETS

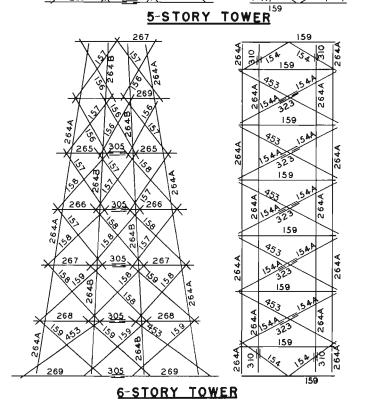
GENERAL NOTES
SUPPLEMENTAL MATERIALS

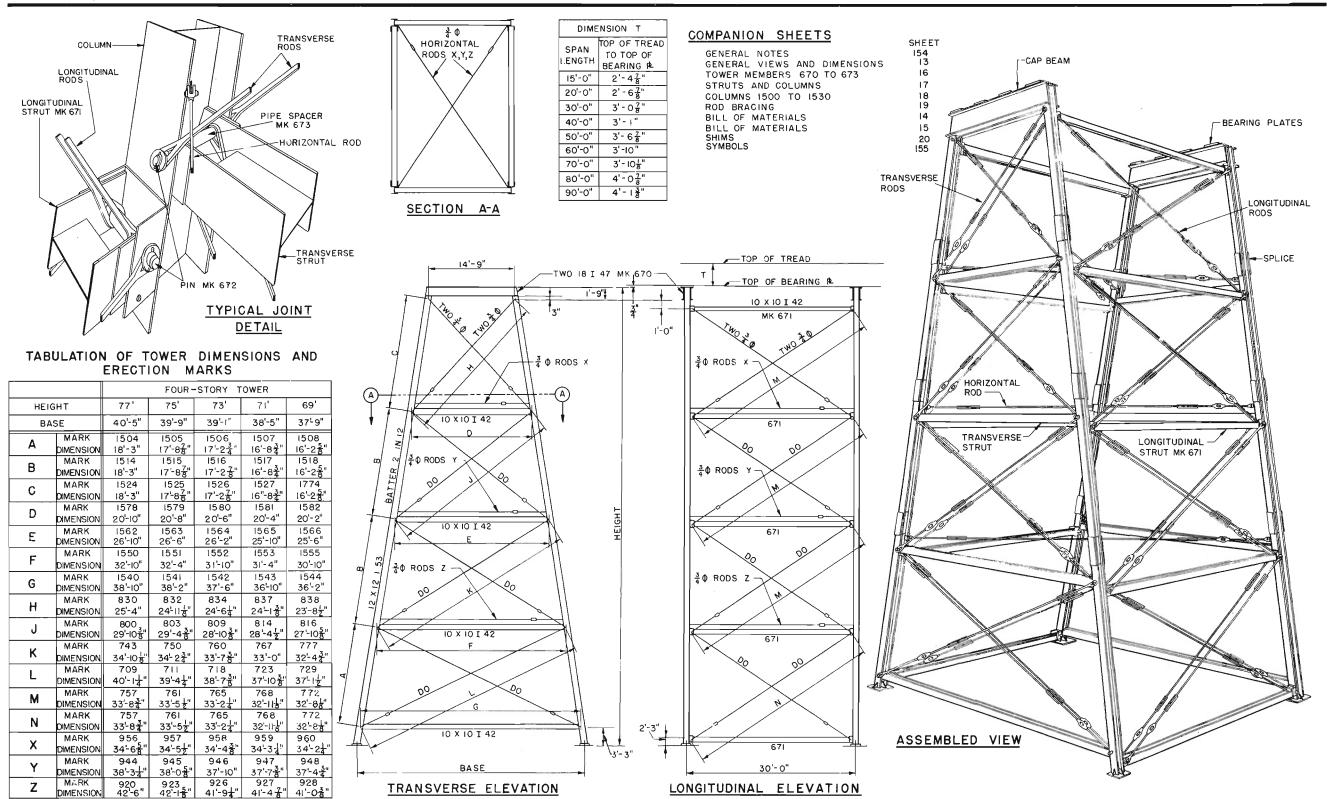
2-STORY TOWER

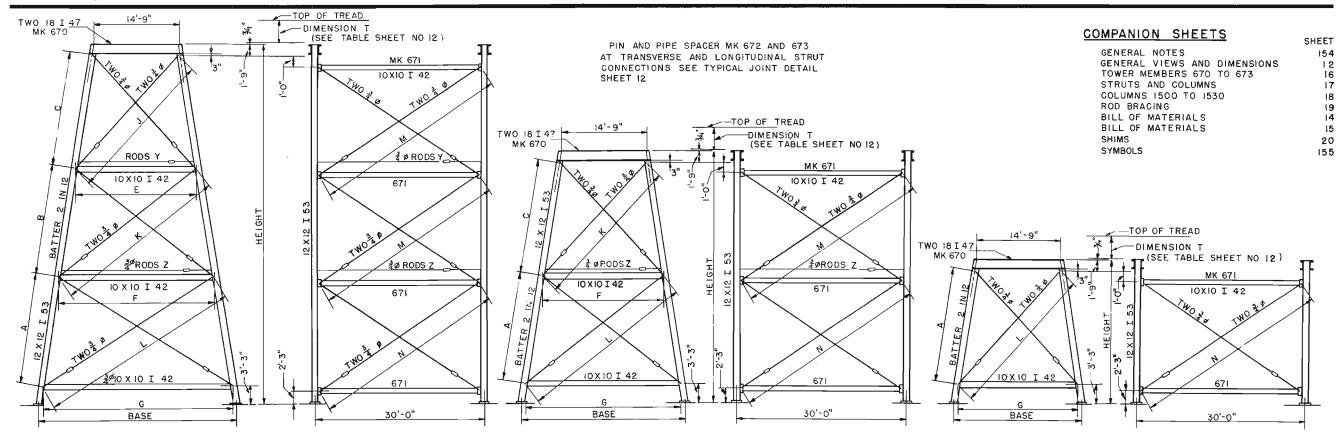
3-STORY TOWER

4-STORY TOWER

				NO OF S	TORIES		6-57	ORY	5-ST	ORY	4-ST	ORY	3-5	TORY	2-ST	TORY	1-5	STORY
				TOWER H	EIGIT		75'-	10 "	65'-	4*	50'-	10 -	381	-u=	25'-	10"	131	'-u*
.INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT WEIGHT (POUNDS)	OURNT ITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	CONTRACTOR	FBM	QUANTITY	MEH
	LUMBER SOFT-WOOD											•						
-	CAP	39-6620.1-18	267	10 X 10	18'-0"	560	4	600	4	600	4	500	ц	600	4	600	4	600
2	SILL	39-6620.1-18	267	10 × 10	18'-0-	560	8	1200	9	1200	3	1200						
,	00	39-6620.1-16	255	10 × 10	161-0*	500	8	1067	8	1057	8	1057	8	1067				
и		59-6620, 1-14	265	10 × 10	14'-0"	440	8	933	8	533	8	933	è	933	8	933		
5		39-6620.1-22	269	10 Y 10	22'-0"	690	12	2200	ц	753	4	733	4	753	4	733	4	73
6	00	39-6620, 1-2	268	10 X 10	201-0"	630	8	1333	8	1333								
7	COLUMN	39-6620.1-12	2643	10 X 10	121-0"	370	48	4800	40	4000	32	3200	24	2400	16	1600	3	800
а	20	39-6620.1-12	2648	10 × 10	12'-0"	370	48	4300	40	4000	32	3200	24	2400	15	1600	8	300
Q	STRUT	39-3340.09-22	159	4 × 8	22'-0"	220	32	1877	28	1643	24	1403	20	1173	15	Ç 3G	12	70
10	SRACING	39-334 0.08-24	453	4 X 8	24'-0"	240	28	1792	15	1024	12	768	8	512	4	256		
11_	80	39-3540.09-2	158	4 x 8	20'-0"	200	40	2133	40	2133	24	1280	8	427				
12	80	39-3340.08-18	157	4 X 8	18'-0"	180	49	1920	40	1920	40	1920	32	1540	15	770	а	38-
تد	80	39-3340.08-15	156	4 × 8	16'-0"	160	24	1024	24	1024	24	1024	24	1024	24	1024	9	341
14	<u>po</u>	39-3340.08-12	154	4 Y 8	121-04	150	16	512	16	512	16	512	15	512	16	512	16	51.
15	8	39-3340.08-12	1543	4 X 8	12'-0"	120	40	1230	32	1024	24	768	15	512	8	255		
16		59-3340.03-22	159	4 X 8	22'-0"	227	24	1403	3	469								
17_	SCAB	39~3340.1	305	4 × 10	3'-0"	40	40	400	32	320	24	240	16	160	3	80		
19		39-2228.03	523	2 × 8	3'-8"	20	40	195	32	157	24	118	16	78	3	39		
19	100	39-3340.1	510	4 X 10	21-0#	30	16	107	15	107	16	107	16	107	16	107	24	160
;	STEEL HAROWARE, BLACK							,										
20	MACHINE BOLF WITH SQUARE	43-2325. 1-104	E10	1	10=	3.45	132		112		92		72		52		32	
_	NUT OND TWO WASHERS																	
21	20	43-2325. 1-164	€16	1	16"	4. 75	556		560		464		368		272		144	
22	ω	43-2325.1-2	E20	1	20-	5.61	360		296		232		168		104		64	
23	DRIFT BOLT PLAIN	43-1536.07-2	020	3/4	20"	2.50	289		240		192		100		96		48	







TABL	JLATION OF TO	HER DIMENSIO	N_AND ERECTI	ON MARKS							1									_								
					T-	IREE-STORY T	OWER								TWO-STORY IT	MER						ONE	E-STORY TOWER	1				
HEIGH	чт	67'	65'	63'	61'	591	57'	55'	531	51'	49'	47'	45'	45'	41'	391	37'	351	531	311	291	27'	251	231	21'	19'	17'	15"
BASI	ξ	37'-1"	36'-5"	3519*	35'-1"	341-5"	33'-9*	33"-1"	32'-5*	31'-9"	31'-1"	30'-5"	29'-9"	29'-1"	28'-5"	27'-9*	27'-1"	26'-5"	251-9*	25'-1"	24'-5"	231-9*	23'-1"	22'-5*	21'-9"	21'-1"	201-5"	10'-0"
А	MARK DIMENSION	1500 22'-3 5/8"	1502 20'-34"	1503 19'-3 1/8*	1504 181-3	1504 18'-3"	1506 17'-2 3/4"	1506 17'-2 1/8"	1508 16'-2 5/8"	1509 15'-2½".	1500 22'-3 5/8"	1501 21'-3½"	1502 20"-34"	1503 19'-3 1/8*	1504 18'-3"	1506 17'-2 3/4"	1508 16'-2 5/8*	1509 15'-2½"	1510 14'-2 3/8°	1551 26'-44"	1532 24'-4*	1553 22'-3 5/8*	1534 201-34*	1535 18'-3"	1536 16'-2_5/8#	1537 14'-2-5/8*	1558 12!=2"	1539 10'-1 5/8*
8	MARK DIMENSION	1511 20'-3å"	1511 20'-34"	1512 19'-94"	1513 19'-3 1/8"	1514 18'-3"	1515 17'-8 7/8*	1517 16'-8 3/4"	1518 16'-2 5/8"	1519 15'-8 5/8"																		
С	MARK DIMENSION	1521 20*-34*	1521 20'-3å"	1522 19'-94"	1525 19'-3 1/8"	1524 18'-3"	1525 17'-8 7/8*	1527 16'-8 3/4"	1774 16'-2 5/8"	1528 15'-8 5/8*	1520 22'-5 5/8"	1773 21'- 3 4"	1521 20'-34"	1523 19'-3 1/8*	1524 18'-5"	1525 17'-2 3/4"	1774 16'-2 5/8"	1529 15'-2½"	1550 14'-2 3/8"									
E	MARK DIMENSION	1573 21'-6*	1573 21'-6"	1575 21'-4"	1576 21'-2"	1578 20'-10"	1579 20'-8"	1581 20'-4"	1582 20'~2"	1577 20'-0"																		
F	MARK DIMENSION	1558 28'-2"	1558 28'-2*	1560 27'-10"	1561 27'-6"	1562 26'-10"	1563 261-6"	1565 25'-10*	1566 25'-6"	1567 25'2*	1572 22'-2"	1574 21'-10"	1573 21'-6"	1576 21'-2"	1578 20'-10*	1580 20'-6"	1582 201-2*	1583 19'-10"	1584 19'-6"									
G	MARK DIMENSION	1545 35'-6*	1546 34'-10*	1547 34'-2"	1548 33'-6"	1550 32'-10"	1549 32'-2"	1554 31'-6"	1555 30'-10"	1556 30'-2"	1557 29¹−6°	1559 28'-10"	1558 28'-2"	1561 27'-6"	1562 26'-10"	1564 26'-2"	1566 251-6*	1568 24'-10"	1569 24'-2"	1570 25'-6"	1571 22'-10"	1572 22'-2"	1573 21'-6"	1578 201-10	1582 20'-2"	1584 19'-6"	1585 18'-10"	1586 181-24
J	MARK DIMENSION	823 27'-04"	823 27'-04"	825 26'-7 1/8*	828 26'-2 1/8"	830 25'-4*	832 24'-11 1/8"	857 24'-1 3/8*	858 25'-8±"	841 23'-3 3/4"																		
к	MARK DIMENSION	784 31'-10 5/8"	784 31'-10 5/8	787 31'-4½"	793 30'-10½"	800 29'-10 3/8	90 3 29'-4 3/8"	814 28'-4½"	816 27'-10 5/8*	819 27'-4 3/4"	811 28' -8 7/8"	816 27'-10½*	823 27'-04"	828 26'-2 1/8"	830 25'-4"	834 24'-64"	838 23'-8½ *	843 22'-11 1/8"	847 22'-1 7/8"									
L	MARK DIMENSION	716 38'-8 3/8"	728 37'-3 3/4"	733 36'-46"	740 35'-5*	743 34'-10 1/8	755 35'-10_7/8*	763 33'-4"	777 32'~4 3/4"	788 31'-5 5/8"	754 33'-11 1/8'	770 32'-10 7/8*	784 31'-10 5/8'	793 30'-10½"	1054 29'-10 3/8'	809 281-10 3/8	816 27'-10 5/8*	823 271-04"	829 25'-114"	779 32'-3 5/8"	795 30'-6 1/3"	811 28'-8 7/8*	823 27'-04	830 25'~4"	838 23'-8½*	847 22'-1 7/8"	851 20' -8 1/8*	857 19'-4 3/8"
м	MARK DIMENSION	742 54'-10 3/8"	742 34'-10 3/8'	745 34'-6 7/8*	749 34'-5 3/8"	757 33'-8 3/4"	761 33'-5½*	768 32'-11 1/8"	772 32'-8 1/8"	774 32'-5 1/8	735 36'-1"	738 35'-5 5/8"	742 34'-10 3/8	749 34'-3 3/8"	757 53' -8 3/4"	765 531-24*	771 321-64*	780 32'-2à*	785 31'-8 5/8"									
N	MARK DIMENSION	735 36'-1"	742 34'-10 3/8	749 34'-3 3/8"	757 33'-8 3/4"	757 33'-8 3/4"	765 33'-24*	765 33'-24"	772 32'-8 1/8"	780 32'-2#*	735 36'-1"	738 35'-5 5/8*	742 34'-10 3/9'	749 34'-3 3/8"	757 33' -8 3/4"	765 33'-24"	771 52"-64"	780 32'-2å"	785 31'-8 5/8*	715 38'-8 5/8"	726 37'-4½ *	735 36'-1"	742 34'-10 3/8"	757 33'-8 3/4*	824 32 '-8 1/8'	785 31' -8 5/8*	792 50'-10 3/8"	799 30'-12"
CLEVIS ROD Y	MARK DIMENSION	953 34'-114"	953 34'-114"	954 34'-10 1/8	955 341-9*	956 34'-6 5/8"	957 34'-5½"	959 341-341	989 34'-24"	961 34'~1 1/8"	+		251	070	0.4		900	040				_						
CLEVIS	MARK DIMENSION	972 39'-2 1/8"	972 391-2 1/8*	941	943 381-6 5/8*	944 381-34°	945 381-0 5/8*	947 37'-7 3/8"	948 37'-4 3/4"	949 37'-2 1/8	951 351-4"	952 35'~1 5/8"	953 34'-11±"	974 34' ~9 *	956 341~6 5/8*	958 341-4 3/84	989 34'24"	962 34'-0"	990 33'-9 7/8*									

	SHEET
GENERAL NOTES	154
SYMBOLS	155
FRAMED STEEL TOWERS	12,13
BILL OF MATERIALS	15
TOWER DETAILS	16,17, 18,19

	1			ļ l					TOWER H	EIGHT GRO	UP CLASS	IFICATION		
LINE	DESCRIPTION	STOCK NUMBER	MARK	DETAILED ON SHEET	SIZE (INCHES)	LENGTH		TORY TO 79'		TURY TO 671		TORY TO 49'		TORY TO 31'
							NUMBER	UNIT WEIGHT (POUNDS)	NUMBER	UNIT WEIGHT (POUNDS)	NUMBER	UNIT WEIGHT (PCUNDS)	NUMBER	UNIT WEIGHT (POUNDS)
1	CAP BEAM	48-2900.18-047	670	16	18 <u>I</u> 47	16'-2"	4	760	4	760	4	760	4	760
2	BEARING PLATE	47-7844.07-7	Р6	16	20 X 3/4	1'-10"	8	93	8	93	8	93	8	زو
3	DIAPHRAGM		01	16	12 × 12 I 53	1 - 4 =	4	71	3	71	Ł,	71	4	71
4	RIVETS IN BEARING PLATES	43-6353.08		16	7/8	4 3/4"	64	.66	64	.66	64	. 66	6.4	.66
5	RIVERS IN WEB OF CAP	45-6353.08		16	7/8	2 1/2*	128	.62	128	.62	128	.62	128	,62
6	LONGITUDINAL STRUT		671	16	10 I 42	28'-10 3/4"	10	1215	8	1215	6	1215	4	1215
7	PIN PLATE	47-7844.04-1	Р8	16	9 x 3/8	0'-10"	40	10	52	10	24	10	16	10
8	DO	47-7844.04-1	Ρ5	17	9 x 3/8	0'-10"	32	10	24	10	16	10	8	.10
9	COLUMN BASE PLATE	47-7844.1-5	Ρ4	17	18 × 1	1'-6"	4	92	4	92	4	92	4	92
10	STIFFENERS	47-7844.04-08	PS.10.11	17	5 x 3/8	1'-5 1/2"	ц	11	4	11	4	11	4	11
11	BRACING CONNECTOR		C1	17.18	12 X 12 I 55	1'-1 1/4"	20	40	16	40	12	40	8	40
12	DO	47-7844.05-22	Ρ3	18	4 x 1/2	1'-0"	12	7	8	7	4	7		
13	WEB SPLICE	47-7844.05-22	P1	18	10 x 1/2	1'-10 1/4"	24	31	16	31	8	31		
14	FLANGE SPLICE	47-7844.05-22	Ρ2	18	12 X 1/2	1'-10 1/4"	24	38	16	38	8	38		
15	RIVETS, WEB SPLICE	43-6355.08		18	7/8	5 1/4"	144	.74	96	.74	48	.74		
16	RIVETS, FLANGE SPLICE	43-4553.08-25		18	7/8	2 1/2*	288	.62	192	.62	96	.62		
17	PPIN		672	16	1 1/2 Ø	1'-4 1/2"	40	8	32	8	24	8	16	8
18	SCOTTER PIN			16	1/4 × 2 1/2		80	,1	54	٠.١	48	.1	32	.1
19	SPIPE SPACER	44-6246.7-02	673	16	2	0'-7*	40	2	32	2	24	2	16	2
20	J-WASHER		658	16	3 3/4 x 1 9/6" HOLE	3¾	144	1.24	128	1.24	112	1.24	96	1.24
21	3 LOOP ROD, UPSET		677	19	3/4 ^D	41-74	128	11	¥6	11	64	11	32	11
22	SPLICE HOD	46-6375.5-07	678	15	3/4 #	1,-1.	256	1.6	152	1.6	128	1.0	64	1.6
23	9TURNBUCKLE			15	1 1/8	. 6"	64	2.7	4ô	2.7	32	2.7	16	2.7
24	DCLEVIS ROD, HORIZONTAL MPSE	т	680	15	3/4 D	リーフリ	6	4.3	4	4.3	2	4.5		
25	3) DC		680	19	3/4 p	1'-3"	6	3.7	4	5.7	2	5.7		
26	SPLICE HOD	46-6375.5-07	678	19	3/4 Ø	1'-1"	24	1.6	16	1.6	Ü	1.6		
<u> </u>	3 TURNBUCKLE			19	1 1/8	6"	6	2.7	4	2.7	2	2.7		
	3/CLEVIS			15	NO 3 FOR 1 1/8" THREAD	5×	12	4.0	8	4.0	4	4.0		
29	FIN HEADED, CLEVIS			19	1 3/16 p	\$ 1/4"	12	1.5	8	1.5	4	1.5		
30	Acorter PIN			19	1/4 8 x 2 1/2		12	ا،	8	-1	ц	.1_		
31	WELDING ELECTRODE	48-3773:3-75			3/16 AND 7/32			330 LB		260 LB		180 LB		100 LB

リ CONNECTOR PIN ASSEMBLY、14*
シ LOOP ROD ASSEMBLY、34*
シ CLEVIS ROD ASSEMBLY、34*

ABLE 4 - BILL OF MATERIALS FOR PIECES WHICH VARY FOR DIFFERENT TOWER HEIGHTS REQUISITIONED WEIGHT LENGTH POINCES REQUISITIONED WEIGHT (POINNES) MARK REQUISITIONED UNIT WEIGHT (POLIMBE) MARK REQUISITIONED WEIGHT DETAILED NUMBER MARK MARK REQUISITIONED WEIGHT MARK LENGTH 751 TOWER HEIGHT 77' 71' DESCRIPTION 69 1500 | 1506R | 241-0 3/4" 1504R 25'-1" 1505R 241-6 7/8" 1275 1507R 23'-6 3/4* 1250 1508R 23'-0 5/8* 1220 3 1504L 25'-1" 1330 1505L 241-6 7/8* 1300 1506L 24'-0 3/4" 127' 1507L 23'-6 3/4" 1250 1508L 23'-0 5/8" 1220 TOWER COLUMNS 12 X 12 I 53 STOCK NO 965 1515R 17'-8 5/8" 940 1516R 17'-2 5/8" 915 1517R 16'-8 1/2" 885 1518R 16'-2 3/8" 860 4 1514R 18'-2 3/4" 1514L 18"-2 3/4" 965 1515L 17'-8 5/8" 940 1516L 17-2 5/8* 915 1517L 16'-8 1/2" 885 1518L 16'-2 3/8" 860 4 820 1527R 14'-11 1/4" 790 1774R 14'-5 1/8 765 5 1524R 16'-5 1/2" 870 1525R 15'-11 3/8" 845 1526R 15'-5 1/4" 845 1526L 151-5 1/4* 6 2 1524L 16°-5 1/2" 870 1525L 15'-11 3/8" 820 | 1527L | 14'-11 1/4" | 790 | 1774L | 14'-5 1/8" 765 895 1579 21'--1" 1578 21'-3" 885 1580 201-111 880 1581 20'-9" 7 870 1582 20'-7" 865 2 TRANSVERSE STRUTS 1562 27"-3" 1145 | 1563 | 26'-11" 1130 1564 26'-7" 1120 1565 261-3" 1100 1566 25'-11" 1090 8 2 10 I 42 STOCK NO 1400 1551 521-9* 1375 1552 32'-3" 1365 1553 1335 1555 9 1550 33'-3" 31.-9* 31'-3" 1515 1540 39'-3<u>*</u> 1650 1541 381<u>-7*</u> 1620 1542 37*-11* 1595 1543 37'-3" 1565 1544 361-7" 1540 23 901 14°-6° 29 892 19°-0° 15'-0" 11 8 899 15'-6" 23 900 22 901 14'-6" 22 902 14'-0" TRANSVERSE RODS 21 3/4 # ROOS STOCK NO 46-6375.5-07 30 891 19'-6" 29 893 18'-6" 28 894 12_ 19 890 20'-0" 18'-0" 27 8 37 882 24"-0" 36 894 38 881 24'-6" 880 25'-0" 25'-0" 35 885 13 22'-6" 34 44 872 29'-0" 870 30'-6-46 871 29'-6" 44 874 281-0" 42 875 41 8 271-61 36 883 231-61 35 883 23'-6" 43 884 882 24'-0" 25.-0* 35 885 .22'-6" 15 24 34 LONGITUDINAL ROOS 3/4 Ø ROOS STOCK NO 46-6375,5-07 8 882 24'-0" 36 883 231-6" 35 883 231-6" 45 884 35 BF 16 19 221-6" 34 1008 50'-6" 46 1008 301-5" 46 1009 30'-0" 45 1009 30'-0° 45 1009 501-01 45 34'-O* 51 1003 34'-0" 51 1003 34'-0" 51 1004 50 1004 19 2 1003 33'-6" 18 53'-6" 3/4 Ø ROOS 50 STOCK NO. 46-6375.5-07 995 58 996 38'-0" 57 997 37'-6* 56 997 56 MARK REQUISITIONED WEIGHT MARK REQUISITIONED WEIGHT MARK REQUISITIONED WITT MARK REQUISITIONED WEIGHT MARK 381-6" 57'-5" 56 998 37'-0"

COMPANION SHEETS

SHEET GENERAL NOTES 154 SYMBOLS 155 FRAMED STEEL TOWERS 12,13 BILL OF MATERIALS TOWER DETAILS 16, 17, 18 19

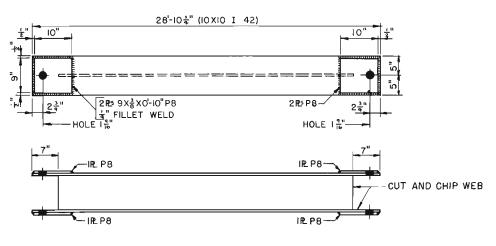
																			· Paran	LENGTH	(POUNOS)	MARK	LENGTH	(POUNBS)	маюх	LENGTH	(POUNDS)	MARK	LENGTH	WEIGHT (POLKIDS)
		TOWES	RHEIGHT		67'			651	Uto		63			61			59			57			55.			53			51'	
	20	18	2	1500R	29'-1 5/8*	1545	1502R	27*-1_1/4*	1435	1503R	26-1 1/8*	1380	1504R	25'-1"	1550	1504R	25:-1"	1330	1506R	24"-0 3/4"	1280	1506R	24'-0 3/4"	1280	1508R	23'-0 5/8"	1220	1509R	22'-0 1/2*	1170
	21		2	1500L	29'-1 5/8*	1545	1502L	27'-1 1/4"	1435	1503L	26-1 1/8"	1380	1504L	25'-1"	1330	1504L	25'-1"	1330	1506L	24'-0 3/4"	1280	1506L	24'-0 3/4"	1280	1508L	23'-0 5/8"	1220	1509L	22'-0 1/2-	
TOWER COLUMNS 12 X 12 I 53	22		2	15118	20'-3"	1075	1511R	201-3"	1075	1512R	19'-9"	1045	1513R	191-2 7/8*	1020	1514R	18'-2 5/4"	970	.515R	17'-3 5/8"	940	1517R	16'-8 1/2"	885	1518R			1519R		
STOCK NO	23	18	2	1511L	20'-3"	1075	1511L	20'-3"	1075	1512L	199*	1045	1513L	19'-2 7/8"	1020	1514L	18'-2 3/4	970	1515L	17'-3 5/8"	940	1517L	16'-8 1/2"	885	1518L	16'-2 3/8"	860	1519L	1	
	24		2	1521R	18'-5 3/4"	980	1521R	18'-5 3/4"	980	1522R	17'-11 3/4"	955	1523R	17'-5 5/8-	925	15248	16'-5 1/2"	875	1525R	15'-11 3/8"	845	1527R	14'-11 1/4"	790)774R	14'~5 1/8*	765	1528R	13'-11 1/8"	
	25		2	1521L	18'-5 3/4"	980	1521L	18'-5 5/4"	980	1522L	17'-11 3/4"	955	1523L	17'-5 5/8"	925	1524L	16'-5 1/2"	375	1525L	15'-11 3/3"	845	1527L	141-11 1/4"	790	1774L	14'-5 1/8"	765	1528L	13"-11 1/8"	740
TRANSVERSE STRUTS	26		2	1573	21'-11"	920	1573	21'-11"	920	1575	211-9-	915	1576	21'-7"	905	1578	21'-5"	895	1579	21'-1"	885	1581	20'-9*	870	1582	20'-7"	865	1577	20 *-5*	860
10 I 42	27	17	2	1558	28'-7"	1200	1558	28'-7"	1200	1560	28'-3"	1180	1561	27'-11"	1170	1562	27'-3"	1145	1563	56,-11.	1130	1565	26'-3"	1105	1566	25*-11*	1090	1567	25*-7*	1075
STOCK NO	28		2	1545	35'-1 <u>1"</u>	1510	1546	351-31	1480	1547	341-7=	1450	1548	33'-11"	1425	1550	331-3"	1395	1549	321-7"	1570	1554	31"-11"	1340	1555	31'-3"	1310	1556	30'-7"	1285
TRANSVERSE ROOS	_29		8	896			896	17'-0"	26	897	16'-6"	25	897	16'-6"	25	899	15'-6"	25	900	15'-0"	23	901	14'-6"	22	902	14'-0"	21	903	13!-6"	20
3/4 19 STOCK NO 46-6375,5-07	_30	19	8	886	224-0*	33	.886	22*-0*	33	887	21'-6"	32	888	21'-0"	32	890	200.		891	19'-6"	29	893	180.	28	894	16'-0"	27	895	17'-6"	26
	<i>ا</i> ذ		8	872	29'-0"	44	875	271-6"	41	877	26'-6"	40	879	25'-6"	38	880	∠5°-0°	38	882	24'-0"	36	883	23'-6"	35	885	22"-6"	34	887	21'-6"	32
LONG TUDINAL RODS	32	19	16	880	25'-0"	38	880	25'-0"	38	880	25'-0"		881	241-6*	37	882	24'-0"	35	883	23'-6"	35	884	23'-0"	35	885	22'-6"	34	885	22'-6"	34
STOCK NO 46-6375.5-07	ند		8	877	25'-6"	40	880	25'-0"		881	241-6"	37	882	24"-0"	36	882	_54,-0.	36	883	23'-6"	35	883	25'-6"	35	885	22'-6"	34	885	22'-6"	34
HORTZÖNTÁL ROOS 3/4 Ø	.34	19	2	1007	31,-0.	47	1007	31'-0"	47	1008	301-6"	46_	1008	30'-6"	46	1008	30'-5"	46	1008	JO1-6*	46	1009	30*-0*	45	1009	30'-0 <i>"</i>	45	1009	30'-0"	- 45
STOCK NO 46-6375.5-07	35		2	1001	35'-0"	55	1001	35'-0"	53	1001	35'-0-	53	1002	34'-5"	52	1002	541-0-	-51	1003	34'-0"	51	1004	33'-6"	50	1004	35'-6"	50	1005	33'-0"	50

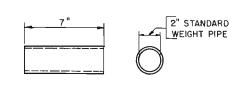
		TOWE	R HEIGHT		49'			47'			45'			43'			41.		ļ	59			37			35'			33'	
	36	18	2	1500R	29'-1 5/8"	1540	1501R	28'-1 1/2"	1490	1502R	27'-1 1/4"	1440	1503R	26'-1 1/8-	1380	1504R	25'-1"	1330	1506R	24'-0 3/4"	1275	1508R	23'-0 5/8*	1220	1509R	22'-0 1/2"	1170	1510R	21'-0 3/8"	1115
TOWER COLUMNS 12 X 12 I 53	37		2	1500L	29'-1 5/8"	1540	1501L	28'-1 1/2"	1490	1502L	27'-1 1/4"	1440	1503L	26'-1 1/8"	1.380	1504L	25'-1"	1530	1506L	24'-0 3/4"	1275	1508L	23'-0 5/8"	1220						
STOCK NO	38	18	2	1520R	20'-6 1/8"	1080	1773R	19'-6"	1035	1521R	18'-5 3/4"	930	1523R	17'-5 5/8"	925	1524R	16'-5 1/2"	870	1526R	15'-5 1/4"	820	1774R	14'-5 1/8"	765	1529R	13'-5"	710	1550R	12'-4 7/8"	_660
	39		2	1520L	201-6 1/8"	1080	1775L	191-61	1035	1521L	18'-5 3/4"	980	15231	17'-5 5/8"	925	15241	16:-5 1/2"	870	1525L	15'-5 1/4"	820	1774L	14'-5 1/8*	765	1529L	13'-5"	710	1530L	12'-4 7/8"	660
TRANSVERSE STRUTS	40	17	2	1572	22'-7"	950	1574	22*-3*	935	1573	21'-11"	920	1576	21 -7"	905	1578	21:-3*	995	1580	20'-11"	880	1582	20'-7"	865	1585	201-5"	850	1584	19'-11"	835
10 I 42 STOOK NO	41		2	1557	29*-11"	1260	1559	29'-3"	1230	1558	28'-7"	1200	1561	27'-11"	1170	1562	27'-3"	1150	1564	26'-7"	1115	1566	25'-11"	1090	1568	251-31	1060	1569	241-7*	1030
TRANSVERSE ROOS	42	19	8	892	190-	29	894	78,-0-	27	896	17'-0"	26	897	16 -5"	25	899	15'-6"	23	901	14'-6"	22	902	14*-0*	21	904	151-0"	20	905	12'-6"	19
3/4 Ø SCIOCK NO 146-6375,5-07	43		8	882	24'-0"	36	884	23'-0"	35	886	22'-0"	33	888	21'-0"	32	890	20,-0-	30	892	19'-0"	29	894	18"-0"	27	896	17'-0-	26	898	16'-0"	211
LONGITUDINAL RODS	44	19	8	877	26*-6*	40	879	251-67	38	830	25'-0"	38	881	24'-6"	37	882	24'-0"	36	883	23'-6"	35	885	221-6"	34	885	22'-6*	34	886	22'-0"	33
3/4 Ø STOCK NO. 46-6375.5-07	45		8	877	261-6"	40	879	25'-6"		880	25'-0"	38	881	24'-6"	37	882	24'-0"	36	883	23'-6"	35	885	22'-6"	34	885	22'-6"	34	886	22'-0"	33
HORIZONTAL ROOS	46	19	2	1007	51'-0"	47	1007	31'-0"	47	1007	310.	47	1008	70,-6"	46	1008	30'-6-	46	1005	30,-0.	45	1009	30'-0"	45	1009	-0-0	45	1010	29'-6"	44
STOCK NO 46-6375.5-07																														

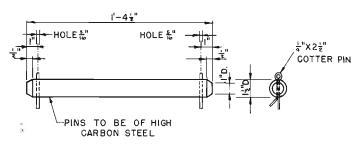
		TOWER	HEIGHT		31'			291	2010 100		27'			25.			23'			21'			19.			17			15'	
TOWER COLUMNS 12 × 12 I 53	47	19	2 .	1531R	31'-5"	1665	1532R	291-4 3/4"	1560	1535R	27'-4 5/8"	1450	1534R	25'-4"	1340	1535R	23'-3 3/4"	1235	1555R	211-3 5/8*	1150	1537R	19'-3 1/8'	1020	1538R	17'-2 3/4"	910	1539R	15'-2 3/8"	815
	48		2	1531L	51'-5"	1665	1532L	291-4 3/4"	1560	15534	27'-4 5/8"	1450	1534L	25'-4"	1340	1535L	25'-5 3/4"	1235	1536L	21'-5 3/9"	1150	1537L	19'-3 1/8-	1020	1538L	17'-2 5/4"	910	1539L	15 -2 3/8"	815
STOCK NO TRANSVERSE STRUTS 10 I 42 STOCK NO	49	17	2	1570	23'-11"	1005	1571	23'-3"	980	1572	22'-7"	950	1573	21'-11"	920	1578	21,-3-	895	1582	20*-7*	865	1584	19*-11"	840	1585	19'-3"	810	1586	18 -7"	780
TRANSVERSE ROOS 3/4 Ø STOCK NO 46-6375.5-07	50	19	8	885	22'-6"	34	889	20'-6"	31	892	19'-0"	29	896	171-0"	26	899	15:-6"	23	902	140-	21	905	12'-6"	19	907	11'-0"	17	910	9'-6"	14
LONGITUDINAL ROOS 3/4 # STOCK NO. #6-6375, 5-07	51	19	8	872	29'-0"	44	875	27'-6-	41	877	56,-6=	40	880	25'~0"	58	882	24'-0"	36	885	22'-6"	34	886	22'-0"	33	888	21'-0"	32	889	20'-6"	31

HIGHWAY





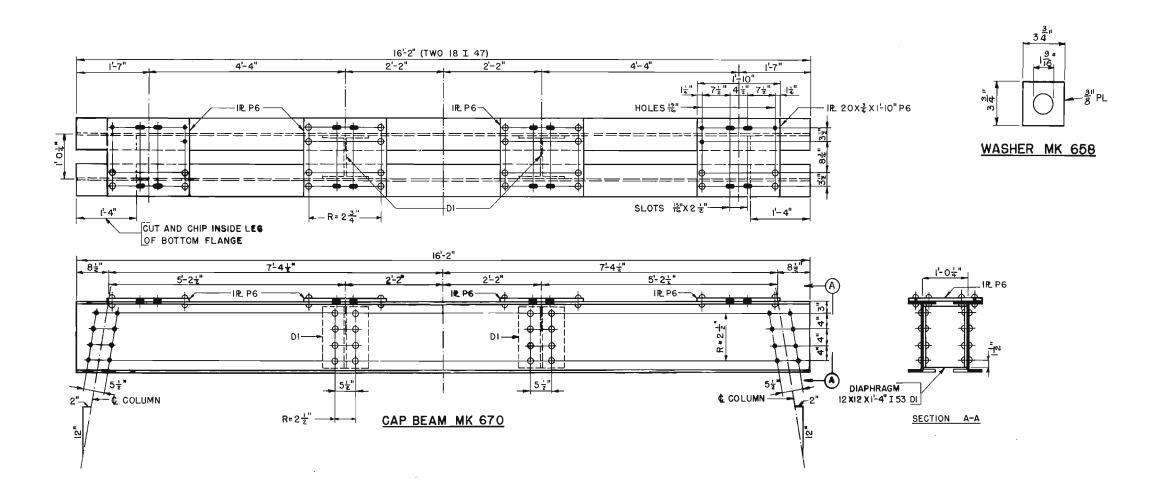




STRUT MK 671

PIPE SPACER MK 673

PIN AND COTTER PIN MK672

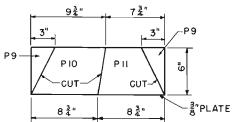


	SHEET
GENERAL NOTES	154
FRAMED STEEL TOWERS	12,13
BILL OF MATERIALS	14
BILL OF MATERIALS	15
SYMBOLS	155

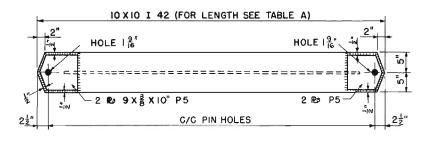
7差" P9-P 10 -cut CUT-8 3 "

ALL WELDS SHOWN TO BE

ALL RIVETS $\frac{7}{8}$ " ϕ ALL HOLES $\frac{15}{16}$ " ϕ UNLESS NOTED



BEARING PLATE STIFFENERS P9, PIO, PII





STRUT MK 1540 TO MK 1586

TABLE	Α
IADLE	<u> </u>

			
MARK	C/C PIN HOLES	LENGTH	WEIGHT
1540	38 '~10"	39'-3"	1687
1541	38'-2"	38'-7"	1659
1542	37'-6"	37'-11"	1631
1543	36-10"	37'-3"	1603
1544	36-2"	36'-7"	1575
1545	35'-6"	35'-11"	1547
1546	34'-10"	35'-3"	1519
1547	34-2	34-7"	1491
1548	33'-6"	33'-11"	1463
1549	32'-2"	32'-7"	1407
1550	32'-10"	33-3"	1435
1551	32'-4"	32'-9"	1414
1552	31'-10"	32'-3"	1393
1553	31'- 4"	31'-9"	1372
1554	31'-6"	31-11"	1379
1555	30'-10"	31'-3"	1351
1556	30'-2"	30-7"	1323
1557	29'-6"	29'-11"	1295
1558	28'-2"	28'- 7"	1239
1559	28'-10"	29-3"	1267
1560	27'-10"	28-3"	1225
1561	27'-6"	27-11"	1211
1562	26'-10"	27-3"	1183
1563	26'-6"	26-11"	1169

TABLE A

MARK	C/C PIN HOLES	LENGTH	WEIGHT
1564	26'-2"	26'-7"	1155
1565	25'-10"	26-3"	1141
1566	25'-6"	25'-11"	1127
1567	25'-2"	2 5'- 7"	1113
1568	24'-10"	25'-3"	1099
1569	24'-2"	24'-7"	1071
1570	23'-6"	23-11"	1043
1571	22'-10"	23'- 3"	1015
1572	22'-2"	22'-7"	987
1573	21'-6"	21'-11"	959
1574	21-10"	22'-3"	973
1575	21'-4"	21-9"	952
1576	21'-2"	21'-7"	945
1577	20'-0"	20'-5"	896
1578	20'-10"	21'-3"	931
1579	20'-8"	21'-1"	924
1580	20-6	20'-11"	917
1581	20'-4"	20'-9"	016
1582	20'-2"	20-7"	903
1583	19'-10"	20'-3"	889
1584	19'-6"	19'-11"	975
1585	18'-10"	19'-3"	847
1586	18-2"	18'-7"	819

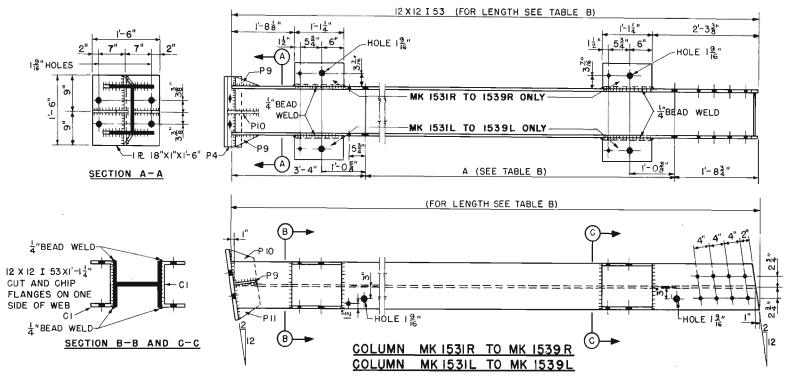
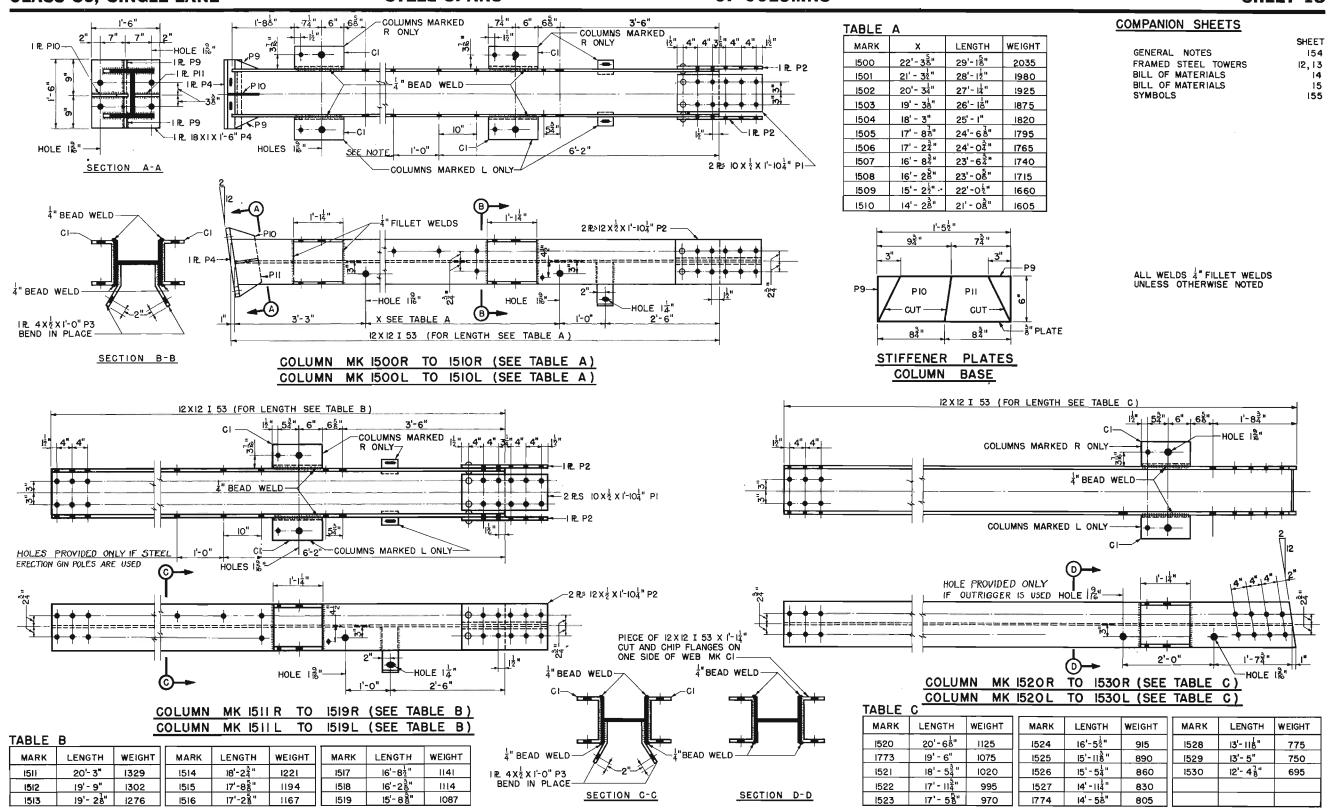
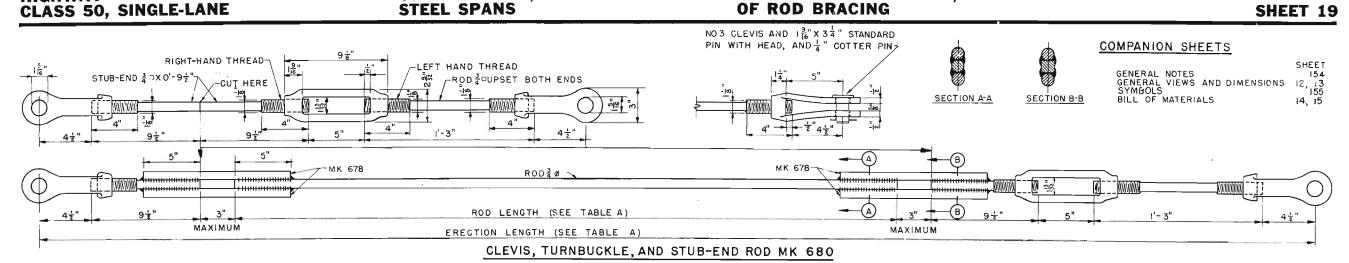


TABLE B

MARK	Α	LENGTH	WEIGHT
1531	26'-44"	31'- 5"	1935
1532	24'-4"	29-4월"	1830
1533	22'-38"	27'-48"	1715
1534	20'- 34"	25'-4"	1610
1535	18'-3"	23-33"	1500
1536	16'-2출"	21-3%	1395
1537	14-28"	19-3景"	1290
1538	12-2"	17-24"	1185
1539	10'- 18"	15'-2हे"	1075



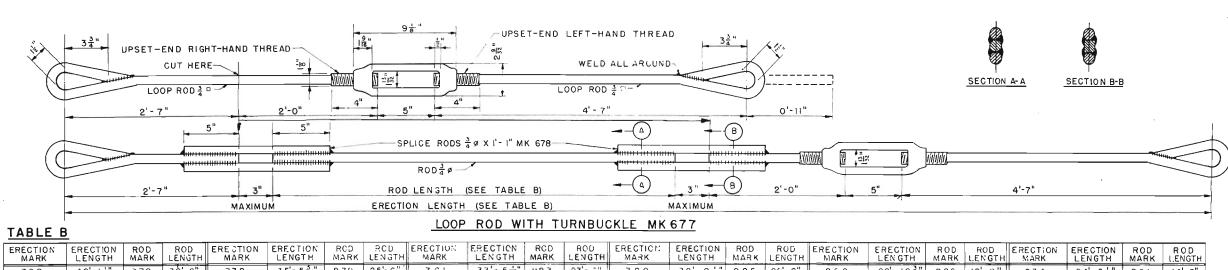


RIVETED CONSTRUCTION, FABRICATION OF ROD BRACING

TABLE A

HIGHWAY

ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROU MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH		ROD LENGTH
920	42'-6"	995	38'-6"	937	39'- 2 1 ''	10 01	35'-0"	946	37'-10"	1003	34'-0'	952	35'-1 5 "	1007	31' - 0"	957	34'-51	1008	30'-6"	962	34'-0"	1009	30'-0"
923	42'-15"	996	38'-0"	941	38¹-11 3 "	1001	35'-0"	947	37'- 7 3 "	1004	33'-6"	953	34' - 11 = "	1007	31'- 0"	958	34'-43"	1009	30'-0"	963	33'- 9 7"	_	29'-6
926	41'-94"	997	37'-6"	943	38'- 8 \frac{5}{8}"	1002	34'-€"	948	37'- 4 출"	1004	33' - 6"	954	34'-10 '8 "	1008	30'- 6"	959	34'-34"		30'-0"			1010	
927	41'-47"	997	37'-6"	944	38' - 34"	1003	3 4'-0"	949	37'- 2 '	1005	33'-0"	955	34'-9"	1008	30'- 6"	960	34'-24"	1009	30'- 0"				
9 2 8	41'-0ई"	998	37'- 0"	945	38'- 0 ⁵	1003	34' - 0"	951	35' - 4"	1007	31'-0"	95 6	34' - 6 5 "	1008	30'-6"	961	34'- 1 = "		30'-0"	_			



	_		_																				
ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	RCD MARK	RCD LENGTH	ERECTION MARK	ERECTION LENGTH	RCD MARK	ROU LENGTH	:10IT03R3 MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	R O D L.ENGTH
709	40'-14"	870	30'-6"	738	35'-5 \$ "	879	25'-6"	76!	33'-5 2 "	883	23'- 6"	780	32'-24"	885	22'-6"	909	28'-103"	892	19'-0"	834	24'-64"	901	14'-6"
711	39' - 44"	871	29'-6"	740	35'-5"	879	25'-6"	763	33'- 4"	883	23'- 6"	784	31' - 10흥"	886	2 2'- 0"	811	28'- 8 7 "	8 9 2	19'- 0"	837	24'-13"	901	14'-6"
7 5	38'-8 § "	872	29'-0"	742	34'-10 8 "	880	25'-0"	765	33'-24"	883	23'.6"	785	31' - 8 - 3"	886	22'-0"	814	28'- 41"	893	18'- 6"	838	23'-8 ½"	902	14'- 0"
716	38'-83"	872	29'-0"	743	34'-10 1 "	880	25'-0"	767	33'-0"	884	23'-0"	787	31' - 4½"	887	2:'-ε"	816	27'-105"	894	18'- 0"	841	23'- 33"	903	13'- 6"
7 8	38'-78"	872	29'-0"	745	34'- 74"	880	25'-0"	768	32'-11 8 "	884	23'-0"	788	31'~ 5ᇂ"	887	21,-6	819	27'- 43"	895	17'- 6"	843	22'-118"	904	13'- 0"
723	37'-108"	874	28'-0"	749	34'- 3音"	188	2 4'- 6"	770	32'-10€"	884	23'-0"	792	30'~10 3 "	888	21'-0"	823	27'- 04"	896	17'-0"	847	22'- 13"	905	12'- 6"
726	37'- 4호"	875	27'-6"	750	34'- 23"	881	2 4'- 6"	772	32' - 8늫"	885	22'-6"	793	30'-10½"	888	21'- 0"	825	26'- 7냠"	897	16'-6"	851	20'-8 6"	907	11,- 0,,
728	. 37'- 3출"	875	27'- 6"	754	33'-11 k "	882	2 4'-0"	771	32'- 64"	885	2 2' - 6"	795	30'- 6 "	889	20'- 6"	828	26'- 2 g ''	897	16'-6"	857	19'-4\frac{3}{8}"	910	9'-6"
729	37'- 12"	875	27'- 6"	755	33'-10 { "	882	2 4'-0"	774	32'- 5 8 "	885	22'-6"	799	30'- 12"	889	20'- 6"	829	25'-114"	898	16'-0"				
733	36' - 4 4"	877	26'-6"	757	33'-8 1 "	882	24'-0"	77 7	32'- 4불"	885	22'-6"	800	29'-10층"	890	20' - 0"	830	25'- 4"	899	15'-6"				
735	36'-1"	877	26'-6"	760	33' - 7출"	882	24'-0"	779	32'- 3 \$ "	885	2 2' - 6"	8.03	29' - 4 3 "	891	19' - 6"	832	24'-।। है "	900	15'- 0"				

47-7844.07

47-7844.1

ANCHOR BOLT 43-2219.08-04 7/8

10×3/4 1'-0" 26

10×1 1'-0" 34

4" 1.2

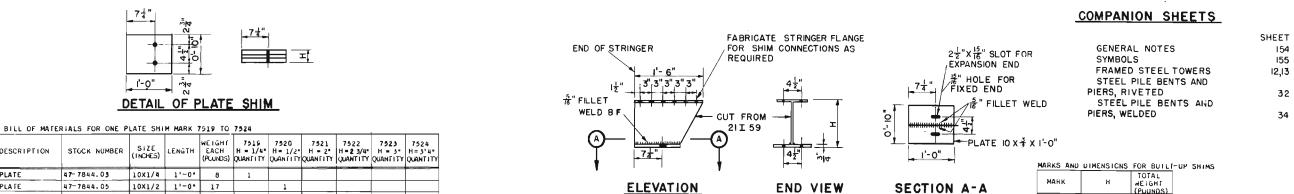
DESCRIPTION

PLATE

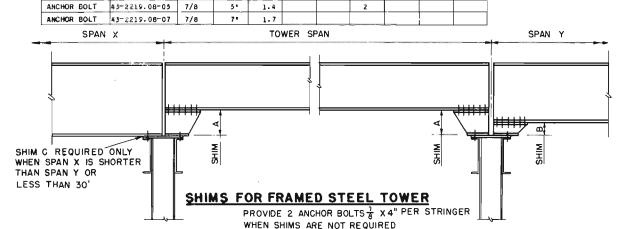
PLATE

PLATE

PLATE



ELECTRODE

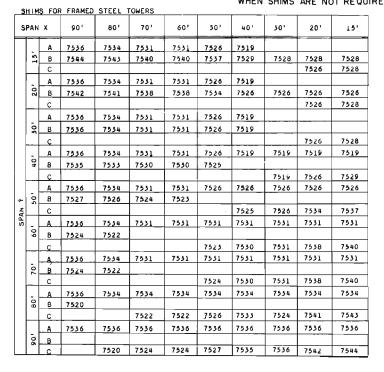


2

BILL OF MATERI	ALS FOR ONE BUI	LT-UP SI	HIM MARK	7525 TO 7544	ı
DESCRIPTION	STOCK NUMBER	SIZE (INCHES)	LENGTH	YIITHAUQ	
BEAM	48-2900.21-059	∠1 I 59	1'-6"	1	
PLATE	47-7844.07	10 × 3/4	1'-0"	1	
RIVET	43-6353.08	7/8	2 3/4"	12	
ANCHOR BOLT	43-2219-08-04	7/8	4.	2	

46-3772.2-7 3/16

******	l	TOTAL	
MARK	н	MEIGHT	
		(PUUNDS)	
7525	5 3/4"	57	
7526	6'-6"	57	
7527	6'-61/2"	58	
7528	8 *	60	
7529	8'-8 1/4"	61	
7530	8 7/8	62	
7531	9 1/8"	62	
7535	11 3/4"	66	
7534	12*	66	
7536	12 1/2"	67	
7537	14"	69	
7538	15 1/8*	71	
7540	17 1/8"	75	
7541	18*	76	
7542	18 1/2"	77	
7535	12*-4*	67	
7543	20*	79	
7544	20 1/2"	80	



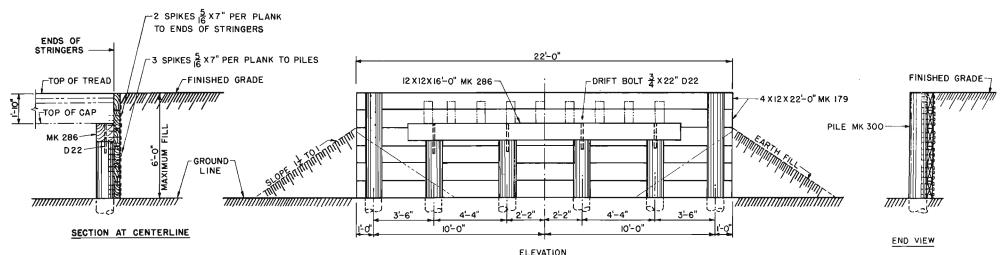
BILL OF	MATERIALS FO	OR ANCHOR BOLTS ONLY_	WI THOUT	SHIMS	
DESC	CRIPTION	STOCK NO	SIZE (INCHES)	LENGTH	WEIGHT EACH (POUNDS)
ANCHOR	BOLT	43-2219.08-04	7/8	0,-4*	1.2

TWO BOLTS REQUIRED FOR EACH STRINGER SUPPORT CONSTRUCTION INDICATED BY BLANK SPACES IN TABLES FOR SHIMS

SPAN X	SPAN Y	SPAN X	SPAN Y
3	*****		
	M H H	WIHS	
	SHIMS FOR STEEL	PILE BENTS AN	ID PIERS

Si	PAN X	901	80'	70'	60'	501	40'	30'	20'	15'
Ţ	15'	7544	7543	7540	7540	7557	7529	7528	7521	
	20'	7542	7541	7538	7538	7534	7526	7526		7521
	30'	7536	7534	7531	7531	7526	7519		7526	7528
۳.	40'	7535	7533	7530	7530	7525		7519	7526	7529
ž [501	7527	7526	7524	7523		7525	7526	7534	7537
3	60'	7524	7522			7523	7530	7531	7538	7540
	761	7524	7522			7524	7530	7531	7538	7540
Ĺ	96,	7520		7522	7522	7526	7533	7534	7541	7543
ſ	90'		7520	7524	7524	7527	7555	7536	7542	7544

SHEET
TIMBER ABUTMENTS FOR TIMBER SPANS 22
GENERAL NOTES 154
SYMBOLS 155

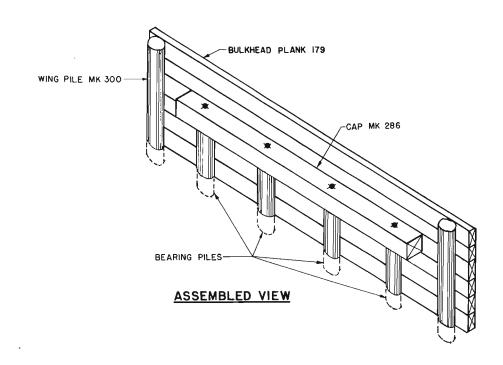


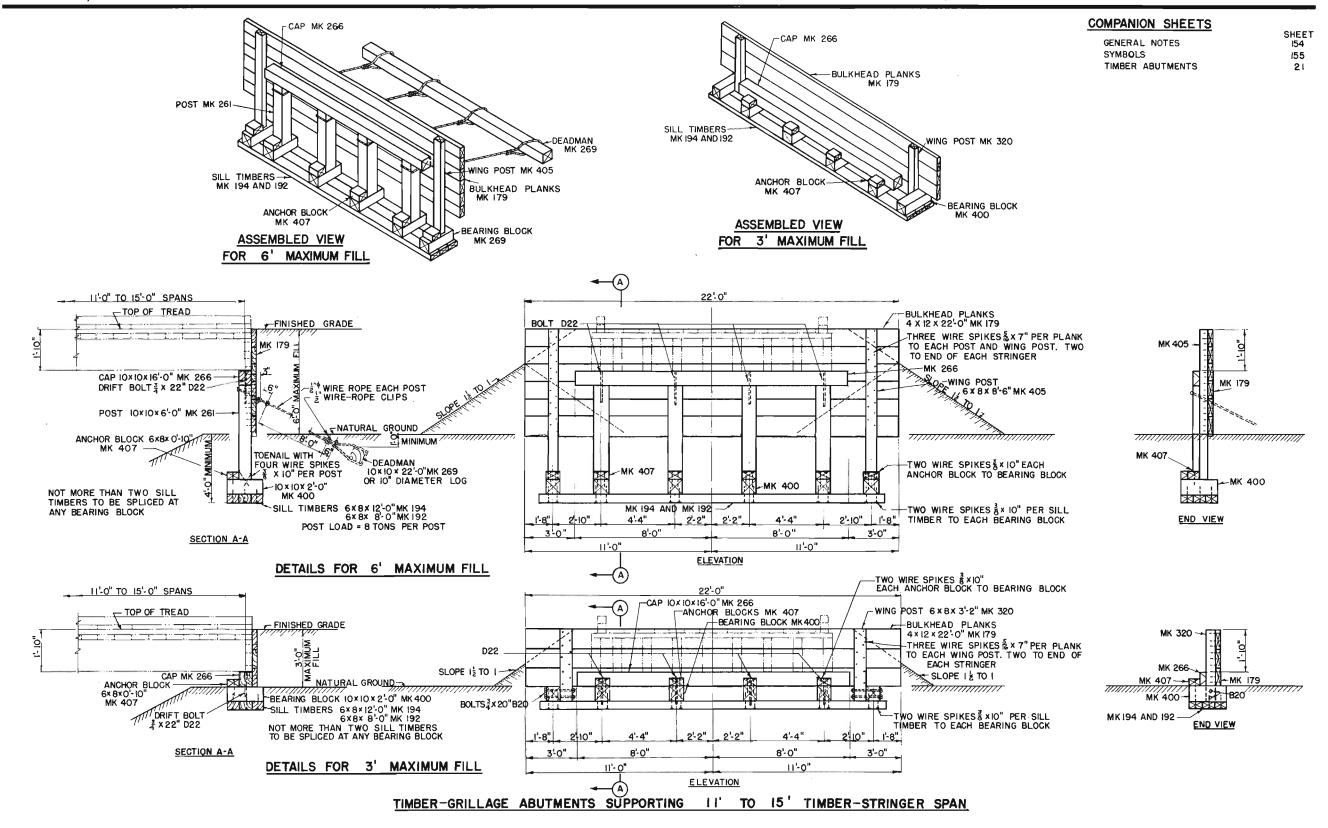
MAXIMUM LOAD PER PILE = 8 TONS

, A	MAXIMUM PILE	LOADS
	TONS	PER PILE
SPAN	STF	RINGERS
	TIMBER	STEEL
11'	8	
13'	8	
15'	8	8

		ELEVATION			
TIMBER PILE ABUTMENT	SUPPORTING S	SINGLE-LANE	CLASS 50	TIMBER-STRINGER	SPANS

		TYPE OF ABUTME	NT				TIMBER PILE	THEMTURA	TIMBE	ER GRILLA	GE ABUTMENT		
		FILL HEIGHT				Aprilia de la composición dela composición de la composición dela composición de la	6' MAX	CIMUM	6' NAX	HMUN	3' MA	KIMUM	7
LINE	DESCRIPTION	STOCK NUMBER	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	F8M	LINE
1	1 BULKHEAD PLANK	39-3340.12-22	179	4 X 12	22'-0"	330	6	528	6	528	3	264	1
2	PILE (WING)		300		15'-0"		2						2
3 .	2 PILE (BEARING)		_		2		4						1
4	3 POST (WING)	39-3360-08	320	6 X 8	31-2"	47					2	25	4
5	3 DO	39-3360.08	405	6 X 8	8'-6"	128			2	68			5
6	」POST (BEARING)	39-6620-1	261	10 × 10	6'-0"	188			4	200			6
7	CAP	39-6620.1-16	266	10 X 10	16'-0"	500			1	155	1	133	7
8	DO	39-6630-12-16	286	12 × 12	16'-0"	720	1	192					8
9	SILL TIMBER	39-3360-08	192	6 X 8	8'-0"	120			3	96	3	\$6	9
10	DO	39-3360-08-12	194	6 X 8	12'-0"	180			3	144	3	144	0 د
11	BEARING BLOCK	39-662C-1	400	10 X 10	2'-0"	163			6	17	6	17	11
12	DEADMAN	39-6620-1-22	269	10 × 10	22'-0"	687			1	183			12
13	ANCHOR BLOCK	39-3360.08	407	6 X 8	0'-10"	1.5)		6	20	4	14	13
	STEEL HARDWARE, BLACK												
14	WIRE ROPE	22-4567.4-05		1/2	20'-0"	13			6				14
15	WIRE-ROPE CLIPS	42-5544.5-05		1/2		0.7			24				15
16	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.07-2	820	3/4	20	3.1					4		16
17	DRIFT BOLT WITH SQUARE HEAD AND ONE WASHER	45-1636.07-22	022	3/4	22	3.0	4		ц		4		17
18	WIRE SPIKES	42-8488.035-07		5/16	7*	. 15	108		120		72		18.
19	DO	42-8488-04-1		3/8	10*	. 33			72		44		15
1 N	JMBER OF BULKHEAD PLANKS E	BILLED IS FOR MAX	IMUM FIL	L. USE FEWE	R PLANKS F	OR SHALLO	WER FILLS						
2 B	ARING PILE LENGTH TO BE D	ETERMINED BY FIE	LD CONDI	TIONS									





STEEL TOP OF TREAD

то воттом

CF STRINGER

2'-47"

2 - 6 7

3'-0

31-14

3'-67

3, -10,,

3'-10

4'-07"

STRINGER

16 I 36

18 I 47

SIZE

COMPANION SHEETS

TABLE A

SPAN

LENGTH FEET

20

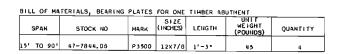
PILE

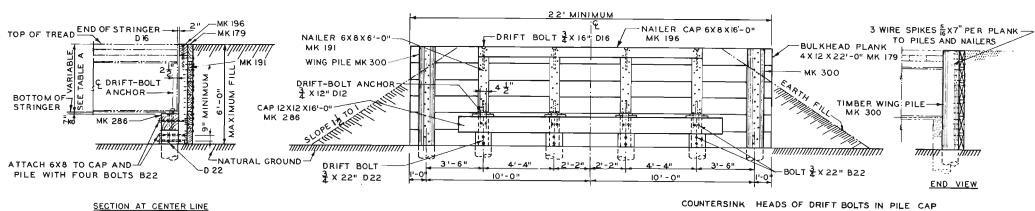
LOAD

TONS

8

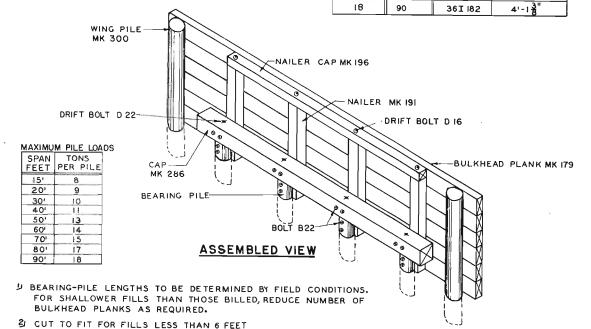
TIMBER ABUTMENTS FOR STEE GENERAL NOTES SYMBOLS	_ SPAN	SHEET 24 154 155
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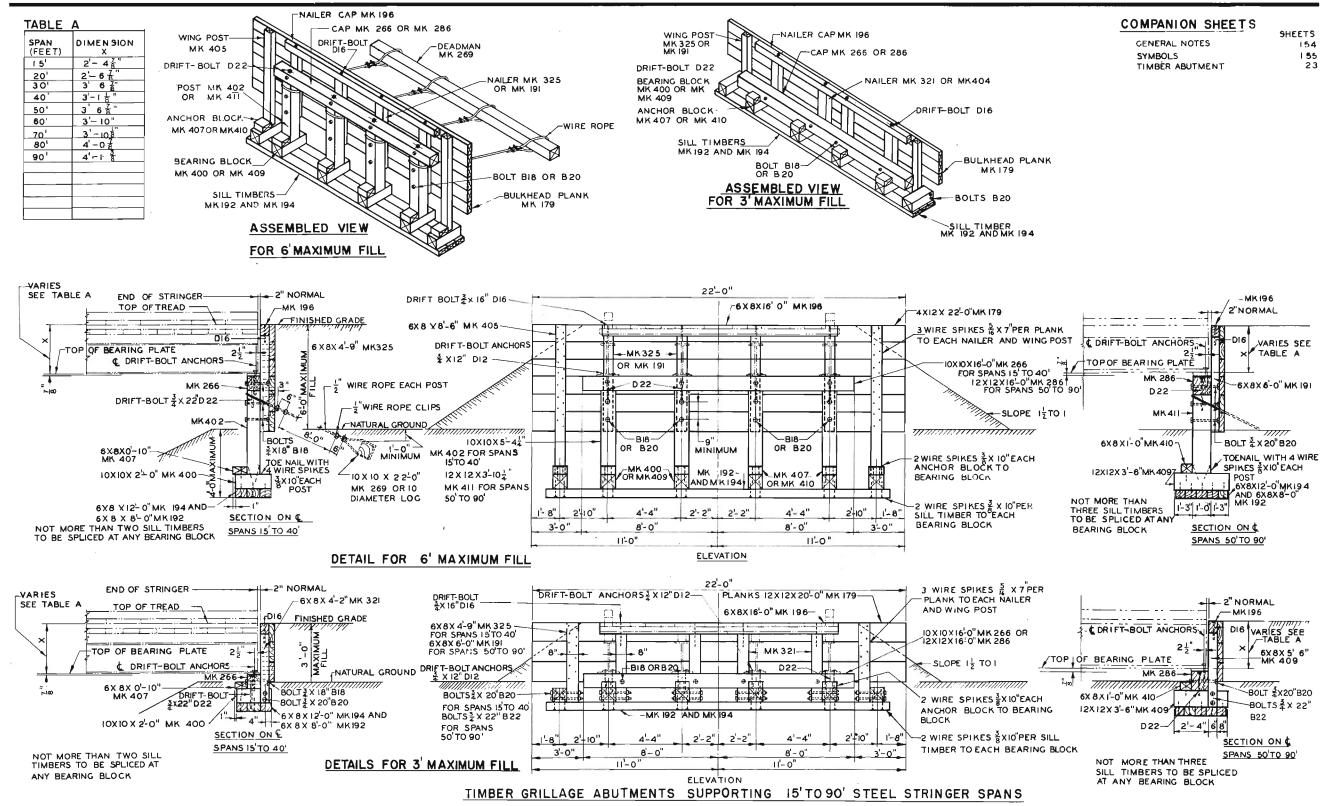




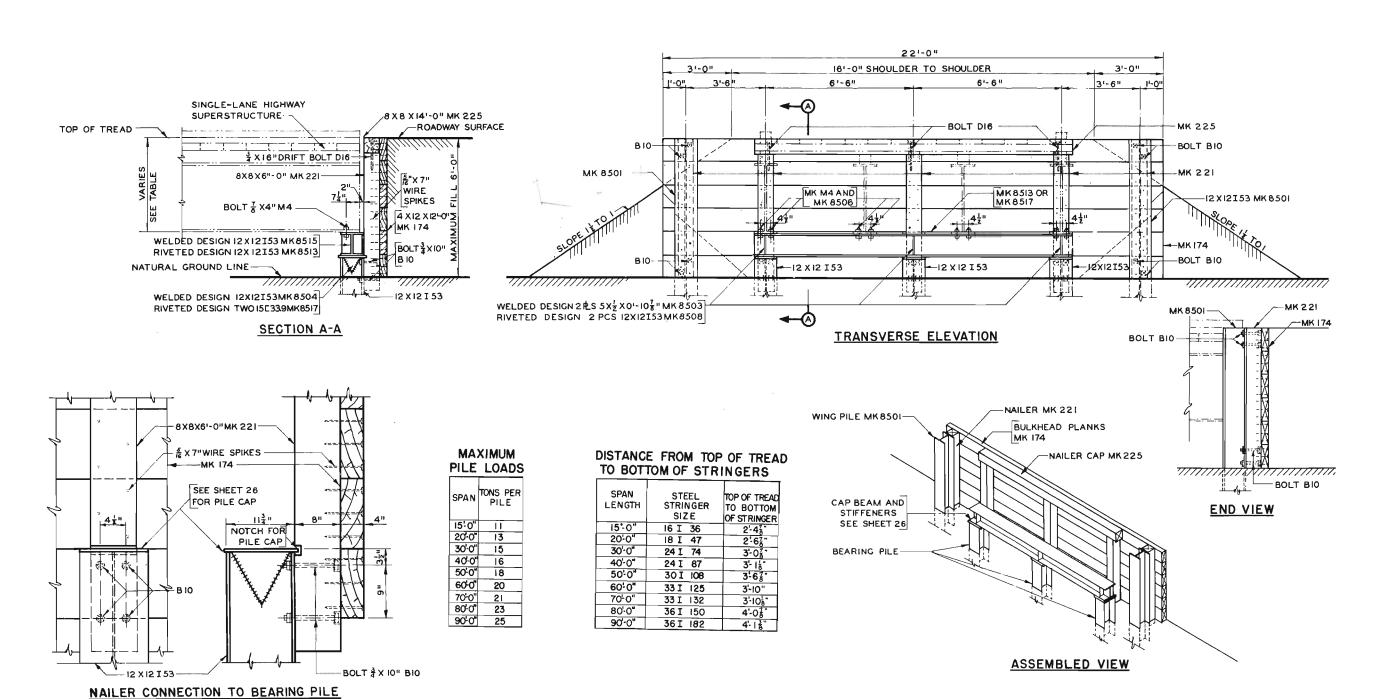
30 24174 10 П 40 24I87 13 50 301108 14 60 33 1125 COUNTERSINK HEADS OF DRIFT BOLTS IN PILE CAP 15 331132 TIMBER PILE ABUTMENT FOR 15' TO 90' SPANS 17 80 36I150

							PILE A				(RILLAGE	ABUTMENT			
	25525107151	2.500		SIZE	LENGTH	WEIGHT	90' MAXII	MUN SPAN		15' TC 8	C' SPAN			50' TO	90' SPAN	
LINE	DESCRIPTION	STOCK NUMBER	MARK	(INCHES)	LENGIN	(POUNDS)	o' MAXII	AUN FILL	6' MAXI	MUM FILL	3' MAX II	AUM FILL	6' MAXIML	M FILL	3' MAXIM	UM FILL
						(FCCMEDS)	QUANTITY	F6M	QUANTITY	FBM	QUANTITY	FBH	QUANTITY	FBM	QUANTITY	FEM
1	JBULKHEAD PLANK	35-3340.12-22	179	4X12	22'-0"	330	6	528	6	528	3	264	6	528	4	352
2	CAP	35-6020.1-16	266	10X10	16'-0"	500			1	133	1	133				
- 3	DO	39-6630-12-16	286	12/12	10,-0.	720	1	192		758			1	192	1	192
4	POST	39-66∠0.1	402	1CX10	5'-4 1/2"	167			ц	178						
5	3 DO	39-6636.12	411	12×12	3'-10 1/4"	173							4	185		
6	WING POST	39-3360.08	465	6.48	8,-0-	128			2	68			2	58		
7	DC DC	39-3360.68	325	6X8	41-9"	71				1250-1250	2	38		8376360 E012		
8	nc	39-3360,08	191	6×8	6'-0"	90									2	46
ç	PILE, BEARING						4						,			
10	MING PILE	1	300		15'-0"		2			. 11.000 0 0 11.000						
11	NAILER	39-3360.08	325	6X8	41-9"	71			4	76			T			
1.2	DO	39-3360.08	191	6X8	6'-0"	90	4	96					4	96		
13	DQ	39-3360.08	321	6X8	4'-2"	63					4	67				
14	DC	39-3360.08	404	6×8	51-6■	83									4	88
15	NAILER CAP	39-3360.08-16	196	6X8	16'-0"	240	1	64	1	64	1	64	1	64	1	64
15	SILL	0.08 € 5 € 60.	192	6XB	8'-0"	120			3	96	5	96	5	160	5	160
17	DO	39-3360.08-12	154	6X8	12'-0"	180			3	144	3	144	5	240	5	ź40
18	BEARING BLOCK	39-6620.1	400	10×10	2'-0"	63			6	100	6	100				
16	DO	39-6630.12	409	12X12	3'-6"	158							6	252	6	252
20_	ANCHOR BLOCK	39-3360.08	407	6X8	0'-10"	13			6	20	4	14				
21	DQ	39-3560.08	410	6x8	1'-0"	15							6	24	4	16
22	DEAUMAN	39-5620.1-22	269	10X10	22'-0"	687			1	185			1	185		
25	MIRE -ROPE	22-4321.4-05		1/2	20'+0"	13			6				6			
24	WIRE-ROPE OUIP	42-3544.5-05		1/2		0.72			24				24			
25	BOLT WITH HUT AND HASHER	43-2325.07-183	818	3/4	18"	2.7			12		4					
26	0.0	45-2325.07-2	B20	3/4	20"	3.,0					12		1.2		4	
27	DO	43-2325.07-223	B22	3/4	22".	3.0	16								12	
28	DRIFT-BOLT ANCHOR	43-1636,07-12	D12	3/4	12*	12	8		8		8		8		8	
29	DRIFT BOLT	43-1636.07-16	016	3/4	16"	8	4		4		4		4		4	
30	DU	43-1636-07-22	D22	3/4	22"	13	4		ц		4		4		4	
31	SPIKE STANDARD WIRE	42-8488.04-1		5/8	10"	0.33			72		44		96		68	
32	DO	42-8488.035-07		5/16	7	0.143	108		108	l	54		108		72	



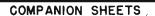


SHEET GENERAL NOTES SYMBOLS 155 STEEL PILE ABUTMENTS 26

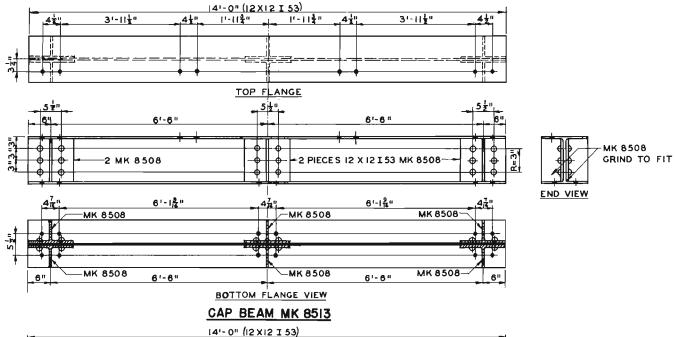


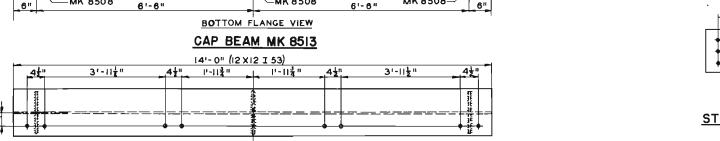
HIGHWAY

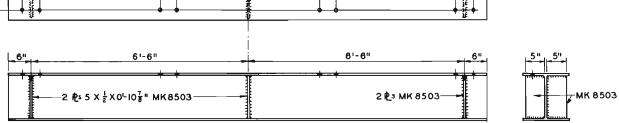
CLASS 50, SINGLE-LANE



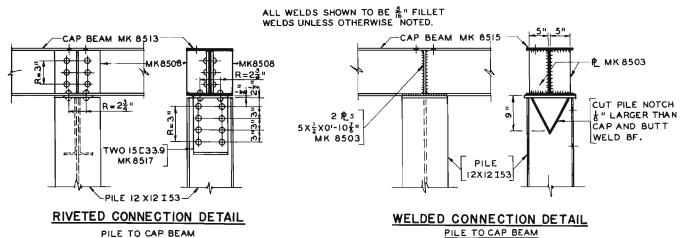
SHEET GENERAL NOTES 154 SYMBOLS 155 STEEL PILE ABUTMENTS 25

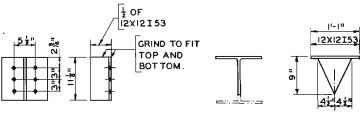






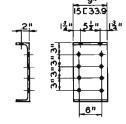
CAP BEAM MK 8515





STIFFENER MK 8508

PILE CAP MK 8504



PILE CAP MK 8517

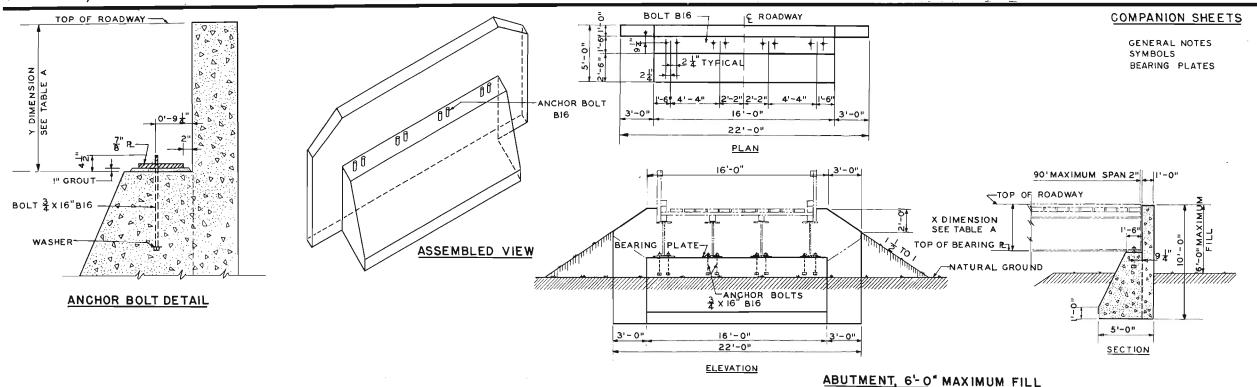
TEM COLUMN	DESCRIPTION	STOCK NUMBER	MARK	SIZE	LENGTH	QUANTITY	FEET BOARD MEASURE	WEIGH EACH
	ALTERNATE NO 1 WELDED DETAILS							
1	WING PILES		8501	12X12 I 53	15'-0"	2		795
2	CAP BEAM		8515	12×12 I 53	14'-0"	1		742
3	STIFFENERS	47-7844.05	8563	PL 5 X 1/2	10 7/8*	6		8
4	PILE CAP		8504	12X12 I 55	1,-1.	3		29
	ALTERNATE NO 2 RIVETED DETAILS							
5	WING PILES	!	6501	12X12 I 53	15'-0"	2		795
6	CAP BEAM		8513	12X12 I 53	14'-0"	ī		742
7	STIFFENERS		8508	1/2-12X12 I 55	10 7/8"	6		24
8	PILE CAP	48-3790.15-34	8517	15 [33.9	0'-9"	6		26
	LUMBER, SOFT WOOD							
و	NAILERS	39-6616-08	221	8 X 8	6'-0"	5	160	120
10	NAILER CAP	39-6616.08	225	8 × 8	14'-0"	1	75	280
11	BULKHEAD TIMBERS	39-3340.12-12	174	4 X 12	12'-0"	.12	576	180
	STEEL HARDWARE, BLACK							
12	BOLTS WITH NUTS AND THO WASHERS	45-2325.07-1	810	3/4	10*	20	ı	35
13	ANCHOR BOLTS WITH NUTS AND IND WASHENS	43-2219.08-04	M4	7/8	4-	8	1	12
14	DRIFT BOLTS WITH WASHERS	43-1636.07-16	016	3/4	16"	3	لد	6
15	WIRE SPIKES	42-8488.035-07		5/16	7.	90	ப	15
16	HIVETS	43-6353.08-25		7/8	2 1/2*	12		.62
17	RIVETS	45-6353.08		7/8	2 3/4"	42		.66
18	WELDING ROD	46-3772.2-7		3/16			لد	1.8

_1 TOTAL WEIGHT

PILE TO CAP BEAM

155

132



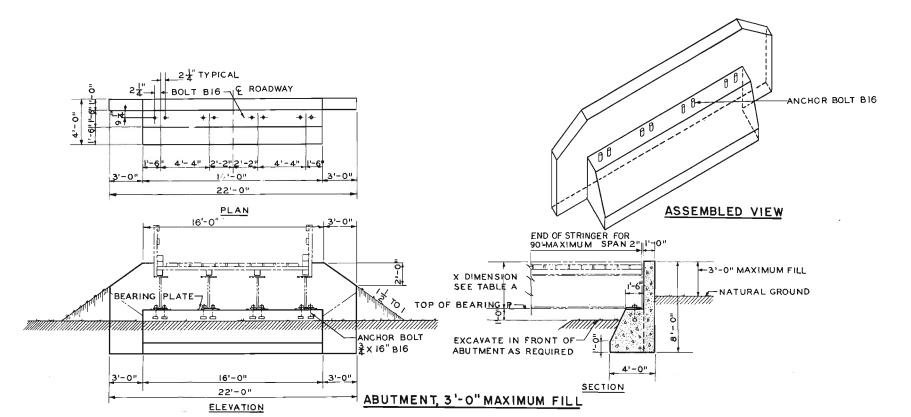


TABLE A - DIMENSIONS AND BILL OF MATERIALS

				OLTS WITH	CONC	RETE
S PAN FEET	Х	Y	WASHERS	3 X 16" B16 2 43-2325,07-16	6' MAXIMUM FILL	3' MAXIMUM FILL
			QUANTITY	WEIGHT EACH	CU YDS	CU YDS
15	2'- 478"	2'-6 3"	8	3.5	20.8	14.0
20	2'-67"	2'-8 \frac{1}{4} "	8	3.5	20.5	13.8
30	3'-07"	3'-23"	8	3.5	19.7	13.1
40	3'- 1 1 "	3'-3 "	8	3.5	19.7	13.1
50	3'-67"	3'-83"	8	3.5	18.9	12.5
60	3'-10"	3'-11 2"	8	3.5	18.4	12.1
70	3'-10g"	4'-0"	8	3.5	↓8.4	12.1
80	4'-08"	4'-23"	8	3.5	18.1	8.11
90	4'-13"	4'- 3 1/4"	8	3.5	18.0	11.7

BEARING PLATES (SHEET 132) 12 X ₹ X 1'-3" MK 3500 FOUR REQUIRED FOR EACH ABUTMENT STOCK NO 47-7844.08 — PILE CAP 12 X 18 -0" MK 287

TYPICAL 4-PILE TRANSVERSE BENT 10'-0" TO 16'-0"

BOLT I x 20 E20

| HEIGHT | SIZE | LENGTH | MARK | 10° 0° 10 | 158 | 150° 0° | 158 | 150° 0° | 159 |

-DRIFT BOLT

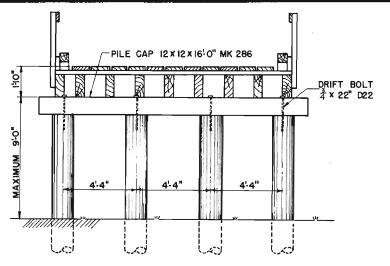
22" D22 BOLT 1×18" E18

BOLTS | X20" E20

COMPANION SHEETS

SHEET

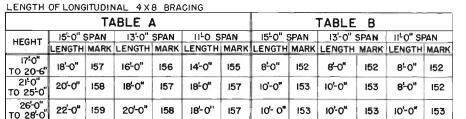
GENERAL NOTES 154
SYMBOLS 155
BENTS 17 TO 28 FEET HIGH 29



TYPICAL 4-PILE TRANSVERSE BENT I'-O" TO 9'-O"

		_			HE	EIGHT	1' W	91	10' T	0 12'	13'_1	O 16'	17' TO 2	20'6 *	21' T	0 25'	26'	TO 28'	┙
INE	DESCRIPTION	STOCK NO	MARK	STZE (INCHES)	LENGTH	MEIGHT	QUARTETY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE
LUM/B	BER, SOFT ACCO					(POUNDS)													
1	TIMBER PILE						4		4		4		4		4		ц		1
2	PILE CAP	39-6630.12-16	286	12 X 12	16'-0"	720	1	192											2
3	PILE CAP	39-6630.12-18	287	12 × 12	18'-0"	810		0.1	1	216	1	216	1	216		216	1	216	3
ц	BRACE	39-3340.08-22	159	4 X 8	22'-0"	220					2	117							4
5		39-3340.08-2	158	4 x 8	201-0*	200			2	107			2	107	2	107	4	213	5
6	00	59-3540.08-18	157	4 x 8	18'-0"	180									2	96			6
7		39-3540.08-16	155	4 x 8	16'-0"	160				_			2	35	2	85	2	85	7
8		39-3340.08-12	154	4 x 8	12'-0-	120							4	128					8
	L HARDWARE, BLACK																		
9	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	45-2525. 1-18	E18	1	18"	5. 1			4		ц		4		4		4		9
10	∞_	43-2325.1-2	E20	1	20"	5.6			8		. 8_		24		20		20		10
11	00	45-2325.1-24	E24	1	24"	6.5							8		6		6		11
12	DRIFT BOLT	43-1636,07-22	E22	3/4	22*	2.8		0.8007.73007	4		4		4		4		ц		12

BILL	OF MATERIALS FOR ONE PANEL OF	LONGITUDINAL BRACIN	IG OR STRU	TS (VIEWS ON	SHEET 29)																									
						HEIGHT			17' 10 20'	-6 *			1		21' TO	25'			l		26' TO	28'				NE SPAN I	NITH STRUTS	ONLY			
			_			SPAN	15'	SPAN	13'	SPAN	11'	SPOH	15' 5	SPAN .	131	SPAN	111'	SPAN	15'	SPAN	13'		11'	SPAN	15' 5	PAN	13'	SPAN	11'	SPAN	
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	- ALIGIN	QUANTITY	FBM	QUANTITY	FBM	QUARTIT	FBM	QUANTITY	FBM	QUANTITY	FBM	CLITHANC	FBM	QUANTIT	r FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE
LUMBE	R SOFT HOOD			•		(POUNDS)	•			<u>. </u>			"		-										"						
1	STRUTS OR BRACE	39-3340.08-22	159	4 X 8	22'-0"	220													2	117											1
2	00	39-3340.08-2	158	4 x 8	201-0*	200	2	107					4	213					2	107	2	107									2
-3	200	39-3340.08-18	157	4 x 8	18'-0"	180	4	192	2	96			2	96	4	192	2	96	2	96	2	96	2	96	2	96					3
п		39-3340.38-15	155	4 × 8	16'-C"	160			ц	171	2	85			2	85	2	85			2	85	2	85	1		2	85			4
5	m	39-3340.08-14	155	4 X 8	14'-0"	140					<u> </u>	150			 -		2	75		1			2	75					2	75	5
6	m	39-3340.08-1	153	4 x 8	10'-0"	100	4	107					8	213	4	107				213		107		107							6
7	m	39-3340.08-08	152	4 X 8	8'-0"	80	и	85	8	171	8	171			u	85	8	171			- A	85		85	1				1		7
8	SCAR	39-3228.08	324	2 X 8	3'-6"	18	<u></u>	19	_ n	19	u u	19	ш	19	и	10		10	,	19	,	10	. 4	10							8
0	no no	39-3228.08	81	2 x 8	61-0"	30	4	32	4	32	4	32	1	32	4	32	4	32	- 4	32		32	<u> </u>	32							9
STEEL	HARDWARE, BLACK								" '																						
	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325. 1-104	E10	1	10*	3, 45	20		20		20		20		20		20		20		20		20								10
11	00	43-2325.1-2	E20	1	20 *	5, 51	32		32		32		32		32		32		12		32		32	-		1					11
12	00	43-2325. 1-24	E24	1	. 24*	6.48	4		4		ų		4		4		4		4		4		4		4		ц		1		12



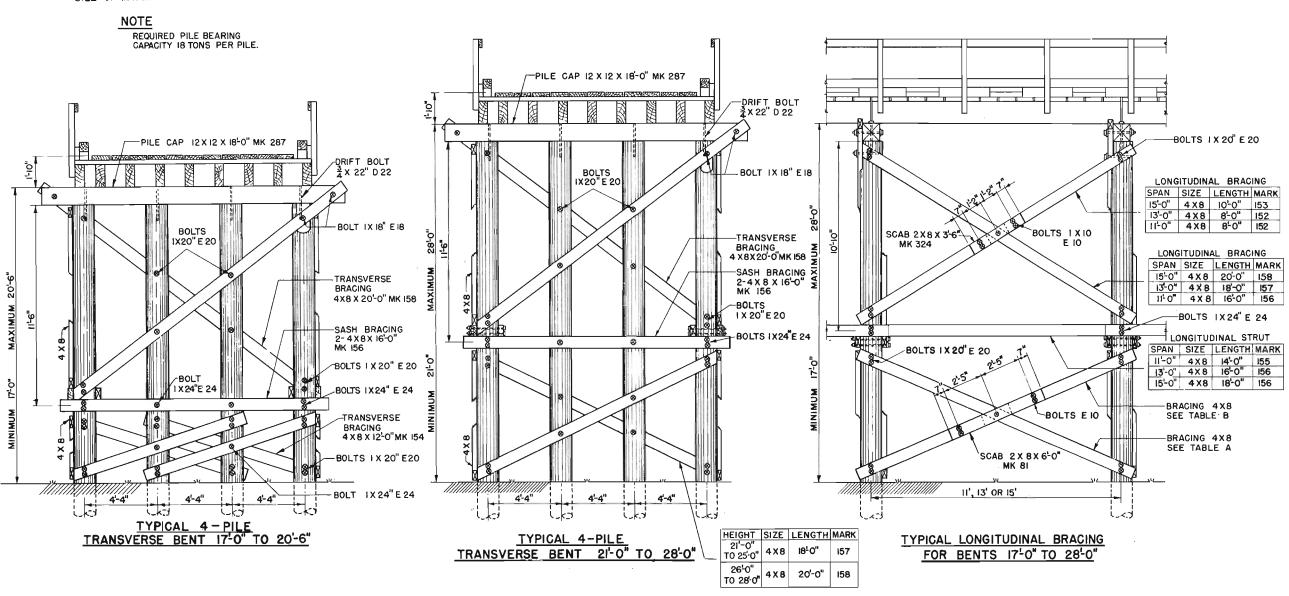
BENTS, 17 TO 28 FEET HIGH, GENERAL VIEWS

COMPANION SHEETS

GENERAL NOTES SYMBOLS I55
SYMBOLS I55
TIMBER PILE BENTS FOR TIMBER SPANS 28

DIAGRAM SHOWING LONGITUDINAL BRACING

TRESTLES OVER 17 FEET HIGH ALL HAVE LONGITUDINAL BRACING IN EVERY THIRD SPAN. STRUTS ARE CARRIED TO BANK AND FASTENED TO PILE NEAR GROUND LINE BILL OF MATERIALS ON SHEET 28



TOP OF

ROADWAY-

L'IME

BOTTOM OF

SHEET

31

154

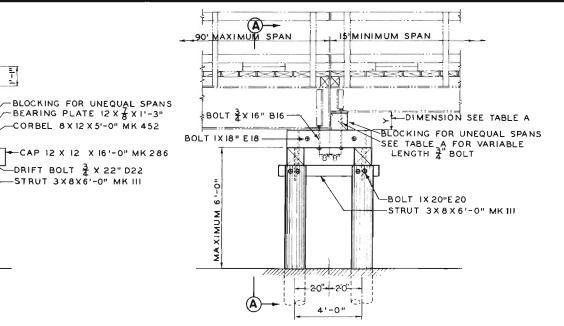
155

COMPANION SHEETS

BILL OF MATERIALS

GENERAL NOTES

SYMBOLS



REQUIRED PILE CAPACITY

··	0771		<u>' </u>	_					
TOTAL LENGTH OF TWO ADJACENT SPANS	30,	40°	60,	80'	100,	120	140	160'	1801
REQUIRED CAPACITY TONS PER PILE	10	10	12	13	14	15	16	17	18

TABLE A HEIGHT OF BLOCKING AND LENGTH OF 3"

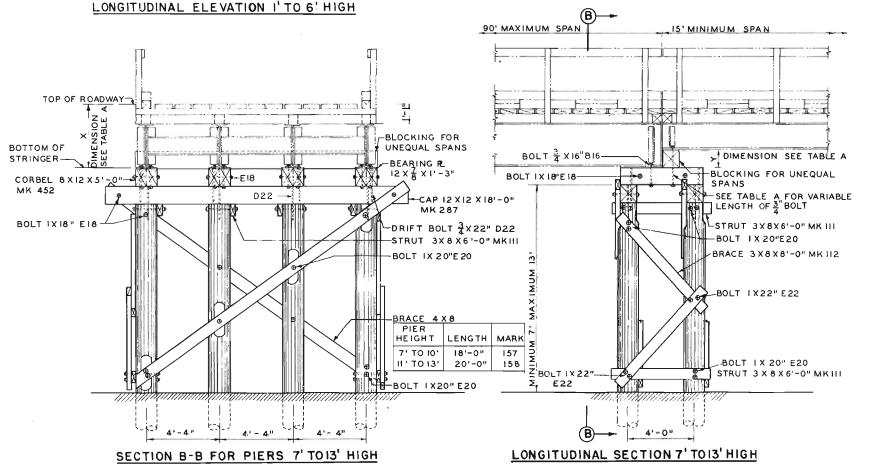
ANCHOR BOLTS FOR UNEQUAL ADJACENT SPANS

SECTION A-A FOR PIERS I' TO 6' HIGH

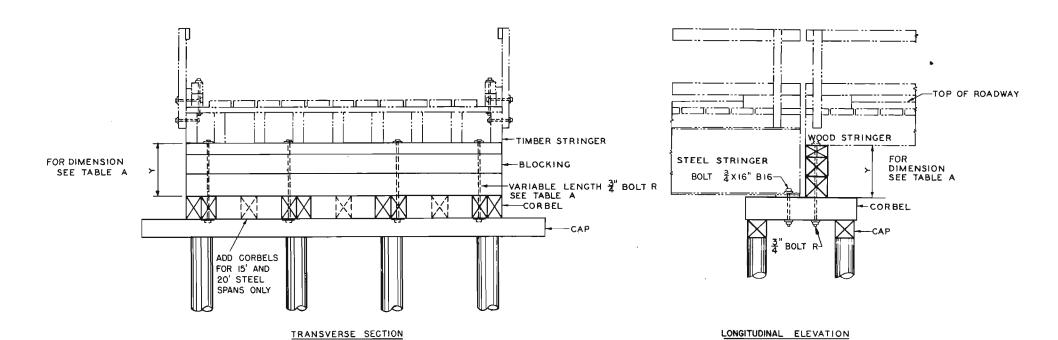
4' - 4"

-022

				ADJACENT SPANS										
			90'	80'	70'	60'	50'	40'	30'	20'	15'			
a S		DIMENSION X	5'-2#	5'-13"	4'-11"	4'-10경	' 4'-7۽'	4'-2"	4'-13"	3'-73"	3'-5 3"			
TIMBER	5,	DIMENSION Y	2'-4 ;"	2'-3¾"	2'-1"	2'-02"	1'-94"	1'-4"	1'-3≩"	0'-9¾"	0'-73"			
E S		BOLT LENGTH	42"	42"	38"	38"	36"	30"	30"	24"	22"			
		, x	5'-24"	5'-1월"	4'-11"	4'-10 ⁴	4'-7#"	4'-2"	4'-13"	3-7∄"				
	-2	Y	1'-8 1"	1'-8"	1'-54"	마-5늘"	1'-2"	0'-84"	0'-8"	0'-2"				
		DO	36"	36"	32"	32"	30"	24"	24"	18"				
i .		×	5'-24"	5'-13"		4'-102"	4'-73"							
	20'	Y	1'-61"	1'-6"	1'-3#"	1'-3 = "	יי 0 – יו	0'-64"	0'-6"					
		DO	34"	34"	30"	30"	28"	22"	22"					
1	30 -	×	5'-2#"		4'-11"	4'-108"	4'-7큐"	4'-2"]			
		Y	1'-07"	1'-0"		0'-9 🖁								
	,	DO	28"				22"	16"						
	40,	×	5'-24"			4'-103*								
SZ		Υ	;'-04"	0'-!!="	0,-9"		0'-5≹"							
SPANS		DO	28"	28"	24"	24"	22".							
	_	×			4'-11"									
1	50'	Y	0'-6 2"	0'-6"	0,-34,	0'-3 <u>f</u> "								
STEEL		00	22"	22"	18"	18"								
, v	_	×		5'-13"										
	09	Y	0'-3	0'-27"	0,-0 ⁸ ,,									
		DO	20"		16"									
	_	×	5'-24"	5'-14"										
	5	Y	0'-3‡"	0'-23										
		DO	20"	18"			<u> </u>							
		DIMENSION X	5'-2 ‡											
	80.	DIMENSION Y	0'-01"								.			
		BOLT LENGTH	16"											



COMPANION SHEETS SHEET GENERAL NOTES 154 SYMBOLS
TIMBER PILE PIERS FOR STEEL SPANS 15.5 30



ABLE	Α	
STEEL SPAN	DIMENSION Y	BOLT R
15'	0'-73"	22" 24"
20'	0'-9¾"	24"
30'	1-33"	30"
40'	('-4"	30"
50'	l'-9 ³ "	36"
60'	2'-0중"	38"
70'	2'-1"	38"
80'	2'-3 3 "	42"
90'	2'-44 "	42"

SPECIAL BLOCKING AT JUNCTION OF STEEL AND TIMBER SPANS

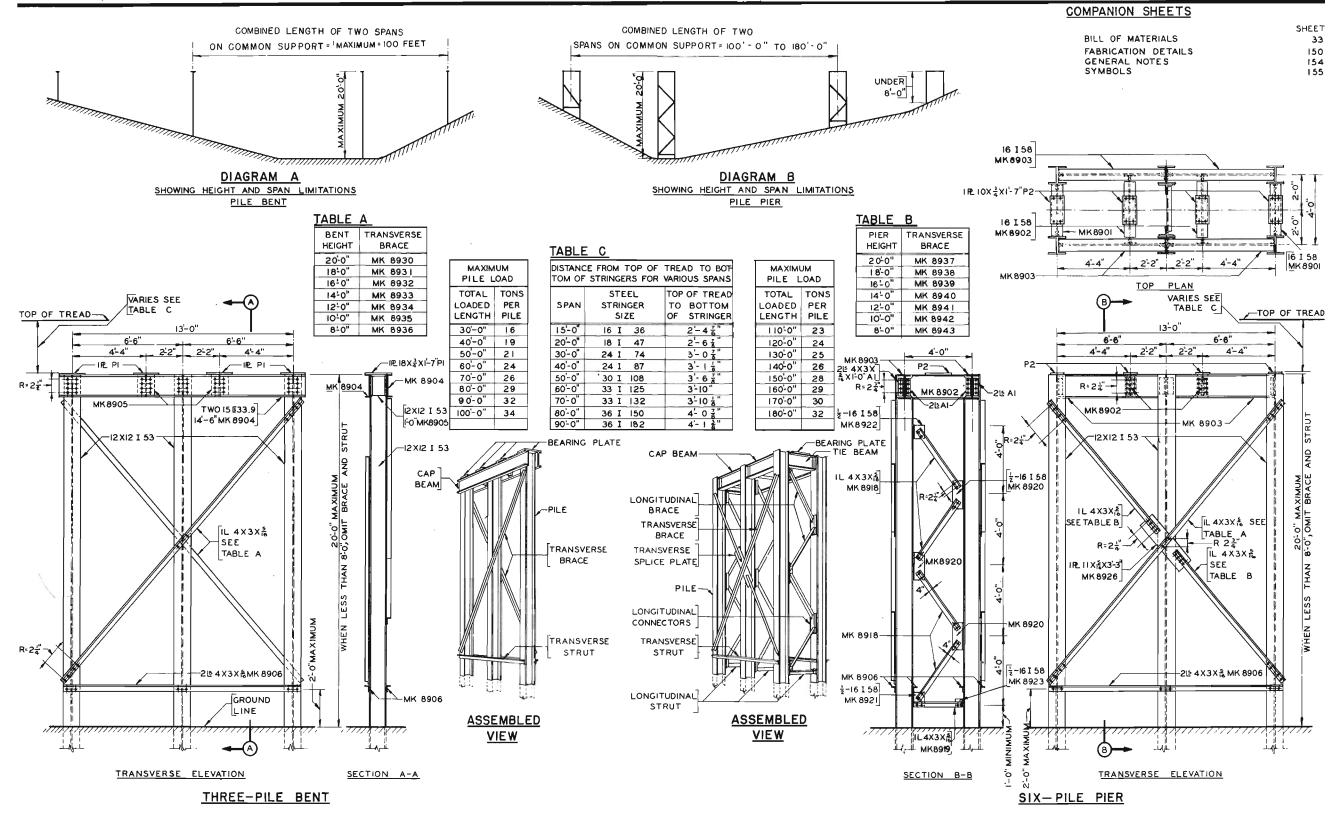
				6.175		UNIT	PIEK HEIGHT							
INE.	DESCRIPTION	STOCK NUMBER	MARK	SIZE (INCHES)		WEIGHT	1' 10 6'		7' TO 10'		11' [0 15'			
						(POUNDS)	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE	
1	TIMBER PILE			7	1		. 8		8		8		1	
2	PILE CAP	39-6630.12-16	286	12 × 12	16'-0"	810	2	384					2	
<u> </u>	DO	39-6630-12-18	287	12 × 12	18'-0"	720			2	452	2	432	3	
4	CORBEL	39-6616.12	452	8 × 12	5'-0"	150	8	320	8	320	8	320	4	
5	FRANSVERSE BRACE	39-3340.08-18	157	4 X B	18'-0"	180			4	192			5	
6	DC	35-3340.08-2	158	4 X 8	20'-0"	200					4	215	6	
7	LONG ITUDINAL BRACE	39-3330.08-08	112	3 × 8	8'-0"	60			4	64	4	64	7	
8	STRUT	39-3330.C8	111	3 X 8	6'-0"	45	4	48	6	72	0	72	8	
	STEEL HARDWARE, BLACK	_												
9	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325-1-22	٤22	1	22"	6.1			8		8		9	
10	DO	43-2525-1-2	E20	1	20"	5.6	16		40		46		10	
11	00	43- 2325-1-18	E18	1	18"	5.2	8		16		16		11	
12	DO	45-2325.07-16	B16	3/4	16"	2.6	16		16		16		12	
13	DRIFT BOLT	43-1636.07-22	D22	3/4	22*	3.0	16		16		16		13	
14	BEARING PLATE	47-7844.08		PL 12 X 7/8	1'-3"	45	8		8		8		14	

3/4" ANCHOR BOLT WITH SQUARE NUT AND TWO WASHERS FOR REQUIRED LENGTH SEE TABLE A FOUR REQUIRED AT EACH SUPPORT FOR EACH TIMBER SPAN EIGHT REQUIRED AT EACH SUPPORT FOR EACH STEEL SPAN							
BOLT LENGTH STOCK NUMBER							
16"	43-2325.07-166						
18 -	43-2325.07-183						
20 •	43-2325.07-2						
22* 43-2325.07-223							
24"	43-2325.07-24						
28 *	43-2325.07-28						
30 °	43-2325.07-305						
32 4	43-2325.07-32						
34*	43-2325.07-346						
36*	43-2325.07-366						
38 43-2325,07-386							
43-2325.07-425							

VARIABLE BLOCKING 12" WIDE X 16'-0" LONG OF DEPTHS REQUIRED AS SHOWN BY DIMENSION Y

HIGHWAY

CLASS 50, SINGLE-LANE



RIVETED CONSTRUCTION, BENTS AND PIERS UP TO 20 FEET HIGH BILL OF MATERIALS

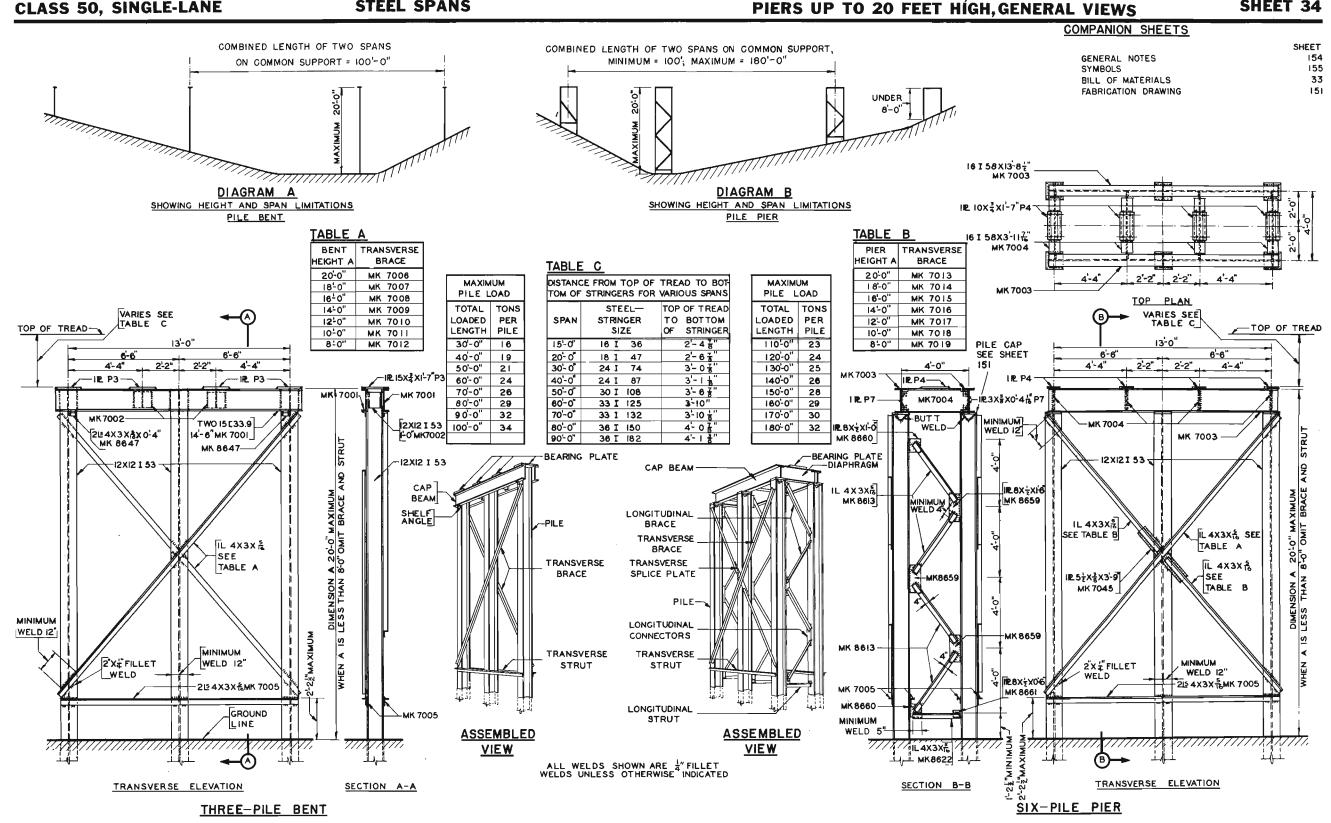
SHEET STEEL PILE BENTS AND PIERS, RIVETED DETAILS GENERAL NOTES SYMBOLS 32 154 155

BILL OF MATERIALS FOR ONE RIVETED STEEL PILE BENT OR PIER

HIGHWAY CLASS 50, SINGLE-LANE

	BILL OF MATERIALS FOR O	NE KIVEIED SIEEL F	TILE BEN	I OR PIER					STEFI	PILE BE	NI HELG	SHT					STEEL	PHE	PIER HEI	СИТ			
			DESCRIP	TION			20'	18'	16'	14'	12'	10'	8'	UNDER 8	20'	18'	16'	14'	12'	16'	8'	UNDER 81	.1
LINE	USE	STOCK NUMBER	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	QUANTITY						QUANTITY									7
1	CAP BEAM	48-2900.16-058	8903	16 I 58	6'-5"	372									4	4	4	4	4	4	4	4	
2	DO	48-3790.15-34	8904	15 € 33.9	14'-6"	492	2	2	2	2	2	2	2	2									2
3	DIAPHRAGM		8905	12X12 I 53	1'-0"	53	2	2	2	2	2	2	2	2									3
4	DO	48-2900.16-058	8901	16 I 58	2'-11 5/8"	172									2	2	2	2	2	2	2	2	4
5	DC	48-2900-16-058	8902	16 I 58	3'-10 3/4"	226				P					2	2	2	2	2	2	2	2	5
6	STRUTS AND BRACES	48-2550.4-035	8906	L4 X 3 X 5/16	14'-0"	101	2	2	2	2	2	2	2		4	4	u	ц	4	4	4		6
7	DC	48-2550-4-035	8918	L4 X 3 X 5/16	4'-11/8"	30									12	y	و	6	6	3	3		7
. 8	DC	48-2550.4-035	8919	L4 X 3 X 5/16	21-5 1/4"	20									3	3	3	3	3	3	3		8
9	DC	48-2550.4-035	8936	L4 X 3 X 5/16	21'-1"	152	2							_	2								ç
10	DC	48-2550.4-035	8931	L4 X 3 X 5/16	15'-8"	142		2								2							10
ū	DC	48-2550.4-035	8932	L4 X 3 X 5/16	18'-3"	132			2								2			_			11
12	DC	48-2550.4-035	8933	L4 X 3 X 5/16	171-1*	123				2								2					12
13	DC	48-2550.4-035	8934	L4 X 3 X 5/16	16'-0"	115					2								2	_			13
14	00	48-2550.4-035	8935	L+ X 3 X 5/16	15'-2*	109						2								2			14
15	DC	48-2550.4-035	8936	L4 X 3 X 5/16	14'-6*	105	<u> </u>						2								2		15
16	DO	48-2550.4-035	8937	L4 X 3 X 5/16	10'-4"	74	L								4								16
17	DO	48-2550.4-055	8938	L4 X 3 X 5/16	91-8*	70										4							17
18	00	48-2550.4-035	8939	L4 X 3 X 5/16	9'-0"	65					200.00			_			4						18
19	DO	48-2550.4-035	8940	L4 X 3 X 5/16	81-3*	60												4					15
20	DO	48-2550.4-035	8941	L4 X 3 X 5/16	7'-8"	55													4				20
21	DO	48-2550.4-035	8942	L4 X 3 X 5/16	71-2*	52								_						4			21
22	DO	48-2550-4-035	8943	L4 X 3 X 5/16	6'-7"	48								_							ц	oxdot	22
23	CONNECTOR	48-2900.16-058	8920	1/2 16 I 58	1'-61/2'	45									9	6	6	3	3				23
24	DO	48-2900.16-058	8921	1/2 16 I 58	0'-10 1/8"	24	ļ								3	3	5	3	3	3	3		24
2.5	DC	48-2900-16-058	8922	1/2 16 I 58	0'-83/4"	21									3	3	3	3	3	3	3		25
26	DG	48-2500.16-058	8923	1/2 16 I 58	0'-6"	15								_	3	3	3	3	3	3	3		26
27	00	47-7844.04	8926	PL 11 × 3/8	31-34	38									2	2	2	2	2	2	2		27
28	DG	48-2550.4-035	Al	L4 X 3 X 5/16	1'-0-	7									32	32	32	52	32	52	32	32	28
29	BEARING PLATE	47-7844.07	Pl	PL 18 X 3/4	1'-7"	73	4	ц	4	4	4	4	4	4									25
30	06	47-7844.07	P2	PL 10 X 3/4	1'-7"	40								-	4	4	4	4	4	4	4	4	30
51	RIVET	45-6353.08-2		7/8	2*	.53									16	16	16	16	16	16	16	16	51
32	DC	43-6353.08-23		7/8	2 1/4"	. 57	32	32	32	32	32	32	32		232	220	220	208	208	196	196	96	32
33	DC	43-6353.08-25		7/8	2 1/2"	.62	60	80	80	80	90	80	80	80	152	140	140	128	128	116	116	80	33
34	00	45-6353.08-3		7/8	3*	. 70	16	16	16	16	16	16	16	16									34
35	PILE			12 × 12 1 53			5	3	3	3	3	3	3	3	6	6	6	6	- 6	6	6	6	35

HIGHWAY



WELDED CONSTRUCTION, BENTS AND

14 30

27 27

6

6

6 6 6 6

24

6

24

	SHEET
GENERAL NOTES	154
SYMBOLS	155
STEEL PILE BENTS AND PIERS	34

BILL OF MATERIALS FOR ONE WELDED STEEL PILE BENT OR PIER STEEL PILE BENT HEIGHT
18' 16' 14' 12' 16' STEEL PILE PIER HEIGHT DESCRIPTION 8' UNDER 8' 18' 16' 14' 12' 10' USE DESCRIPTION SIZE (INCHES) QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY LINE LINE STOCK NUMBER CTITIVAND ALL LINEARD ALL LAND (POUNDS 7001 15 [33.9 14'-6" 492 1 CAP BEAM 48-3790.15-34 7003 16 I 58 13'-81/2" 792 48-2900.16-045 2 DO 3 DIAPHRAGM 7GO2 12X12 I 55 1'-0" 53 3 7004 16 I 58 3'-11 7/16" 229 4 DO 48-2900.16-045 4 4 4 .4 5 STRUTS AND BRACES 48-2550.4-035 7005 L4 X 3 X 5/16 14'-0" 101 4 4 4 5 7006 L4 × 3 × 5/16 21'-1" 152 6 DO 48-2550.4-035 2 7007 L4 X 3 X 5/16 19'-8" 142 2 48-2550.4-035 7 00 7008 L4 X 3 X 5/16 18'-3" 132 2 8 8 DO 48-2550.4-035 7009 L4 X 3 X 5/16 | 17'-1" | 123 9 DO 48-2550.4-035 _ 9 _ 7010 L4 X 3 X 5/16 16'-0" 115 10 00 10 48-2550.4-035 7011 L4 X 3 X 5/16 15'-2" 109 11 48-2550.4-035 DO 7012 L4 X 3 X 5/16 L4'-6" 105 12 DO 48-2550.4-035 12 7013 L4 X 5 X 5/16 10'-4" 74 48-2550.4-035 13 DO 1.5 7014 L4 X 3 X 5/16 9'-8" 70 48-2550-4-035 14 14 00 7015 L4 X 3 X 5/16 9'-0" 65 48-2550.4-035 15 DO 7016 L4 X 3 X 5/16 8'-3" 60 4 48-2550.4-035 16 16 DO 7017 L4 X 3 X 5/16 7'-8" 55 17 48-2550.4-035 17 DO 7018 L4 X 3 X 5/16 7'-2" 52 48-2550.4-035 18 18 DQ 48-2550.4-035 7019 L4 X 3 X 5/16 6'-7" 19 15 DO 48-2550-4-035 8613 L4 X 3 X 5/16 4'~1 13/16' 30 20 DO 20 8622 L4 X 3 X 5/16 2'-9 1/4" 20 3 3 3 3 3 21 3 _21 00 48-2550.4-035 22 CONNECTOR 7045 PL 51/2 x 3/8 3'-9" 26 22 47-7844.04 2 2 8659 PL 8 X 1/2 1'-6" 20 23 00 47-7844.05 6 3 3 23 8660 PL 8 X 1/2 1'-0" DO 47-7844.05 6 6 24 8661 PL 8 X 1/2 01-6" 25 00 47-7844.05 7 25 47-7844.07 P3 PL 15 X 3/4 1'-7" 60 26 BEARING PLATE 26 P4 PL 10 X 3/4 1'-7" 40 27 DO 47-7844.07 27 28 BOLTING CLIP 47-7844.04 P7 PL 3 X 3/8 0'-4 1/16" 16 16 16 16 16 16 16 28 8647 L4 X 3 X 5/16 0'-4" 48-2550-4-035 2 4 4 4 4 29 29 SHELF ANGLE

46-3772.2

3/16

12 × 12 I 53

12 X 12 I 55

11

11

11

3

11

3

11

11

3

11

3

33

30

6

30

6

30 WE'LDING ROD (POUNDS)

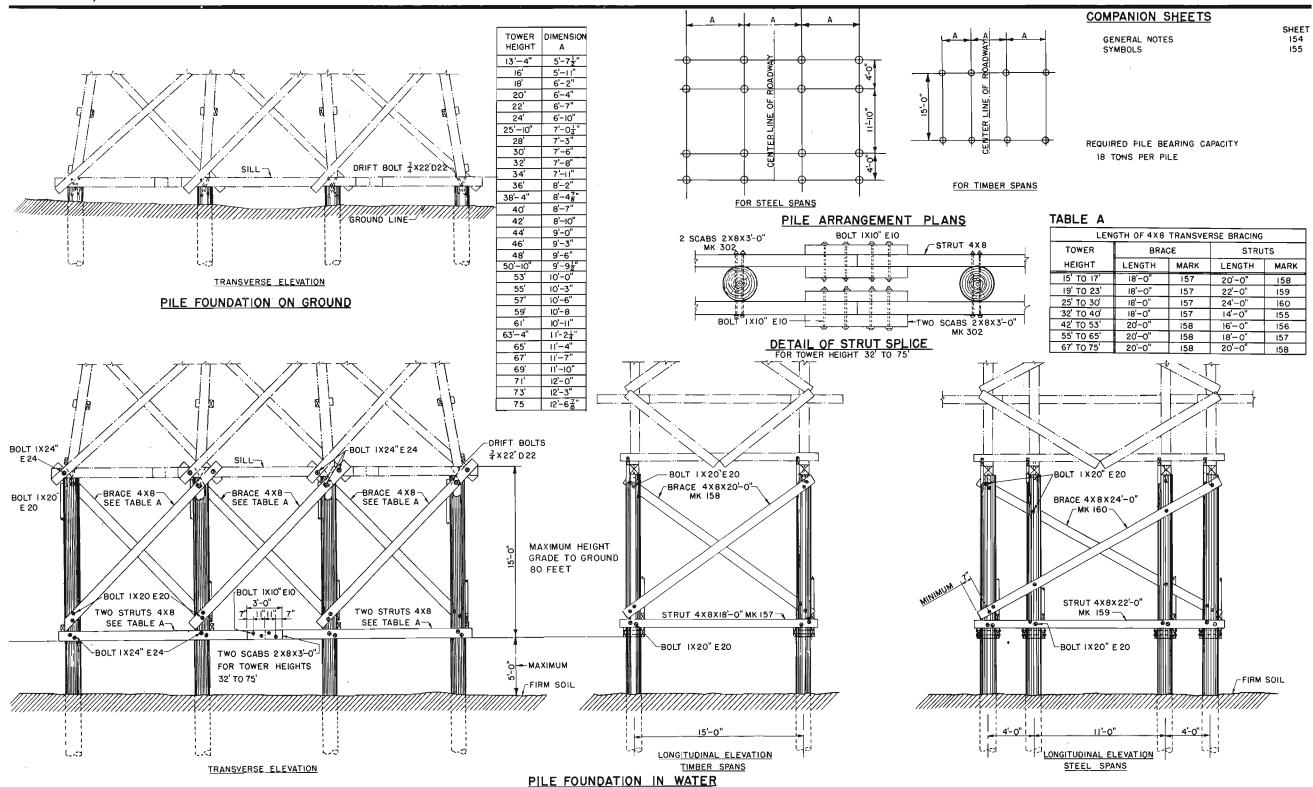
31 PILES

32 PILE CAPS

HIGHWAY

CLASS 50. SINGLE-LANE

____ PILING LENGTH TO BE DETERMINED BY FIELD CONDITIONS



ANCHOR BOLT SETTING PLANS

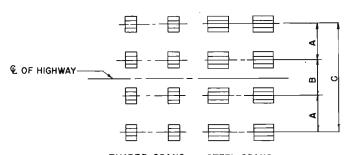
-PARALLEL TO & OF HIGHWAY

FOOTINGS F 105, F107 AND F109

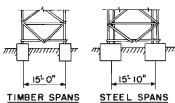
BOLT 1X30

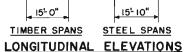
COMPANION SHEETS

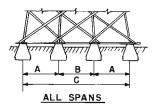
SHEET GENERAL NOTES SYMBOLS 154 155



TIMBER SPANS STEEL SPANS PLAN OF CONCRETE PEDESTALS



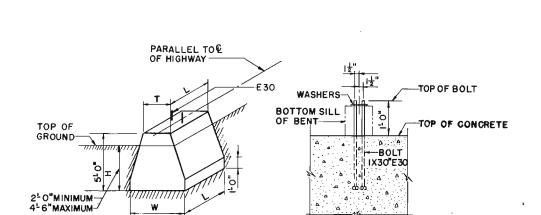




TRANSVERSE ELEVATION

CONCRETE PEDESTALS

	TOWES				FOOTING	MARK
STORIES	TOWER HEIGHT	Α	В	С	TIMBER SPANS	
	. – -				15'	15' TO 90'
1 ,	13-4"	5-7½"	5-7±"	16,10 7,		F-109
	16'	5 <u>'</u> "	5 <u>-</u> 11"	17 ^L 9 ^{II}	F- 115	F- 109
	18'	6 ^L 2"	6 ^r 2"	18º 6"	F- 115	F- 109
2	20'	6 ^L 4"	6 ^L 4"	19,0,	F- 115	F- 109
	22'	6 ^L 7"	6 ^L 7"	19.9.	F- 115	F- 107
	24'	6 <u>r</u> 10,	6 <u>-</u> 10	20 ^L 6"	F- 115	F- 107
	25 ^L 10"	7-04"	7¹0‡"	21 <u>-0</u> ₹,	F- 115	F- 107
	28'	7 ^L 3*	753"	21. 9.	F-115	F- 107
	30'	7 ^L 6"	7 ^L 6"	22'6"	F- 115	F- 107
3	32'	7 <u>'</u> 8"	7-8"	23'0"		F- 107
	34'	7-11	7511	23-9"	F-115	F- 107
	36'	8-2"	8 ^L 2"	24-6"	F- 115	F- 107
	38 ^L 4"	8 ¹ 4 ⁷	8-4 7	25º-28"	F-115	F- 107
	40'	8- 7"	8 <u>'</u> 7	25-9"	F-114	F- 107
	42'	8-10	8-10	26 ¹ 6"	F-114	F- 107
4	44'	9-0"	8 ₇ 0,	2750		F- 107
	46'	9-3*	9' 3"	27-9	F-114	F- 107
	48'	9 ^L 6"	9 ^r 6"	28º6"	F-114	F- 107
	50 ^L 10"	9-9-	9-9#	29 4	F-114	F- 105
	53'	10,0,	10-0"	30-0"	F-114	F- 105
	55'	10-3"	10-3"	30-9"	F-114	F- 105
5	57'	10-6"	10,-6,	31-6"	F-114	F- 105
	59'	10-8"	10-8"	32-0"	F-114	F- 105
	61'	10,11,	10,11,	32-9"	F-113	F- 105
	63 ^L 4"	11-24"	11-24"	33-6₹		F- 105
	65'	11-4"	11-4"	34-0"	F- 113	F- 105
	67'	11-7"	11-7"	34 ^L 9"	F- 113	F- 105
6	69'	11-10"	11,10,	35 ⁻ 6"	F-113	F- 105
	71'	15,0,	12 - 0"	36-0"	F-113	F- 105
	73'	1253	1253	36-9"		F- 105
	75-10"	12-6 중"	12년6 골"	37-8	F-113	F- 105



PARALLEL TO & OF HIGHWAY

FOOTINGS F113, F114 AND F115

CONCRETE PEDESTAL

ANCHOR BOLT DETAIL

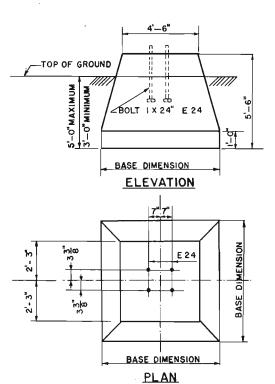
BILL OF MATERIALS FOR ONE CONCRETE PEDESTAL FOR FRAMED TIMBER TOWERS

MARK	WIDTH (W)	TOP WIDTH	LENGTH (L)	CONCRETE (CUBIC YARDS MAXIMUM)	MACHINE BOLT I SQUARE NUT AN WASHERS STOCK NO 43-23 QUANTITY	ID TWO
F-105	5 <u>'</u> 6"	2-6	7 ¹ -6"	6.0	4	31
F-107	5 ^L 0 "	2 6"	7 ^L O"	5.2	4	31
F-109	4'-6"	2-6"	6 '6"	4.5	4	31
F-113	5 ^L 0"	2 <u>'</u> 6"	4'0"	3.0	2	16
F- 114	4 ^L 6"	2'6"	4-0"	2.7	2	16
F-115	4-0"	2 6"	4 ¹ 0"	2,5	2	16

HIGHWAY CLASS 50, SINGLE-LANE

COMPANION SHEETS

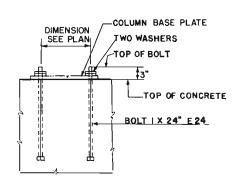
SHEETS 39 12,13 154 155 CONCRETE PEDESTALS FRAMED STEEL TOWERS GENERAL NOTES SYMBOLS



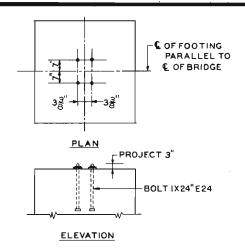
CONCRETE PEDESTALS FOR STEEL TOWERS

TABLE OF DIMENSIONS AND BILL OF MATERIALS FOR ONE PEDESTAL

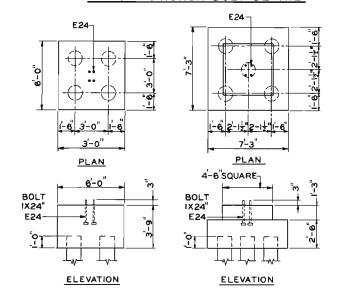
ADJACENT SPAN	HEIGHT OF TOWER	MARK	BASE DIMENSION	CONCRETE (CUBIC YARDS)	TWO WASHER	
15'	39 OR LOWER	F 120	6'-0"	6.0	4	26
15	41' TO 77'	F 121	7'-0"	7.4	4	26
20'	21' OR LOWER	F120	6'-0"	6.0	4	26
20	23' TO 77'	F 121	7'-0"	7.4	4	26
30'	21' OR LOWER	F 120	6'-0"	6.0	4	26
	23' TO 77'	FI21	7'-0"	7.4	4	26
40'	21' OR LOWER	F 120	6'-0"	6.0	4	26
40	23' TO 77'	F 121	7'-0"	7.4	4	26
50'	57' OR LOWER	F121	7'-0"	7. 4	4	26
	59' TO 77'	F 122	8'-0"	9. 1	4	26
60'	39' OR LOWER	F12!	7'-0"	7.4	4	26
- 60	41' TO 77'	F 122	8'-0"	9.1	4	26
70'	39 OR LOWER	FI21	7 <u>'</u> 0"	7.4	4	26
	41' TO 77'	F122	8'-0"	9.1	4	26
80'	21' OR LOWER	FI21	7'-0"	7.4	4	26
	23' TO 77'	FI22	8'-0"	9. l	4	26
90'	21' OR LOWER	FI21	7'-0"	7.4	4	26
90	23' TO 77'	F122	8'-0"	9.1	4	26



TYPICAL BOLT DETAIL



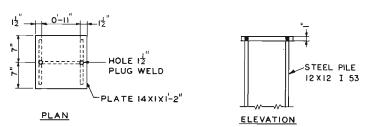
TYPICAL ANCHOR BOLT DETAIL



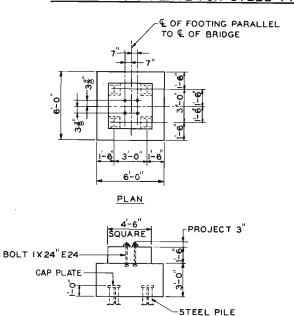
4-PILE FOOTING F134 5-PILE FOOTING F135

BILL OF MATERIALS FOR ONE FOOTING

ADJACENT SPAN (FEET)	HEIGHT OF TOWER (FEET)	FOOTING MARK NUMBER	NUMBER OF PILES	CONCRETE (CUBIC YARDS)	WITH SQUAR TWO WASHER NUMBER 43	
15'	77'OR LOWER	F134	4	5.0	4	6.5
20'	77'OR LOWER	F134	4	5.0	4	6.5
30,	77'OR LOWER	F134	4	5.0	4	6.5
40'	77'OR LOWER	F134	4	5,0	4	6.5
50'	77'OR LOWER	F134	4	5,0	4	6.5
60'	77'OR LOWER	F 134	4	5.0	4	6.5
70'	77'OR LOWER	F134	4	5.0	4	6.5
80'	77'OR LOWER	F134	4	5.0	4	6.5
90'	57'OR LOWER	F134	4	5.0	4	6.5
	59'TO 77'	F 135	5	5.8	4	6. 5



DETAIL OF CAP PLATE FOR STEEL PILE



STEEL-PILE FOOTING

ELEVATION

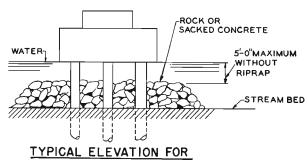
REQUIRED BEARING CAPACITY

OF PILES, TONS PER PILE, 4-PILE FOOTING

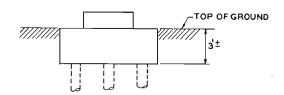
ADJACENT	HEIGHT	-		
SPAN	21'OR LOWER	23 ['] TO 39 '	41 ['] TO 57 [']	59' ⊤O 77'
15 '	- 11	12	14	15
20'_	- 11	13	14	16
30'	12	13	15	17
40'	13	14	16	17
50'	14	15	17	18
60'	15	16	18	19
70'	15	17	19	20
80	16	18	19	21
90'	17	19	20	22 🗓

COMPANION SHEETS

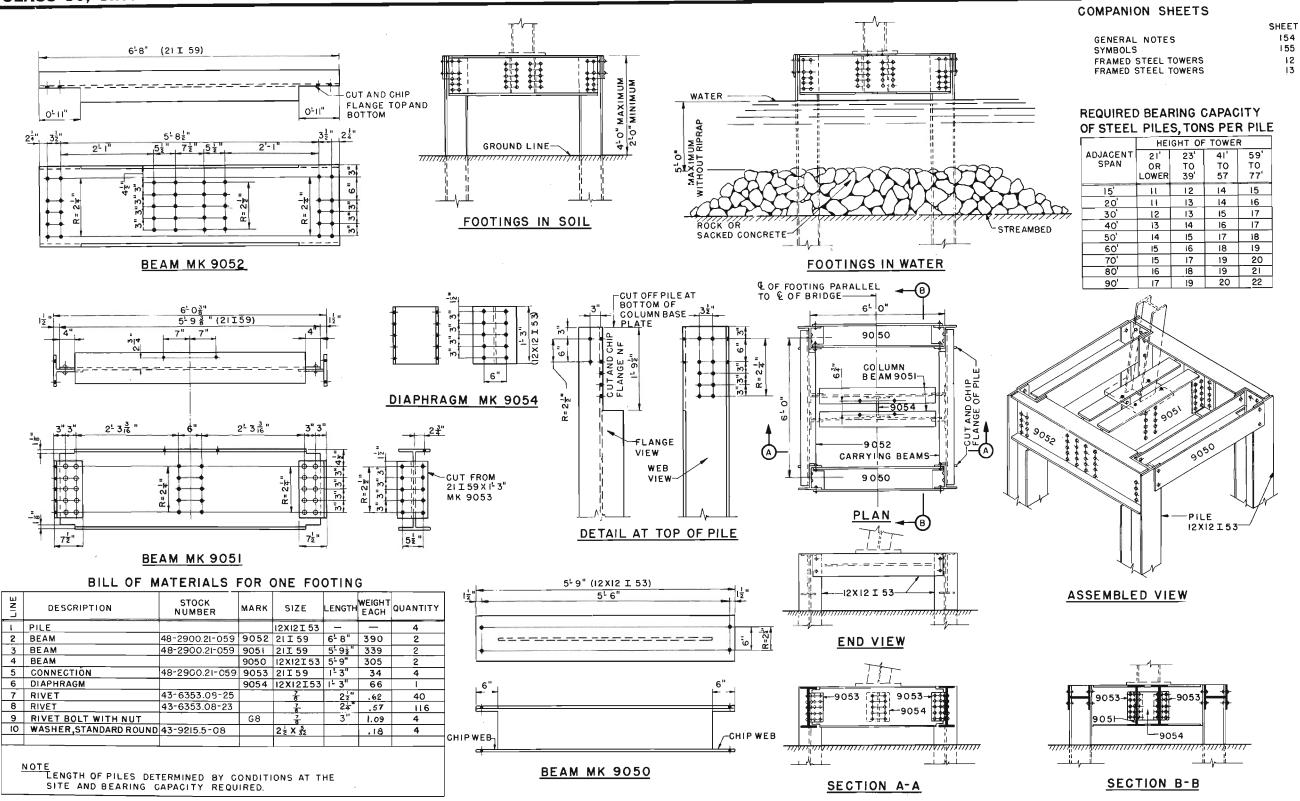
	SHEET
GENERAL NOTES	154
SYMBOLS	155
CONCRETE PEDESTALS	38
FRAMED STEEL TOWERS	12 13

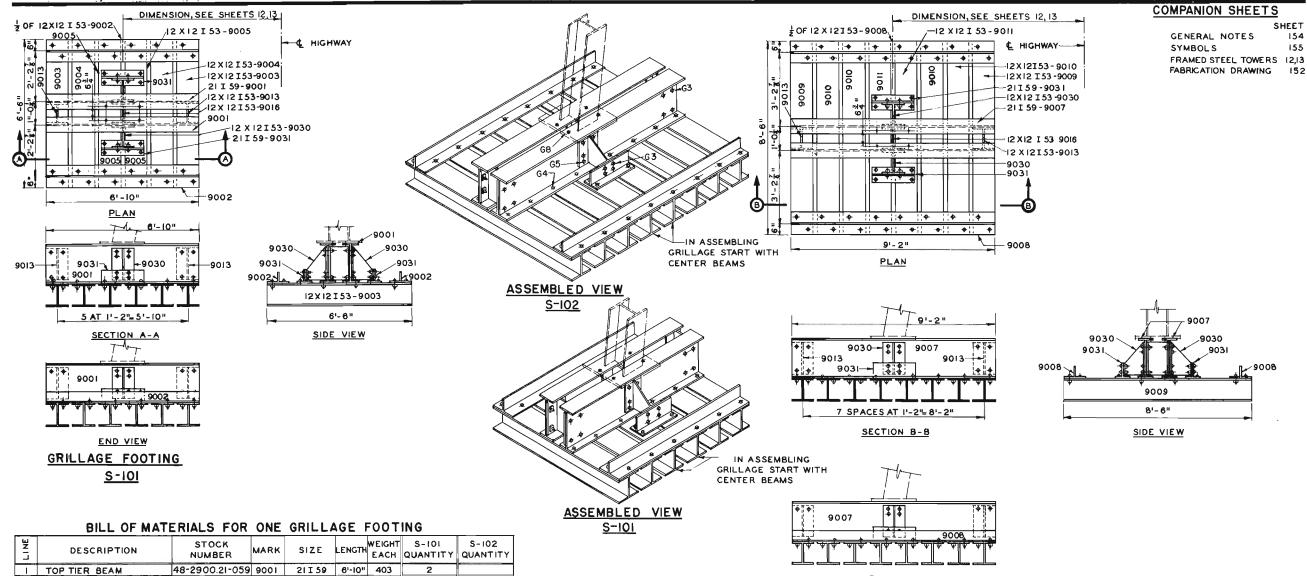


FOOTINGS IN WATER



TYPICAL ELEVATION FOR FOOTINGS IN SOIL





GRILLAGE FOOTING S-102

END VIEW

SCHEDULE FOR SELECTION OF GRILLAGE FOOTING FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

	-	F	OOTINGS	ON SOL	L	FOOTING S
	SPAN	H	EIGHT (OF TOWE	R	ON
DESCRIPTION	BETWEEN	UP	23'	41	5 9'	ROCK
	TOWERS	TO	TO	то	то	ALL TOWER
		211	39'	57'	77'	HEIGHTS
SINGLE LANE CLASS 50	15' TO 50'	S-101	S-101	S-101	S-101	S-101
DO	601	S-101	S-I01	S-101	S-102	\$-101
DO	70'	\$-101	3-101	S-101	S -102	S-101
DO	801	S-101	S-101	S-102	S-102	S-101
DO	901	S-101	S-101	S-102	S-102	S-101

2 TOP TIER HALF BEAM

3 BOTTOM TIER BEAM

4 BOTTOM TIER BEAM

5 BOTTOM TIER BEAM

8 BOTTOM TIER BEAM

9 BOTTOM TIER BEAM

IO BOTTOM TIER BEAM

6 TOP TIER BEAM
7 TOP TIER HALF BEAM

II SEPARATOR
I2 SEPARATOR

15 RIVET BOLT

16 RIVET BOLT

17 RIVET BOLT

18 RIVET BOLT AND WASHER

13 BRACE

14 BRACE

9002 12112 153 6'-10" 180

9003 | 12X12 I 53 | 6'- 6" | 345

9004 | 12X12I53 | 61-61 | 345

9005 | 12 X | 12 T 53 | 6' - 6" | 345

90.08 | 12 X | 2 I 5 3 | 9 1 - 2 " | 243

9009 12 X 12 I 53 8'- 6" 450

9010 12 X 12 T 53 8'-6" 450

9011 12 X 12 T 53 8'-6" 450

9013 12 X 12 I 53 1' - 6" 80

9016 12X12I53 1'-6" 80

TOTAL WEIGHT 2 ½ 45 2 ½ 23

16

5

2 7 "

48

24

16

2

4

2

2

58

28

16

4

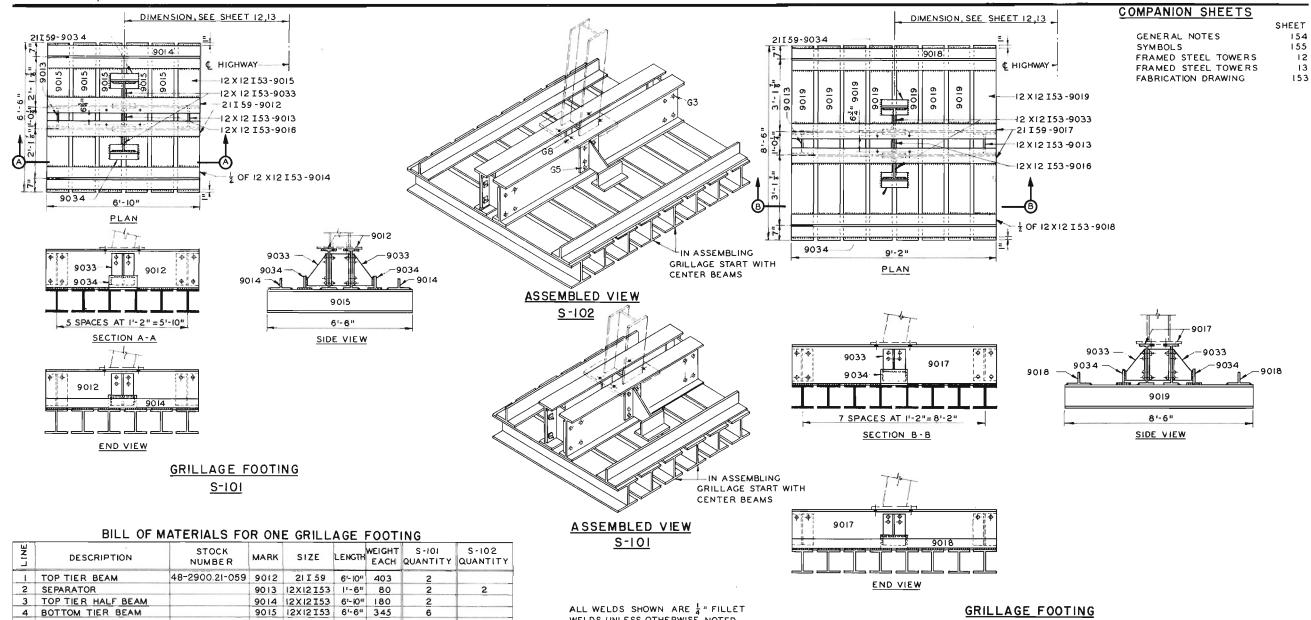
48-2900.21-059 9007 21 159 91-2" 541

9030 | 12X12 | 153 | 1'-6" | 53 | 48-2900.21-059 | 9031 | 21 | 159 | 1'-11" | 50

G3

G 4

G5



ALL WELDS SHOWN ARE 4 " FILLET GRILLAGE FOOTING WELDS UNLESS OTHERWISE NOTED S-102

SCHEDULE FOR SELECTION OF GRILLAGE FOOTINGS FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

	F	DOTINGS	ON SOIL	_	FOOTINGS
SPAN	H	EIGHT C	F TOWE	R	ON ROCK
BETWEEN	UP	231	411	591	ALL
TOWERS	TO	то	TO	TO	TOWER
	21'	391	57'	771	HEIGHTS
151 TO 501	S-101	5-101	S-101	S-101	S-101
601	5-101	S-101	S-10I	S-102	5-101
701	S-101	S-101	5-101	\$-102	S-101
801	S-101	S-101	S-102	S-102	S-101
90'	S-101	5-101	S-102	S-102	S-101

4 BOTTOM TIER BEAM

8 BOTTOM TIER BEAM

5 SEPARATOR

II RIVET BOLT

12 RIVET BOLT

13 RIVET BOLT AND WASHER

14 WELDING ELECTRODE

9 BRACE

10 BRACE

6 TOP TIER BEAM 7 TOP TIER HALF BEAM 9016 12X12T53 (1-6" 80 48-2900.21-059 9017 21T59 91-2" 541

48-2900.21-059 9034 211.59

G3

G5 G8

46-3772.2-7

90 18 | 12X12 I53 | 9'-2" | 243 9019 12X12153 8'-6" 450

9033 |2X|2I53 |1-6" 53

1'-2" 35

WEIGHT

16

9 LBS.

15

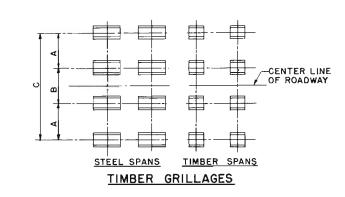
2

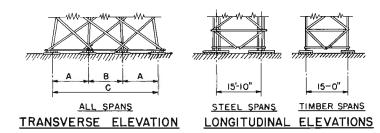
2

16

16

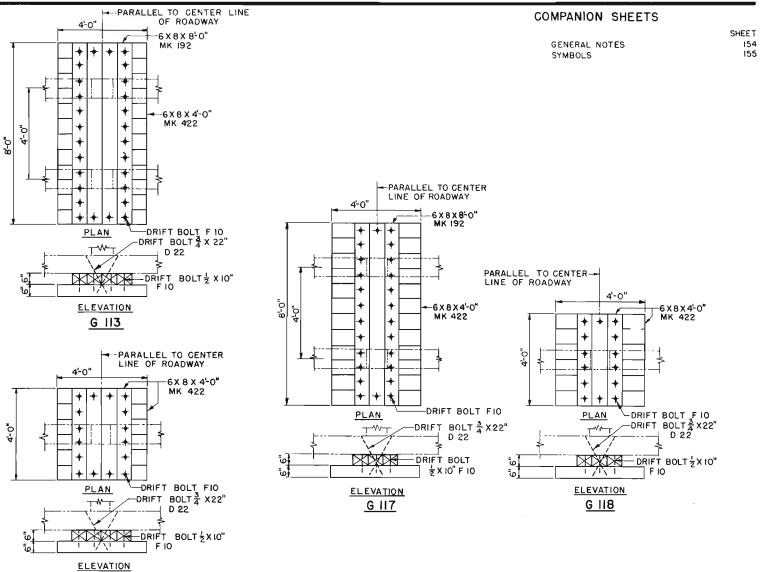
12 LBS.





TIMBER GRILLAGE FOOTINGS

LIMRE	ואט א	LLAG	E FUL	טעוווע	3	
					FOOTING	MARK
STORIES	TOWER HEIGHT	A	В	С	TIMBER SPANS 15'	STEEL SPANS 15' TO 90'
1	13 ^L 4"	5'- 7 <u>1</u> "	5-7분	16-10-	G-118	G-117
	16'	5'-11"	5'-11"	17-9"	G-118	G-117
	18'	6'-2"	6'-2"	18'-6"	G~118	G-117
2	20'	6'-4"	6'-4"	19'-0"	G-118	G-117
	22'	6'-7"	6 ^L 7"	19-9"	G-118	G-117
	24'	6-10"	6-10"	20'-6"	G-118	G-117
	25-10"	7-04" 7-3"	7-0#	21 <mark>-03</mark> "	G-118	G-117
	28'	7-3"	7-3"	21-9"	G-118	G-117
	30'	7-6"	7-6"	22-6"	G-118	G-117
3	32'_	7-8"	7'-8"	23-0"	G-118	G-117
	34'	7-11"	7-11"	23-9"	G-118	G-117
	36'	8'-2"	8'-2"	24'-6"	G-118_	G-117
	38-4"	8'-42"	8-42"	25-25"	G-118	G-117
	40'	8'-7"	8-7"	25-9	G-118	G-117
	42'	8-10"	8-10	26'-6"	G-118	G-117
4	44'	9½0 *	9'-0"	27-0"	G-118	G-117
	46'	9'-3"	9'-3"	27-9"	G-118	G-117
	48'	9-6"	9 ^L 6"	28-6	G-118	G-117
	50'-10'	9-9 1 "	9'-9 \f "	29-42	G-118	G-117
	53'	10'-0"	10'-0"	30-0	G-114	G-113
	55'	10'-3"	10-3"	30-9"	G-114	G-113
5	57	10,-6,	10'-6"	31-6"	G-114	G-113
	59'	10,-8,	10-8"	32'-0"	G-114	G-113
	61'	10'-11"	10,-11,	32-9"	G-114	G-113
	63'-4"	11'-2‡"	ロー2本	33-63"	G-114	G-113
	65'	-4"	11-4"	34-0"	G-114	G-113
	67'	11-7'	16-7"	34'-9"	G-114	G-1 <u>113</u>
6	69'	11,-10,,	11'-10"	35'-6"	G-114	G-113
	71'	12-0"	12'-0"	36'-0"	G 114	G-113
	73'	12-3"	12-3"	36-9"	G-114	G-113
	75-10"	12'-62''	12-63	37-8 8 "	G-114	G-113



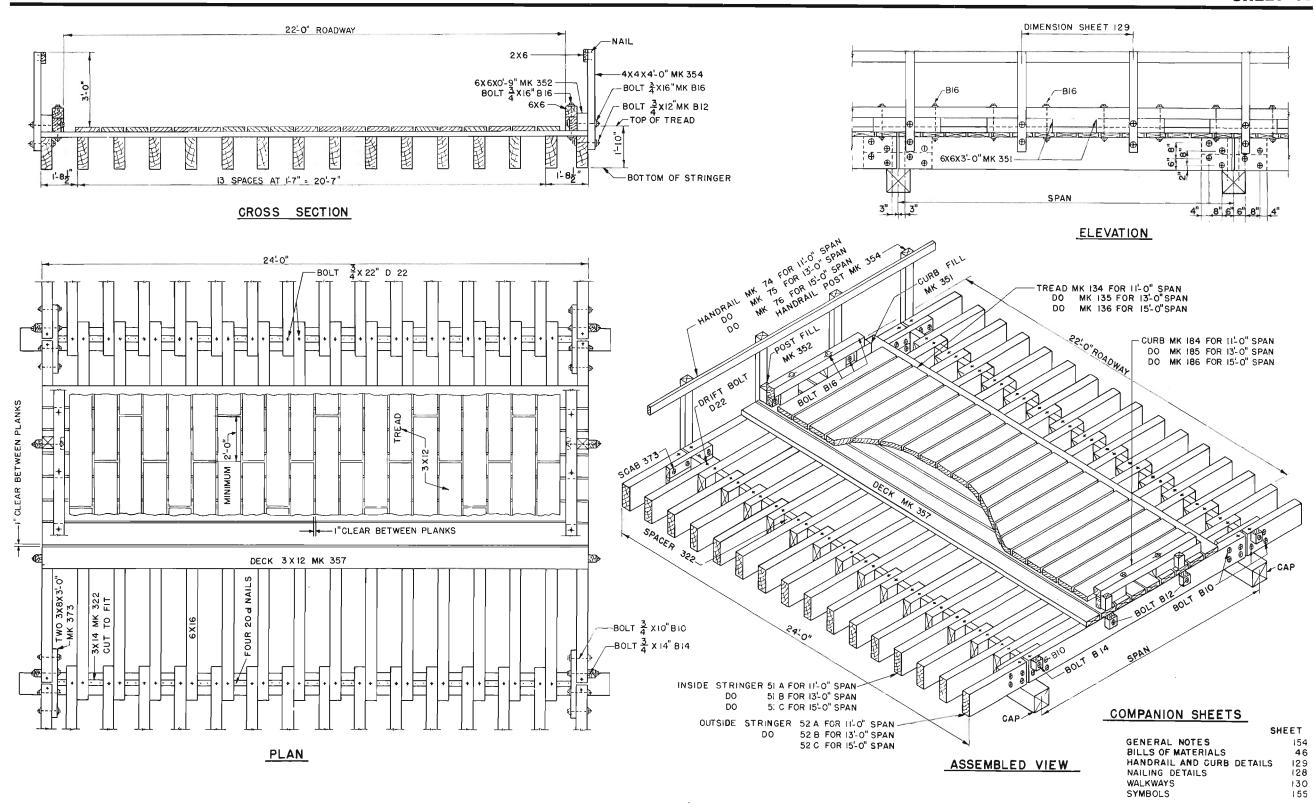
BILL OF MATERIALS FOR ONE TIMBER GRILLAGE

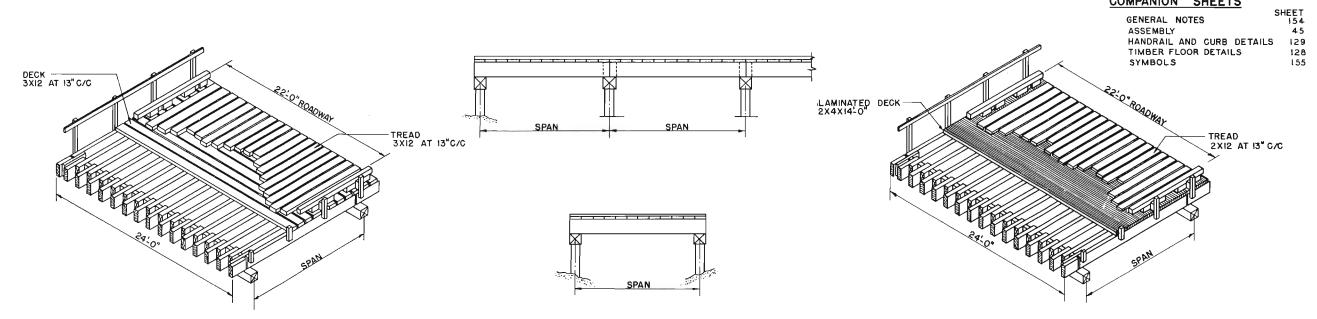
G 114

				GRILLA	GE NUME	BER	G II	3	GII	4	GII	7	G H	18
LINE	DESCRIPTION	STOCK NUMBER	MARK	SIZE	LENGTH	WEIGHT EACH	QUANTITY	FEET B.M.	QUANTITY	FEET B,M,	QUANTITY	FEET B,M,	QUANTITY	FEET B,M,
LUMBE	R, SOFT WOOD													
1	GRILLAGE	39-9352.680-	192	6 X 8	8,-0,	120	4	128			3	96		
2	GRILLAGE	39-9352.680-	422	6x8	4'-0"	60	12	192	10	160	12	192	9	144
STEEL	HARDWARE, BLAC	K												
3	DRIFT BOLT	43-1636.07-22	D22	3 4	22"	2.75	4		2		4		2	
4	DRIFT BOLT	43-1636.05-10	F 10	1/2	10"	0,6	28		16		26		14	

INDEX DRAWING

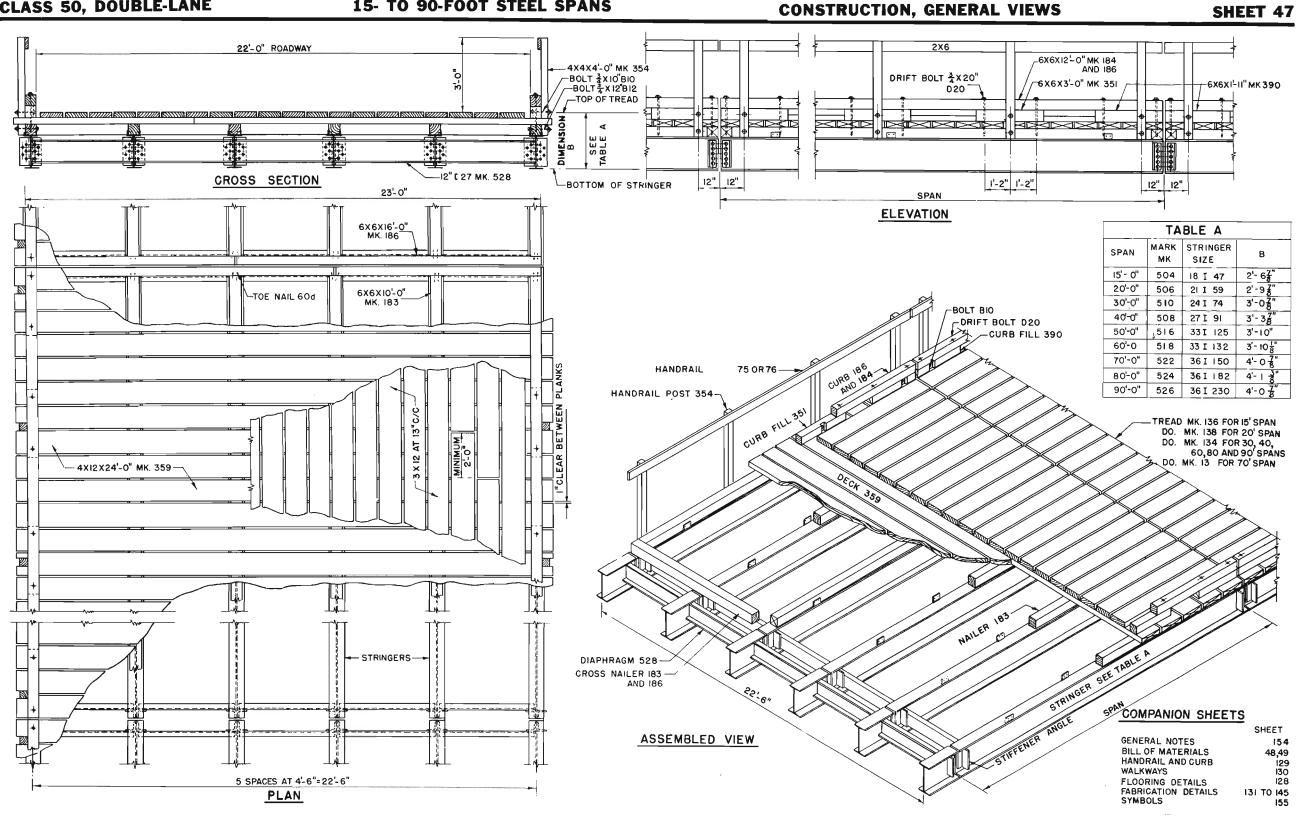
	SET NUMBER 50D-1		SET NUMBER 50D-5		SET NUMBER 50D-10
	TIMBER SPANS (11 to 15 feet long)		STEEL TOWERS FOR STEEL SPANS (15 to 77 feet high)		STEEL PILE BENTS AND PIERS FOR STEEL SPANS (1 to 20 feet high)
SHEET	(11 to 13 feet folig)	SHEET	(10.007).001.1113.17	SHEET	(1 to 20 feet high)
45	General views	55 56	General views of 69- to 77-foot towers General views of 15- to 67-foot towers	76	Riveted construction: general views of bents
46 128	Bill of materials Details of floor construction and attachment of nailers to steel stringers	57	Bill of materials common to all towers	77 78	Riveted construction: general views of piers Riveted and welded construction: bill of materials
129	Details of handrail and curb	58 59	Bill of materials which vary with tower height Riveted construction: fabrication of cap beam, strut, and pin	79	Welded construction: general views of bents
130	General views and bill of materials for walkway	60	Riveted construction: fabrication of columns	80	Welded construction: general views of piers
154	General notes	61	Riveted construction: fabrication of columns and struts	150	Riveted construction: fabrication of cap beams, corbels, bracing, and connec-
155	Structural symbols	62	Fabrication of rod bracing	151	tions Welded construction: fabrication of cap beams, corbels, and bearing plates
		63	Details and bill of materials for shims under stringers of different depths; superstructure anchor bolts	154	General notes
	SET NUMBER 50D-2	226	Welded construction with rod bracing: cap beams and column splices welded in fabrication and erection	155	Structural symbols
	STEEL SPANS	227	Welded construction with welded angle bracing: cap beams and column		SET NUMBER 50D-11
	(15 to 90 feet long)		splices welded in fabrication and erection		TIMBER SILL AND PILE FOUNDATIONS FOR TIMBER TOWERS
		154 155	General notes Structural symbols		
47 48	General views Bill of materials: steel for riveted construction; lumber and hardware for stan-	155	NOTE: When welded construction is used in accordance with sheets 226	81	General views
40	dard plank floor		or 227, bills of materials on sheets 57 and 58 and fabrication de-	82	Additional views and bill of materials
49	Bill of materials: steel for welded construction: lumber and hardware for alter-		tails on sheets 59, 60, and 61 must be adjusted in the field. When	154	General notes
	nate laminated floor		sheet 227 is used, sheet 62 does not apply.	155	Structural symbols
128	Details of floor construction and attachment of nailers to steel stringers				SET NUMBER 50D-12
129 130	Details of handrail and curb General views and bill of materials for walkway		SET NUMBER 50D-6		CONCRETE PEDESTALS FOR TIMBER TOWERS
131	Riveted construction: fabrication of stringers 501 to 511 and of diaphragms 527				CONCRETE FEDESTALS FOR HIMBER TOWERS
	and 528		TIMBER ABUTMENTS FOR TIMBER SPANS	83	General views and bill of materials
132	Riveted construction: fabrication of stringers 516 and 521 and of bearing plates			154	General notes
134	3500 and 3501 Riveted construction: fabrication of stringers 519 and 526	64	General views of pile abutments; bill of materials for pile and grillage abut-	155	Structural symbols
135	Riveted construction: fabrication of stringers 515 and 522		ments		SET NUMBER 50D-13
137	Riveted construction: fabrication of stringers 514, 517, and 518	65	General views of grillage abutments		CO. (COSTE DEDECT.) (C. FOR CITE) TO ((FOR
138	Riveted construction: fabrication of stringers 520 and 524	154 155	General notes Structural symbols		CONCRETE PEDESTALS FOR STEEL TOWERS
139	Welded construction: fabrication of stringers 501W to 511W and of diaphragms C3 and C4	133	Sirectoral symbols	SHEET	
141	Welded construction: fabrication of stringers 513W, 522W, and 523W			84	General views and bill of materials for pedestals on timber piles
142	Welded construction: fabrication of stringers 514W, 515W, and 516W		SET NUMBER 50D-7	85	General views and bill of materials for pedestals on ground and on steel piles
144	Welded construction: fabrication of stringers 517W and 526W		ABUTMENTS FOR STEEL SPANS	55	General views of 69- to 77-foot towers
145 154	Welded construction: fabrication of stringers 518W, 519W, and 524W General notes		7,551112110701101	56 154	General views of 15- to 67-foot towers General notes
155	Structural symbols	66	General views of timber pile abutments	155	Structural symbols
		67	General views of timber grillage abutments		SET NUMBER 50D-14
	SET NUMBER 50D-3	68	Bill of materials for timber pile and grillage abutments		
	SET NOMBER SOD-S	69	General views of steel pile abutments		STEEL FRAME ON STEEL PILE FOUNDATIONS FOR STEEL TOWERS
	TIMBER TOWERS FOR TIMBER SPANS	70 71	Fabrication details and bill of materials for steel pile abutments General views and bill of materials for concrete abutments		
	(15 to 76 feet high)	154	General notes	86	General views and bill of materials
		155	Structural symbols	55	General views of 69- to 77-foot towers
50	General views			56 154	General views of 15- to 67-foot towers General notes
50 51	Bill of materials			155	Structural symbols
146	Details of bracing connections		SET NUMBER 50D-8		SET NUMBER 50D-15
147	Details of bracing connections				
148 154	Details of bracing connection and of columns; column dimensions General notes		TIMBER PILE BENTS FOR TIMBER SPANS		STEEL GRILLAGE FOUNDATIONS FOR STEEL TOWERS
155	Structural symbols		(1 to 28 feet high)		The state of the s
	•	70	Bill to a set of the s	87 88	Bolted construction: general views and bill of materials Welded construction: general views and bill of materials
	SET NUMBER 50D-4	72 73	Bill of materials; general views of 1- to 16-foot bents General views of 17- to 28-foot bents	88 152	Bolted construction: fabrication of grillage beams
	3E1 NOMBER 300-4	154	General notes	153	Welded construction: fabrication of grillage beams
	TIMBER TOWERS FOR STEEL SPANS	155	Structural symbols	55	General views of 69- to 77- foot towers
	(15 to 76 feet high)		•	56	General views of 15- to 67-foot towers
			SET NUMBER 50D-9	154 155	General notes Structural symbols
52	Details and bill of materials for connection of spans to towers		JET HOMBER JUD-7	133	SET NUMBER 50D-16
53 54	General views Bill of materials		TIMBER PILE PIERS FOR STEEL SPANS		SET NUMBER SUU-10
54 146	Details of bracing connections		(1 to 13 feet high)		TIMBER GRILLAGE FOUNDATIONS FOR TIMBER TOWERS
147	Details of bracing connections				
148	Details of bracing connections and of columns; column dimensions	74	General views	89	General views
149	Details of towers supporting both timber and steel spans	75 154	Bill of materials; details of piers supporting one steel and one timber span General notes	90	Additional views and bill of materials
154 155	General notes Structural symbols	155	Structural symbols	154	General notes
100			- · · · · · · · · · · · · · · · · · · ·	155	Structural symbols





	BILL OF MATERIALS FOR S	TANDARD PLANK FLO	OR									
]			11' S	PAN	15' SP	AN	15, 2	PAN
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	MEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	F8M	QUANTITY	FBM
	LUMBER, SOFT WOOD											
1	STRINGERS		51C	6×16	16'-0"	480					14	1792
2	DO		52C	6X16	16'~0"	480					2	256
3	DO		51B	6X16	14'-0"	420			14	1568		
4	DO		52B	6X16	14'-0"	420			2	224		
3	DO		51A	6X16	12'-0"	360	14	1344				
6	DO		52A	6X16	12'-0"	360	2	192				
7	SPACER	39-3330.14-1	322	3X14	10'-0"	131	1	35	1	35	1	35
8	SCAB	39-3330.08	373	3×8	5'-0"	25	4	24	4	24	4	24
9	DECK	39-3952.12	357	3X12	241-0"	270	10	720	12	864	14	1008
10	TREAD	39-3330.12-16	136	3X12	16'-0"	180					20	960
11	DO	39-3330.12	135	3X12	14'-0"	158			20	840		
12	po	39-3952-12-12	154	3X12	12'-0"	135	20	720	 			
13	CURB	39-3360.06-16	186	6×6	16'-0"	180			ĺ		2	96
14	DO	39-3360.06-14	185	6X6	14'-0"	158			2	84		
15	90	39-4096-06-12	184	6X6	12'-0"	135	2	72				
16	CURB FILL	39-4096.06	351	6×6	31-0"	54	4	36	4	36	6	54
17	HANDRAIL POST	39-3340.04	354	4X4	4'-0"	20		22	4	22	6	32
16	POST FILL	39-4096.06	352	6X6	0'-9"	8	4	9	4	9	6	13
19	HANDRAIL	39-3880.06-16	76	2×6	16'-0"	60					2	32
20	DO	39-3880.06-14	75	2X6	14'-0"	52			2	28		
21	DO	39-3880,06-12	74	2×6	12'-0"	45	2	24			_	
	STEEL HARDWARE, BLACK	,										1
22	MACHINE BOLT WITH SQUARE HEAD, NUT, AND THO WASHERS	43-2325.07-16	816	3/4	16"	2.52	12		12		18	
2.5	DO	43-2525.07-144	814	3/4	14*	2.27	2		2		2	
24	DO	43-2325.07-124	812	3/4	12.	2.02	2		2		4	
25	DO	43.2325.07-1	B10	3/4	10"	177	14		14		14	
26	DRIFT BOLT	43-1636.07-22	D22	3/4	22"	3.00	32		32		32	
27	WIRE NAIL	42-6028.3-5		504		0.10	260		500		340	
28	DO	42-6028-3-2		200		0.04	136		136		144	
29	WIRE SPIKE	42-8488.035-07		5/16	7.	0.15	190		222		254	

					1		11' 8	PAN	13' S	PAN	15' 5	PAN
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT (POUNDS)	QUANTETY	FBM	QUANTITY	FBM	QUANTITY	FBM
	LUMBER, SOFT WOOD		•									
1	STRINGERS		51C	6X16	16'-0"	480				_	14	179
2	DO		52C	6X16	16'-0"	480			1		2	25
3	00		51B	6X16	14'-0"	420			14	1568		
4	DO		528	6×16	14'-0"	420			2	224		
5	DO		51A	6X16	12'-0"	360	14	1344				
6	00		52A	6X16	12'-0"	360	2	192				
7	SPACER	39-3350.14-1	322	3X14	10'-0"	151	1	35	1	35	1	3
8	SCAB	39-3380.08	373	5×8	3'-0"	23	4	24	4	24	ı,	
9	DECK	39-3880.04	360	2X4	24'-0"	60	82	1310	96	1535	111	177
10	TREAD	39-3880.12-16	106	2×12	16'-0"	120					20	64
11	DO	39-3880.12-14	105	2X12	14'-0"	106			20	560	1 1	
12	00	39-5228-12-12	104	2×12	12'-0"	90	20	480	1 -		1	
13	CURB	39-4096.06	186	6X6	16'-0"	180	•	700_			2	9
14	DO	39-3360.06	185	6X6	14'-0"	158			2	84	1 1	
15	DO	39-4096-06-12	184	6X6	12'-0"	135	2	72	 			
16	CURB FILL	39-4096.06	351	6X6	31-01	34	4	36	ц	36	6	5
17	HANDRAIL POST	39-3340.04	354	4X4	4'-0"	20	4	22	-	22	6	3
18	POST FILL	39-4096.06	352	6X6	0'-9"	8	4	9	4	9	6	1
19	HANDRA I L	39-3880.06-16	76	2X6	16'-0"	60	1 1		1 7 1		2	3
20	DO	39-3880.06-14	75	2X6	14'-0"	52			2	28	+	
21	DO	39-3880.06-12	74	2X6	12'-0"	45	2	24	1 -1			
	STEEL HARDWARE, BLACK	77 700010	74	2.00	12 0						1	
	MACHINE BOLT WITH SQUARE HEAD, NUT, AND TWO WASHERS			_							l	
22	· · · · · · · · · · · · · · · · · · ·	43-2325.07-16	B16	3/4	16*	2.52	12		12		18	
23	DO	45-2325.07-144	814	3/4	14"	2.27	2		2		2	
25	00	43-2325.07-124	B12 B10	3/4 3/4	12"	1.77	14		2		4	
26	DRIFT BOLT	43-1636.07-22	D22	3/4					14		14	
27	WIRE NAIL	42-6028.3-5	022	500	22.	3.00	32		32		32	
28	DO DO			304		0.10	260		300		340	
29	00	42-6028.3-3		204		0.04	136		2560		2960 144	



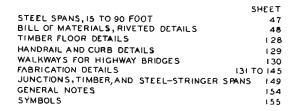
SHEET

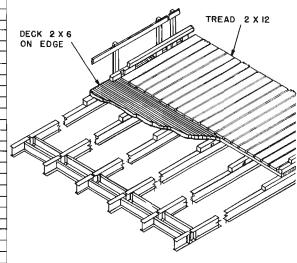
COMPANION SHEETS

STEEL SPANS. 15-TO 90-FOOT 47 BILL OF MATERIALS , WELDED DETAILS 49 TIMBER FLOOR DETAILS 128 HANDRAIL AND CURB DETAILS 129 BILL OF MATERIALS - STANDARD PLANK FLOOR WALKWAYS FOR HIGHWAY BRIDGES 130 SPAN LENGTH 20' 30' 15' 401 501 501 / 701 90' FABRICATION DRAWINGS 131 TO 145 STRINGER SIZE 18 T 47 21 I 59 2 L T 7 L 27 T G1 33 I 125 33 I 132 56 I 150 36 I 182 36 I 230 JUNCTIONS TIMBER AND STEEL-STRINGER SPANS 149 UNIT SIZE (INCHES) GENERAL NOTES 154 DESCRIPTION STOCK NO MARK LENGTH NATE ITY FBM QUANTITY FBM OUANT ITY FBM CHANGITY FBM CHANGETY FBM FBM LINE QUANT ITY FBM LINE SYMBOLS 155 LUMBER, SOFT WOOD 39-3330.12-2 138 39-3330.12-16 156 20'-0" 225 50 3000 1 FLOOR TREAD 20 1200 70 4200 20 960 40 1440 2 00 100 4800 100 4800 50 1800 3 00 100 3600 37 3952 46 4416 55 5280 2 96 2 96 2 96 26 780 32 960 38 1140 1825 28 2688 4 FLOOR, DECK 5 NAILER 96 2 96 2 96 44 1520 2 96 2 96 50 1500 56 1680 420 600 6 00 CURB 48 144 6 288 4 192 452 144 59-3360.06-12 184 6 X 6 12'-0" 135 4 144 a DO 39-3360.06 390 6 X 6 3'-0' 34 390 6 X 6 3'-0' 30 390 6 X 6 390 36 4 36 72 10 90 64 14 75 4 36 4 36 4 36 14 126 16 144 20 180 18 96 20 107 24 128 4 36 4 36 9 22 198 26 234 10 26 139 30 160 11 9 DO 10 CURB FILL 6 2 8 18 12 HANDRAIL POST 11 HANDRAIL 32 STEEL, STRUCTURAL 48-2900.36-23 526 36 I 230 40'-0' 9200 48-2900.36-23 526 36 I 230 9'-91/2' 2250 524 36 I 182 40'-0' 7280 524 36 I 182 19'-10.3/4' 3620 48-2900.36-15 522 36 I 150 40'-0' 6000 48-2900.36-15 522 46 I 50 40'-0' 6000 14 STRINGER 15 DO TREAD 3X12 17 DO 18 DO 18 48-2900.35-152 518 35 I 132 40'-0' 5280 48-2900.35-152 518 35 I 132 19'-10' 2618 48-2900.33-125 516 35 I 125 40'-0' 5000 19 00 12 19 20 DECK 4 X I2 20 00 21 21 22 00 48-2900.33-125 516 33 I 125 9'-10' 1229 23 48-2900.33-125 516 33 1 127 7 10 1-2-48-2900.27-091 508 27 1 91 39'-10 1/2' 5629 48-2900.24-074 510 24 1 74 29'-10 1/2' 2211 48-2900.21-059 506 21 1 59 19'-10 1/2' 1173 48-2900.10-047 504 18 1 47 14'-10 1/2' 699 48-3790.12-21 528 12 20.7 4'-4' 90 23 00 24 DO 25 DO 26 00 27 27 00 46-2900.16-047 504 16 147 16-101/2 699 46-3790.12-21 528 12 □ 20.7 4'-4* 90 46-2240.64-04 A9 8X4X3/8 2'-3* 28 46-2240.64-04 A5 6X4X3/8 2'-0* 25 46-2240.64-04 A6 6X4X3/8 1'-9* 22 46-2240.64-04 A6 6X4X3/8 1'-6* 18 48-2240.64-04 A6 6X4X3/8 1'-6* 18 48-2240.64-04 A6 6X4X3/8 1'-6* 18 10 28 DIAPHRAGM 15 15 . 15 20. 20 25 25 28 29 ANGLE 20 30 30 00 36 31 DO 36 31. 24 32 00 3.2 4 A3 6×4×3/8 1'-2' 16 P15, P4 14 × 3/8 2'-3' 40 P16 17 × 7/8 6'-8' 337 P17 6 1/2 × 7/8 4'-8' 95 24 3.4 47-7844.04 47-7844.08 47-7844.08 34 MEB SPLICE PLATE 35 FLANGE SPLICE PLATE 12 _12__ 24 24 _____ 24 DO 46 36 37 DO 47-7844.07 P1 12 1/2 X 3/4 3'-11" 125 24 3.7 P2 5 X 1 3'-11' 67 P11 12 X 5/8 2'-11' 74 P12 5 X 7/8 2'-11' 43 P13 12 X 5/8 4'-6' 115 P14 4 3/4 X 4 5/4 4'-6' 55 38 00 47-7844.1 38 36 40 41 39 DO 40 DO 47-7844.06 24 48 47-7844-06 12 42 DO 47-7844.07 #2 43 P18 12 X 1/2 2'-8" 54 P19 4 3/4 X 1/2 2'-8" 22 43 DO 47-7844.05 12 ME DO 47-7844.05 24 44 -5- 1.04 46 47 45-6353.08 7/8 1440 45 RIVET BILL OF MATERIALS -4 3/4" 1.00 -4 1/4" .91 1056 43-6353.08 46 00 47 DO FOR FLOOR AND STRINGER COMBINATIONS -4-.87 480 48 45-6355.08 7/8 7/8 48 00 49 50 51 -3 3/4" .83 -3 1/4" .74 288 43-6553.08 SHEET 49 DO 378 546 STANDARD PLANK FLOOR RIVETED STEEL DETAILS 50 DO 51 DO 43-6353.08 43-6353.08-3 48 48 504 294 336 -3° .70 -2 3/4° .66 HARDWARE 45-6555.08 -2 3/4" .66 48 -2 1/4" .57 100 60 100 108 52 48 52 DO 200 200 250 250 43-6353.08-25 7/B 53 53 DO 2. STANDARD PLANK FLOOR WELDED STEEL DETAILS STEEL HARDWARE, BLACK 49 HARDWARE 48 MACHINE BOLT WITH SQUARE 20 2.1 12 14 18 24 26 30 43-2325.07-124 812 NUT AND THO WASHERS ALTERNATE LAMINATED FLOOR 49 43-2325.07-1 B10 20 30 12 14 18 24 26 55 1.8 55 DO RIVETED STEEL DETAILS HARDWARE DRIFT BOLT WITH SQUARE 48 49 16 24 28 36 40 48 60 43-1636-07-2 3/4 20* 3.0 12 52 56 D20 1070 1780 57 STEEL HIRE NAIL 42-6028.3-5 50d .08 344 222 710 920 400 1510 1990 57 ALTERNATE LAMINATED FLOOR 49 108 68 14 444 34 .05 48 60 38 14 42-6028.3-3 84 132 88 156 98 180 204 228 58 WELDED STEEL DETAILS .04 24 .10 14 .15 168 58 14 336 49 49 59 DO 60 DO 42-6028.3-2 118 128 148 59 HARDWARE 42-6028.3-6 42-8488.035-07 60d 5/16 60 660 780 90 888 996 61 STEEL WIRE SPIKE 228 552 78 52 NAILER ATTACHMENT PLATE 47-7844.03 2 X 1/4 0'-4" 0.6 24 30 2.2 LB 42 3.1 LB 4.8 LB 5.8 LB 63 ELECTRODE, WELDING 46-3772.2-7 3/16 1.8 LB 4.0 LB 6.6 LB 7.5 LB

BILL OF MATERIALS

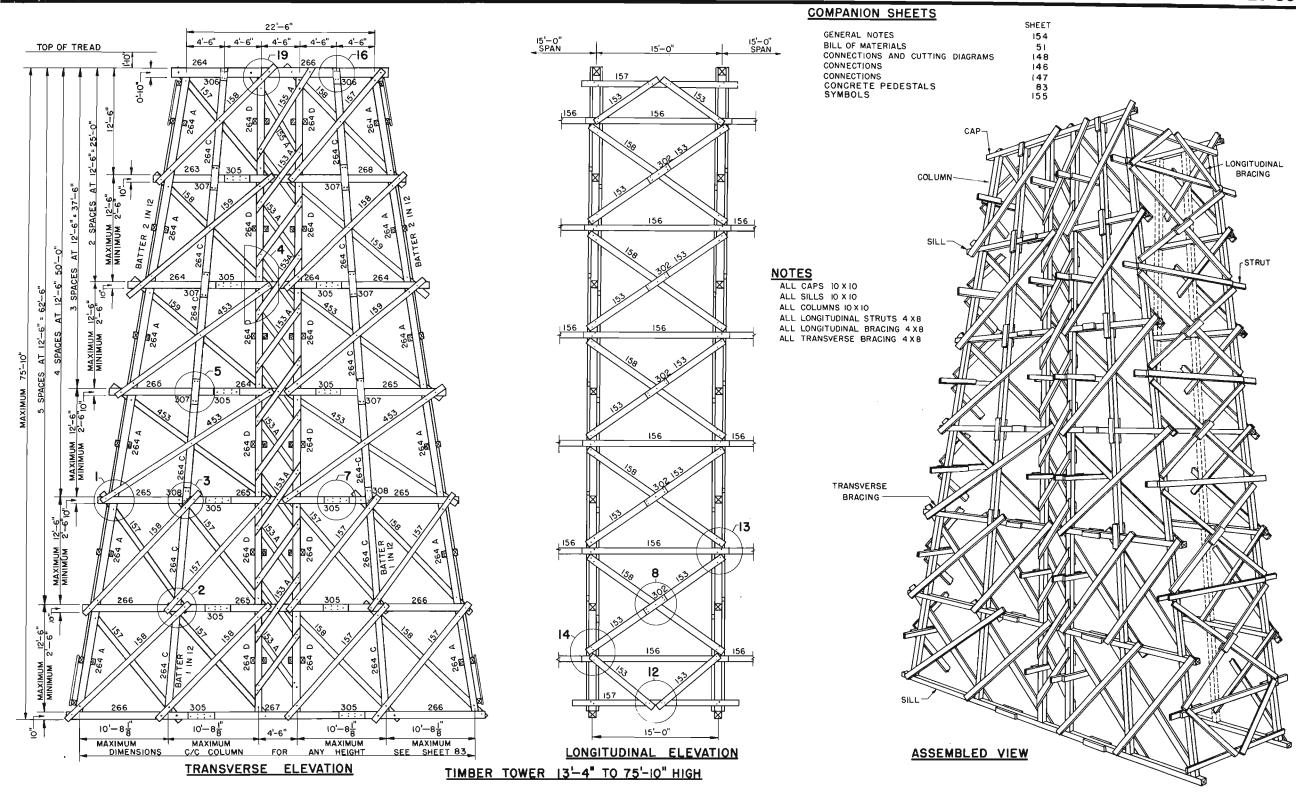
E	BILL OF MATERIALS FOR ALTE	ERNATE LAMINATED		ND WELDED ST I LENGTH	EEL DETAIL	.5	,	.5'	20	11	31	n i	1	40 '		50'		\ !			_		ı. —		
				INGER SIZE			-	T 47	21		-	I 74	+	1 91	+	I 125	33.1	132	70 36 I			I 182	 	0' I 230	-
INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT	CUANTLEY		QUANTITY	T	QUANTITY	T	QUANTIT		QUANTITY		QUANTITY		QUANTITY		QUANTITY		DUANTITY		LINE
1 (19)	BER, SOFT WOOD			(111011110)		(POULDS)			1		Π.	<u> </u>	-		II ⁻		<u> </u>		Ι,				,	1 / 5.	
1	FLOOR, TREAD	39-3228.12-2	108	2 X 12	20'-0"	150			20	900			I		Π										1
2	DO	39-3228.12-16	106	2 × 12	16'-0"	120	20	540							i -						100	3200	1	1	2
3	DO	59-5228.12-14	105	2 X 12	14'-0"	105									72	2016			100	2300					3
4	DO	39-3228.12-12		2 X 12	12'-0"	90			1		50	1200	67	1608			100	2400					150	3600	4
5	FLOOR, DECK	39-3880.05-14	75	2 X 6	14'-0"	53	111	1554	148	2J72	221	3094	295	4130	369	5166	443	6202	516	7224	590	8260	564	9295	5
6	00	39-3880.06-1	73	2 X 5	10'-0"	37	111	1110	148	1480	221	2210	295	2950	369	3690	443	4430	516	5160	590	5900	664	6643	
_ 1	NAILER	39-3360.06-15	136	6 X 5	16'-0"	180	11	96 330	14	96 420	20	95	2	96	2	96	2	96	2	95	2	96	2	96	-
3	CURB	39-3360.06-1 39-3360.06-15	186	6 X 6	16'-0"	112	2	96	3	144	1	43	26 6	780 288	32	960 192	38	1140 432	44 11	1320 528	50 12	1500 576	56	1680	3
10.	DO	39-3360.06-12	134	6 x 5	12'-0"	135		70	1	144	4	144		200	4	144	,	472	11	728	12	276	14	672	10
11	CURB FILL	39-3360.06	351	6 x 6	3'-0"	34	2	13	1 4	36	8	72	10	90	14	126	16	144	20	180	22	193	26	234	1
12	00	39-3360.06	390	6 × 6	3'-0"	34	4	55	4	36	4	35	4	36	4	35	14	36	20	36	4	36	4	36	1
13	HANDRAIL POST	39-3340.04	354	4 × 4	#,-0.	20	6	32	8	45	12	64	14	75	18	96	20	107	24	128	26	139	30		13
14	HANDRAIL	39-3880.06-16	76	2 × 6	16'-0"	60	2	32	1																14
15	DO	39-3880.06-14	75	2 X 6	14'-0"	53			3	42	5	70	5	84	8	112	9	126	11	154	12	158	14	195	15
STE				1	1	1	П		п		П		П	ı	n .		п						11	1	п-
16_	STRINGER	48-2900.36-23	526W	36 I 230	40'-0"	9200	<u> </u>	-	1		#	-	1	-			 		₩		-		12		16
17	00		1		9'-10 1/2			-	+	-	₩	-	-		 - -				 		.		6	ļ <u>.</u>	1.7
18_	00	1	524W	36 I 182	40'-0" 59'-10 1/2"	7290 7257			1	 	 	<u> </u>	-		 						6		 		18
20	00		 		40'-0"	6000			 				 						6		0				20
21	00	48-2900.36-15	522W	36 I 150	29'-10 1/2"	4481			 		 								6		_		 		21
22	20				40'-0"	5280			1		Ĭ				l		6		ľ						22
23	00	48-2900.33-132	518W	53 I 132	19'-10 1/2"	2524											5								23
24	00	48-2900.33-125	61.60	33 I 125	40 ' -0 "	5000			<u> </u>						6										211
25	DO	48-2900.33-123	3104	77 1 127	8,-10 1\s.	1234			<u> </u>				ļ		6										25
26	00	48-2900.27-091	508W	27 I 91	39'-10 1/2"	3629			 				6				<u> </u>								2.5
27	00	48-2900.24-074		24 I 74	29'-10 1/2"				4		6						<u> </u>								27
29	DO	48-2900.21-059		21 1 59	19'-10 1/2"				6						<u> </u>		ļ. <u>. </u>		ļ						28
29	00	48-2900.18-047		18 I 47	4'-10 1/2"	699	10		H		1.4		15		15		20		20		0.5		26		29 30
30 31	DIAPHRAGM STIFFENER	48-3790.12-21	P15	12 C 20.7	2'-5"	13	10	ļ <u>-</u>	10		15		12		12		20		48		25 60		25 60		31
32	50	47-7844.04	P10, P5	4 x 3/8	2'-0"	10			1				36	· · · · ·	36		48		1-5-		- "				32
33	00	47-7844.04	P4	4 × 3/8	1'-9"	9			1		36						1		†	- 1					33
34	00	47-7844.04	P6	4 × 3/8	1'-7"	8			24				l												34
35	DO	47-7844.04	P3	4 × 5/9	1"-4"	7	24								Ì										35
36	WEB SPLICE PLATE	47-7844.04	99	12 X 3/8	1'-6"	23									12		12								36
37	00	47-7844.04	P14	12 × 3/8	11-9-	27													12		12		24		37
38	FLANGE SPLICE PLATE	47-7944.03	P16	9 × 7/8	3'-7*	96															6				38
39		47-7844.08	P17	10 1/2 × 7/8	8'-0"	250			↓				ļ								6				39
40_	00	47-7844.05	P24	10 X-5/8	5'-4"	50	-		1.		I		-						6		6				40
41	00	47-7844.1	P25	10 X 1	3'-8"	125	ļ		-		-	-	 		ļ				6						41
42	00	47-7844.04	P23	9 x 3/8	1,-8,	19	1	-	1		#	 	₩		6		 		 						43
43	00	47-7844.05	P31	3 X 1/2	2'-4"	32			-										6						11
44	DO DO	47-7844.04	P34	9 x 5/8 6 x 5/4	2'-0"	92	+		1		-		#		6						 		24		44
46	00	47-7944.03	P41	3 x 7/8	1'-0"	9			1		 	-	Ħ T		1								24		45
47	90	47-7844.1	P42	8 × 1	4'-0"	109				_		-											24		47
48	DO	47-7844.1	P43	9 X 1	4'-0"	122					1		1				6								43
49	90	47-7844.05	PB	7 X 1/2	1'-10*	22											5								49
50	00	47-7844.05	P38	9 x 1/2	#1-4"	65											6								50
51	NATLER ATTACHMENT PLATE	47-7844.03		2 × 1/4	0'-4"	0.6	24		30		42		54		66		73		90		102		114		51
5 2	WELDING ELECTRODE	46-5772.25-5		7/32											35 LB		118 LB		129 LB		227 LB		773 L		52
53	<u>D</u> O	46-3772.2-7		3/15			35 L3		37 LB	l	45 LB		50 LB		63 LB	ļ	98 L8		108 LB		103 LB		58 L8		53
	EL HARDWARE, BLACK		1		1	1	П	I	1		J		ıl.												ı
	NACHINE BOLT, SOLAPE HEAD, TWO WASHED			3/4	12"	2.1	6		8		12		14		16		20		24		26		30		54
55	DO TO THE SOURCE HEAD HOSSES	43-2325.07-1	B10 D20	3/4	20 *	3.0			3 15	 	12 24		28		18 36		20 40		24		2 6 5 2		50 60		5 5 5 6
56 57	DRIFT BOLT, SQUARE HEAD, WASHER	43-1636.07-2	520	50 d	20	.10		_	14		14		14		14		14		14		14		14		57
58	00	42-6028.3-5	1	50 d	1	.08			444		710		920		1070		1400		1510		1780		1990		58
59	20	42-6028.3-3		30 d		.05			2650	245	3952		5271		6590		7910		9210		10530		11850		59
60	50	42-6028.3-2	<u> </u>	20 d		.04			38		58		68		88		98		118		128		148		60
_											_								-						

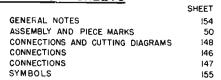


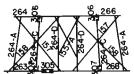


BILL OF MATERIALS FOR FLOOR AND STRINGER COMBINATIONS

1.	STANDARD PLANK FLOOR RIVETED STEEL DETAILS HARDWARE	SHEET 48 48 48
2.	STANDARD PLANK FLOOR WELDED STEEL DETAILS HARDWARE	48 49 48
3.	ALTERNATE LAMINATED FLOOR RIVETED STEEL DETAILS HARDWARE	49 48 49
4.	ALTERNATE LAMINATED FLOOR WELDED STEEL DETAILS HARDWARE	49 49 49

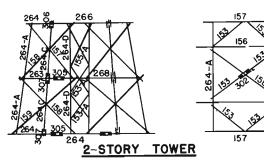


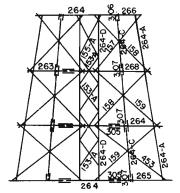




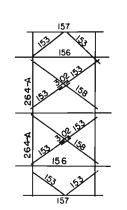


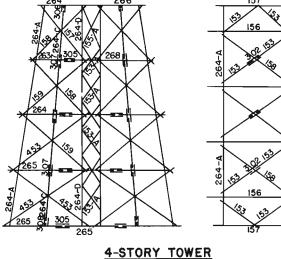
HSTORY TOWER

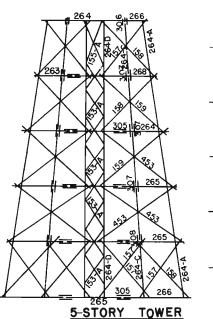




3-STORY TOWER

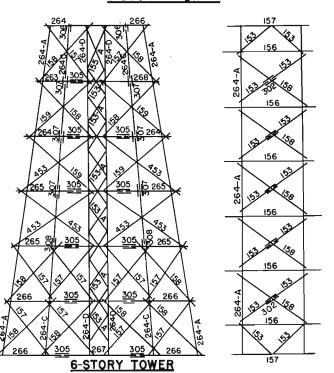


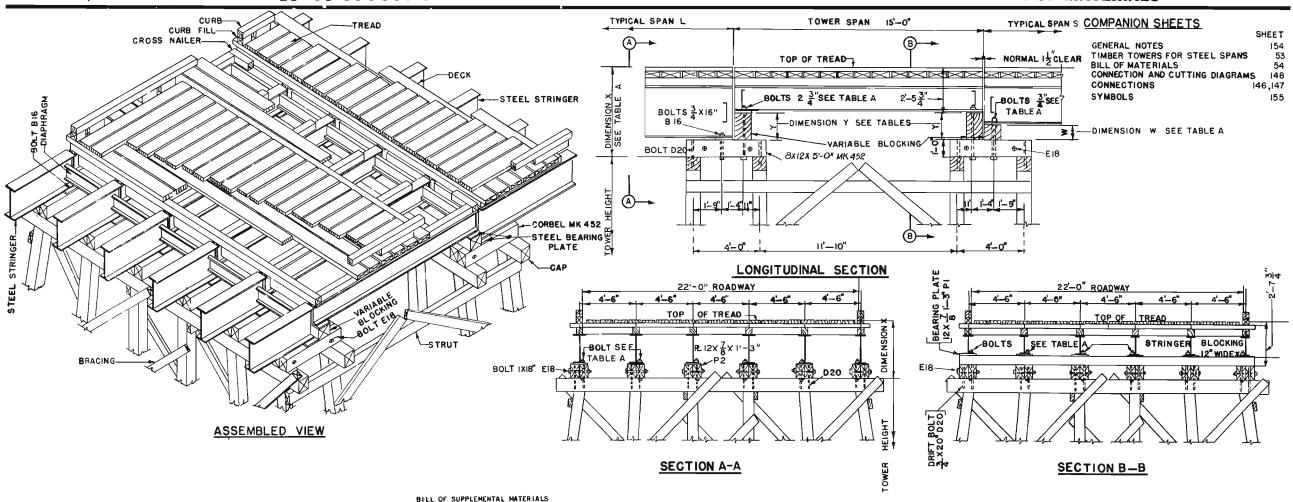




BILL OF MATERIALS FOR ONE TOWER OF NUMBER OF STORIES INDICATED

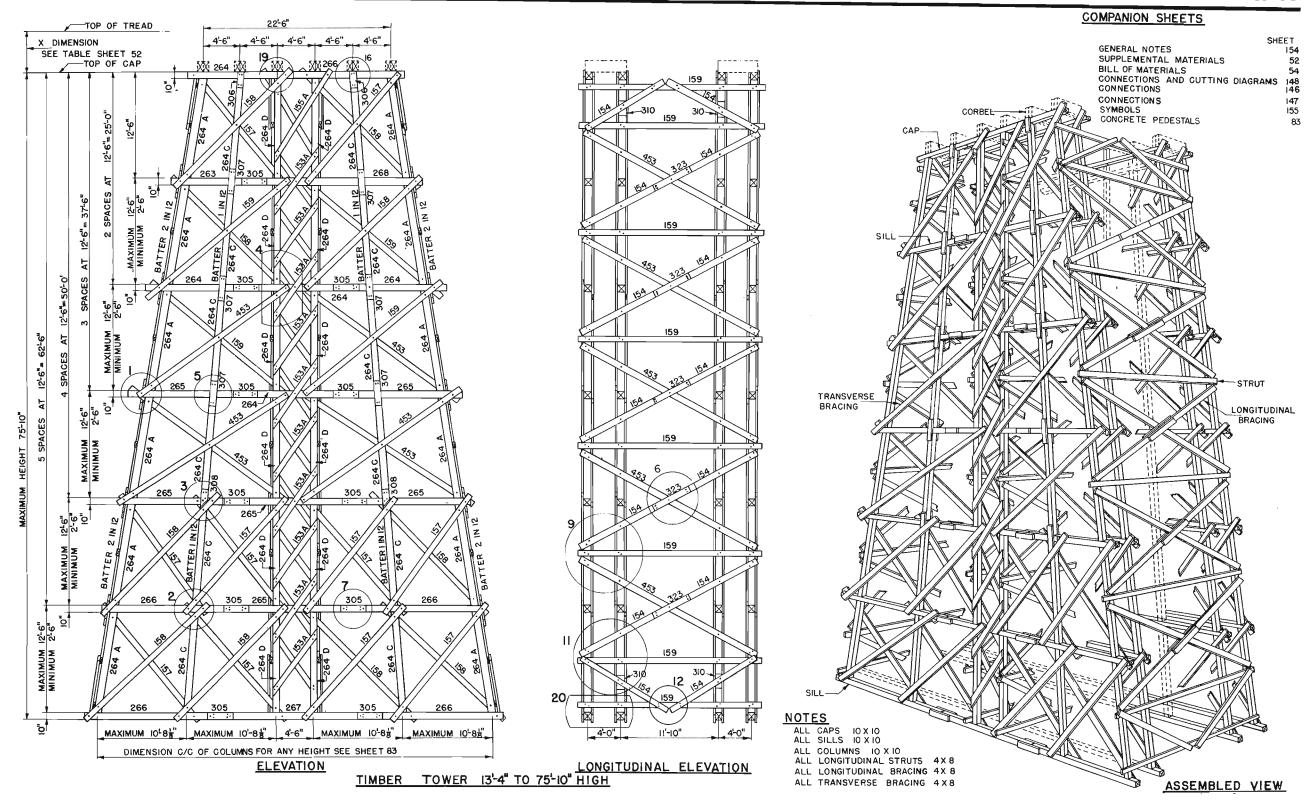
	BILL OF MATERIALS FOR CHE TOM			NO OF 6	BTORIES		6-sr0	ORY	5-SF	DRY	4-61	CRY	3-51	TORY	2-\$1	ORY	1-5	TORY .
				TOWER H	HEIGHT		75'∸1	0.	65'-	4"	50'-	10"	-164	-4-	25'-	10"	13'-	-u×
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POLINOS)	QUAHFITY	FBM	QUANT I TY	FBM	QUANTI TY	FRM	אוואגנו	FBH	QU VITI I TY	FBM	ÖNJULLITA	
	LUMBER SOFT-HOOD																	
1	CAP	39- 6620. 1-16	266	10 X 10	16'-0"	500	2	267	2	267	2	267	2	267	2	267	2	267
2	_∞ 1	39-6620.1-12	254	10 × 10	12'-0"	375	2	200	2	200	2	200	2	200	2	200	2	200
3	SILL	59- 6620. 1-2	268	10 X 10	20'-0"	625	2	353	2	333	2	353	2	333	2	333	2	. 333
4	90	39- 6620. 1-18	267	10 × 10	18'-0"	563	2	500										
5	∞	39-5620.1-16	256	10 < 10	16'-0*	500	8	1057	4	533								
6	30	39-6620.1-14	255	10 x 10	14'-0=	438	12	1400	12	1400	10	1157	ц	467				
7	20	39-6520. 1-12	254	10 x 10	12'-0"	575	8	800	8	800	3	800	8	300	6	600		
8	DO	39-6620.1-1	253	10 × 10	10'-0"	313	2	167	2	167	2	157	2	157	2	167	2	157
9	COLUMN	39-6620.1-12	2644	10 × 10	12'-0"	375	24	2400	20	2000	16	1600	12	1200	В	900	4	400
10	00	39-6620. 1-12	264C	10 × 10	12'-0	375	24	2400	20	2000	15	1600	12	1200	1	300	4	400
11	no	39-6620.1-12	2640	10 × 10	12'-0"	375	24	2400	20	2000	16	1600	12	1200	8	800	4	400
12	STRUT	39-3540.08-18	157	4 X 3	18'-0"	180	4	192	4	192	4	192	ц	192	4	192	4	192
13	DC	59-3540.08-16	156	4 X 8	16'-0"	160	48	2048	40	1707	32	1355	24	1024	16	د88	8	342
14	BRACING	39-3340.08-24	453	4 x 8	241-0*	240	12	768	12	768	12	768	4	256				
15	DO	39-3340.08-22	159	4 x 8	22'-0"	220	8	469	8	469	8	469	8	459	4	235		
16	00	39-3340.08-2	158	4 X 8	20'-0"	200	30	1600	20	1067	14	747	12	640	10	533	4	213
17	00	39-5340.08-18	157	4 x 8	18'-0"	180	24	1152	16	768	4	192	4	192	4	192	1 4	192
18	00	39-3340.08-14	155	4 . 8	10'-0"	100	28	747	24	640	20	533	16	427	12	320	3	213
19	00	39-3340.08-1	155A	4 X 8	14,-0-	140	4	149	4	149	4	149	4	149	4	149	4	149
20	DO	39-3340.08	1534	4 × 8	10'-0"	100	40	1067	32	355	24	640	16	427	9	213		
21	SCA8	39-3340.1	305	4 X 10	3'-0•	33	44	440	36	360	28	280	20	200	12	1.50	4	40
22	20	39-3330·1	306	3 X 10	2'-0"	19	8	40	8	40	3	40	8	40	8	40	8	40
23	00	39-5952-1	307	3 × 10	3'-0"	23	24	180	24	130	24	180	24	180	16	120	8	60
24	00	39-3330.1	308	3 × 10	2'-0"	19	8	40	8	40	8	40		-				
25	∞	39-3228.08	502	2 x 3	3'~4"	17_	20	89	16	71	12	53	8	36	ц	18		
	STEEL HARDWARE, BLACK																	
26	MACHINE BOLT WITH SQUARE NUT	43-2325. 1-24	€24	1	24"	6.48	16		16		16		16		16		. 8	
L	AND TWO WASHERS																	
27	00	45-2325. 1-2	E20	1	20 *	5.61	382		500		226		156		85		24	
28	00	45-2325. 1-18	E18	1	18*	5. 18	80		87		86		64		48		52	
29	20	45-2325.1-164	E16	1	16*	4.75	240		203		160		128		96		. 72	
X Q	ро	43-2325 <u>. 1-1</u> 04	E10	1	10=	5.45	66		56		46		36		26		16	
31	DRIFT BOLT, PLAIN	43-1636.07-2	E20	3/4	20 *	2.50	186		150		114		86		58	_	30	

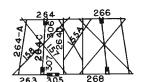


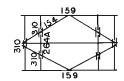


TΑ	BL	ΕA										
	SP	AN L		90'	80'	70'	60'	50'	40'	30'	20'	15'
			х	5-13"		5-13"	4'-11"	4-103"	4-44	4-14"	3-103	3'-72"
			Υ	1'-6 "	1'-6½"	1'-6"	1,-34,	1-38	o'-9"	0'-6"	0'-3"	0"
3ER	SPAN		w	2'-23"	2'-2‡"	2'- 3 ³ "	2'- 1"	2'-07"	I'-6¾"	1'-3¾"	1-03"	0'-93"
TIMBER	SP	BOLT	Α	42"	42"	42"	38"	38"	32"	30"	26"	24"
	5'		8	1'-6"	l'-6≟"	1'-6"	1-34"	1,-34.	0'-9"	0,-6,	0'-3"	
	-1	BOLT	Α	34"	3.4"	34"	30"	30"	24"	22"	18"	
	20		8	I'-3"	I-3₺"	1-3"	1-04"	1'-0å"	0'-6"	0'-3"		
	2	BOLT	Α	3ď'	32 "	30"	28"	28"	·22"	18"		
	30		W	1,-0,	1,-01,	1,-0,,	0'-9‡"	0,-94,	0'-3"			
	(N)	BOLT	Α	28"	26"	28"	24"	24"	18"			
S	40		W	0'-9 "	0'-9 ½"	0'-9 "	0-64	0'-6 ₈				
z	4	BOLT	Α	24"	26"	24"	22"	22"				
SPAN	50'		W	0'-27"	0'-3濟"	0-23"	0-08					
လ	2	BOLT	Α	18"	18"	18"	16"					
	-09		W	0'-2¾"	0'-34"	어-2훏"						
	9	BOLT	Α	16"	16"	18 9						
	2		W	•	0'-0불"							
	F	BOLT	Α	16"	16"							
	F0		W	0-0취	-	BLOCK	NG IS	UNDER	90' SP	NA		
	90	BOLT	Α	16"								

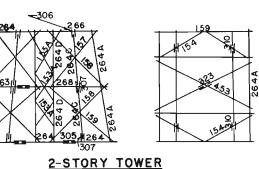
		BILL OF SUPPLEMENTAL I	MATERIALS											_												
					MAIN S	SPAN		15		20		301		40)'	50	•	60,		70'		80'		90	<i>j</i> •	
					STRING	SER SIZE	Ε	18 I	47	21 I	59	24 I	74	27 I	91	33 I	125	33 I	132	36 I	150	56 I	182	36 I	230	ا اي
,					DIMENS	SION X		51-7	3/4"	3'-10	3/4*	4'-1	3/4"	4'-4	3/4"	41-1	0 7/8*	4'-11	.•	51-1	3/4"	5'-2	1/4*	5'~1	3/41	1 1
					DIMENS	SION Y		0'-0		01-31		0'-6"		0'-9	•	1'-3	1/8"	1'~3	1/4"	1'-6"		1'-6	1/2"	1'-6	į.	
l	LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANT I IY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE
	1	BEARING PLATE	47-7844.08	P2 1	2 X 7/8	1'-4"	47.6																	12		
	2	DO	47-7844,08	Pala	2 X 7/8	11-30	44.6	24		24		24		24		24		24		24		24		12	ш	2
i L	LUMBER, SOFT WOOD																									
1 [3	CORBEL	39-6616.12	452	8 X 12	5'-0"	150	24	960	. 24	960	.24	960	24	960	24	960	24	960	24	960	24	960	24	960	
lL	4	BLOCKING	39-6630-12-12	284 1	2 X 12	12'-0"	540										576	4	576	4	576	*	576	4	.576	4
1 L	5	00	39-3360-12-12	214	6 X 12	12'-0"	270					4	288	4	288					4	288	4	288	4	288	5
1 L	6	00	39-3952-12-12	134	3 X 12	12'-0"	90							4	144	4	144	4	144						لــــــا	6
1 L		STEEL HARDWARE, BLACK									,															
	7	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.1-18	E18	1	18*	5.0	24		24		24		24		24		24		24		24		24		7
\	8	DO	43-2325.07-346	B34	3/4	344.	4.74													12		12		12		8
1	9	DO	43-2325.07-506	B30	3/4	30.	4.26									12		12								
1	10	DO	43-2325.07-24	824	3/4	24"	3.54							12												10
1 [11	DO	43-2325.07-223	B22	3/4	22"	3.30					12														11
1 [1.2	00	43-2325-07-183	818	3/4	18"	2.82			12																12
J	13	00	45-2525.07-16		3/4	16"	2.58	24		12		12		12		12		12		12		12		12		13
1 [14	DRIFT BOLT WITH SQUARE HEAD AND HASHER	43-1636.07-2	DEO	3/4	20"	3.0	48		48		48		48		48		48		48		46		46		14

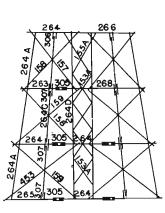


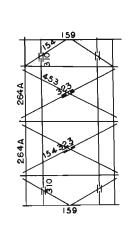


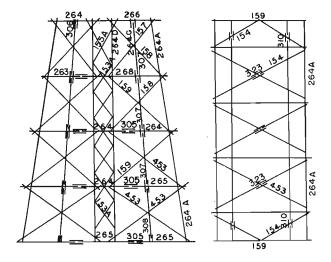


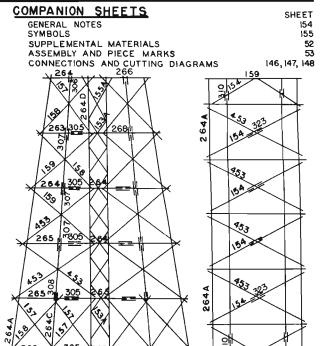
LSTORY TOWER







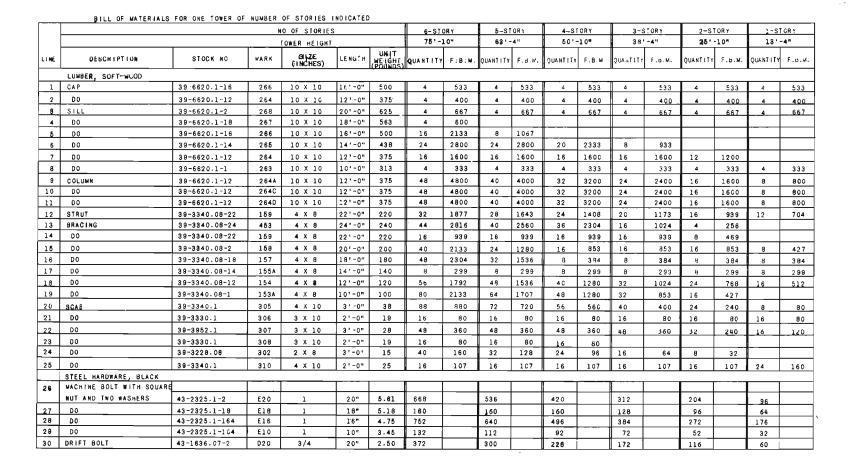


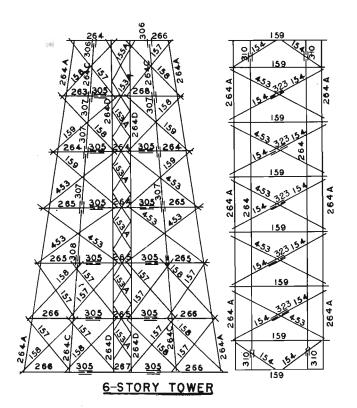


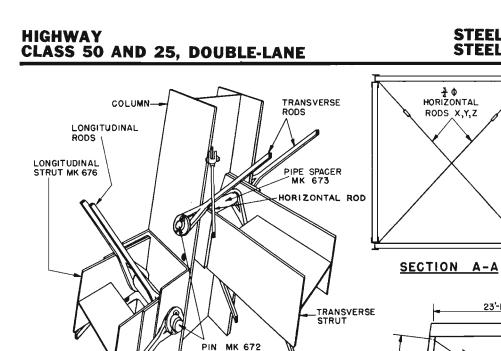
3-STORY TOWER

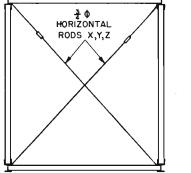
4-STORY TOWER

5-STORY TOWER

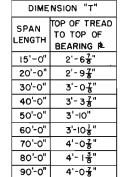






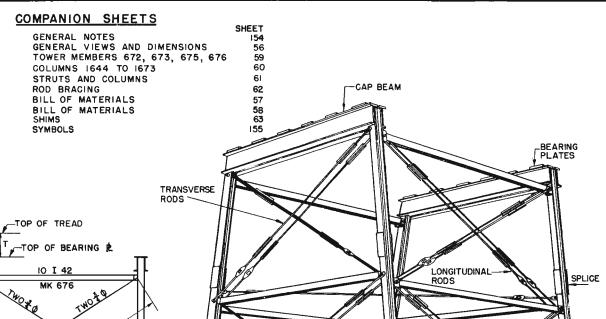


23'-11"



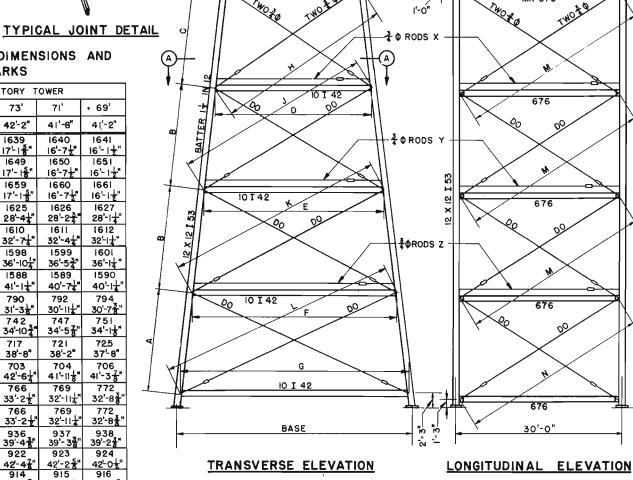
CLASS 25: TWO 24 I74 MK 615 CLASS 50: TWO 30 I 108 MK 675

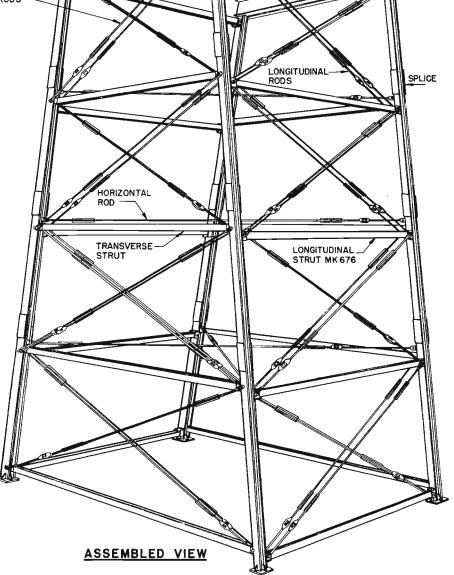
FOUR-STORY TOWERS, 69 TO 77 FEET HIGH, **GENERAL VIEWS AND DIMENSIONS**

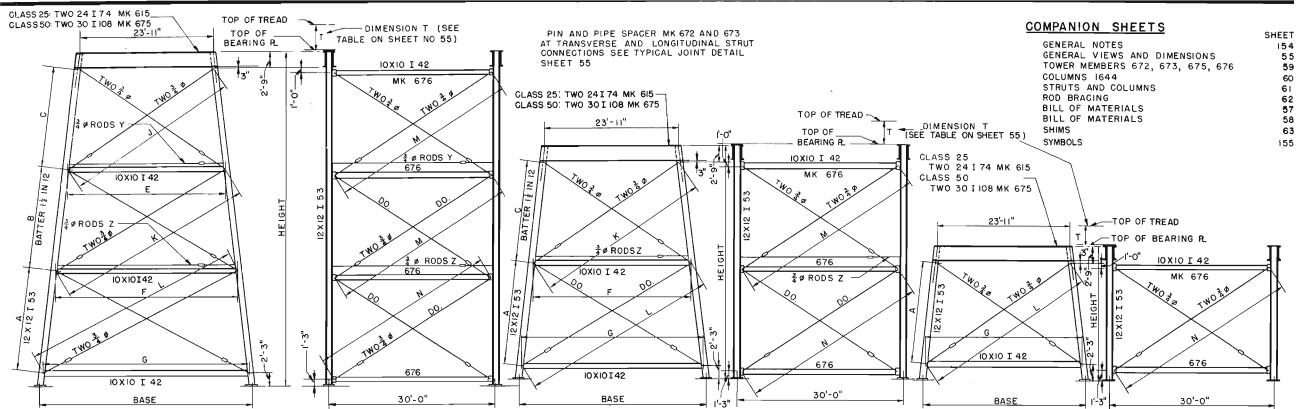


TABULATION OF TOWER DIMENSIONS AND **ERECTION MARKS**

			FOUR-	STORY T	OWER	
HEI	ЭНТ	77'	75'	73'	71'	• 69'
ВА	SE	43'-2"	42'-8"	42'-2"	41'-8"	4 ('-2"
Α	MARK	1637	1638	1639	1640	1641
	DIMENSION	18'-1 8 "	17 ¹ -7 5 "	17- 1 5 "	16'-7½"	16'-1 1 ''
В	MARK	1647	1648	।649	1650	1651
	DIMENSION	18 ¹ -1 5 "	17'-7 8 "	।7'- ।ई "	16'-7±"	16'-1 1 "
С	MARK	1657	1658	1659	1660	1661
	DIMENSION	18'- 1 5 "	i7'-7 \$ "	17'-1 5 "	16'-7 ½ "	16'-1 ½ "
D	MARK	1623	1624	1625	1626	1627
	DIMENSION	28'-7 "	28 ¹ -5 1 1"	28'-4 1 "	28'-2 3 "	28'-1 ‡ "
E	MARK	1608	1609	1610	1611	1612
	DIMENSION	33'-1 1 "	32'-10 ∤"	32'-7 ∤"	32'-4 1 "	32'-1 1 "_
F	MARK	1595	15 96	1598	1599	160।
	DIMENSION	37'-7 4 "	37'-2 3 "	36'-104'	36'-5 3 "	36'-। <mark>दे</mark> "_
G	MARK	1586	1587	1588	1589	1590
	DIMENSION	42'-1 1 *	41'-7 ‡"	41'-1 ↓ "	40'-74"	40'-1 1 "
H	MARK	783	786	790	792	794
	DIMIENSION	31'-11"	31'-7"	31'-3 a"	30'-11 ' 2"	30'-7 3 "
J	MARK	737	741	742	747	751
	DIMENSION	35 ^L 8 § "	35'-3 } "	34'-10 1 "	34'-5 8 "	34'-1 3 "
К	MARK	710	712	717	721	725
	DIMENSION	39'-8 18"	39'-2"	38'-8"	38'-2"	37 ^L 8"
L	MARK	700	70 l	703	704	706
	DIMENSION	43'-8¾"	43¹-1 ½*	42'-6 ¹	41-⊓ <mark>‡</mark> "	41'-3 7 "
М	MARK	758 ₇ "	762	766	769	772
	DIMENSION	33'-8 1 "	33'-5 8 "	33'-2 1 "	32'-11 <u>↓</u> "	32'-8 3 "
N	MARK	758	762	766	769	772
	DIMENSION	33'-8 7 "	33'-5 1 ''	33'-2±"	32'-11 1 "	32'-8 1 "
X	MARK DIMENSION	934 39'-6 ½ "	33 32	936 39'-4 3 "	937 39'-3 1 "	938 39'-2 1 "
Y	MARK	920	921	922	923	924
	DIMENSION	42'-9 1 "	42'-7 1	42-4 1	42'-2 { "	42-01/2"
Z	MARK	912	913	914	915	916
	DIMENSION	46 ^L 2 1	45'-11 <u>+</u> "	45 ¹ 7∰"	45'-4 1 "	45'-0 1







					THREE-STOR	Y TOWER								TWO-STOR	Y TOWER								01	E-STORY TO	WER			
HEIG	SHT	67'	65'	63'	61'	59'	57'	55'	53'	51'	491	47'	45'	43 '	41'	39'	37'	35'	33	31'	29'	27'	25'	23'	21'	19'	17'	15'
BASE		401~8"	40'-2"	391-8"	39'-2"	38'-8"	381-2"	37'-8"	37'-2"	36'-8"	36'-2"	35'-8"	35'-2"	34'-8"	34'-2"	33'-8"	33'-2'	32 ' -8"	32'-2"	31'-8"	31'-2"	30'-8"	30'-2"	29'-8"	29'-2"	281-34	28'-2"	27'-8"
٨	MARK DIMENSION	1633 22'-2"	1635 20'-1 7/8'	1636 '18'-1 3/4"	1637 18-1 5/8"	1637 18' -1 5/8"	1639 17'-1 5/8"	1639 17'-1 5/8"	1641	1642 15'-1 3/8"	1633 22'-2"	1634 21'-2"	1635 20'-1 7/8"	1636 19'-1 3/4'	1637 18'-1 5/8"	1639 17'-1 5/8"	1641	1642 15'-1 3/8"	1643 14'-1 1/4"	1665 26'-2 3/8"	1666 24'-2 1/4"	1667 22'-2"	1668 20'-1 7/8"	1669 18'-1 5/8"	1670 16'-1 1/2"	1671 14'-1 1/4"	1672 12'-1 1/8"	1673 10'-0 7/8
8	MARK DIMENSION	1644 20'-1 7/3"	1644 20'-1 7/8'	1645 19'-7 7/8'	1646 19'-1 3/4	1647 "18'-1 5/a"	1648 17'-7 5/8"	1650 16' -7 1/2"	1651 16'-1 1/2"	1652 15'-7 1/2"																		
С	MARK DIMENSION	1654 20'-1 7/8"	1654 20'-1 7/8"	1655 19'-7 7/8"	1656 13'-1 3/4'	1657 18'-1 5/3"	1658 17'-7 5/8"	1660 16' -7 1/2"	1661 16'-1 1/2"	1662 15'-7 1/2"	1652 22'-2"	1653 21'-2"	1654 20'-1 7/8"	1656 19-1 3/4"	1657 18'1 5/8"	1659 17'-1 5/8"	1661 16'-1 1/2"	1663 15-1 3/8"	1664 14'-1 1/4"									
Ε	MARK DIMENSION	1618 29'-1 1/4"	1618 29'~1 1/4"	1621 28'-11 3/4"	1622 28'-101/4"	1623 28'-7 1/4'	1624 28'-5 3/4"	1626 28'-2 3/4"	1627 28'-1 1/4"	1629 27'-113/4"																		
F	MARK DIMENSION	1605 34'-1 1/4"	1605 34'-1 1/4"	1606 33'-101/4"	1607 33'-7 1/4"	1608 33'-1 1/4"	1609	1611 32'-4 1/4"	1612 32'-1 1/4"	1613 31'-101/4"	1619 29'-7 1/4"	1620 29'-4 1/4"	1618 29'-1 1/4"	1622 28'-101/4	1623 28'-7 1/4"	1625 28'-4 1/4'	1627 28'-1 1/4"	1630 27'-101/4"	1631 27'-71/4"									
G	MARK D:MENSION	1591 39'-7 1/4"	1592 39'-1 1/4"	1593 38'-7 1/4"	1594 38'-1 1/4"	1595 37'-7 1/4'	1597 " 37'-1 1/4"	1600 36'-7 1/4"	1601 36'-1 1/4"	1602 35'-7 1/4"	1603 35'-l 1/4"	1604 34'-7 1/4"	1605 34'-1 1/4"	1607 33'-7 <u>1</u> /4"	1608 33'-1 1/4"	1610 32'-7 1/4"	1612 32'-1 1/4"	1614 31'-7 1/4"	1615 31'-1 1/4"	1616 30'-7 1/4"	1617 30'-1 1/4"	1619 29'-7 1/4"	1618 29'-1 1/4"	1623 28'-7 1/4"	1627 28'-1 1/4"	1631 27'-7 1/4"	1628 27'-1 1/4"	1632 26'-71/4"
J	WARK CIMENSION	764 33'-3 3/8"	764 33'-3 3/8'	769 32'-11 1/4"	773 32'-7 1/8"	783 31'-11"	786 31'-7"	792 30'-11 1/4"	794 30'-7 3/8"	797 36'-35/8"																		
К	MARK DIVENSION	727 37'-4 3/4"	727 37'-4 3/4"	730 36'-113/4"	732 36'~6 5/8'	737 1 351-8 5/91	741 " 35'-3 3/4"	747 34'-5 7/8"	751 34'-1 1/8"	759 39'-8 3/a"	744 34'-8 5/8"	753 33'-11 7/8"	764 331~3 3/8"	773 32'-71/8"	783 31'-11"	790 31'-3 1/8"	794 30'-7 3/6'	801	806 29'-4 7/8"									
L	MARK DIMENSION	702 42'-11"	705 41'-8 1/2"	707 40'-107/8"	708 40'-1 3/8"	710 39'-4 1/9'	714	719 38'-5 1/4"	725 37'-8"	731 36'-11"	713 39'~1 1/2"	720 38'-8 1/8"	727 37'-4 3/4"	732 36'-65/8"	737 35'-8 5/8"	742 34*-103/4	751 34'-1 1/8	764 33'-3 5/8"	774 32'-6 1/4"	724 37'-8 7/8"	734 36' <i>-</i> 2 3/8"	744 34'-8 5/8"	764 33'-3 3/8"	783 31'-11"	794 30' ~7 3/8"	806 29' -41/8"	815 28'-3 3/8"	82 0 27' -3"
M	MARK DIÆNSION	743 34'-103/8"	743 34'-103/8"	746 34'-6 7/8"	1056 34'-3 1/2"	758 33'-8 7/8"	762 33'-5 5/8"	769 32'-111/4"	772 32'-8 3/8"	77 6 32'-5 1/2"	736 36'-0 3/4"	739 36'-5 1/2"	743 34' -10 3/8"	1 056 34"-3 1 /2"	758 33'-8 7/8"	766 33'-2 1/2"	7 72 32 ' -8 3/8"	781 32' -2 5/8"	785 31'-9"	1 37'-8 7/8" 36'-2 3/8" 34'-8 5/8" 33'-3 3/8" 31'-11" 30'-7 3/8" 29'-41/8" 28'-3 3/8" 27								
N	MARK DIMENSION	736 36'-0 3/4"	743 341-103/8"	748 34'-3 1/2"	758 33'-8 7/8"	758 33'-8 7/8'	766 " 33'-2 1/2"	766 33'-2 1/2"	772 32'-8 3/8"	781 32'-2 5/8"	736 36'-0 3/4"	739 35'-5 1/2"	743 34'-103/8"	1056 34'-3 1/2"	758 33'-8 7/8"	766 33'-2 1/2'	772	781 32' -2 5/8"	785 31'-9"	717 38'-8"	728 37'-4 1/8"	736 36'-0 3/4"	743 34'-10 3/8"	758 33'-8 7/8"	772 32'-8 3/8"	785 31'-9"	793 30'-11"	798 30'-21/8"
CLEVIS ROD Y	MARK DIVENSION	931 39'-105/8"	931 39' -10 5/8'	932 39'-9 5/8"	933 39'-8 5/8"	934 39'-6 1/2"	935	937 39'-3 3/8"	938 938	39'-1 3/9"																		
CLEVIS ROD Z	MARK	917 43'-6 1/4"	917 43'-6 1/4"	918 43'-4"	919 43'-1 3/4"	920	921 " 42'-7 1/8"	923 42'-2 5/8"	924	925 41'-101/4"	929 40'~2 7/8"	930 40'-0 3/4"	931	933 38'-8 5/8"	934 39'-6 1/2"	936 39'-4 3/8"	938 39'~2 3/8"	940 39'-0 3/8"	942 88'-101/4"								,	

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									то	OLA FER HEIGHT G	SS 50 HULP OLASS	ITEICATION					_	TOHER HEI	OLASS 25 SHT GACUP	CLASSIFICAT	ION		1
				DETAILED	SIZE	i		STORY TO 79'		STORY TO 67'		STURY 10 49'		STORY TO 31'		ITORY TO 791		STORY TO 67'		STORY TO 49'		STORY TC 31'	
.INE	DESCRIPTION	STUCK NO	MARK	SHEET	(INCHES)	LENGTH	NUMBER	WEIGHT EACH (POUNDS)	HUHBE R	WEIGHT EACH (POUNDS)	N UMBE R	WE IGHT EACH (POUNDS)	NUMBER	WEIGHT EACH (POUNDS)	NUMBER	HEIGHT EACH (POUNDS)	NUMBER	HEIGHT EACH (POUNDS)	NUMBER	HEIGHT EACH (POUNDS)	NUMBER	WEIGHT EACH (POUNDS)	LIN
1	CAP BEAH	49-2900.3-108	675	59	30 I 108	25'-5_1/2"	4	2750	4	2750	4	2750	4	2750									1
2	BEAHING PLATE	47-7844.07	P6	59	22 X 5/4	1'-10"	12	103	12	103	12	103	12	103									2
3	DIAPHRAGM		ບາ	59	12 X 12 I 53	2'-3"	8	119	8	119	8	119	8	119	İ		L		ļ				3
4	CAP BEAM	48-2900.24-074	615	102	24 I 74	25'-4"									4	1875	4	1875	4	1875	4	1875	4
	BEARING PLATE	47-7844.07	P7	102	21 × 3/4	1'-10"									12	98	12	98	12	98	12	98	5
4	DIAPHRAGM		02	102	12 × 12 I 53	1'-9"									В	93	8	93	8	93	8	93	6
7	HIVETS IN BEARING PLATES	43-6353.08		59, 102	7/8	3.1/4"	96	.79	96	.79	96	_7¢_		.79	96	.79	96	. 79	96	.79	96	. 79	7
А	RIVETS IN HEBS OF CAPS	43-6353.08-25		59,102	7/8	2 1/2"	336	67	336	.67	336	.67	336	.67	176	.67	176	. 57	176	.67	176	. 67	8
9	LONGITUDINAL STRUT		676	59	10 I 42	28'-10 7/8"	10	1215	. 8	1215	6	1215	4	1215	10	1215	8	1215	6	1215	4	1215	9
10	PIN PLATE	47-7844.04	P6	59	9 X 5/8	0'-10"	40	10	32	10	24	LO	16	10	40	10	32	10	24	10	16	10	.10
11	00	47-7844.04	P5	61	9 x 3/8	0'-10"	32	10	24	10	16	10	8	10	32	10	24	10	16	10	8	10	11
12	COLUMN BASE PLATE	47-7844.1	Ρ4	60,61	18 X 1	1'-6"	4	92	4	92	4	92	4	92	ц	92	4	92	4	92	4	92	12
15	STIFFENERS	47-7844.04	P\$.15.16	60	6 X 3/8	1'-5 1/2"							4	11							4	11	13
14	DO	47-7844.04	P9.10.11		6 x 3/8	1'-5 1/2"	4	11	4	11	4	11			4	11	4	11	4	11			14
15	BRACING CONNECTOR	_	Cı	60,61	12 × 12 I 53	1'-1 1/4"	20	40	16	40	12	40	8	40	20	40	16	40	12	40	в	40	15
	DO DO	47-7844.05	P5	60,61	4 X 1/2	1'-0"	12	7	8	7	4	7			_12	7	8	7	4	7			16
.16 17	HEB SPLICE	47-7844.05	P5	60	10 × 1/2	2'-0 1/4"	16	34	8	54					16	34	8	34					17
18	FLANGE SPLICE	47-7844.05	P6	60	12 × 1/2	2'-0 1/4"	16	41	8	41		_			16	41	8	41					18
19	HEB SPLICE	47-7844.05	P15	61	10 X 1/2	2'-0 1/4"	8	34	8	34	В	34			8	34	8	34	8	34			19
20	FLANGE SPLICE	47-7844.05	P16	61	12 × 1/2	2'-0 1/4"	- 8	41	8	41	8	41			8	41	8	41	8	41			20
20	RIVETS, WEB SPLICE	43-6353.08		60,61	7/8	3 1/4"	192	.79	128	.79	64	.79			192	. 79	128	. 79	64	.79			21
21	RIVETS, FLANGE SPLICE	43-6353.08-25		60,61	7/8	2 1/2"	384	.67	256	,67	128	.67			384	.67	256	- 67	128	.67	İ		22
23	PPIN	47 0777.00 27	672	59	1 1/2 #	1'-4 1/2"	40	8	32	8	24	8	16	8	40	8	32	8	24	8	16	8	23
	POOTTER PIN			56	1/4 × 2 1/2		80	• 1	64	.1	48	.1	32	.1	80		64	.1	48	.1	32	-1	24
24		44-6246.7-02	673	59	2 Ø	0'-7"	40	2	32	2	24	2	16	2	40	2	32	2	24	2	16	2	25
25	PPIPE SPACER	44-0240.7-02	658	50	3 3/4 X 1 % 6 HOLE	334"	144	1.24	128	1.24	112	1.24	96	1.24	144	1.24	128	1.24	112	1.24	96	1.24	26
26	//WASHER		677	62	3/4 8	4'-7"	128	11	96	11	64	11	32	11	128	11	96	11	64	11	32	11	27
27	3LOOP ROD, UPSET		678	62	3/4 Ø	1'-1"	256	1.6	192	1.6	128	1.6	64	1.6	256	1.6	192	1.6	128	1.6	64	1.6	28
28	SPLICE ROD	46-6375.5-07	0/8	62	1 1/8	6 4	64	2.7	48	2.7	32	2.7	16	2.7	64	2.7	48	2.7	32	.2.7	16	2.7	29
20	3TURNBUCKLE		600	62	3/4 5	1'-79	6	4.3	1 11	4.3	2	4.3			6	4.5	4	4.3	2	4.5		£,	50
30	SCLEVIS ROD, HORIZONTAL UPSET		680		3/4 13	1'-3"	6	3.7	4	3.7	,	3.7			6	3.7	4	3.7	2	3.7			31
_بد	PO FE		680	62	3/4 D	1'-1"	24	1.6	16	1.6	8	1.6			24	1.6	16	1,6	-	1.6			32
32	SPLICE HOD	46-6575.5-07	678	62	1 1/8	6"	6	2.7	4	2.7	2	2.7			6	2.7	4	2.7	2	2.7		<u> </u>	33
33	3/URNBUCKLE			62	NO 3 FOR 1 1/8 THREAD	5×	12	4.0	8	4.0	4	4.0			12	4.0	8	4.0	4	4.0			34
34	₹cievis		+		1 3/16 p	3 1/4"	12	1.5	8	1.5	4	1.5			12	1.6		1.5		7.0		Pol -	35
55	PPIN, HEADED, CLEVIS,		+-	62	1/4 × 21/2	7.4.4	12	.,	8	.,	4	.1			12	.1	8	. 1	4	1.3			35
36	OTTER PIN	46-3772.2 46-3772.25	_ [02	1/4 ^ < 1/2		# **	+ "	H V			- '' -	t			• • •	-		<u> </u>	180 LBS	#		+-0-

リ CONNECTOR PIN ASSEMBLY, 1½"
シ LOOP ROD ASSEMBLY, 注"
シ CLEVIS ROD ASSEMBLY, 注"

HIGHWAY CLASS 50 AND 25, DOUBLE-LANE

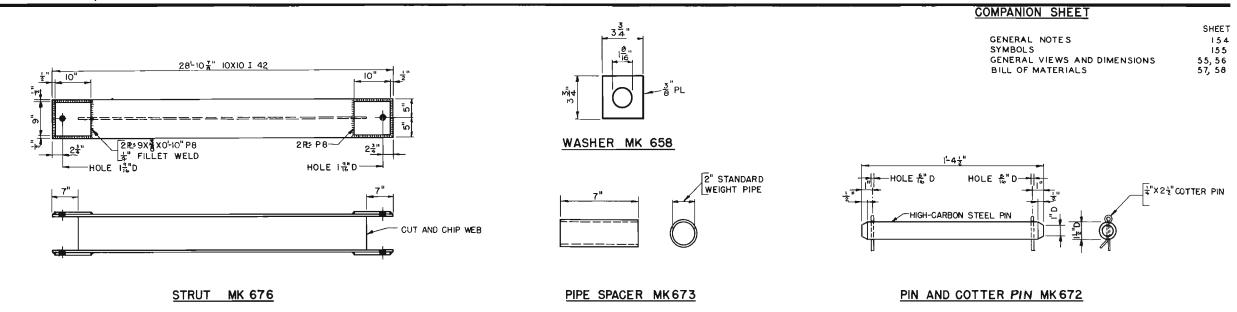
r	TABLE A - BILL OF MATERIALS FOR P			col		 	J neit					r	-[1011.7	П		d unit	1	T	O UT	COMPANION SHEETS	
			ON SHE		R MARK	STTIONED NOTI	WEIGHT (POUNDS)	Mark	LENGTH	WEIGHT (POUUDS)	MARK	REQUISITIONE LENGTH	WEIGHT (POUNDS)	Mark	REQUISITIONE LENGTH	MEIGHT	MARK	RECOURSE FLOCKE	WEIGHT (POUMDS)	SHEE	
	DESCRIPTION	LINE	TOWE	R HEIGHT		771			75'	1		73'			711			69'		SYMBOLS 15	54 55
	TOWER COLUMNS	1 2	61	2	1637R	 -11* 11*	1270	1638R 1638L	23'-5"	1240	1539R 1539L	22'-11"	1215	1640R	. 22'-4 7/8"	1190	1641R	21'-10 7/8"		BILL OF MATERIALS 5 TOWER DETAILS 59TO 6	57 62

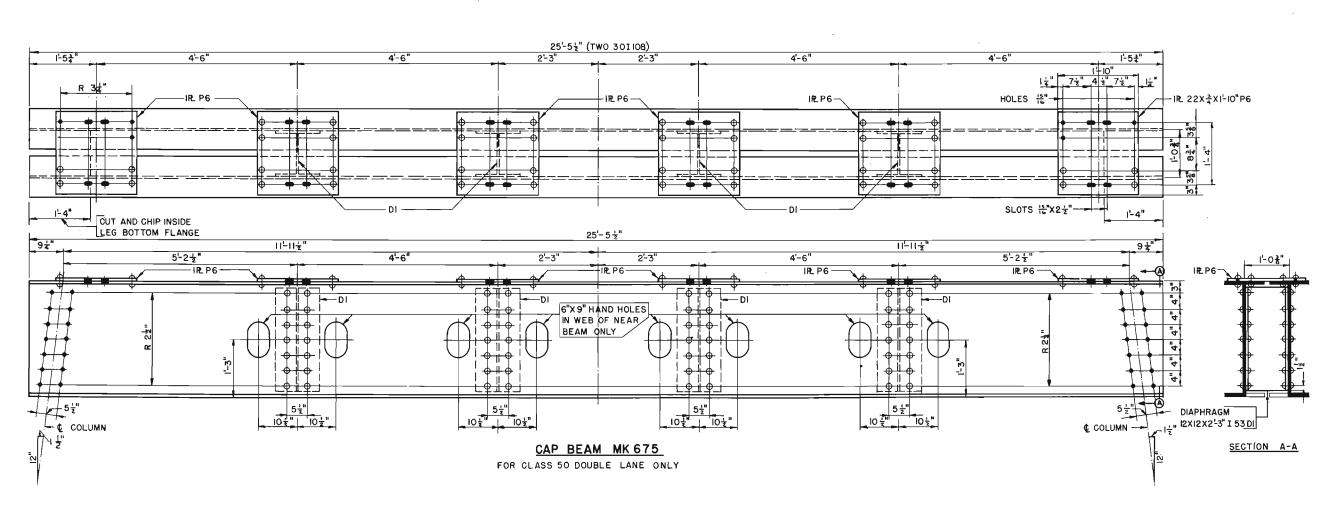
		ON SHEE	r manber	171-UKK	LENGRI	WEIGHT (POUNDS)	riveror.	LENGTH	(SOUCE)	LEALTHY	LEHSTH	WEIGHT (POUNDS)	(-1:4-0K	LENGTH	(SOUPS)	MAURA	FERSIN	WEIGHT (POUNDS)		
DESCRIPTION	LINE		HEIGHT		77'			75'		î	73'			71'			69'			GENERAL NOTES SYMBOLS
	1	61	2	1637R	23'-11'	1270	1638R	23'-5"	1240	1539R	22'-11"	1215	1640R	. 22'-4 7/8"	1190	1641R	21'-10 7/8"	1160		BILL OF MATERIALS
TOWER COLUMNS	2]	2	1637L	23'-11"	1270	1638L	23'-5"	1240	1539L	22'~11*	1215	1640L	221-4 7/84	1190	1641L	21'-10 7/8"	1160		TOWER DETAILS
12 X 12 I 53 STOCK NO	3		4	1647R	18'-1 5/8*	950	1648R	17'-7 3/8"	935	1649R	17'-1 3/8*	905	1650R	16'-7 1/4"	880	1651R	16'-1 1/4"	855		
3164.10	4	60	4	1647L	18'-1 3/8"	960	1648L	17'-7 3/8"	935	1649L	17'-1 3/8"	905	1650L	16'-7 1/4"	880	1651L	16'-1 1/4"	855		
	5	1	2	1657R	17'-3 1/2"	915	1658R	15'-9 1/2"	890	1659R	16'-3 1/2"	865	1650R	15'-9 3/8"	835	1661R	15'-3 3/8"	810		
	6		2	1657L	17'-3 1/2"	915	1658L	16'-9 1/2"	890	1659L	16'-3 1/2"	865	1650L	15'-9 3/8"	835	1661L	15'-3 3/8"	810	_	
	7		2_	1623	29'-0 1/4"	1220	1624	28'-10 3/4"	1215	1625	281-9 1/41	1210	1626	28'-7 3/4"	1205	1627	28'-6 1/4"	1200		
TRANSVERSE STRUTS 10 I 42	-8	61	2	1608	33'-6 1/4"	1410	1609	35'-3 1/4"	1400	1610	33'-0 1/4"	1385	1611	32'-9 1/4"	1375	1612	32'-6 1/4"	1365		
STOCK NO	9		2	1595	J8'-0 1/4°	1595	1596	37'-7 3/4"	1580	1598	37'-3 1/4"	1565	1599	36'-10 3/4"	1550	1601	36'-5 1/4"	1535		
	10		2	1586	42'-6 1/4"	1785	1587	42'-0 1/4"	1765	1588	41'-6 1/4"	1745	1589	41'-0 1/4*	1720	1590	40'-6 1/4"	1700		
•	11		8	887	22'-0"	33	887	22'-0"	33	888	21'-6"	32	889	21'-0*	32	889	21'-0*	32_		
TRANSVERSE ROOS	12	62 ,	8	879	26'-0*	39	880	25'-6*	38	881	25'-0"	38	882	241-6"	37	882	24'-6"	57		
3/4 \$ ROO STOOK NO 46-6375.5-07	13		8	871	30'-0*	45	872	29'-6"	44	373	29'-0"	44	874	281-6"	43	875	28'-0"	42		
	14		8_	863	34'-0"	51	864	33'-6"	50	866	32'-6"	49	867	32'-0"	48	868	31'-6"	47		
LONGITUDINAL ROOS 3/4 # ROD	15	62	24	883	241-0=	36	884	25'-6"	35	884	23'-6*	35	885	23'-0"	35	885	23'-0*	55	4	
STOCK NO 46-6375.5-07	_16		8	883	24'-0"	36	884	23"-6"	35	684	23'-6*	35	885	25'-0"	35	885	23'-0"	35	4	
HORIZONTAL ROOS	17		2	1000	35'-6"	55	1001	35'-0"	53	1001	35'-0"	53	1001	35'-0"	53	1001	351-0*	55		
3/4 # ROD	18	62	2	995	38'-6"	58	995	38'-6"	58	996	38'-0"	57	996	38'-0"	57	996	38'-0"	57		
STOCK NO 46-6375.5-07	19		2	990	42'-0°	63	991	41'-6"	62	991	41'-6"	62	992	41'-0"	62	992	41'-0*	62	MARK REQUISITIONED UNIT WEIGHT MARK LENGTH WEIGHT M	REQUISITIONED UNIT
-																			MARK REQUISITIONED WEIGHT MARK LENGTH WEIGHT M	ARK LENGTH WEIGHT MARI

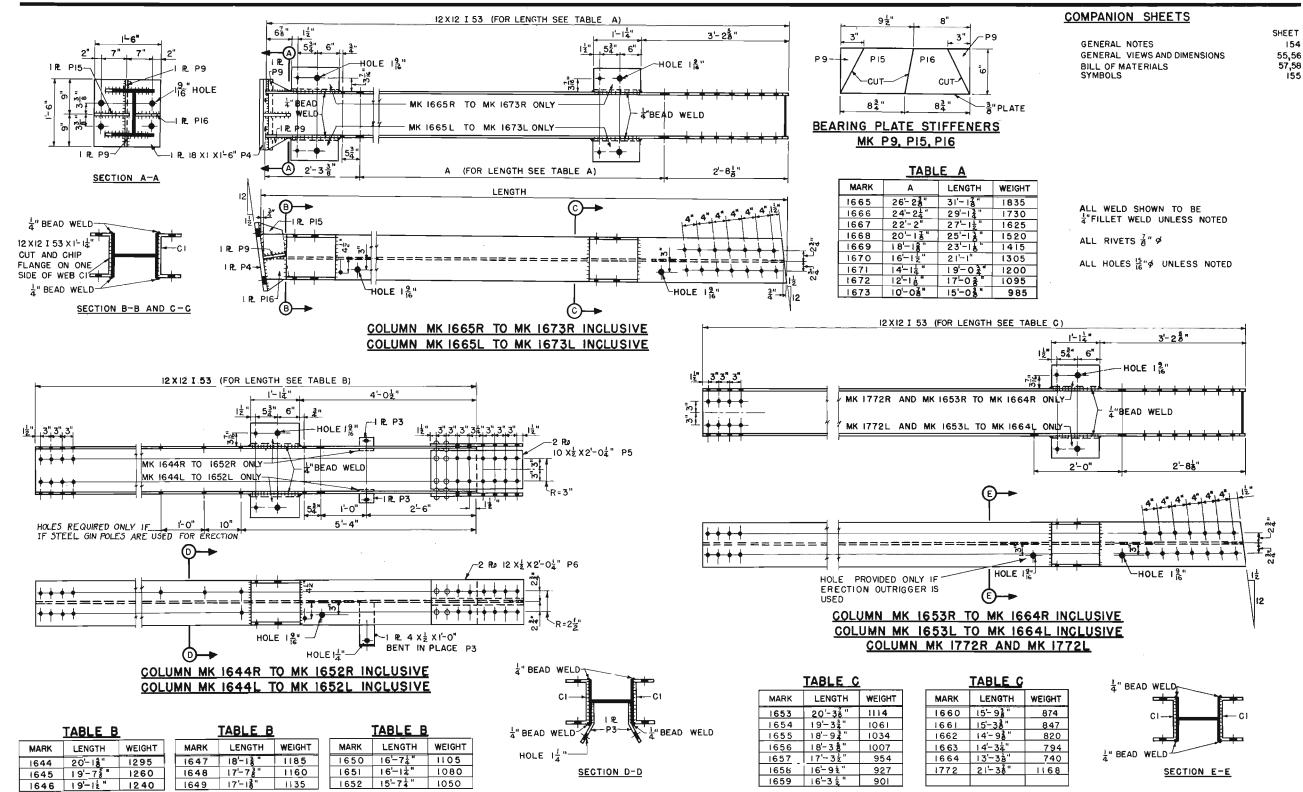
				720	1 42 0			1 41 0			1 12 0								MARK	LENGTH	WEIGHT (PCUNDS	MARK	LENGTH	WEIGHT (POUNDS	MARK	LENGTH	WEIGHT (POUNDS)	MARK	LENGTH	WEIGHT
		TOHER	HEIGHT		67'			651			63'			61'			591			£7'			55'			531			51'	
	20	61	2	1633R	27'-11 3/8"	1480	1635R	25'-11 1/4"	1380	1636R	24'-11 1/8"	1320	1637R	23'-11"	1270	1637R	23'-11"	1270	1639R	22"-11"	1215	1639R	22'-11"	1215	1641R	21'-10 3/8"	11.60	1642R	20'-10 3/4"	me
TOHER COLUMNS	21_		2	1633L	27'-11 3/8"	1480	1635L	25'-11 1/4"	1,580	1636L	24'-11 1/8"	1320	1637L	23'-11"	1270	1637L	25'-11"	1270	16381	22'-11"	1215	_1639L	22'-11"	1215	16411	21'-10 3/8"	1160	1642L	20'-10 3/4"	1110
12 X 12 I 53 STOCK NO	.22		2	1644R	201-1 5/8"	1070	1644R	20'-1 5/8"	1070	1645R	19'-7 5/8*	1040	1646R	19'-1 1/2"	1015	1647R	18'-1 3/8"	960	7.64 8 R	17'-7 1/8"	\$35	1650R	16'-7 1/4"	880	1651R	16'-1 1/4"_	855	1652R	15'-7 1/4"	830
SIOCK NO	23	60	2	1644L	20'-1 5/8"	1070	1644L	20'-1 5/8"	1070	1645L	19'-7 5/8"	1040	1646L	19'-1 1/2"	1015	1647L	18'-1 3/8"	960	16481	. 17!-7 3/8*	935	1650L	16'-7 1/4"	680	1651	16'-1 1/4"	855	1652L	15'-7 1/4"	830
	24		2	1654R	19'-3 3/4"	1025	1654R	19'-3 3/4"	1025	1655R	18'-9 5/4"	1000	1656R	18'-3 5/8"	970	1657R	17'-3 1/2"	915	1658R	16'-9 1/2"	890	1660R	15'-9 3/8"	835	1661R	15'-3 3/8"	810	1662R	14'-9 3/8"	785
	25		2	1654L	19'-3 3/4"	1025	1654L	19'-3 3/4"	1025	1655L	18'~9 3/4"	1900	1656L	18'-3 5/8*	970	1657L	17'-5 1/2"	915	1658L	16'-9 1/2"	890	1660L	15'-9 5/8"	835	16611	15'-3 3/8"	810	1662L	14'-9 3/8*	785
TRANSVERSE STRUTS	26		2	1618	29'-6 1/4"	1240	1618	29'-6 1/4"	1240	1621	291-4 3/4*	1235	1622	29'-3 1/4'	1230	1623	29'-0 1/4"	1220	1624	28'-10 3/4"	1215	1626	28'-7_3/4"	1205	1627	28'-6 1/4"	1200	1629	28'-4 5/4"	1195
10 I 42 STOOK NO	27	61	2	1605	34'-6 1/4"	1450	1605	34'-6 1/4"	1450	1606	34'-3 1/4"	1440	1607	34'-0 1/4"	1430	1608	33'-6 1/4"	1410	1609	33'-3 1/4"	1400	1611	32'-5 1/4"	1375	1612	32'-6 1/4"	1370	1613	32'-3 1/4"	1360
	28		2	1591	40'-0 1/4"	1680	1592	391-6 1/4*	1660	1593	391-0 1/4*	1640	1594	58'-6 1/4"	1620	1595	36'-0 1/4"	1600	1597	37'-6 1/4"	1580	1600	37'-0 1/4"	1555	1601	36'-6 1/4"	1535	1602	36'-0 1/4"	1515
Transverse roos 3/4 Ø roo	29		8	884	23'-6"	35		23'-6"	35	885	23'-0	35	885	23'-0*	35		22'-0"	33	887	221-0*	دد	889	21'-0"	32	889	21'-0"	32	890	20'-6"	- 31
STOCK NO 46-6375.5-07	30	62	8	876	27'-6"	41	876	27'-6*	41	877	27'-0"	41	878_	26'-6"	40	879	26'-0"	29	880	25'-6"	38	882	24'-6"	57	882	24'-6"	37	.883	24'-0"	36
	31		8	865	35'-0"	50	887	32'-0"	48	869	51'-0°	47	870	<i>5</i> 0′ −6°	46	871	30'-0°	45	د87	291-04	44	874	28'-6"	43	875	28'-0"	42	877	27'-0"	41
Longitudinal Roos 3/4 # Rod	52	62	16	881	251-01	38	581	25'-0"	38	881	25'-0"	38	882	24'-6*	37	883	241-0*	36	884	25'-6"	35	885	23'-0"	35	885	25'-0"	35	886	22'-6"	34
STOCK NO 46-6375.5-07	33		8	879	26'-0"	39	881	25'-0"	38	882	24'-6"	37	883	24'-0"	36	883	24'-0"	36	884	25'-6"	35	884	25'-6"	35	885	23'-0"	35	886	22'-6"	34
HORIZONTAL RODS 3/4 B ROD STOCK NO 46-6375.5-07	34	62	2	1000	35'-6"	53	1000	35'-6"	53	1000	35'-6"	53	1000	35'-6*	53	1000	35'-6"	53	7007	35'-0"	53	1001	35'-0"	53	1001	351-0"	53	1001	55'-0"	53
STOCK NO 46-6375.5-07	35		2	993	391-6*	59	993	39'-6"	59	994	39'-0"	59	994	39'-0"	59	995	38'-6"	58	995	38'-6"	58	996	58°-0 -	57	995	38'-0"	57	997	37'-6"	56

		TOHER	HEIGHT		49'	•		47'			45'			43'			41'			391			37'			35'			33'	
	36	61	2	1633R	27'-11 3/8*	1480	1634R	26'-11 3/8"	1430	1635R	25'-11 1/4"	1375	1636R	24'-11 1/8"	1320	1637R	23'-11"	1270	1639R	22'-11"	1215	16418	21'-10 7/8"	1160	1642R	20'-10 3/4"	1110	1643R	19'-10 5/8'	1065
TOHER COLLIMNS	.37		2	1633L	27'-11 3/8"	1480	1634L	26'-11 3/8"			25'-11 1/4"	1375	1636L	24'-11 1/8"	1320	1637L	23'-11"	1270	1639L	22'-11"	1215	1641L	21'-10 7/8*	1160	1642L	201-10 3/4"	1110	1643L	19'-10 5/8"	1065
12 X 12 I 53 STOCK NO	38	60	2	1772R	21'-3 7/8"	1130	1653R	20'-3 7/8"	1080	1654R	19'-3 5/4"	1025	1656R	18'-3 5/8"	970	1657R	17'-3 1/2"	940	1659R	16'-3 1/2*	865	1661R	15'-3 3/8"	810	1663R	141-3 1/4"	755	1664R	15!-3 1/8*	ر70
	59		2	1772L	21'-3 7/8"	1130	1653L	201-3 7/8*	1080	1654L	19'-3 3/4"	1025	1656L	18'-3_5/8"	970	1657L	17'-3 1/2"	940	1659L	16'-3 1/2"	865	1661L	15'-3 3/8"	810	1663L	14'-3 1/4"	755	166#L	13'-5 1/8"	ر705
TRANSVERSE STRUTS 10 I 42	\$	61	2	1619	30'-0 1/4"	1260	1620	29'-9 1/4"	1250	1618	29'-6 1/4*	1240	1622	29'-3 1/4"	1220	1623	29'-0 1/4"	1220	1625	28'-9 1/4"	1210	1627	28'-6 1/4"	1200	L630	28'-3 1/4"	1150	1631	28*-0 1/4*	1180
STOOK NO	41		2	1603	35'-6 1/4"	1490	1604	35'-0 1/4"	1470	1605	34'-6 1/4"	1450	1607	341-0 1/4*	1430	1608	33'-6 1/4"	1410	1610	35'-0 1/4"	1390	1612	32'-6 1/4"	1370	1614	32'-0 1/4"	1345	1615	31'-6 1/4"	1325
TRANSVERSE RODS 3/4 Ø ROO	42	62	8_	881	25'-0"	38	883	24'~0"	36	884	23'-6"	35	885	23'-0"	35	887	221-0"	33	888	21'-6"	32	889	21'-0"	32	891	20'-0"	30	892	19'-6"	29
STOCK NO 46-6375.5-07	43		8	872	29'~6"	44	874	28'-6"	43	876	27'-6"	41	878	26'-6"	40	879	26'-0"	39	881	25'-0"	38	882	24'-6"	37	884	23'-6"	35	886	22'-6"	34
LONGITUDINAL ROOS 3/4 gl ROO	44	62	8	879	26'-0"	39	880	25'-6"	38	881	25'-0"	38	882	24'-6"	37	883	24'-0"	_36	864	23'-6"	35	885	23'-0"	35	886	22'-6"	54	887	22'-0"	33
STOOK NO 46-6375, 5-07	45		8	879	261-0*	39	880	25'-6"	38	881	25'-0"	38	882	241-6"		883	24'~0*	36	884	23'-6"	35	885	23'-0"	35	886	22'-6"	34	887	22'-0"	33
HORIZONTAL RODS 3/4 Ø ROD																														
STOCK NO 46-6375, 5-07	46	62	2	999	36'−0*	54	999	36'-0"	54	1000	35'-6"	53	1000	35'-6"	53	1000	35'-6"	53	1001	35'-0"	53	1001	35'-0"	53	1001	35'-0"	53	1002	34'-6"	52

		TOHER	HEIGHT		31'			291			27'			25'		1	25†			21'			19'			17'			15'	
FOMER COLUMNS 12 X 12 I 53 STOCK NO	47	60	2	1665R	31'-1 7/8"	1650	1666R	29'-1 5/4"	1490	1667R	27'-1 1/2"	1440	1668R	25'-1 3/8"	1350	1669R	23'-1 1/8"	1225	1670R	21'-1"	1120	1671h	19'-0 3/4"	1010	1672R	17'-0 5/8"	905	1673R	15'-0 3/8"	800
- STOCK NO	48		2	1665L	31'-1 7/8*	1650	1666L	291-1 3/4"	1490	1667L	27'-1 1/2"	1440	1668L	25'-1 3/8"	1330	1669L	23'-1 1/8"	1225	1670L	21'-1"	1120	1671L	19'-0 3/4"	1010	1672L	17'-0 5/8"	905	1673L	15'-0 3/8"	809
TRANSVERSE STRUTS 12 I #2 STOCK NO	49	61	2	1616	31'-0 1/4"	1300	1617	30'-6 1/4"	1280	1619	30'-0 1/4"	1260	1618	29'-6 1/4"	1240	1623	29'-0 1/4"	1220	1627	28'-6 1/4"	1200	1631	28'-0 1/4"	1180	1628	27'-6 1/4"	1160	1632	27'-0 1/4"	113
TRANSVERSE ROOS 3/4 # ROO STOCK NO 46-6375.5-07	50	62	8	875	28"-0"	42	878	26'-6"	40	881	25'-0"	38	684	231-6"	35	887	22'-0"	33	889	.21'~0"	32	892	19'-6"	29	693	18'~6"	-26	895	17'-6"	
LONG I TUD INAL HOOS 3/4 Ø ROO STOCK NO 46-6375, 5-07	51	62	8	873	29'-0"	44	876	27'-6"	41	879	26'-0"	39	881	251-0*	38	883	24-0"	36	885	23'-0"	35	887	22'~0*	53	889	21'-0"	32	890	.20'-6"	







IR PI6-

-IRLP3

2 R5 10 X 2 X 2 - 0 2 P15

BEAD WELD

-C1

HOLES 18"

SHEET GENERAL NOTES SYMBOLS 154 155 55, 56 57, 58 GENERAL VIEWS AND DIMENSIONS BILL OF MATERIALS

-IR PI6

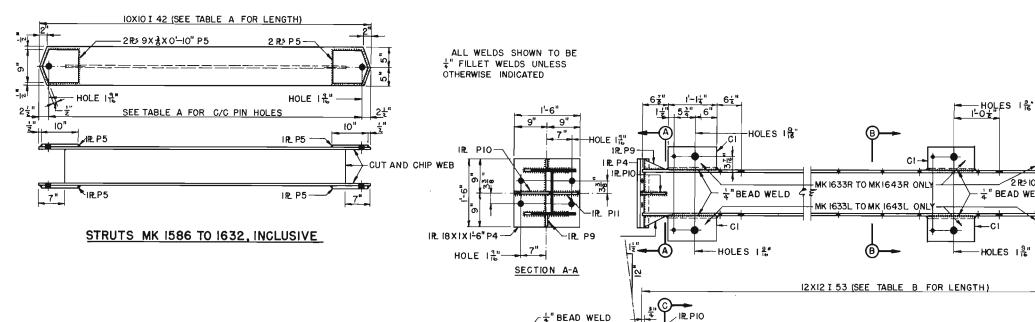


TABLE A

MARK	C/C PIN HOLE	LENGTH	WEIGHT
1586	42'- I±"	42'- 6\dag{*}"	1795
1587	41 - 74"	42'- 0급"	1775
1588	41 - 14"	41-64	1755
1589	40- 7-	41'- 0="	1734
1590	40년 15	4년-6분	1713
1591	39- 74"	40'- 0남"	1692
1592	39 🖑 _	39'- 6눝"	1671
1593	30 - 74	39'− 0≟"	1650
1594	38'- 1날"	38'∽ 6‡"	1639
1595	37 ∸ 7≩"	38'- 0₽"	1608
1596	37'- 2*"	37'- 7 % "	1592
1597	37ー は"	37'- 6‡"	1587
1598	36'-10╬"	37'− 3₺"	1576
1599	36 - 53"	36′−10∄"	1561
1600	36'- 7 '	37'- 04"	1566
1601	36년 급박	36' 64"	1545
1602	35'- 7\frac{1}{4"}	36'- 0분"	1524
1603	35' - 1날"	35'- 6 \ "	1503
1604	34'7±"	35'- O±"	1482
1605	34'- (1±"	34년 6분"	1461
1606	33-104"	34'- 34"	1445
1607	33'- 7;"	34└ 0₺"	1441
1608	33년 1출	33'- 64"	14 19
1609	32'-104"	33'- 3₺"	1408

TABLE A

			
MARK	C/C PIN HOLE	LENGTH	WEIGHT
1610	32-74"	33-04"	1398
1611	32'- 4 4"	32'- 9\["	1387
1612	32 - 1 + "	32- 6-	1377
1613	31 −10‡"	32-3+	1366
1614	31 – 7ਵਾ	32'- 0 \ "	1355
1615	31- 14"	31 - 6 -	1335
1616	30- 7 4 "	31 - 0 - "	1314
1617	30'- 1±" 29'- 1±"	30- 6-	1293
1618	29'- ⊹"	29 - 6 ₺"	1251
1619	29'- 7 \ "	30'- 0t" 29'- 9t"	1272
1620	29'- 44"	2 9'- 9 \ #"	1261
1621	28'-113"	29 느 4골"	1246
1622	28-104"	29'- 3\\\	1240
1623	28'- 78"	29'- 0#"	1230
1624	28'- 52"	28-103"	1225
1625	28'- 4+"	28-94"	1219
1626	28- 23"	28'- 7≹"	1214
1627	28'- 1+"	28'- 6 ' ''	1209
1628		27-64	1167
1629	27년11鏊"	28 – 4 1 "	1204
1630	27-10-	28 - 3½"	1198
1631	27- 7#	28'- 0;"	1189
16 32	26'- 71"	27'- 04"	1146
		*	

#BEAD WELD -[HOLE 1호리 _ IR 4X 2 XI-0" P3 BEND IN PLACE SECTION B-B 12 X12 X1-14" 53 I CI CUT AND CHIP FLANGES ON ONE SIDE 4" BEAD WELD

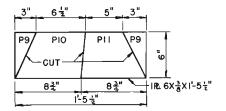
SECTION C-C

BEAD WELD

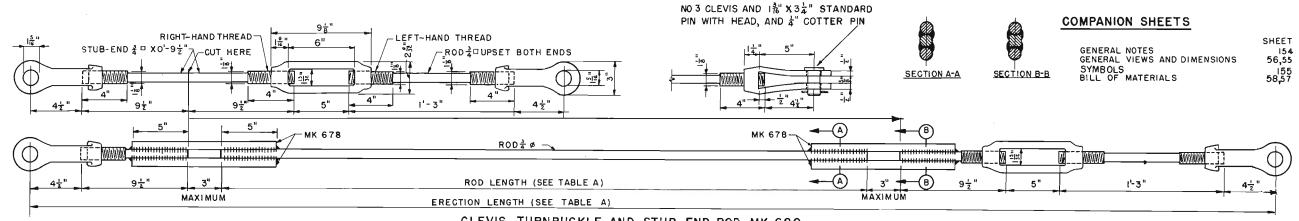
C				<u> </u>	/cl 3 "
Ĭ	IRLPIO			3",3"3",	/3" 3" 3" ½"
ţ	2№ P9CI	*			· · · · · · · · · · · · · · · · · · ·
1		~		• • •	2
dillia hann	15 ES	(No. 1)	4 35 mm		
ł	IR PII 4 53" SEE NOTE ON	SHEET 60 I'O" IO"	1'-44" 53" IR P3-	2 PLS 12 X ½ X 2'-0	4"PI6 R=2½"
c	2'-38" HOLES I	HOL A (SEE TABLE B)	LES 110"	2'-6"	
	ÇOLU	MNS MK 1633R TO	1643R INCLUSIVE	'	

COLUMNS MK 1633L TO 1643L INCLUSIVE

TABLE B MARK LENGTH WEIGHT 22¹ 2 " 27¹ 11³ 1850 21¹ 2 " 26¹ 11³ 1795 1633 1634 20-17 25-11- 1740 1635 24-115* 23-11 " 1636 19느 1출* 1690 18- 1동 1635 1637 17-78 23-5" 1638 1610 17'- 18" 22-11" 1639 1640 1641 1642 [643



BEARING PLATE STIFFENERS P9, PIO, PII,



CLEVIS, TURNBUCKLE, AND STUB-END ROD MK 680

TABLE A

ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK			ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH			ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH
912	46'-25"	990	42'-0"	917	43'- 64"	993	39'- 6"	922	42' - 42"	996	38'-0"	930	40'-03"	999	36'-0"	935	39'- 5 ½"	1001	35'- 0"	940	39'- 03"	1001	35'- O"
9 1 3	45'-118"	991	41'-6"	918	43' - 4"	994	39'-0"	923	42'- 25"	996	38'-0"	931	39'- 10종"	1000	35 - 6 "	936	39'-4 🕏 "	1001	35'- 0"	942	38'-107	1002	34 6"
914	45'- 7 ⁵ "	991	41'-6"	919	43'-14"	994	39'-0"	924	42'-02"	996	38'-0"	932	39' - 9 훑"	1000	35'-6"	937	39'-3를"	10 01	35'-0"				
9 5	45' - 4 g*	992	41'-0"	920	42' - 9 1	995	38'-6"	925	41-104"	997	37' - 6"	933	39'-8 5 "	1000	35'- 6"	938	39'-23"	1001	35'-0"				
9 6	45'-05"	992	41'- 0"	921	42'-78"	995	38' - 6"	929	40'-2 3"	999	36'-0"	934	39'-62"	1000	35'-6"	939	39' - 13"	1001	35'-0"				

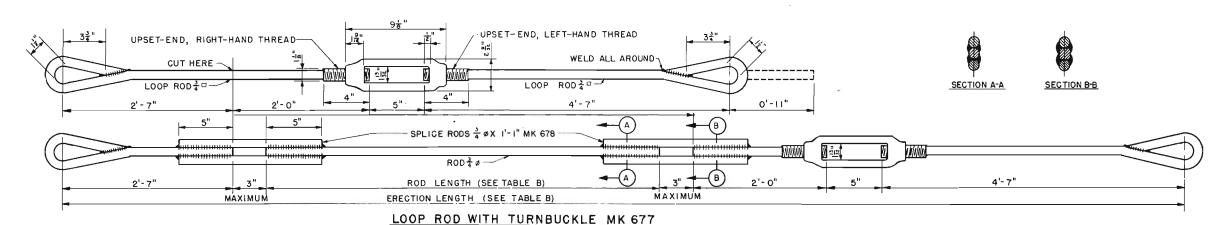
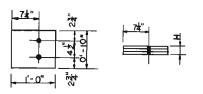
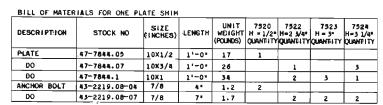


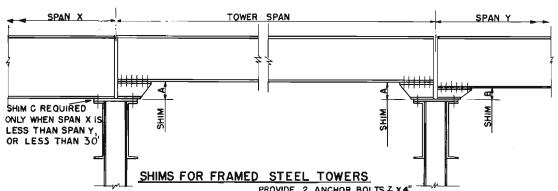
TABLE B

					_																		
ERECTION	ERECTION	ROD	ROD	ERECTION	ERECTION	ROD	ROD	ERECTION	ERECTION	ROD	ROD	ERECTION	ERECTION		ROD	ERECTION	ERECTION	ROD	ROD	ERECTION	ERECTION	ROD	ROD
MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH	MARK	LENGTH
700	43'- 84"	863	34'- 0"	713	39'- 12"	872	29'-6"	731	36'-11"	877	27'-0"	747	34' - 5 2 "	882	24'- 6"	773	32'-7 \	885	23'- 0"	797	30'-3 5 "	890	20'-6"
701	43'- 12"	864	33'- 6"	714	38'-10 3 "	873	29'-0"	7 3 2	36' - 6 5 "	878	26'-6"	748	34'- 3½"	882	24'-6"	774	32'-64"	886	22'-6"	798	30'- 2늉"	890	20'-6"
702	42'-11"	865	33'- 0"	717	38'- 8"	873	29'-0"	734	36'- 2 3 "	878	26'-6"	751	34'- 1ਵਾਂ "	882	24'-6"	776	32 - 5 2"	886	22'-6"	801	30'-0"	891	20'-0"
7 0 3	42' - 64"	866	32' - 6"	719	38 5 1	874	28'- 6"	7 3 6	36' - 0 ^출 "	879	26'- 0"	753	33'-118"	883	24'-0"	78 I	32' - 2흏"	886	22'-6"	806	29'- 4중"	. 8 9 2	19'-6"
7 0 4	41'-118"	867	32'-0"	720	38'-3 8 "	874	28'- 6"	737	35'- 8 \$ "	879	26'-0"	758	33'- 82"	883	24'-0"	783	31'-11"	887	22'-0"	815	28'- 3출"	893	18'-6"
705	41' - 8½"	867	32'-0"	721	38'-2"	874	2 8' - 6"	739	35'-5 1 "	880	2 5' - 6"	759	33'- 8출"	883	24'-0"	785	31'-9"	887	22' - 0"	820	27'-3"	895	17'-6"
7 0 6	41'- 3 7 "	868	31'-6"	724	$37' - 8\frac{7}{8}"$	8 7 5	2 8' - 0"	741	35'- 3 3 "	880	25'-6"	762	3 3' - 5 5 "	884	23'-6"	786	31'-7"	887	22'-0"				
707	40'-107"	869	31'- 0"	725	37'-8"	875	28'-0"	742	34'-10 3 "	881	25'-0"	764	3 3' - 3출"	884	23'-6"	790	31'-3#;"	888	21'-6"				
708	40'- 1출"	870	30'- 6"	727	37'- 44"	876	27'-6"	743	34'-10층"	881	2 5' - 0"	766	33' - 2½"	884	23'-6"	792	30'-114"	889	21'-0"				
7 0	39'-8#"	871	30'-0"	728	37' - 4 "	876	27' - 6"	744	34'- 8 5 "	188	2 5'- 0"	769	32'-114"	885	23'- 0"	79 3	30'11"	889	21'-0"				
712	39'-2"	872	29'-6"	730	36'-11 3 "	877	27'-0"	746	34'- 62"	881	25'-0"	772	32'-8 3 "	885	23'-0"	794	30'-7 ह े"	889	21' - 0"				

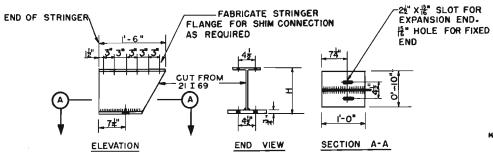


DETAIL OF PLATE SHIM





	SH	IMS	FOR FRAI	MED STEE	L TOMER	DE			HEN SH		RE NOT
Si	PAN		80,	80'	70'	60'	50'	401	30'	20'	15'
	:	A	7534	7536	7534	7531	7531	7523	-		
	7	В	7541	7542	7541	7538	7538	7530	7526	7526	7526
ı	\perp	С								7523	7526
1	_l	A	7534	7536	7534	7531	7531	7523			
1	20	В	7538	7539	7538	7535	7534	7526	7523	7523	7523
	\Box	С								7523	7526
	- [A	7534	7536	7554	7531	7531	7523			
	2	В	7534	7536	7534	7551	7531	7523			
L		С								7523	7526
		A	7534	7536	7534	7531	7531	7523	7523	7523	7523
	\$	В	7530	7532	7530	7526	7526				
		С							7523	7526	7530
	-	A	7554	7536	7534	7531	7531	7531	7531	7531	7531
-	50	В	7522	7524	7522						
27.0		С						7526	7551	7534	7538
<u>ا</u> "		Α	7534	7536	7534	7531	7531	7531	7531	7531	7531
	8	В	7522	7524	7522						
		С					Τ -	7528	7531	7535	7538
1	-	A	7534	7536	7534	7934	7534	7534	7534	7534	7534
	5	В		7520							
	[С				7522	7522	7530	7534	7538	7541
		Α	7536	7536	7536	7536	7536	7536	7556	7536	7536
	8	В									
		С	7520		7520	7524	7524	7532	7536	7539	7542
ſ	_	A.	7534	7536	7534	7534	7534	7534	7534	7534	7534
	8	В		7520							
		С				7522	7522	7530	7534	7538	7541



DETAIL OF BUILT-UP SHIM

BILL OF MATER	HALS FOR ONE BU	ILT-UP S	нін	
DESCRIPTION	STOCK NO	SIZE (INCHES)	LENGTH	QUANTITY
BEAM	48-2900.21-059	21 I 59	16*	1
PLATE	47-7844.07	10X3/4	1'-0"	1
RIVET	43-6353.08	7/8	2 3/4"	12
ANCHOR BOLT	43-2219.08-04	7/8	4"	2
E·LECTRODE	46-3772.2-7	3/16		1 ·LB

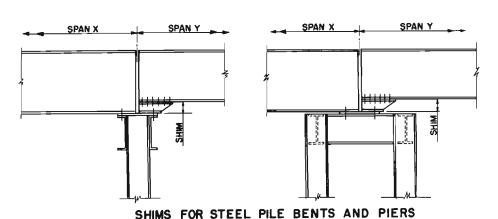
COMPANION SHEETS SHEET GENERAL NOTES 154 SYMBOLS 155 STEEL PILE BENTS AND PIERS, RIVETED 76,77 STEEL PILE BENTS AND PIERS, WELDED FRAMED STEEL TOWERS 79,80 55,56

> TOTAL WEIGHT (POUNDS) MARK 7526 6 1/8" 57 7530 8 7/8*-62 7531 9 1/8" 62 7532 9 1/2 63 7534 12 66 7535 12 1/4" 67 12 1/2" 67 7556

15 1/8"- 71 7539 15 1/2" 72 7541 18" 76 7542 18 1/2" 77

7538

MARKS AND DIMENSIONS FOR BUFLT-UP SHIMS

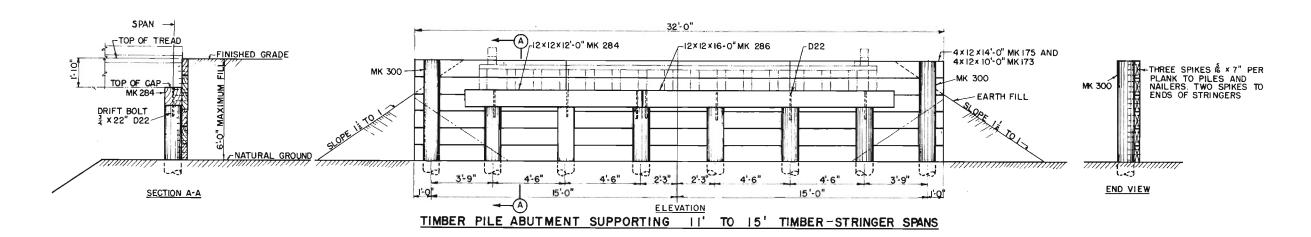


BILL OF MATERIALS	FOR ANCHOR BOL	LS ORTA MI.	THOUT BHI	MB
IMESCRIPTION	STOCK NO	SIZE (INCHAS)	LIMOTH	WHIGHT ECH (POWIOT)
ANCHOR BOLT	43-2219.08-04	7/8	Os-Thu	1.2

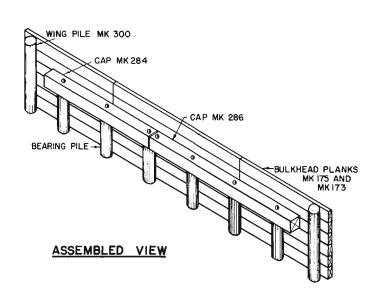
TWO BOLTS REQUIRED FOR MACH STRINGER SUPPORT CONSTRUCTION INDICATED BY BLANK SPACES IN TARLES FOR SHINS

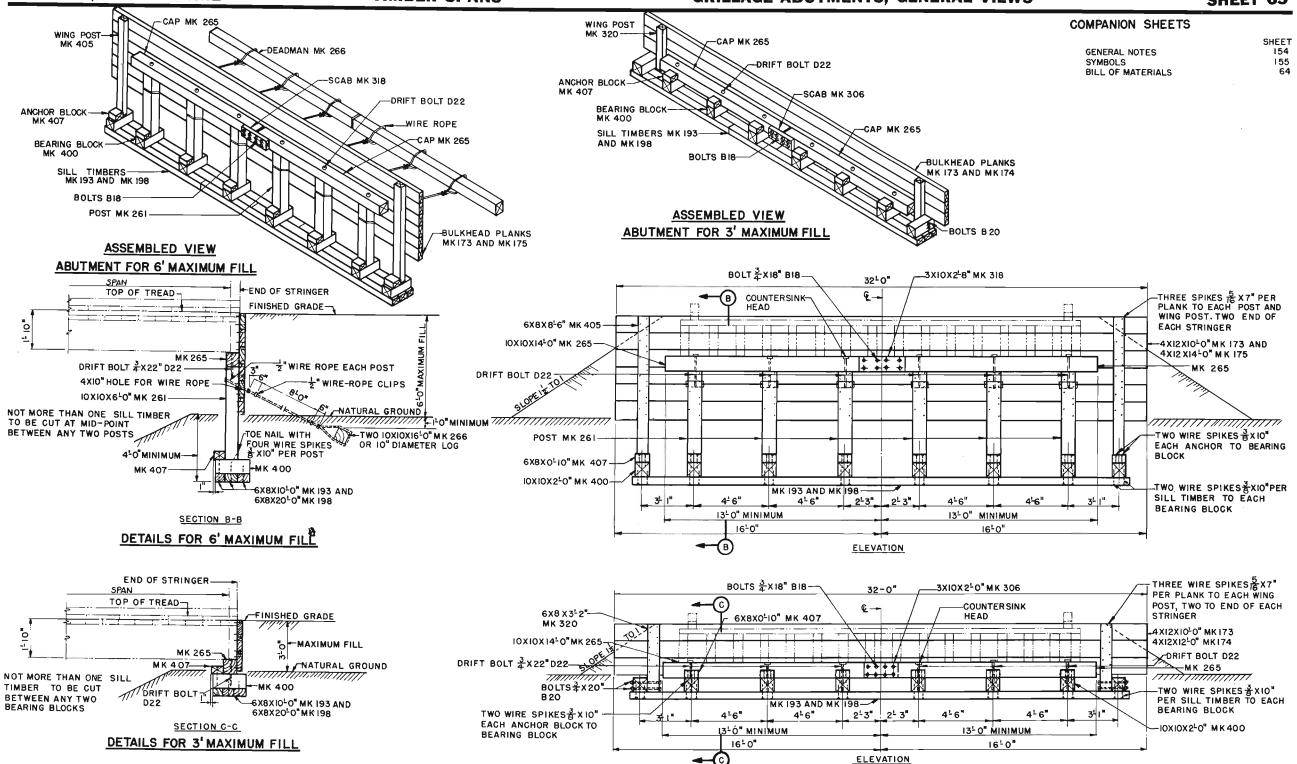
s	PAN X	90'	80'	701	60'	50'	401	30'	20'	15'
	15'	7541	7542	7541	7538	7538	7530	7526	7523	
ſ	20'	7538	7539	7538	7535	7534	7526	7523		7523
	30'	7534	7556	7534	7531	7531	7523		7523	7526
-[40'	7530	7532	7530	7526	7526		7523	7526	7530
SPAN	50'	7522	7524	7522			7526	7531	7534	7538
S	60'	7522	7524	7522			7526	7531	7535	7538
Ì	70'		7520		7522	7522	7530	7534	7538	7541
ı	60'	7520		7520	7524	7524	7532	7536	7539	7542
ı	90'		7520		7522	7522	7530	7534	7538	7541

GENERAL NOTES SYMBOLS TIMBER ABUTMENTS



	וז	PE OF ABUTMENT					TIMBER ABUTM		τ	IMBER GR	ILLAGE ABUTHE	NT	
		FILL HEIGHT				_	6' MAX	MUM	6' MAX	IMUM	3 MAX	IMUM,	
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	F8M	QUANTITY	FBM	QUANTITY	FBM	LINE
1	3 BULKHEAD PLANK	39-3340-12-14	175	4 X 12	14'-0"	210	6	336	6	336			1
2	٥٥ لا	39-3340.12-12	174	4 X 12	12'-0"	180					3	144	2
3	.≱ po	39-3340.12	173	4 X 12	10'-0"	150	12	480	12	480	6	240	3
4	PILE (WING)		300		15'-0"		2						4
5	2 PILE (BEARING)				2		6						5
6	→ POST (WING)	39-3360.08	405	6 X 8	8'~6"	128			2	68			6
7	1 DO	39-3360.08	320	6 X B	3'-2"	47					2	25	7
6	1 POST (BEARING)	39-6620.1	261	10 X 10	6'-0"	188			6	300			8
9	CAP	39-6630.12-16	286	12 X 12	16'-0"	720	1	192					9
10	DO	39-6630.12-12	284	12 X 12	12'-0"	540	1	144			1 1		10
11	DO	39-6620.1-14	265	10 X 10	14'-0"	437			2	255	2	233	11
12	SCAB	39-3330-1	318	5 X 10	2'-8"	25			2	13			12
15	DO	39-3330.1	506	3 × 10	2'-0"	19					2	10	13
14	SILL TIMBER	39~3360.08	195	6 X 8	10'-0*	150			3	120	5	120	14
15	DO	39-3360.08-2	198	6 X B	20'-0"	300			3	240	3	240	15
16	BEARING BLOCK	39-6620.1	400	10 × 10	2'-0"	63			8	133	8	133	16
17	DEADHAN	39-6620.1-16	266	10 × 10	16'-0"	500			2	267			17
18	ANCHOR BLOCK	39-3360.08	407	6 X 8	0'-10"	15			8	26	6	20	18
	STEEL HARDWARE, BLACK												
19	WIRE ROPE	22-4567.4-05		1/2	20'-0"	13			8				19
20	WIRE-ROPE CLIP	42-3544.5-05		1/2		0.72			32	_			20
21	MACHINE BOLT WITH NUT AND WASHER	43-2325.07-2	B20	3/4	20"	3.06					4		21
22	DO	43-2525-07-183	818	3/4	16*	2.82			8		8		22
23	DRIFT BOLT	45-1656.07-22	D22	3/4	22*	2.76	7		6		6		23
24	STANDARD WIRE SPIKE	42-8488.04-1		3/8	10*	0.33			96		60		24
25	00	42-8488.035-07		5/16	7*	0.143	196		196		76		25
<u>1</u> j	CUT TO FIT FOR FILLS U	NDER 6-FOOT.											
2)	BEARING PILE LENGTHS I	O BE DETERMINED B	Y FIELD	CONDITIONS.									





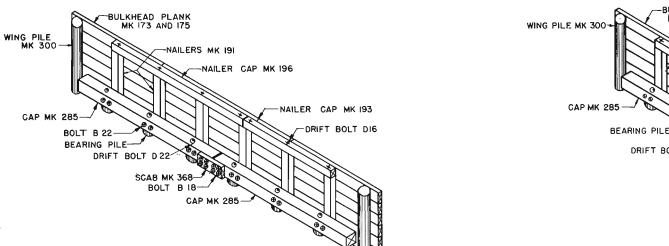
ASSEMBLED VIEW

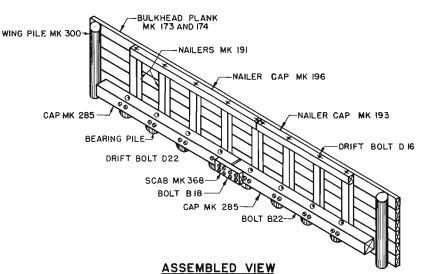
ABUTMENT FOR 15' TO 50' SPAN

SHEET

154 155

67,68





ABUTMENT FOR 60' TO 90' SPAN

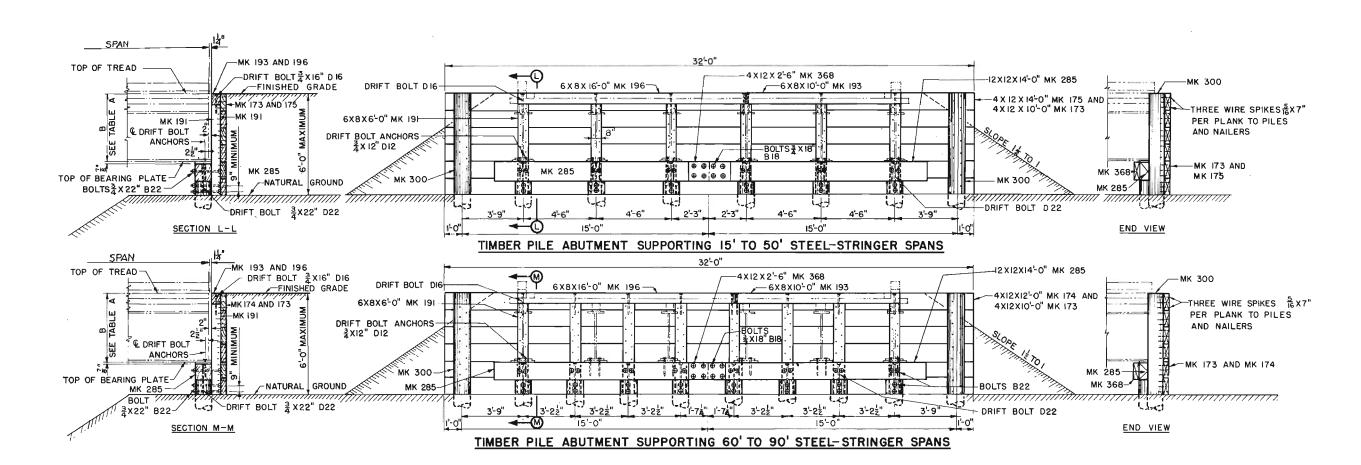
TA	BLE A
SPAN	DIMENSION B
15 '	2'-4 8 "
20 '	2'-67"
30 '	3'-0 7 "
40 '	3' - । ਫ਼ ਿ"
50 '	3'.~ 6 7 "
60 '	3'- 10"
70 '	3'-10∦"
80 '	4'-0 7 "
90 '	4'- 1 8 "

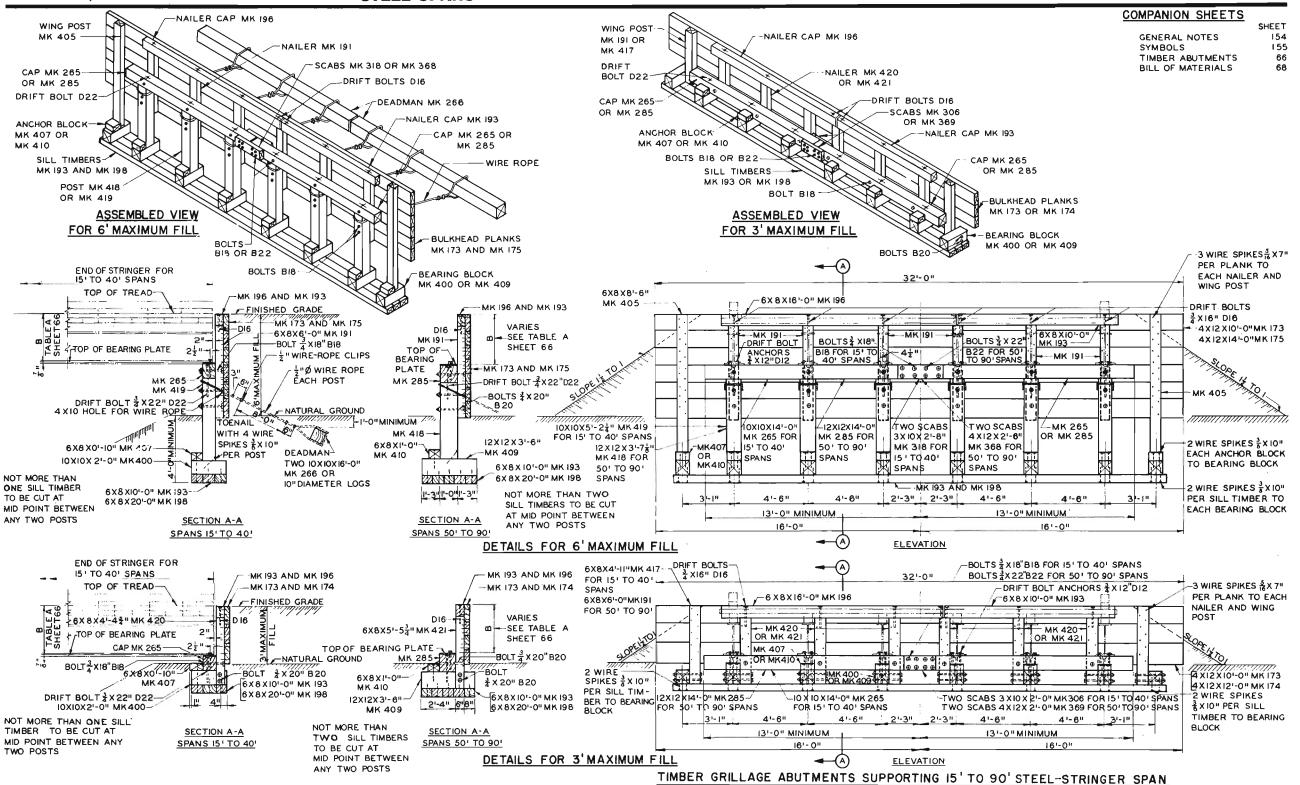
COMPANION SHEETS

TIMBER ABUTMENTS

GENERAL NOTES

SYMBOLS





HIGHWAY CLASS 50, DOUBLE-LANE

COMPANION SHEETS

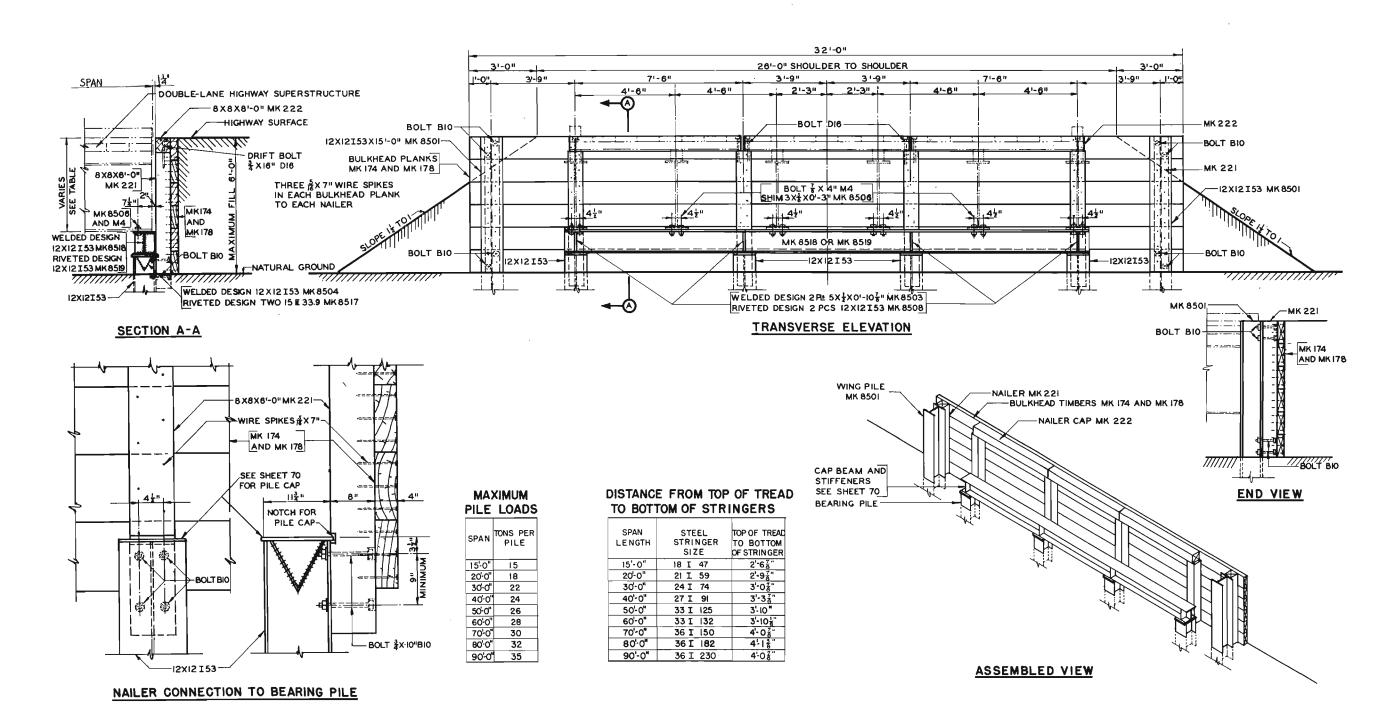
SHEET

GENERAL NOTES 154

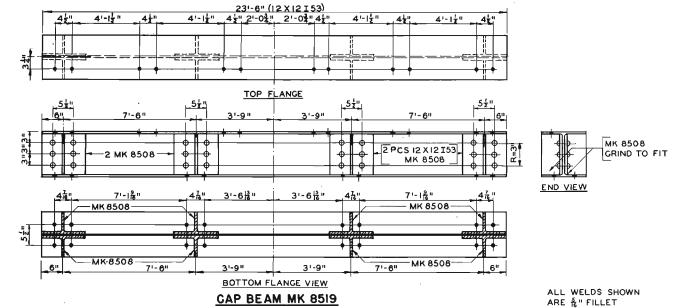
SYMBOLS 155

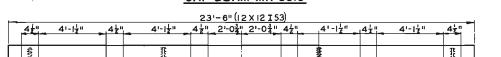
FRAMED ABUTMENTS 66, 67

2 P P S P P S P P P P P P P P P P P P P	DESCRIPTION BULKHEAD, PLANK DO DO PILE (MING) PICST (MING) DO DO DO DO DO DO DO DO DO D	STOCK NO 39-3340.12 39-3340.12-12 39-3540.12-14	FILL HE MARK 173 174 175 300		LENGTH 10'-0" 12'-0"	UNIT WEIGHT (POUNDS)	15' TO 50' G' MAX QUANTITY		60' TO 90'		6' MAX		40' SPAN	IMUM	6' Ma		70 90' SPAN	MUM	
2 B 2 1 2 P P 3 1 P 3 3 P	BULKHEAD, PLANK DO DO PILE (MING) PLE (BEARING) POST (MING) DO DO	39-3340.12 39-3340.12-12 39-3340.12-14 39-3360.08	MARK 173 174 175	SIZE (INCHES) 4 X 12 4 X 12	10'-0"	WEIGHT (POUNDS)				IMUM	6' MAX	IMUM	3' MAX	IMUM	6' MA	KIMUM		MUM	
2 B 2 1 2 P P 3 1 P 3 3 P	BULKHEAD, PLANK DO DO PILE (MING) PLE (BEARING) POST (MING) DO DO	39-3340.12 39-3340.12-12 39-3340.12-14 39-3360.08	173 174 175	4 X 12 4 X 12	10'-0"	WEIGHT (POUNDS)	QUANTITY	FВM	QUANTITY										7
2 P P S P P S P P P P P P P P P P P P P	DO DO PILE (MING) PICE (BEARING) POST (MING) DO	39-3340.12-12 39-3340.12-14 39-3360.08	174 175	4 X 12						FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LIN
2 P P S P P S P P P P P P P P P P P P P	DO DO PILE (MING) PICE (BEARING) POST (MING) DO	39-3340.12-12 39-3340.12-14 39-3360.08	174 175	4 X 12			12	480	6	240	12	480	6	240	12	480	8	520	1
2 P	DO PILE (MING) PILE (BEARING) POST (MING) DO DO	39-3340.12-14 39-3360.08		4 X 12		180			12	576	1		3	144	1		4	192	2
P 1 P 3 P 3 P 3 P 3 P 3 P 3 P 3 P 3 P 3	PILE (HING) PILE (BEARING) POST (HING) DO	39-3360.08			14'-0"	210	6	336			6	336			6	336			Τ,
3 3 p	PILE (BEARING) POST (WING) DO DO				15'-0"		2		2										
3 3 3 0 2 0	POST (WING) DO DO				1		6		8										
3 3 3 p	00		417 .	6 X 8	4'-11"	74							2	39			1		
3 3 9 3	00		191	6 X 8	6'-0"	90							<u> </u>				2	48	
م <u>د</u>		39-3360.08 39-3360.08	405	6 X 8	81-61	128					2	68	1		2	68	1 -		1
3	PUSI (BEARING)			10 X 10	5'-2 1/4"	162					6	259	1						1
	no.	39-6620-1	419	12 × 12	3'-7 1/8"	161						-//			6	258		-	10
		35-6630.12			14'-0"	630	2	336	2	336	 		1 - 1		2				1
	CAP	39-6630.12-14	285	12 X 12			-	220	-	330	2	233	2	233		336	2	336	1
-	DO	39-6620.1-14	265	10 × 10	14'-0"	437					-	233		233			! .		+ -
S	SCAB	35-3340.12	369	4 X 12	2'-0"	30							-				2	16	1.
+-	00	39-3340.12	368	4 X 12	2'-6"	38	1	10	1 1	10	+ , -				2	20			1
_	DO	39-3330.1	318	3 X 10	2,-8-	25			1 1		2	13	 		1				1
-	DG	39-3350-1	306	3 X 10	2'-0"	20			1				4	10					1
	NA I LER	39-3360.08	191	6 X B	6'-0"	90	6	144	- 6	192	6	144	1 -		6	144	4		1
1 2	DO	39-3360.08	420	6 X 8	4'-4 3/4"	66			1		-		6	106					41
	DO	39-3560.08	421	6 X 8	51-5 3/4"	82			1				-		-		6	132	1:
N.	NA I-LER CAP	39-3360.08	193	6 X 8	10'-0"	150	1	40	1	40	1	40	1	40	1	40	1	40	21
	DC	39-3360.08	196	6 X 8	16'-0"	240	1	64	1	64	1	64	1	64	1	64	1 1	64	2
_ ε	EILL TIMBERS	39-3360.08	190	6 X 8	20'-0"	300			_		ļ		<u>l</u>		5	400			2
	DO	39-3360.08	193	6 X 8	10'-0"	150	1	40	1	40	3	120	3	120	5	200	5	200	2.
	00	39-3360.08	198	6 X 8	20'-0"	300					3	240	3	240	5	400	5	400	21
В	BEARING BLOCK	39-6620.1	400	10 × 10	21-0-	63					8	155	8	133					2 !
	DO	39-6630.12	409	12 × 12	3'-6"	158									8	336	6	336	20
	DEADMAN	39-6620.1-16	266	10 × 10	16'-0"	500					2	267			2	267			2
	ANCHOR BLOCK	39-3360.08	410	6 × 8	1'-0"	15									8	32	6	24	28
	DO	39-3360.08	407	6 X 8	0'-10-	15				_	8	26	6	20					29
STEE	EL HARDWARE, BLACK											_							
	HIRE ROPE	22-4567.4-05	Γ	1/2"	20'~0"	13					8		:		8				30
	HIRE-ROPE CLIP	42-3544.5-05		1/2*	1	0.72					32				32				31
															1				+
MACH.	HINE BOLT WITH SQUARE AND TWO WASHERS	43-2325.07-223	B22	3/4*	22*	3.30	24		32										32
	ро	43-2325.07-2	820	3/4"	20"	3.06							16		18				3.
	DO	45-2325.07-183	B18	3/4"	18*	2.82	8		8		18		6						3
	ORIFT BOLT	43-1636.67-22	D22	3/4-	22*	2.76	6		8		6		6	- 1	6		6		3:
	DO	43-1636-07-16	D16	3/4"	16.	2.00	7		9		7		7		7		7		36
	DRIFT BOLT ANCHOR	43-1636.07-12	D12	5/4"	12*	1.50	12		12		12		12		12		12		3
	STANDARD WIRE SPIKE	42-8488.04-1	012	5/8"	10-	0.33	**		**		96		60		128		92	-	1
	DU DU	42-8488.035-07		5/10"	7-	0.145	180		216		180		90		160		120		13/
	ARING PILE LENGTHS TO I		CICIO O			0.143	100		-10		100				1 100		120		3:

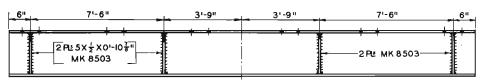




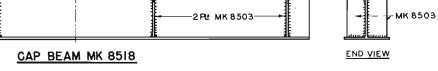




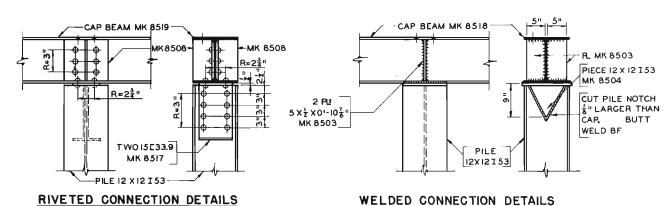




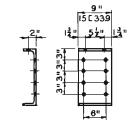
PILE TO CAP BEAM



PILE TO CAP BEAM



OF 12 X 12 I 53 [1-]16 12 X I2 I 53 GRIND TO FIT TOP AND воттом



STIFFENER MK 8508

WELDS UNLESS

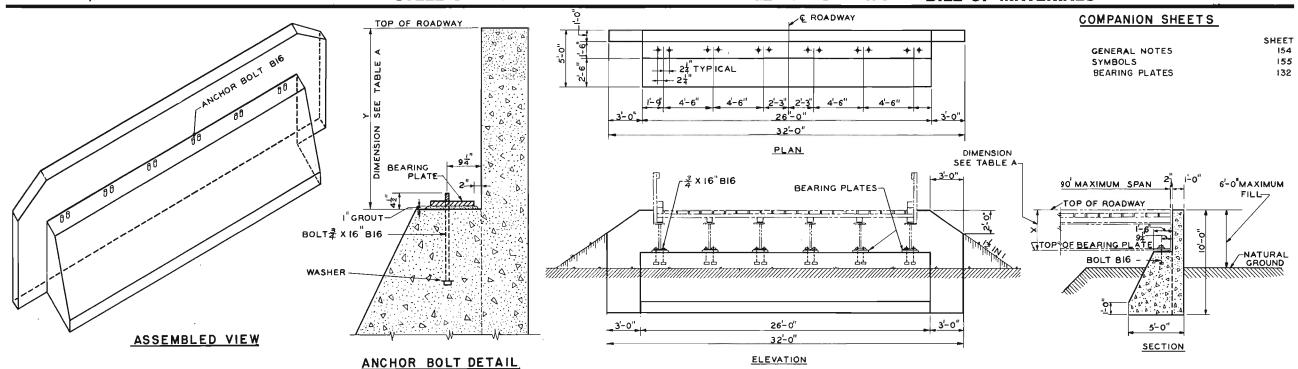
OTHERWISE NOTED

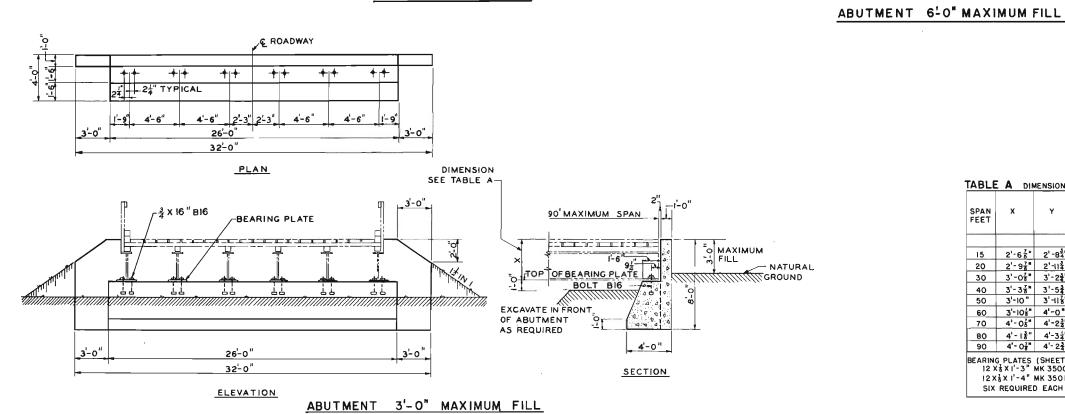
PILE CAP MK 8504

PILE CAP MK 8517

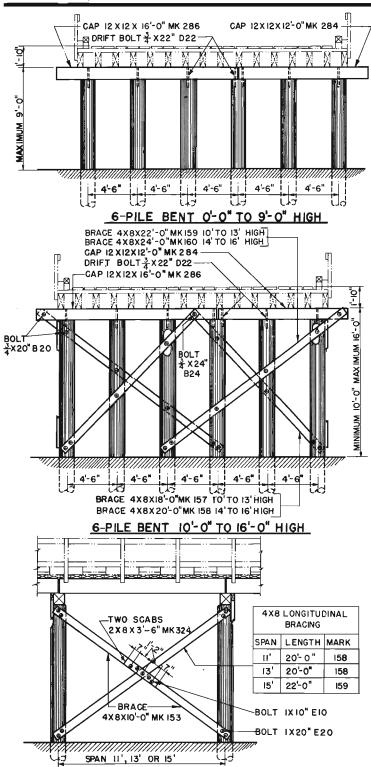
14-17	WIN 0300	TIEL ON MIT	<u>, 000</u>	_				<u> </u>
	BILL OF MATERIAL FOR ONE ABUTMENT	-						
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	QUANTITY	FBM	WEIGHT
ALTE	RNATE NO 1 WELDED DETAILS							
1	WING PILES		8501	12 X 12 I 53	15'-0"	2		79:
_ 2	CAP BEAM		8516	12 X 12 I 53	23'-6"	1		12
3	STIFFENERS	47-7844.05	8503	PL 5 X 1/2	10 7/8*	8		
ц	PILE CAP_		8504	12 X 12 I 53	1'-1"	4		2
ALTE	RNATE NO 2 RIVETED DETAILS							
5	WING PILES		8501	12 × 12 T 53	15'-0"	2		7
6	CAP BEAM		8519	12 X 12 I 53	23'-6"	1		12
7	STIFFENERS		8508	1/2-12X12 I 53	10 7/8	8		T .
8	PILE CAP	48-3790.15-34	8517	15 □ 33.9	0'-9"	8		
LUMB	ER, SOFT WOOD							
ç	NATLERS	39-6616.08	221	8 × 8	6'-0"	6	192	1
10	HAILER CAPS	39-6616.08	222	8 X 8	8'-0-	3_	128	. 1
11	BULKHEAD TIMBERS	39-3340.12-2	178	4 X 12	20'-0"	6	480	3
12	00	39-3340.12-12	174	4 X 12	12'-0"	6	288	1
STEE	L HARDWARE, BLACK							
15	BOLTS WITH NUTS AND TWO WASHERS	43-2325.07-1	B10	3/4	10.	24		1
14	ANCHOR BOLTS WITH NUTS AND TWO WASHERS	43-2219.08-04	Mu	7/8	4-	12		(3)
15	DRIFT BOLTS WITH WASHERS	43-1636.07-16	_D16	3/4	16"	4		Ŋ
16	WIRE SPIKES	42-8488.035-07		5/16	7-	108		Ш
17	RIVETS	43-6353.08-25		7/8	2 1/2*	16	L	
18	DO	43-6353.08		7/8	2 3/4"	56		٠.
19	WELDING ROD (POUNDS)	46-3772.2.7		3/16] 1

¹ TOTAL WEIGHT

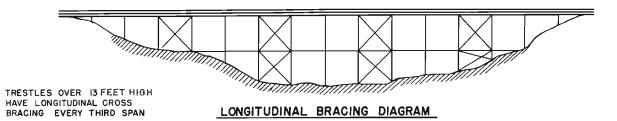




				OLTS WITH UT AND TWO	CONC	RETE
SPAN FEET	x	Y	WASHERS STOCK NO	3 × 16 B16	6' MAXIMUM FILL	3' MAXIMUM FILL
			QUANTITY	WEIGHT EACH	CU YDS	CU YDS
15	2'-67"	2' -84"	12	3.5	32.1	21.4
20	2'-9 ⁷	2'-113#	12	3.5	31.4	20.9
30	3'-07	3'-2*	12	3.5	30.8	20.2
40	3'-38"	3'-5≹"	12	3.5	30.1	19.8
50	3'-10 "	3'-117"	12	3.5	28.8	18.7
60	3'-108"	4'-0"	12	3.5	28.8	18.7
70	4'-08"	4'-23"	12	3.5	28. l	18.2
80	4'-18"	4'-34"	12	3.5	28.0	18.1
90	4'- 01"	4'- 23"	12	3.5	28.1	18.2



LONGITUDINAL ELEVATION 13'-0" TO 16'-0" HIGH



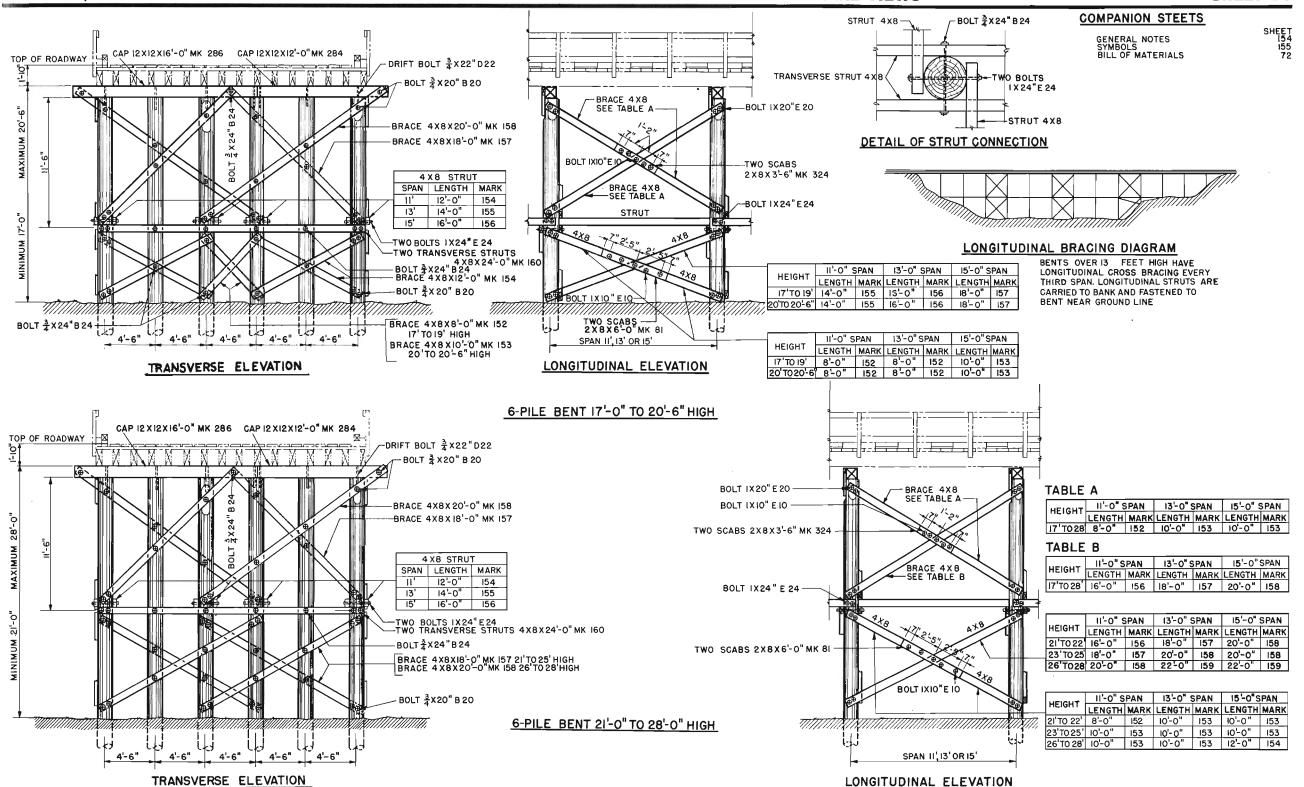
COMPANION SHEETS

 GENERAL NOTES
 154

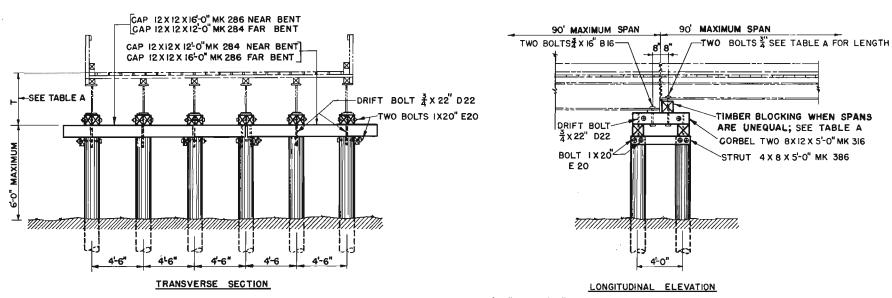
 SYMBOLS
 155

 TIMBER PILE BENTS
 73

		E TRANSVERSE BENT HEIGHT OF BENT					0 T	0 9'	10' I	0 13'	14' 7	0 16'	17'	10 19'	20' (0	20'-6"	21'	ΓO 22'	23' 10	25'	26' 1	0 28'	
INE	DESCRIPTION	STOCK NUMBER	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (PCUNDS;	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANEITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LIN
Bil	L OF MATERIALS FOR ONE BE	INT																					
1	PILE		T .				6		6		6		6		6		6		6		6		Tī
	LUMBER, SOFT WOOD																						
2	CAP	39-6630-12-12	284	12×12	12'-0"	540	1	144	1	144	1	144	1	144	1	144	1	144	1	144	1	144	2
3	CAP	39-6630-12-16	286	12412	16'-0"	720	1	192	1	192	1	192	1	192	1	192	1	192	1	192	1	192	3
4	SASH BRACE	39-3340.06-24	160	4×8	24'-0"	240							2	128	2	128	2	128	2	128	2	128	4
5	BRACE	39-3340.06-08	152	4X8	8'-0"	80							2 ,	43									5
6	DO	39-3340.06-1	153	4X8	101-0"	100									2	53			1				6
7	00	39-3340.08-12	154	4X6	12'-0"	120							4	128	4	128							7
8	DO	39-3340.08-18	157	448	18"-0"	180			2	96			2	96	2	96	6	288	6	288	6	288	В
9	uo	39-3340.08-2	158	4X6	20'-0"	200	0002222				2	107	2	107	2	107	2	107	2	107	6	320	ç
10	DC	39-3340.08-22	159	4×8	221-0"	220			2	,117													10
11	DO	39-3340.08-24	160	4×8	24'-0"	240				1	2	128											11
	STEEL HARDWARE, BLACK							POUNUS		POUNDS		POUNDS		POUNDS		POUNDS		POUNDS		POUNDS		POUNDS	
12	PRIFT BOLT WITH SQUARE HEAD AND WASHER	43-1636-07-22	022	3/4	22*	3.0	7	21	7	21	7	21	7	21	7	21	7	21	7	21	7	21	12
13	MACHINE BOLF WITH SOURCE	43-2325.07-2	820	3/4	20"	3.06			20	61	20	61	28	86	28	86	44	135	44	135	44	135	13
14	DO	43-2325.07-24	824	3/4	24*	3.54			1	ц	1	4	15	53	15	53	9	32	9	32	9	32	14
BIL	L OF MATERIALS FOR ONE SP	AN OF STRUTS		22.75							_		100										
	STEEL HARDWARE, BLACK												0.0000000000000000000000000000000000000										
15	MACHINE BOLT WITH SQUARE	43-2325.1-24	E24	1	24	6.48							8	52	8	52	8	52	8	52	8	52	15
	LUMBER, SOFT WOOD													FBM		FBM		FBM		FBM		FBM	
16	STRUT FOR 11'-0" SPAN	39-3340.08-12	154	4X8	12'-0-	120							4	128	4	128	4	128	4	128	4	128	16
17	STRUT FOR 13'-0" SPAN	39-3340.68-14	155	448	14'-0"	140							4	149	4	149	4	149	4	149	4	149	17
8	STRUT FOR 15'-0" SPAN	39-3340.08-46	156	418	16'-0"	160							ų.	171	4	171	4	171	4	171	4	171	18
BII	L OF MATERIALS FOR ONE SP	AN OF LONGITUDINA	L BRAC	CING																			
	STEEL HARDWARE, BLACK FO	R 11', 13' AND 15	' SPAI	≀S								PCUNUS		PCUNDS		PCUNDS		POUNDS		POUNDS		POUNDS	
19	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43- 2325.1-104	٤10	1	10*	3.45	1000				10	35	20	65	20	69	20	69	20	69	20	69	15
20	DO	43- 2325.1-2	E26	1	20"	5.61	A.00030000				16	90	52	179	32	179	32	179	32	179	32	179	20
	LUMBER, SOFT WOOD FOR 11	', 13' AND 15' SP	ANS					•				FBM		FBM		FBM		FBM		FBM		FBM	
21	SCAB	39-2228.08	324	2×8	3'-6"	18					4	19	4	19	4	19	4	19	4	19	4	19	21
22	90	39- 2228.06	81	2×8	6'-0"	30							4	32	4	32	4	32	4	32	4	32	22
	LUMBER SOFT WOOD FOR 11	'-O" SPAN																					
23	BRACE	39-3340.08-08	152	4 X 8	6'-0"	80							8	171	8	171	8	171	4	85	4	85	.23
24	ს	39- 3340.08-1	153	4 . 8	10'-0"	100					4	107							4	107	4	107	24
25	90	39-3340.08-14	1:5	478	14'-0"	140					·		2	75	. 2	75			L				25
26	DO	39-3340.08-16	156	4.48	16'-0-	160							2	85	2	85	4	171	2	85	2	85	26
27_	DO	39-3340-08-18	157	4×8	18'-0"	180													2	96	_		27
28	00	39- 3340.08- 20	15ò	4.48	20'-0"	200		L	<u> </u>		2	107	L								2	107	28
	LUMBER, SOLE WOOD FOR 13	'- 0" SPAN																					
29	BRACE	39-3340.08-08	152	4×8	8'-0"	80							4	85	4	85							29
30	υo	39-3340-06-1	153	448	10'-0"	100			_		4	107	4	107	ц	107	8	213	8	213	8	213	30
31	DC	39-3340.08-16	156	4X8	16'-0"	160			1				2	85	2	85							31
32	00	39-3340-08-18	157	4X8	18'-0-	180							2	96	2	5.6	4	192	2	96	2	96	32
33	DC	39-3340.08-2	158	4×8	20'-0"	200					2	107							2	107			33
34	00	39-3346.68-22	159	4 X 8	22'~0"	220															2	117	34
	LUMBER, SOFT WOOD FOR 15	'-0" SPAN																					
15	DO	39-3340.68-1	153	4×8	10'-0"	100			1		ц	167	8	213	8	213	8	213	8	213	4	107	35
6	00	39-3340.CE-12	154	4×8	12'-0"	120							1		1						4	128	36
3 7	00	39-3340.08-18	157	4.48	16'-0"	180							2	96	2	96							37
38	эc	39- 3340.08-2	158	4×8	20'-0"	200							2	107	2	107	4	213	4	213	2	107	38
39	0C	39-3340.08-22	159	4X8	22'-0"	220					2	117			1						2	117	35
. У																							







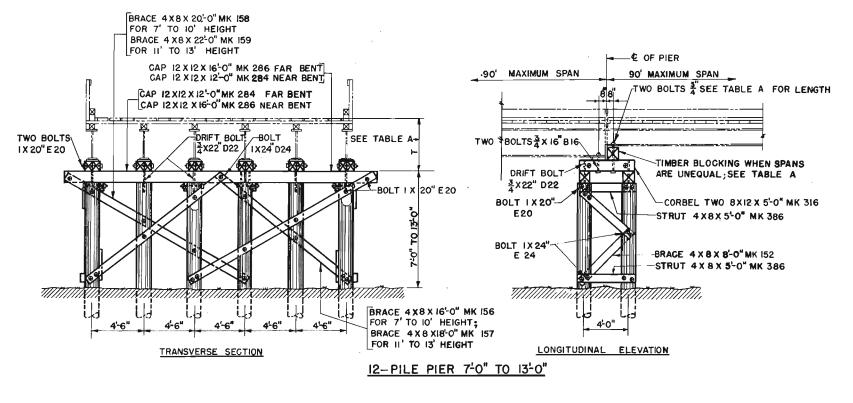
12 PILE PIER 0'-0" TO 6-0"

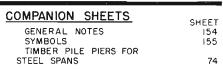
REQUIRED PILE CAPACITY

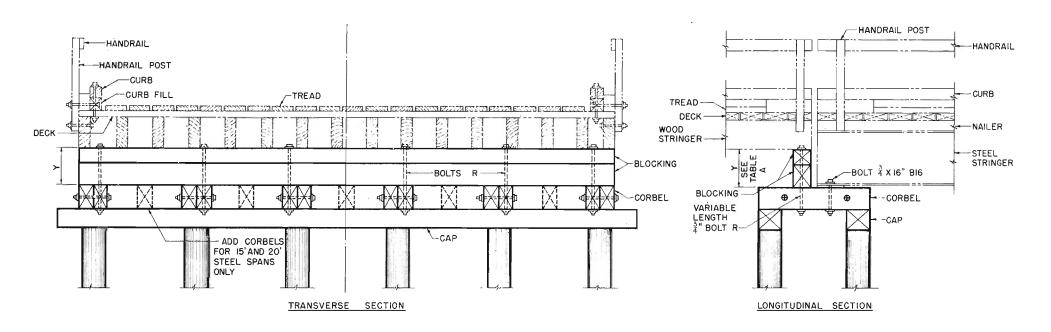
TOTAL LENGTH OF TWO ADJACENT SPANS	30'	4 0'	60,	80'	100,	120'	140	160	180'
TONS PER PILE	10	10	12	14	15	17	18	18	18

_	DEPTH	OF BLOCKING AND LENGTH OF ANCHOR BO	LT
TABLE A	WHEN	ADJACENT SPANS ARE NOT EQUAL	

IADL	E A		WHEN AL	DJAGENT	SPANS AF	RE NOT E	EQUAL		
SPAN	Т		TIMBER SPAN		s ⁻	TEEL SPA	N N		
			15'	15'	20'	30'	40'	50	60'
90'	5-13"	BLOCKING BOLT	2 ^L 4 42"	1'-6" 34"	1'- 3" 32"	I ^L 0" 28"	0'- 9" 26"	0'-3" 20"	0'-3" 20"
80,	5'- 2 <u>1</u> "	BLOCKING BOLT	2 ^L 4" 42"	1'-6" 34"	1'- 3" 32"	1'-0" 28"	0'- 9" 26"	0'-3" 20"	0'-3 20"
70'	ぢ- เ <u>ล</u> ื"	BLOCKING BOLT	2'-4" 42"	!'-6" 34"	I'- 3" 32"	ľ- 0" 28"	0'-9" 26"	0'-3" 20"	0'- 3" 20"
60'	4 ^L -11 [#]	BLOCKING BOLT	2 ^L 1 * 40*	1 ^L 3" 32"	l'-0" 28"	0'-9" 26"	0'-6" 22 "		
50'	4-107"	BLOCKING BOLT	2'-1" 40"	l'~3" 32"	1-0*	0'-9" 26"	0'-6" 22"		
40'	4'-43"	BLOCKING BOLT)'-7" 34"	0'-9" 26"	o-e"	0'-3" 20"			
30'	4'-13"	BLOCKING BOLT	1'- 4" 30"	0'-6" 22"	0'- 3" 20"				
20'	3'-10 ^{3''}	BLOCKING BOLT	l'-l" 28"	Q'−3" 20"					
15'	3'-7 3 "	BLOCKING BOLT	0'-10" 24"						







SPECIAL BLOCKING AT JUNCTION OF STEEL AND TIMBER SPANS

8	BILL OF MATERIALS FOR ANCHOR BOLTS AND BEARING PLA	res
	3/4" AUCHOR BOLT WITH SQUARE BUT AND THO WASHERS	
i	FOR REQUIRED LENGTH SEE TABLE 4 SHEET 74 SIX REDUIRED AT EACH SUPPORT FOR EACH TIMBER SPAN	
	I'WELVE REQUIRED AT EACH SUPPORT FOR EACH STEEL SPAN	

BOLT LENGTH	STOCK NUMBER
20 *	45-2325.07-2
22*	43-2325.07-223
24.	43-2325,07-24
26*	43-2325.07-265
28 •	43-2325.07-28
30 *	43-2325.07-305
52*	43-2325.07-52
34*	43-2325,07-346
40 •	43-2325.07-406
42*	43-2325.07-425

SEARING PLATES 12 x 7/8 x 1'-3' P350C FOR 15 TO 80 FOOT SPAN SEARING PLATES 12 x 7/8 x 1'-4" P3501 FOR 50 FOOT SPAN SIX REQUIRED FOR EACH SEEL SPAN AT EACH SUPPORT STOCK INSPECT 40-7844.08

VARIABLE BLOCKING 12" WIDE X 12"-0" LONG OF DEPTHS REQUIRED AS SHOWN BY DIMENSION Y

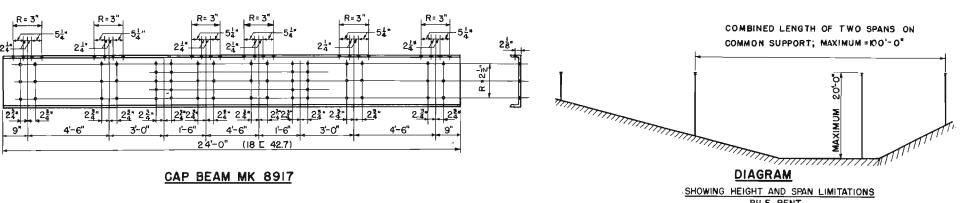
: 1 A	SS 50 - DOUBLE LANE								PIER HEIC	Hr.		
					UNIT	0' 1	U 6'	7' TG 10'		111 TO 131		
INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT (PCUIDS)	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM
ı	PILE				100000		12		12		12	
LU	MBER, SOFT WOOD											
2	CAP	39-6630.12-12	284	12 X 12	12'-0"	540	2	288	2	288	2	288
3	00	39-6630.12-16	286	12 × 12	16'-0"	720	2	384	2	384	2	384
4	CORBEL	39-6616.12	316	8 X 12	5'-0=	150	12	480	12	480	12	480
3 .	STRUT	39-5340.08	386	4 × 8	5'-0"	50	4	53	6	80	6	80
6	BRACE	39-3340.08-08	152	4 X 8	81-0-	90			4	86	4	86
7	DO	39-3340.08-16	156	4 X 8	16'-0"	160			ц	171		
8	DO	39-3340.08-18	157	4 X 8	18'-0"	180					4	192
9	DC	35-3340.08-2	158	4 X B	20'-0"	200			4	213		
٥	DŮ	39-3340.08-22	159	4 X 8	22'-0"	220					4	235
ST	EEL HARDWARE, BLACK											
٠	DRIFT BOLT WITH SQUARE HEAD AND ONE WASHER	43-1636.07-22	022	3/4	22*	3.0	26		26		26	
2	MACHINE BOLT WITH SQUARE HEAD AND ONE WASHER	43-2325.1-2	£20	1	20"	5.6	28		76		76	
3	00	43-2325.1-24	E24	1	24"	6.5			10		10	
4	DO	43-2325.07-16	816	3/4	161	2.6	24		24		24	

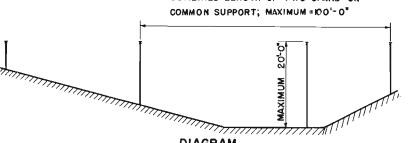
TABLE	_A	
STEEL SPAN	DIMENSION Y	BOLT R
15'	0'- 9칠 "	24"
20'	1'-04"	26"
30'	1'-34"	30"
40'	1'-63"	32"
50'.	2'-0 ਹੈ "	38"
60'	2'-1"	38"
70'	2'-34"	42"
80'	2'-44"	42"
90'	2'-3¾"	42"

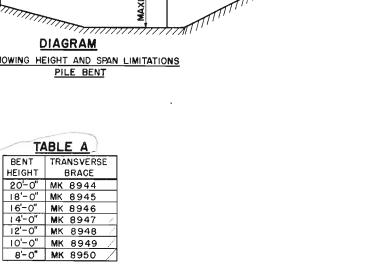
SHEET

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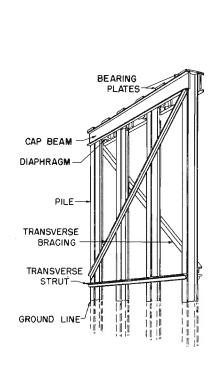
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BILL OF MATERIALS FABRICATION DETAILS 78 150 12,000 = 46T + O.L. 2000 40 x 1 x 1 x 1 x 1 x 1 2 0



COMPANION SHEETS

GENERAL NOTES

SYMBOLS

ASSEMBLED VIEW

I.	22'-6"		TOP OF TREA	D
7'-6"	7'-6"	7'-6"	VADIES	S (SEE TABLE B)
4'-6" 3'-0"	[-6" 4'-6"]'-	6" 3'-0" 4'-6"	VARIES) (SEE MALE B)
FIR. 18X 4 X 1-7" IR. P		IR PI	IR PI-	-12 X 12 I 53 X 1'-3" MK 8911
1441	18 E 42.7 MK 8917		STRUT	- MK 8917
	MK 8911	MK 8911	R=2\frac{1}{4}" 20\tag{-0" MAXIMUM} THAN 8-0" OMIT BRACING AND S	-12 X 12 I 53
12 X 12 1 53	SEE TABLE A	12XI2 I 53	IMUM DIMENSION A A 15 LESS	SEE TABLE A
	_2 & 4X3X € X 23'-6" MK 8916		DIMEN	
1	GROUND LINE	(WHEN DIMENSION	MK 8916
				<i>77).</i>

SECTION A-A

FOUR-PILE BENT

TRANSVERSE ELEVATION

			TABLE B	
MAXIM PILE L		1	E FROM TOP OF TRE	
TOTAL LOADED LENGTH	TONS PER PILE	SPAN	STEEL- STRINGER SIZE	TOP OF TREAD TO BOTTOM OF STRINGER
30'-0"	20	15'-0"	18 I 47	2'-67"
40-0"	23	20-0"	21 I 59	2'- 97"
50'-0"	25	30'-0"	24 I 74	3'- 0å"
60'-0"	28	40'-0"	27 I 91	3'-38"
70'-0"	30	50-0"	33 I 125	3'- 10 "
80'-0"	33	60'-0"	33 I 132	3'-10a"
90'-0"	35	70'-0"	36 I 150	4'-02"
100-0"	38	80'-0"	36 I 182	4'~18"
		90'-0"	36 I 230	4'-08"

TABLE D

2 ಟ 4x3x<u>5</u> x i≒3"

21159

MK 8913

SHEET 77

SHEET

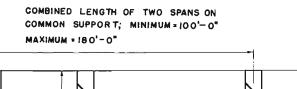
155



FABRICATION DRAWINGS

GENERAL NOTES

SYMBOLS



PLAN AT TOP OF PIER

21159-

MK 8914

2 4 4 4 3 X 16 X 1'- 3" A 3 (X) END 2 4 4 X 3 X 16 X 1'- 3" A 3 MK 8915

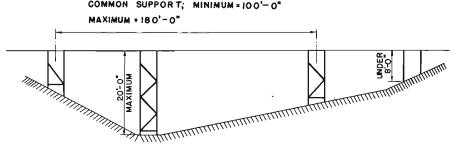
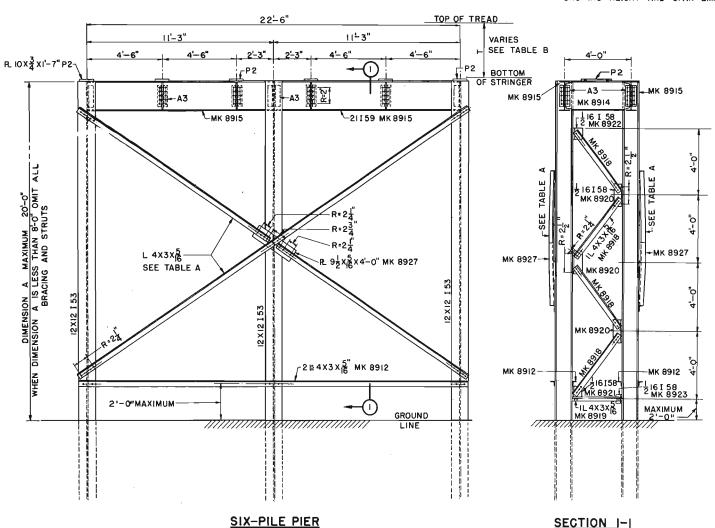


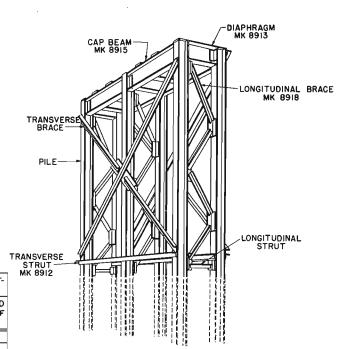
DIAGRAM
SHOWING HEIGHT AND SPAN LIMITATIONS



MAXIMI PILE LO		
TOTAL LOADED LENGTH	TONS PER PILE	
110	32	
120	34	
130	35	
140	37	
150	39	
160	40	
170	42	
180	44	

1	TABLE	<u>A</u>	
Γ	PIER	TRANS	VERSE
L	HEIGHT A	BRACE	MARK
	8'-O"	8950	8951
	10'-0"	8949	8952
	12'-0"	8948	8953
	14'-0"	8947	8954
	16'-0"	8946	8955
	18,-0,	8945	8956
	20'-0"	8944	8957

TABLE B DISTANCE FROM TOP OF TREAD TO BOTTOM OF STRINGER FOR VARIOUS SPANS STEEL-TOP OF TREAD STRINGER TO BOTTOM OF SIZE STRINGER T 15'-0" 18 I 47 2'-6² 20'-0" 21 I 59 2'-97 30'-0" 24 I 74 3'-08 3'- 3 40'-0" 27 191 50-0" 33 I 125 3'-10' 60'-0" 33 I 132 3,-10₽ 70'-0" 36 I 150 4'-07 36 I 182 4'-13 90'-0" 36 I 230 4'-07



ASSEMBLED VIEW

STEEL PILE BENTS AND PIERS

STEEL PILE BENTS AND PIERS

STEEL PILE BENTS AND PIERS

STEEL PILE BENTS AND PIERS

SHEET

80

COMPANION SHEETS

GENERAL NOTES

SYMBOLS

BILL OF MATERIALS FOR ONE RIVETED PILE BENT OR PIER | STEEL PILE BENT HEIGHT | SEE SHEET 76 | 18' | 16' | 14' | 12' | 10' | 8' | UNDER 8' | STEEL PILE PIER HEIGHT DESCRIPTION 201 20' 18' 16' 14' 12' 10' 8' UNDER 8' SIZE (INCHES) LENGTH WEIGHT QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY LINE QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY LINE STOCK NO 48-2900.21-059 8195 21 I 59 1 CAP BEAM 1 48-3790.18-45 8917 18 [42.7 24'-0" 1025 DO 2 DIAPHRAGM 8911 12X12 I 53 1'-3" 66 3 48-2900.21-059 8913 21 I 59 2'-115/8* 175 48-2900.21-059 8914 21 I 59 3'-11* 231 48-2900.4-035 A2 L4X5X5/16* 1'-3* 9 u DO 2 2 2 2_____ 4 5 DO 6 CONNECTION ANGLE 7 DO 8 CONNECTOR 5 6 7 4 4 4 4 4 4 4 16 16 16 16 16 16 16 48-2550.4-035 A3 L8X3X5/16 1'-3* 9 48-2900.16-058 892C 1/2 16 I 58 1'-6 1/2* 45 48-2900.16-058 892I 1/2 16 I 58 0'-10 1/6* 24 24 24 24 24 24 24 6 3 3 3 3 3 8 9 DO 10 DO 11 DO 48-2900.16-058 8922 1/2 16 158 01-8 1/4 21 48-2900.16-058 8923 1/2 16 158 01-6 1/4 21 48-2900.16-058 8923 1/2 16 158 01-6 15 47-7844.04 8927 PL 9 1/283/8 41-0 40 47-7844.07 P1 PL 18 X 3/4 1'-7* 75 47-7844.07 P2 PL 10 X 3/4 1'-7* 40 11 12 13 12 DO 13 BEARING PLATE 2 2 2 2 2 2 6 6 6 14 14 DO 14 DO 15 STRUTS AND BRACES 16 DO 17 DO 18 DO 19 DO 20 DO 21 DO 22 DO 48-2550.4-035 8912 L4X3X5/16 23'-6" 169 4 4 4 15 16 48-2550.4-035 8916 L4X3X5/16 23'-6" 170 48-2550.4-035 8918 L4X3X5/16 4*-1 11/10* 30 48-2550.4-035 8919 L4X3X5/16 2*-9 1/4* 20 48-2550.4-035 8919 L4X3X5/16 28*-5* 205 48-2550.4-035 8945 L4X3X5/16 28*-5* 205 48-2550.4-035 8945 L4X3X5/16 26*-4* 190 48-2550.4-035 8946 L4X3X5/16 26*-4* 190 12 6 6 17 18 19 20 21 -22 3 3 3 3 3 2 48-2550.4-035 8947 L4X3X5/16 25'-6" 184 2 23 DO 48-2550.4-035 8948 L4X3X5/16 24'-10" 179 2 23 24 48-2550.4-035 8949 L4X3X5/16 241-57 175 2 2 28 DO 28 DO 25 DU 26 DO 27 DO 28 DO 29 DO 10 DU 31 DO 32 DO 33 RIYET 48-2550.4-035 8950 L4X5X5/16 23'-10" 172 2 25 48-2550.4-055 8951 L4X3X5/16 11'-0" 75 48-2550.4-055 8952 L4X3X5/16 11'-4" 82 26 27 _#_ 48-2550.4-035 8953 L4X3X5/16 11'-10" 86 28 48-2550.4-055 8954 L4X3X5/16 12'-4" 89 29 48-2550.4-035 8955 L4X3X5/16 12'-10" 48-2550.4-035 8956 L4X3X5/16 13'-4" 96 31 48-2350.4-035 8957 L4X3X5/16 13'-9* 99 43-6355.08-2 7/8 2* .53 43-6353.08-23 7/8 2 1/4* .57 40 -24 24 24 24 24 24 24 35 248 248 226 236 224 224 128 34 192 192 166 168 144 144 104 35 34 DO 35 DO 43-6353.08-25 7/8 7/8 3° 12X12 I 53 _____ 36 DO 45-6353.08-3 37 PILE

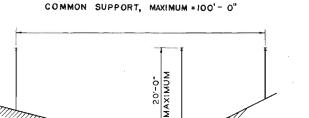
BILL OF MATERIALS FOR ONE WELDED PILE BENT OR PIER
--

			DESCRIP	MT 1411				STEEL PL				SEE SHE					PILE PIE				E SHEET	
			DESCRIP	TION			201	181	16'	14'	1.21	10'	81	UNDER 81	201	18'	16'	141	12'	10'	81	UNDER 8
INE	USE	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANT ETY	QUANTITY	QUANT ITY	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTITO	QUANTIT	QUANTITY	QUANTIT
1.	CAP BEAM	48-3790.18-43	7023	18 E 42.7	24'-0"	1025	2	2	2	2	2	2	2	2								
2	DO -	48-2900.21-059	7043	21 I 59	251-2 1/4"	1368									2	2	2	2	2	2	2	2
3	DIAPHRAGM		7024	12×12 I 53	11-3=	66	44	4	4	4	4	4	4	4								
ш	DO	48-2900-21-059	7044	21 I 59	3'-11 5/8"	234									6	6	6	6	6	6	6	6
5_	BOLTING CLIP	47-7844-04	P7		0'-4 1/16"	1.	I								24	24	24	24	24	24	24	24
6	BEARING PLATE	47-7844-07	P3	PL 15 X 3/4	11-7-	60	6	6	6	6	6	6	6	6								
7	DO	47-7844.07	P4	PL 10 X 3/4	· 11-7"	46									6	6	6	6	6	6	6	6
8	PILE CAP			1/2 12X12 I 53	1'-0-	26									6	6	6	6	6	6	6	6
9	CCNNECTOR	47-7844.05	8659	PL 8 X 1/2	1'-6"	20									9	6	6	3	3			
0	DC	47-7844.05	8660	PL 8 X 1/2	1'-0"	14									6	6	6	6	6	6	6	
_	DC	47-7844.05	8661	PL 8 X 1/2	6,-64	7									3	3	3	3	3	5	3	
2	DO	47-7844.04	7045	PL 5 1/2 x 3/8	51-9"	26									2	2	2	2	2	2	2	\Box
5	SHELF ANGLE	48-2550.4-035	8647	L 4X3X5/16	0'-4"	. 2	4	4	4	4	4	4	4	4								
4_	STRUTS AND BRACES	48~2550.4-055	7026	L 4X3X5/16	28'-5"	205	2								2							
5	_ 00	48-2550.4-035	7025	L 4X3X5/16	25'-6"	169	2	2	2	2	2	2	2		4	4	4	4	4	4 .	4	
ے	DC	48-2550.4-035	7027	L 4X3X5/16	27'-4"	197	L	2								2						
7_	DQ	48-2550.4-035	7028	L 4X3X5/16	261-4"	190			2								2			L		
8	00	48-2550.4-035	7029	L 4X3X5/16	251~6"	184				2								2				
0	DG	48-2550-4-055	7050	L 4X3X5/16	24'-10"	179					2		ļ						2		<u> </u>	
0	DO	48-2550.4-035	7031	L 4x3x5/16	24'-3"	175						2								2		├
1	DO	48-2550.4-035	7032		23!-10"								2	002-02073				l		I	2	
2	DO	48-2550.4-035	7035		15'-9"	99				ļ					4							
3_	00	48-2550.4-035	7036	L 4X5X5/16	15'-4"	96	<u> </u>									4						
4	DO	48-2550.4-035	7057	L 4X3X5/16	12'-10"	93	ļ										4					
5_	DO	48-2550.4-035	7038	L 4×5×5/16	12'-4×	89	ļ											4				<u> </u>
6	DO	48-2550.4-055	7039		11'-10"	86													4			1
7_	DO	48-2550.4-035	7040	L 4X3X5/16	11'-4"	82	 						L							4		
28	00	48-2550.4-035	7041	L 4X5X5/16	11'-0"	79															4	
29	00	48-2550.4-055	8613	L 4X5X5/16		30									12	9	9	6	6	3	3	
30	DÚ	48-2550.4-055	8622	L 4X3X5/16	21-9 1/4"	20									3	3	3	3	3	3	3	
٤١_	WELDING ROD (POUNDS)	46-3772.2-7		3/16			17	17	17	17	17	17	17	12	40	37	37	34	34	31	31	20
32	PILE	1		12X12 I 55	للسا	1	4	1 4	1 4	4	4	Ħ	14	11	- 6	6	6	6	- 6	6	6	1 6

____ PILE LENGTH TO BE DETERMINED BY FIELD CONDITIONS.

¹ MILE LENGTH TO BE DETERMINED BY FIELD CONDITIONS.

COMPANION SHEETS
COMBINED LENGTH OF SPANS ON



BILL OF MATERIALS 78
FABRICATION DRAWING 151
GENERAL NOTES 154
SYMBOLS 155
SHIMS 63

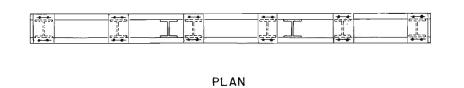
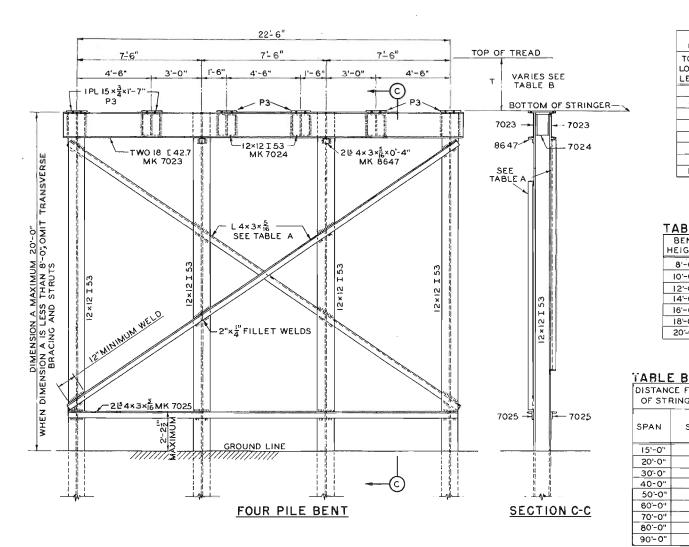


DIAGRAM
SHOWING HEIGHT AND SPAN LIMITATIONS

ALL WELDS SHOWN ARE $\frac{1}{4}$ FILLET WELDS UNLESS OTHERWISE NOTED



MAXIMUM PILE LOAD							
TONS							
PER							
PILE							
20							
23							
25							
28							
30							
33							
35							
38	ı						
	OAD TONS PER PILE 20 23 25 28 30 33 35						

TABLE A

BENT TRANSVERSE BRACE MARK

8'-0" 7032

10'-0" 7031

12'-0" 7030

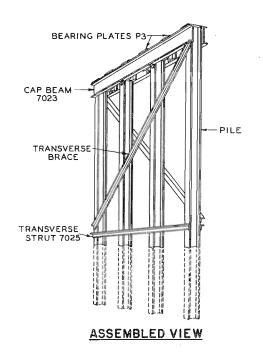
14'-0" 7029

16'-0" 7028

18'-0" 7027

20'-0" 7026

ANELD									
DISTANC	CE FROM TOP OF	TREAD TO BOTTOM							
OF STE	RINGERS FOR V	ARIOUS SPANS							
	STEEL	TOP OF TREAD TO							
SPAN	STRINGER	BOTTOM OF							
	SIZE	STRINGER T							
15'-0"	18 I 47	2'-67"							
20'-0"	21 I 59	2'-97"							
_30'-0"	24 I 74	3'-07"							
40-0"	24 I 91	3'-3 7							
50'-0"	33 I125	3'-10"							
60'-0"	33 I 132	3-108"							
70'-0"	36 I 150	4'-0 2"							
80'-0"	36 I 182	4'-। है"							
90'-0"	36 I 230	4'-0.7"							



1 12 10 x 3 x 1-7

4'-6"

21 I 59 MK 7044

TOP PLAN

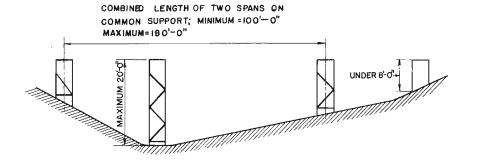
MK 7043

SHEET

154 155

78 151

63



DIAGRAM

TADIE A

SHOWING HEIGHT AND SPAN LIMITATIONS
PILE PIER

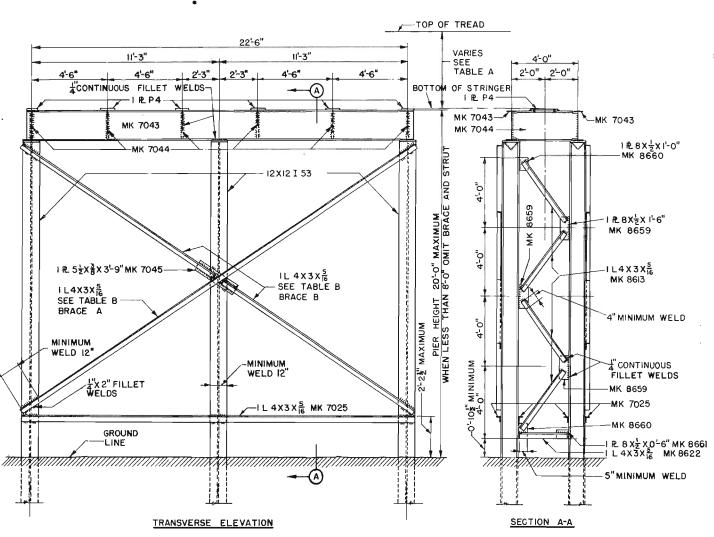
ALL WELDS SHOWN ARE # FILLET WELDS UNLESS OTHERWISE NOTED

COMPANION SHEETS

GENERAL NOTES 'SYMBOLS

BILL OF MATERIALS FABRICATION DRAWING

SHIMS

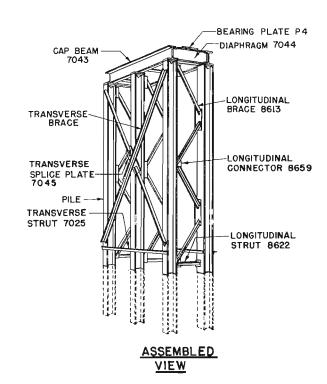


-21 I 59 MK 7043

IADLE	A								
	FROM TOP OF TRE								
OF STRINGERS FOR VARIOUS SPANS									
	STEEL-	TOP OF TREAD							
SPAN	STRINGER SIZE	TO BOTTOM OF STRINGER							
50'-0"	33 I 125	3'-10"							
60'-0"	33 I 132	3'- 10 g"							
70'-0"	36 I 150	4'-0 8 "							
80'-0"	36 I 182	4'-1 8 "							
90'- 0"	36 I 230	4'- 0급"							

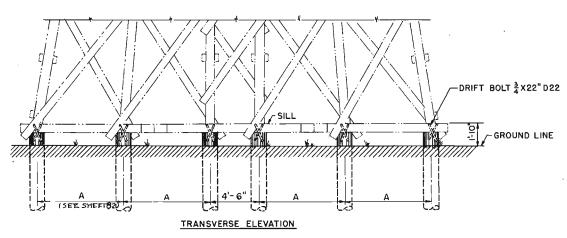
<u>TABLE</u>	В	
PIER	TRANS	VERSE
HEIGHT	BRACE A	BRACE B
20-0"	MK 7026	MK 7035
18'-0"	MK 7027	MK 7036
16'-0"	MK 7028	MK 7037
14'-0"	MK 7029	MK 7038
12'- O"	MK 7030	MK 7039
10-0"	MK 7031	MK 7040
8'- 0"	MK 7032	MK 7041

MAXIM PILE LO	
TOTAL	TONS
LOADED	PER
LENGTH	PILE
110-0"	32
120'-0"	34
130'-0"	35
140-0"	37
150'-0"	39
160'-0"	40
170'-0"	42
180'-0"	44



SIX PILE PIER

SHEET 154 155 82 GENERAL NOTES SYMBOLS BILL OF MATERIALS



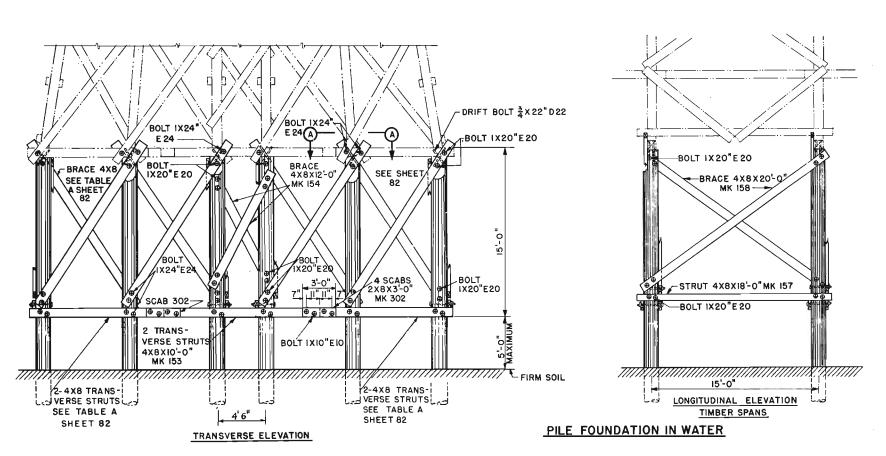
PILE FOUNDATION ON GROUND

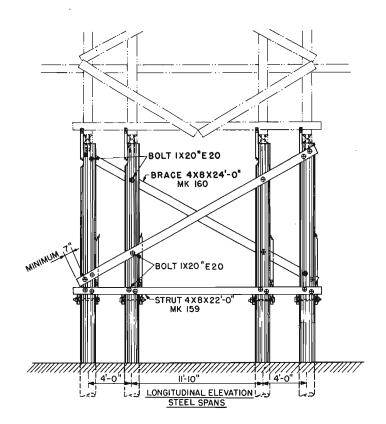
FOR SECTION A-A SEE SHEET 82

FOR DETAIL OF TRANSVERSE STRUT SPLICE, SEE SHEET 82

MAXIMUM HEIGHT OF STRUCTURE GRADE TO GROUND = 80 FEET

REQUIRED BEARING CAPACITY OF PILES **18 TONS PER PILE**





HIGHWAY

TOWER DIMENSION

13'-4" 5'-5\frac{6}{8}"
16' 5'-8"
18' 5'-10"

Α

6'-0"

6'-4"

6'-10" 7'-0" 7'-2" 7'-4"

46' 8'-2" 48' 8'-4" 50'-10" 8'-7"

53' 8'-9"
55' 8'-11"
57' 9'-1"
59' 9'-3"
61' 9'-5"
63'-4" 9'-7\frac{1}{3}"

9'-11" 10'-1" 10'-3" 10'-5"

75'-10" 10'-8<u>k</u>"

69'

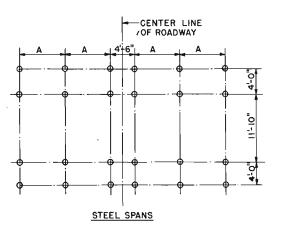
38'-4" 7'-6 5" 40' 7'-8" 42' 7'-10" 44' 8'-0"

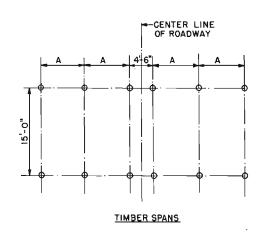
HEIGHT

20'

COMPANION SHEETS

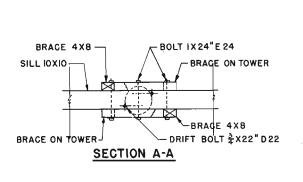
HEET
154
155
81

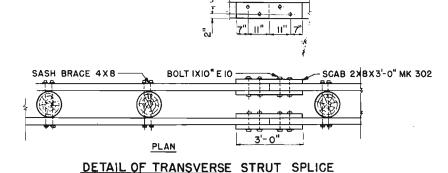




PILE ARRANGEMENT PLANS

REQUIRED BEARING CAPACITY OF PILES 18 TONS PER PILE





2 DRIFT BOLT 43-1636.07-22 D 22 3

TABLE A

LENGTH OF 4 X8 TRANSVERSE BRACING									
TOWER	BRA	CE	STRUT						
HEIGHT	LENGTH	MARK	LENGTH	MARK					
15'TO 21'	16'-0"	156	10'-0"	153					
23'TO 32'	18'-0"	157	12'-0"	154					
34' TO 44'	18'-0"	157	14'-0"	155					
46'TO 57'	18'-0"	157	16'-0"	156					
59' TO 69'	20'-0"	158	18'-0"	157					
71' TO 75	20'-0"	158	20'-0"	158					

BILL OF MATERIALS MATERIALS FOR FOUNDATIONS UNDER ONE TOWER											
							I2 PIL FOUNDA		24 PILE FOUNDATION		
LINE	DESCRIPTION	STOCK NO.	MARK	SIZE	LENGTH	WEIGHT	QUANTITY	WEIGHT	QUANTITY	WEIGHT	
1	PILE						12		24		

22"

24

72

48

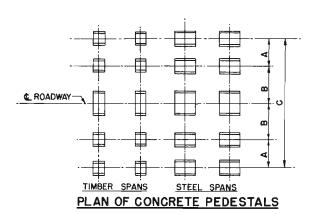
144

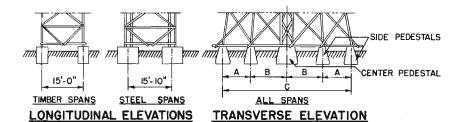
154 155

COMPANION SHEETS

GENERAL NOTES

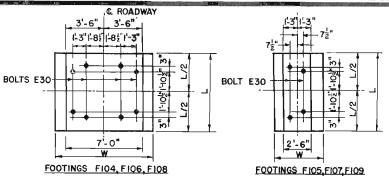
SYMBOLS

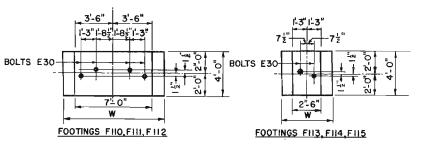




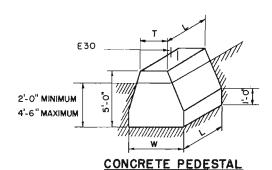
CONCRETE PEDESTALS

							IARK	
STORY	TOWER				TIMBER SP		STEEL SPANS	
	HEIGHT	A	В	С	END	CENTER	END	CENTER
					PEDESTAL	PEDESTAL	PEDESTAL	PEDESTAL
- 1	13'-4"	5'-5 %"	7'-8 !"	26'-4 1	F 115	F 112	F 109	F-108
	16'-0"	5'-8"	7'-11"	27'-2"	F 115	F 112	F 109	F108
	18'-0"	5'-10"	8'-1"	27-10	F ! 15	F 12	F109	F108
2	20'-0"		8,-3,	28'-6"	F 115	FII2	F 109	F108
	22'-0"	6'-2"	8'-5"	29'-2"	F 115	F 112	F109	F108
	24'-0"	6'-4"	8'-7"	29'-10"		F 112	F 109	FI08
	25'-10"	6'-6 å"	8'-9 ±"	30'-6±	F 115	F 11 2	F 109	F108
	28'-0"	6'-8"	8'-11"	31-2"	F 115	F 112	F 109	F106
	30'-0"	6'-10"	9'-1"	31'-10"	F 115	F 112	F109	F106
_	32'- 0"	7'-0"	9'-3"	32'-6"	F II5	FIL2	F 107	F106
3	34'-0"	7'-2"	9'- 5"	33'-2"	F 115	F II 2	F 107	F106
	36'-0"	7'-4"	9'-7"	33'-10"	F 115	F II 2	F 107	F 106
	38'-4"	7'-68"	9'-9 §"	34-82	F 115	F 11 2	F107	F106
	40'-0"	7'-8"	9'-11"	35'-2"	F 114	FIII	F 107	F106
	42'-0"	7'-10"	10'-1"	35'-10"		FIII	F 107	F106
	44'-0"	8'-0"	10'-3"	36'-6"	F 114	FIII	F 107	F106
4	46'-0"	8'-2"	10'-5"	37'-2"	F 114	FIII	F107	F106
	48'-0"		10-7"	37'-10"	F 114	FIII	F 107	F106
	50'-10"		10-10 # "	38'-10 [±]		F 111	F 107	F106
	53'-0"	8'-9	11'-0"	39'-6"	F 114	FIII	F107	F104
	55'-0"	8'-11"	11'-2"	40'-2"	F 114	FIII	F107	F104
	57'-0"	9'-1"	11'-4"	40'-10"	F 114	FIII	F 107	F104
5	59'-0"	9'-3"	11'-6"	41'-6"	F 114	FIII	F I 05	F104
	61'-0"	9'-5"	11'-8"	42-2"	F 113	FIIO	F105	F104
	63'-4"		11-108	43-0±	F 113	FIIO	F 105	F104
	65'-0"	9'-9"	12'-0"	43'-6"		FIIO	F105	F104
	67-0"	9'-11"	12'-2"	44-2"		FIIO	F 105	F104
1	69'-0"	10'-1"	12'-4"	44'-10"		FIIO	F105	F104
6	71'-0"	10'-3"	12'-6"	45'-6"		FIIO	F 105	F104
	73'-0"	10'-5"	12 - 8"	46-2"		FIIO	F 105	F104
	75'-10"	10-84"	12'-118"	47'-21	FII3	FIIO	F 105	F104
					1			





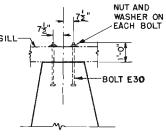
ANCHOR BOLT SETTING PLANS FRAMED TIMBER TOWERS FOR HIGHWAY SPANS



TYPICAL ANCHOR BOLT DETAILS

TABLE OF DIMENSIONS AND

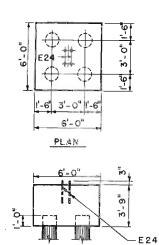
BILL OF MATERIALS FOR ONE PEDESTAL MACHINE BOLT 1 X 30" E 30 CONCRETE WITH SQUARE NUT MARK WIDTH WIDTH LENGTH (CUBIC AND TWO WASHERS (W) (L) (T) YARDS STOCK NO 43-2325.1-30 MAXIMUM) QUANTITY POUNDS F104 9'-0" 7'-0" 7'-6" F105 5'-6" 2'-6" 7'-6" F106 8'-6" 7'-0" 7'-0" 62 10.2 62 F107 5'-0" 2'-6" 7'-0" F108 8'-0" 7'-0" 6'-6" 5.2 31 9.1 62 F109 4'-6" 2'-6", 6'-6" F110 9'-0" 7'-0" 4'-0" F111 8'-6" 7'-0" 4'-0" F112 8'-0" 7'-0" 4'-0" 4.5 31 6.1 31 5.9 31 5.6 31 Fil3 5'-0" 2'-6" 4'-0" Fil4 4'-6" 2'-6" 4'-0" 16 3.0 16 F115 4'-0" 2'-6" 4'-0" 2.5 16



SHEET 84

COMPANION SHEETS

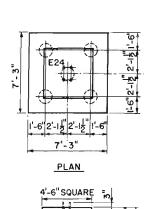
GENERAL NOTES SYMBOLS SHEET 154 155

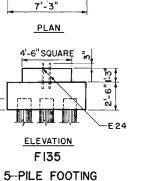


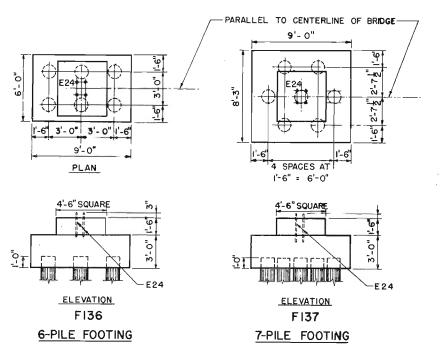
ELEVATION

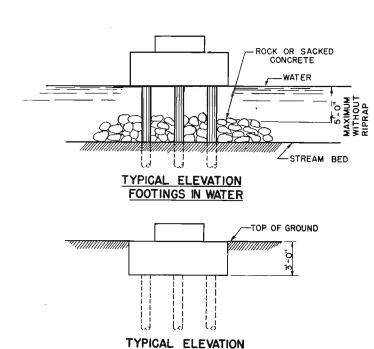
F134

4-PILE FOOTING





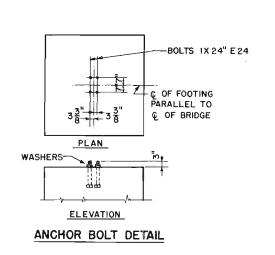




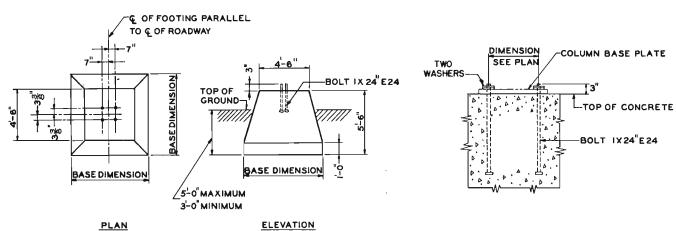
FOOTINGS IN SOIL

BILL OF MATERIALS FOR ONE FOOTING PILE BEARING CAPACITY 18 TONS

ADJACENT SPAN (FEET)	HEIGHT OF TOWER	FOOTING MARK NUMBER	NUMBER OF PILES	CONCRETE (CUBIC YARDS)	WITH SQUAR	
(1 221)					QUANTITY	POUNDS EACH
15'	57'OR LOWER	F134	4	5.0	4	6.5
15	59' TO 77'	F 135	5	5.8	4	6.5
20'	57' OR LOWER	F 134	4	5.0	4	6.5
20	59' TO 77'	F 135	5	5. 8	4	6.5
30'	57' OR LOWER	F 134	4	5.0	4	6.5
30	59' T077'	F 135	5	5. 8	4	6.5
40'	39' OR LOWER	F 134	4	5.0	4	6.5
40	41' TO 77'	F 135	5	5.8	4	6.5
50'	21' OR LOWER	F 134	4	5.0	4	6.5
50	23'T0 77'	F 135	5	5.8	4	6.5
60'	57' OR LOWER	F 35	5	5.8	4	6.5
00	59' TO 77'	F 136	6	7.1	4	6.5
701	39' OR LOWER	F!35	5	5.8	4	6.5
70'	41'T077'	F 136	6	7.1	4	6.5
30'	21' OR LOWER	F135	5	5.8	4	6.5
	23' TO 77'	F136	6	7.1	4	6.5
90'	57' OR LOWER	F 136	6	7.1	4	6.5
50	59'T077'	F 137	7	9.3	4	6.5







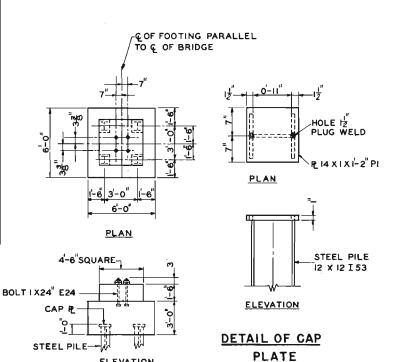
TYPICAL ANCHOR BOLT DETAIL

TOP OF GROUND SACKED CONCRETE WATER STREAM BED STREAM BED

CONCRETE PEDESTALS

TABLE OF DIMENSIONS AND BILL OF MATERIALS FOR ONE PEDESTAL WITHOUT PILES

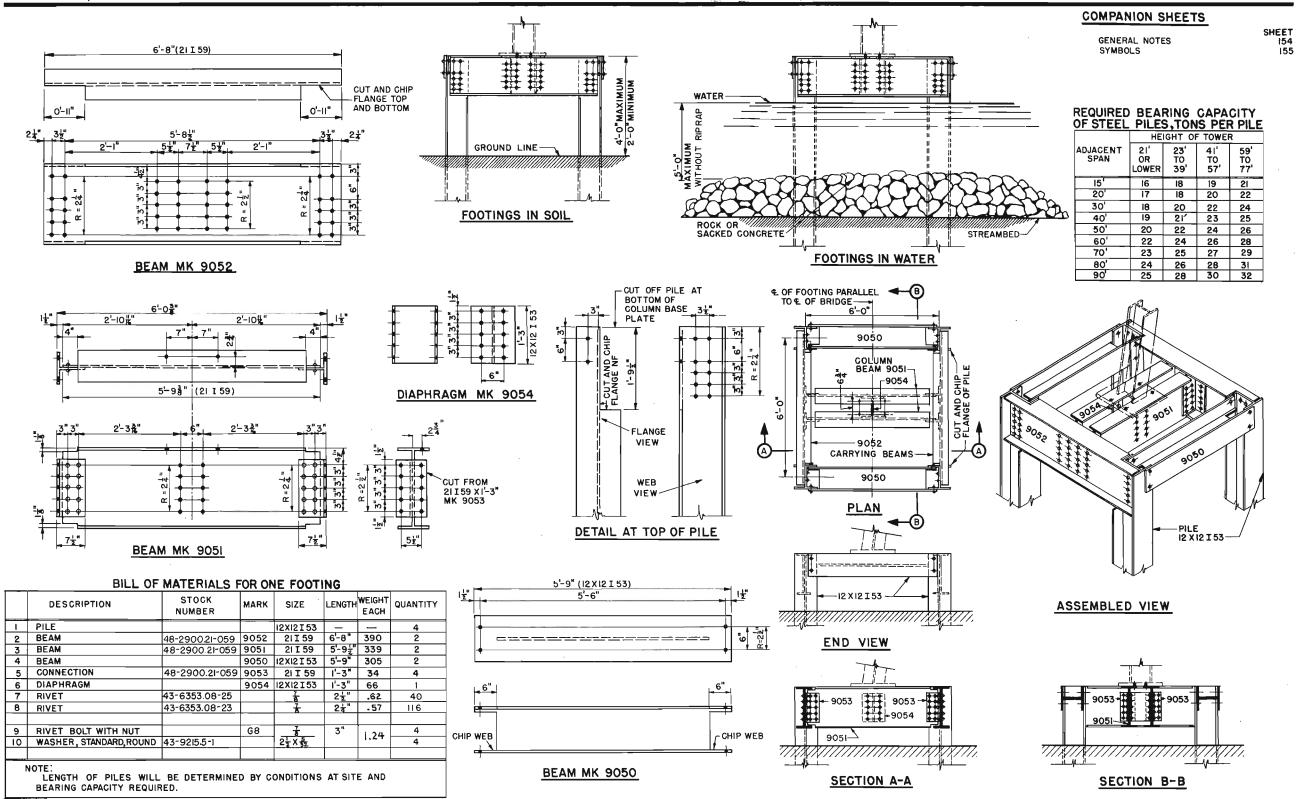
ADJACENT SPAN (FEET)	HEIGHT OF TOWER	MARK	BASE DIMENSION (FEET)	CONCRETE (CUBIC YARDS)	MACHINE BOL SQUARE NUT TWO WASHER NO 43-2325	AND S STOCK
	39'OR LOWER	F 121	7-0	7.4	4	26
15	41' TO 77'	F 122	8-0	9.1	4	26
20	21'OR LOWER	F 121	7 -0	7.4	4	26
20	23' TO 77'	F 122	8-0	9.1	4	26
30	21 OR LOWER	F 121	7-0	7.4	4	26
30	23' TO 77'	F 122	8-0	9.1	4	26
40	57'OR LOWER	F 122	8-0	9.1	4	26
40	59'TO 77'	F 123	9-0	10.8	4	26
50	57'OR LOWER	F 122	8-0	9.1	4	26
30	59'TO 77'	F123	9-0	10.8	4	26
60	39'OR LOWER	F 122	8-0	9.1	4	26
80	41'TO 77'	F 123	9-0	10.8	4	26
70	21 OR LOWER	F 122	8-0	9.1	4	26
	23'TO 77'	F 123	9-0	10.8	4	26
80	57'OR LOWER	F 123	9~0	10.8	4	26
80	59'T0 77'	F 124	10-0	12.9	4	26
90	57'OR LOWER	F 123	9-0	10.8	4	26
80	59 ['] T0 77'	F 124	10~0	12.9	4	26



ELEVATION
4-PILE FOOTING

REQUIRED BEARING CAPACITY OF PILES, TONS PER PILE , 4-PILE FOOTING HEIGHT OF TOWER AD. JACENI 21'OR 23' TO 41' TO 59'TO LOWER 39' 57' 77' SPAN 15 ' 16 18 19 21 20' 17 20 22 30' 18 20 22 24 40' 19 21 23 25 50' 20 22 24 26 60' 22 24 26 70' 23 25 27 80' 24 26 28 29 31 90' 25 28 30

BILL OF MATERI	IALS FOR ONE	FOC	TING WI	TH_S	TEEL	PILE	S	
DESCRIPTION	STOCK NUMBER	MARK	SIZE	LENGTH	EACH	NUMBER OF PIECES		AMOUNT
CONCRETE							CU.YDS,	5.1
PILE			12 X 12 I 53			4		
CAP PLATE	47-7844.1	PI	14X I	1-2"	55	4		
MACHINE BOLT WITH								
SQUARE NUT AND								
TWO WASHERS	43 - 2325100-240	E24	I	24"	6.40	4	POUNDS	26
WELDING ELECTRODE	46-3772.25-5		7 52				POUNDS	_4



345

345

345

541

450

450

80

80

53

50

TINU WEIGHT

.94

.97

1.00

1.09

24 16

2

56

28

16

4

9004 | 12X|2 | 153 | 6¹ 6" | 9005 | 12X|2 | 153 | 6¹ 6"

9009 I2XI2T53 8-6"

9010 12X12I53 8L6"

9016 12X12I53 146*

3

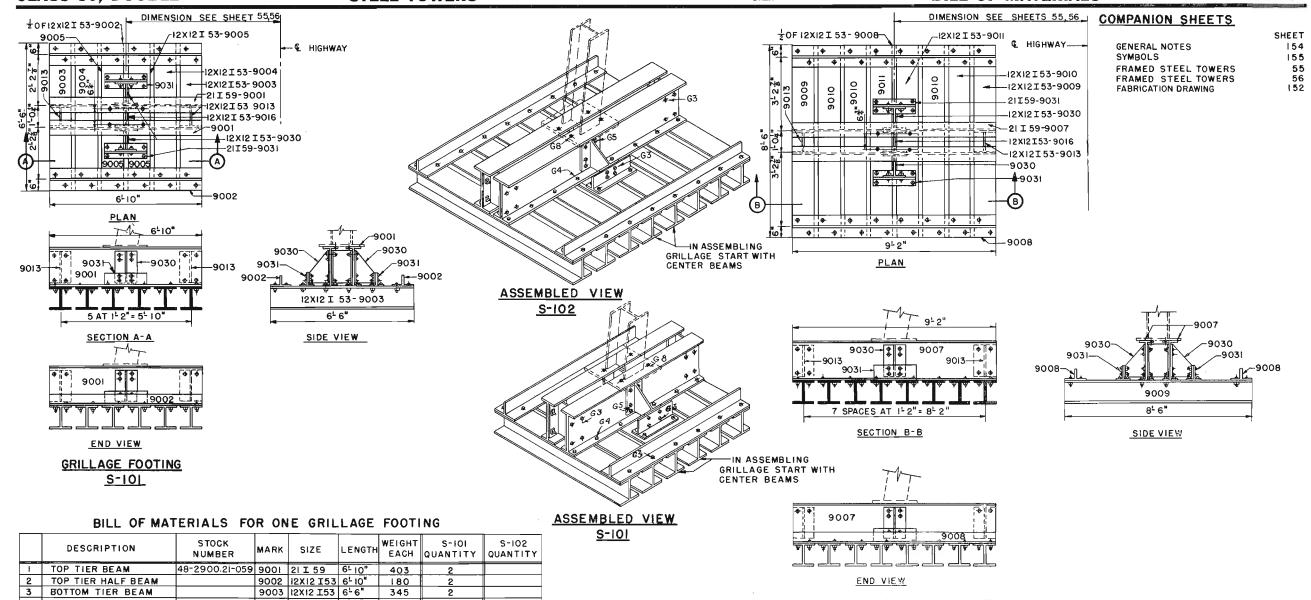
9011 | 12X12I53 | 8^L6" | 9013 | 12X12I53 | 1^L6"

48-2900.21-059 9007 21 I 59 9^L2" 9008 12X12I 53 9^L2"

9030 12X12I53 1^L6" 48-2900.2i-059 9031 21 I 59 1^L11"

G 5

G8



GRILLAGE FOOTING S-102

SCHEDULE FOR SELECTION OF GRILLAGE FOOTING FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

	SPAN		TINGS (FOOTINGS ON
DESCRIPTION	BETWEEN TOWERS	UP TO 21	23' TO 39'	41' TO 57'	59' TO 77'	ROCK ALL TOWER HEIGHTS
DOUBLE LANE CLASS 50	15'	S-101	S-101	S-102	S-102	5-101
DO	20'	S-101	S-101	S-102	S-102	S-101
DO	30'	S-101	S-102	S-102	S-102	S-101
DO	40'	S- 101	5-102	S-102	S-102	S- 101
DO	50'TO 90'	S- 102	5-102	S-102	S-102	S-101

BOTTOM TIER BEAM

BOTTOM TIER BEAM

5 BOTTOM TIER BEAM
6 TOP TIER BEAM
7 TOP TIER HALF BEAM

B BOT TOM TIER BEAM

9 BOTTOM TIER BEAM

10 BOTTOM TIER BEAM

18 RIVET BOLT AND WASHER

11 SEPARATOR

12 SEPARATOR

15 RIVET BOLT

16 RIVET BOLT

17 RIVET BOLT

I3 BRACE

14 BRACE

4 BOTTOM TIER BEAM

7 TOP TIER HALF BEAM 8 BOTTOM TIER BEAM

5 SEPARATOR

II RIVET BOLT

12 RIVET BOLT

13 RIVET BOLT AND WASHER
14 WELDING ELECTRODE 46-3772.2-7

9 BRACE

IO BRACE

6 TOP TIER BEAM

2

2

16

9015 | 12 X | 2 I 53 | 6'- 6" | 345

9016 12 X 12 I 53 1'-6" 80

9018 | 12X12 | 153 | 9'-2" | 243 | 9019 | 12X12 | 153 | 8'-6" | 450 | 9033 | 12X12 | 153 | 1'-6" | 53

TOTAL WEIGHT

15

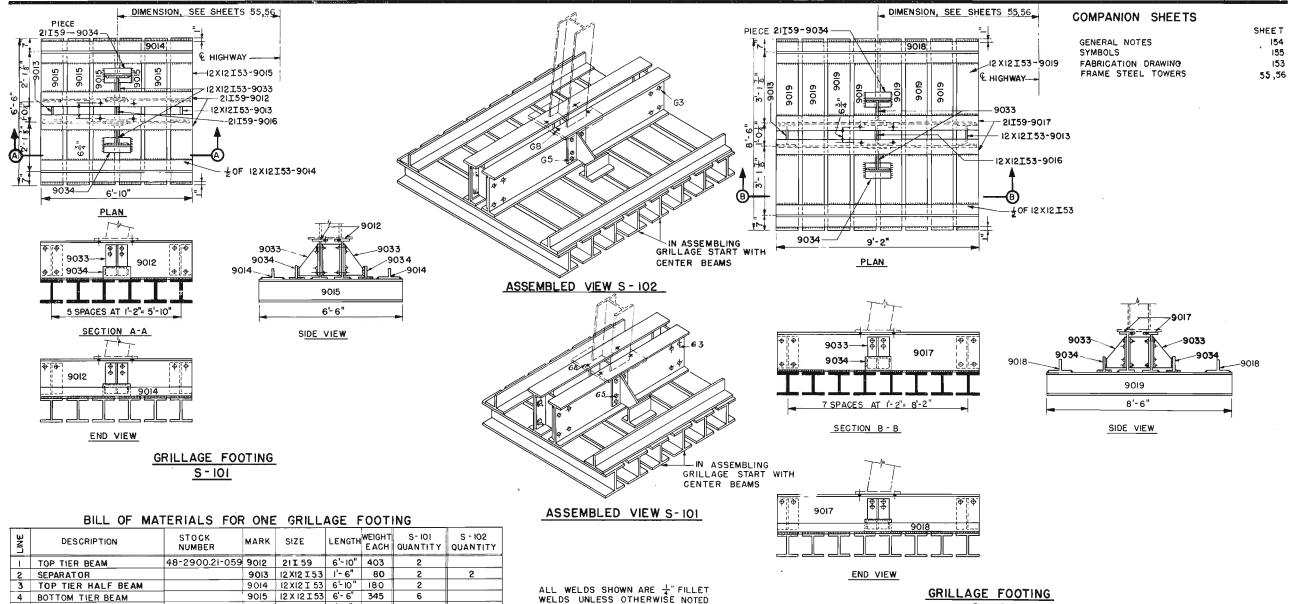
16

48:2900.21-059 9017 21 1 59 9'-2" 541

48-2900.2I-059 9034 2II 59 I'-2" 35

G5

G8

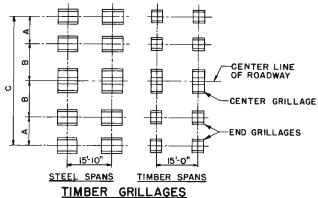


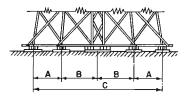
SCHEDULE FOR SELECTION OF GRILLAGE FOOTINGS FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

S - 102

- AITD 1 0 11 1		. 10111			
	FO	OTINGS (N SOIL		FOOTINGS
SPAN	HE	IGHT OF	ON ROCK		
BET WEEN TOWERS	UP TO 21'	23' TO 39'	41' TO 57'	59' TO 77'	ALL TOWER HEIGHTS
15'	S - 101	S- IOI	S-102	S-102	S - 101
20'	S- 101	S - 101	S-102	S-102	S-101
30'	S- [0]	S-102	S- 102	S - IO2	S-10I
40'	S-10I	S - 102	S- 102	S-102	S-10i
50'TO 90'	S-I02	S-102	S-102	S-102	S~101

GENERAL NOTES SHEET
SYMBOLS 155
TIMBER GRILLAGE AND BILL OF MATERIALS 90









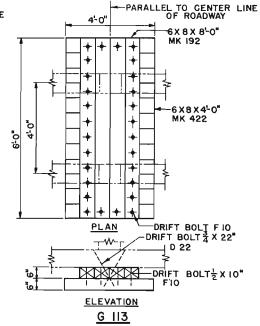
ALL SPANS
TRANSVERSE ELEVATION

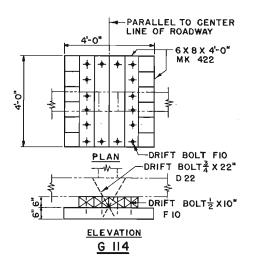
STEEL SPANS TIMBER SPAN

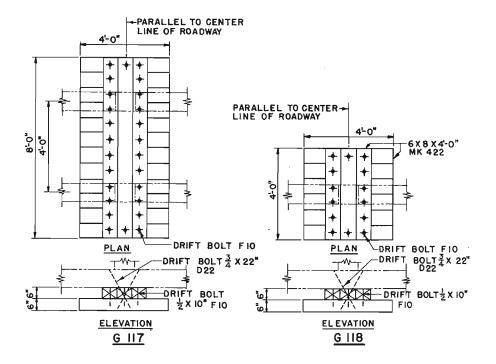
LONGITUDINAL ELEVATIONS

MBER	GRILLA	GE FOOTIN	GS

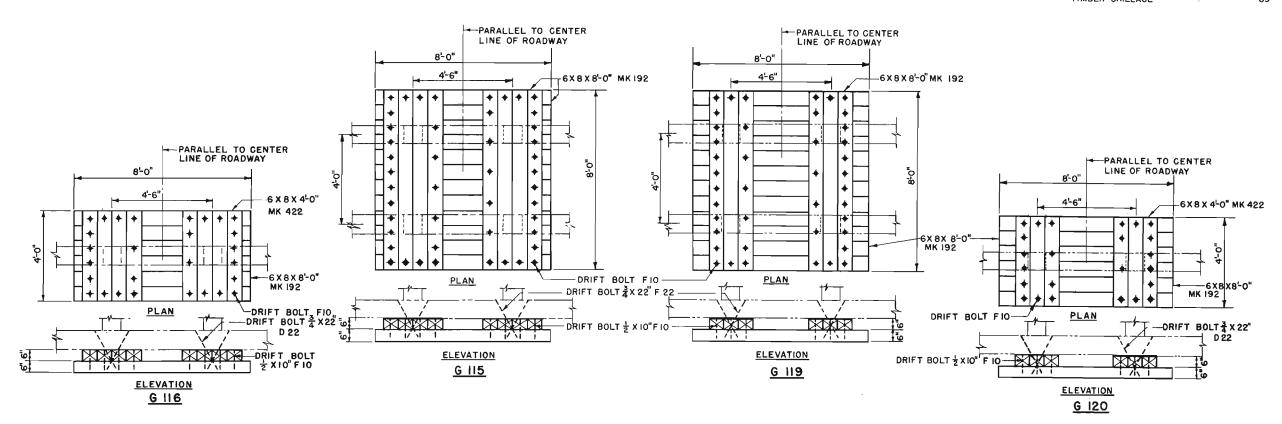
					FOOTING MARK								
			_	_	TIMBER S	PAN 15'	STEEL SPAN	15' TO 90'					
STORIES	HEIGHT	Α	P	С	END	CENTER	END	CENTER					
	-				GRILLAGE	GRILLAGE	GRILLAGE	GRILLAGE					
	13'-4"	5'-55'	7'-88"	26-42	G-118	G - 120	G-/117	G-119					
	16'	5'-8"	7'-11"	27-2 "	G-118	G - 120	G-117	G-119					
	18'	5'- 10"	8'-1"	27º 10"	G-118	G ~ 120	G-117	G-119					
2	20'	6'-0"	8'-3"	28'-6"	G-118	G - 120	G-117	G-119					
-	22'	6'-2"	8'-5"	29'-2"	G - 118	G - 120	G-117	G-119					
	24'	6'-4"	8'-7"	29'-10"	G-118	G - 120	G-117	G-119					
	25-10	6'- 6 8	8 9 9 A	30'-6 ¹	G-118	G - 120	G-117	G-119					
	28'	6'-8"	8'-11"	31-2	G-118	G - 120	G-117	G-119					
	30 ⁴	6'-10"	9'-1"	31'-10"	G-118	G - 120	G-117	G-119					
3	32'	7'-0"	9'-3"	32'-6"	G-118	G - 120	G-117	G-119					
•	34'	7'-2"	9' -5"	33-2"	G-118	G - 120	G-117	G-119					
	36	7'-4"	9'-7"	33-10	G-118	G ~ 120	G-117	·G-I19					
	38'-4"	7'-6	9'-9	34-82	G-118	G - 120	G-117	G-119					
	40'	7'-8"	9'-II"	35-2"	G-118	G - 120	G-117	G-119					
	42'	7 - 10"	10'-1"	35'-10"	G-118	G - 120	G-117	G-119					
4	44'	8'-0"	10'-3"	36'-6"	G-118	G - 120	G-117	6-11-9					
"	46'	8'-2"	10'-5"	37'-2"	G-118	G - 120	G-117	G-119					
	48'	8'-4"	10'-7"	37'-10"	G -118	G ~ 120	G-117	G-119					
	50'-10"	8'-78"	10,-10%	38-10	G-118	G - 120	G-117	G-119					
	53'	8'-9"	11'-0"	39-6"	G-114	G - 116	G-113	G-115					
	55'	8'-11"	11'-2"	40-2"	G-114	G - 116	G-113	G-115					
5	57'	9'-1"	11'-4"	40-10"	G-114	G - 116	G-113	G-115					
	59'	9'-3"	11'-6"	41'-6"	G-114	G - 116	G-113	G-115					
	61	9'-5"	11,-8,	42-2"	G-114	G - 116	G-113	G-115					
	63'-4"	9'-78"	い'-10ई"	43'-0½"	G -114	G - 116	G-113	G-115					
	65'	9'-9"	12'-0"	43'-6"	G- 4	G - 116	G-113	G~115					
	67'	9'-11"	12'-2"	44'-2"	G -114	G - 116	G-113	G-115					
6	69'	lQ-I"	12'-4"	44 10"	G-114	G - 116	G-113	G-115					
	71'	10'-3"	12'-6"	45'-6"	G -114	G - 116	G-113	G-115					
	73'	10'-5"	12'-8"	46'-2"	G -114	G - 116	G-113	G -115					
	75-10"	16'-8밥	12'-11뿝	47'-22	G -114	G - 116	G-113	G-115					







SHEET
| GENERAL NOTES | 154
| SYMBOLS | 155
| TIMBER GRILLAGE | 69



BILL OF MATERIALS FOR ONE TIMBER GRILLAGE

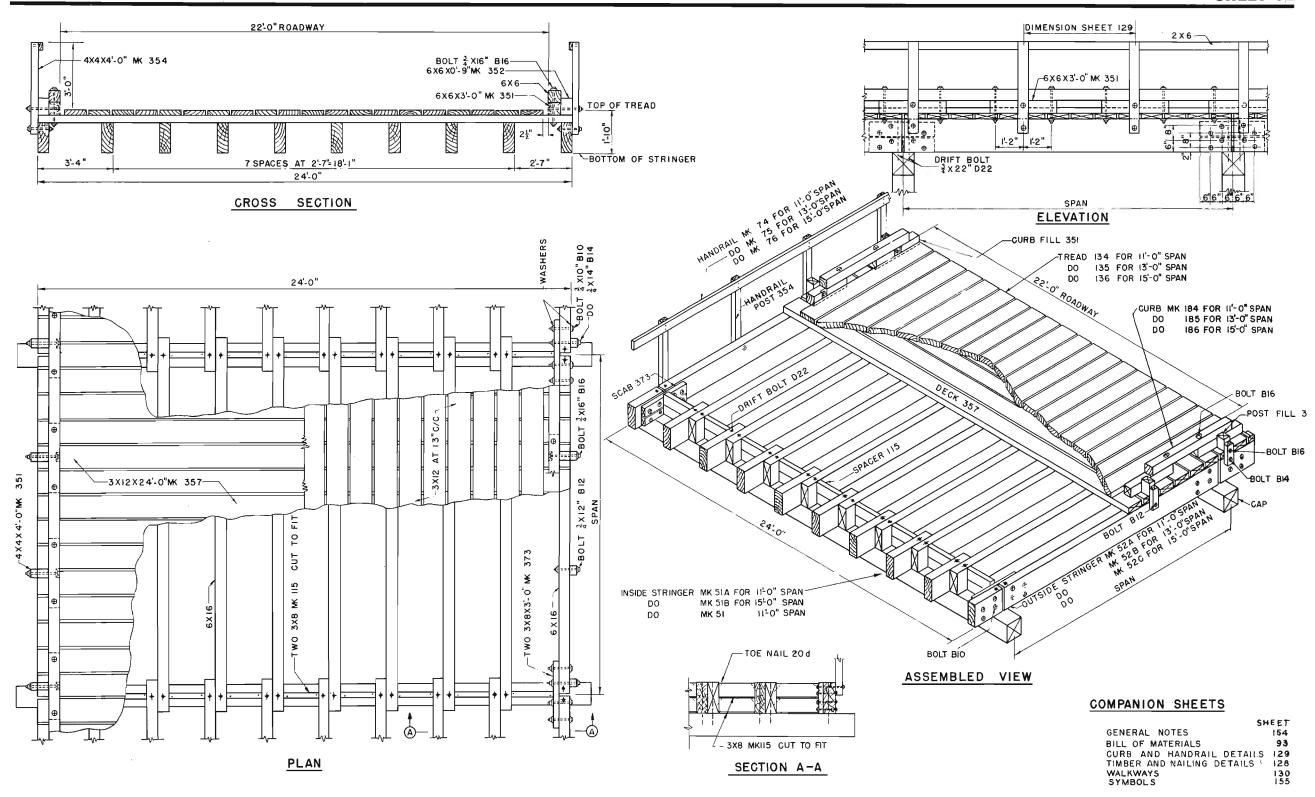
											_				,		r .						
				SRILLAGE NUMB	BER		Gl	13	G	114	G11	5	Gi	16	61	17	G1	18	Gll	. 9	6 ;	120	
INE	DESCRIPTION	STOCK NO	WARK	SIZE (INCHES)	LENGTH	WEIGHT (POUNDS)	QUANTITY	FBM	YTITMAUG	; Bv	QUANTITY	FBM	YII INAUQ	F8м	QUANTITY	FBM	QUANTITY	F8M	YTITHAUÇ	F8M	QUANTITY	F8¥	LIN
	LUMBER, SOFT WOOD									•													
1	GRILLAGE	39-3360.09	192	6 X 8	8'-C"	120	4	128			20	640	6	192	3	96			18	576	6	192	1
2	DO	39-3360.08	422	6 X 8	4 * - 6"	60	12	192	10	160			В	128	12	192	9	144			6	96	2
	STEEL HARDWARE, BLACK																						
3	DRIFT BOLT	43-1636.07-22	022	3/4	22"	2.75	4		2		8		4		4		2		8		4		3
4	0.0	43-1636.05-1	F16	1/2	10"	0.6	28		16		46		28		26		14		42		24		4

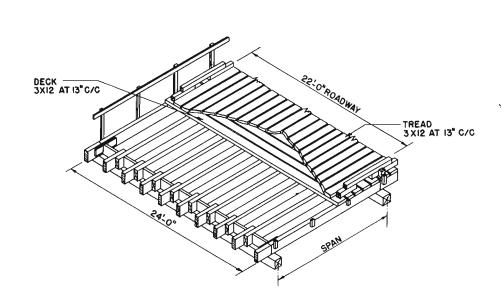
SETS OF DRAWINGS FOR DIFFERENT CONSTRUCTION UNITS

SHEET 91

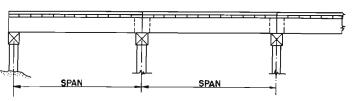
	SET NUMBER 25D-1		SET NUMBER 25D-5		SET NUMBER 25D-10
	TIMBER SPANS		STEEL TOWERS FOR STEEL SPANS		STEEL PILE BENTS AND PIERS FOR STEEL SPANS
	(11 to 15 feet long)	SHEET	(15 to 77 feet high)	SHEET	(1 to 20 feet high)
SHEET		SHEET	·	SHEET	
92	General views	55	General views of 69- to 77-foot towers	116	Riveted construction: general views of bents
93	Bill of materials	56 57	General views of 15- to 67-foot towers Bill of materials common to all towers	117	Riveted construction: general views of piers
128	Details of floor construction and attachment of nailers to steel stringers	58	Bill of materials which vary with tower height	118 119	Riveted and welded construction: bill of materials
129	Details of handrail and curb	59	Riveted construction: fabrication of cap beam, strut, and pin	120	Welded construction: general views of bents Welded construction: general views of piers
130	General views and bill of materials for walkway	102	Riveted construction: fabrication of cap beam	150	Riveted construction: fabrication of cap beams, corbels, bracing, and connec-
154 155	General notes Structural symbols	60	Riveted construction: fabrication of columns		tions
133	Structural symbols	61	Riveted construction: fabrication of columns and struts	151	Welded construction: fabrication of cap beams, corbels, and bearing plates
		62 103	Fabrication of rod bracing Details and bill of materials for shims under stringers of different depths; super-	154	General notes
	SET NUMBER 25D-2	103	structure anchor belts	155	Structural symbols
	2777 27 112	226	Welded construction with rod bracing: cap beams and column splices welded		CET VIIIVADED OF DATA
	STEEL SPANS		in fabrication and erection		SET NUMBER 25D-11
	(15 to 90 feet long)	227	Welded construction with welded angle bracing; cap beams and column splices		TIMBER SILL AND PILE FOUNDATIONS FOR TIMBER TOWERS
		164	welded in fabrication and erection		
94 95	General views Bill of materials: steel for riveted construction; lumber and hardware for stan-	154 155	General notes Structural symbols	121	General views
93	dard plank floor	133	NOTE: When welded construction is used in accordance with sheets 226	154	General notes
96	Bill of materials: steel for welded construction; lumber and hardware for alter-		or 227, bills of materials on sheets 57 and 58 and fabrication	155	Structural symbols
	nate laminate floor		details on sheets 59, 60, and 61 must be adjusted in the field.		
128	Details of floor construction and attachment of nailers to steel stringers		When sheet 227 is used, sheet 62 does not apply.		SET NUMBER 25D-12
129	Details of handrail and curb				
130 131	General views and bill of materials for walkway Riveted construction: fabrication of stringers 501 to 511 and of diaphragms 527		SET NUMBER 25D-6		CONCRETE PEDESTALS FOR TIMBER TOWERS
131	and 528				
132	Riveted construction: fabrication of stringers 516 and 521 and of bearing plates		TIMBER ABUTMENTS FOR TIMBER SPANS	122	General views and bill of materials
	3500 and 3501			154	General notes
133	Riveted construction: fabrication of stringers 513 and 523			155	Structural symbols
135	Riveted construction: fabrication of stringers 515 and 522 Riveted construction: fabrication of stringers 512 and 525	104	General views of pile abutments; bill of materials for pile and grillage abut- ments		CET NUMBER OCK 10
136 138	Riveted construction: fabrication of stringers 520 and 524	105	General views of grillage abutments		SET NUMBER 25D-13
139	Welded construction: fabrication of stringers 501W to 511W, and of diaphragms	154	General notes		CONCRETE PEDESTALS FOR STEEL TOWERS
	C3 and C4	155	Structural symbols		
140	Welded construction: fabrication of stringers 512W and 525W			123	General views and bill of materials
141	Welded construction: fabrication of stringers 513W, and 522W, and 523W		CET NUMBER OFF 7	55	General views of 69- to 7.7-foot towers
142 143	Welded construction: fabrication of stringers 514W, 515W, and 516W Welded construction: fabrication of stringers 520W and 521W		SET NUMBER 25D-7	56	General views of 15- to 67-foot towers
154	General notes		ABUTMENTS FOR STEEL SPANS	154	General notes
155	Structural symbols			155	Structural symbols
	·	106	General views of timber pile abutments; bill of materials for timber pile and		
			timber grillage abutments		SET NUMBER 25D-14
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146 147	Details of bracing connections Details of bracing connections				TIMBER GRILLAGE FOUNDATIONS FOR TIMBER TOWERS
147	Details of bracing connections and of columns; column dimensions	114	General views		
149	Details of towers supporting both timber and steel spans	115	Bill of materials; details of piers supporting one steel and one timber span	127	General views and bill of materials
154	General notes	154	General notes	154	General notes
155	Structural symbols	155	Structural symbols	155	Structural symbols

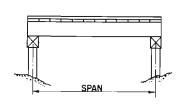
INDEX DRAWING

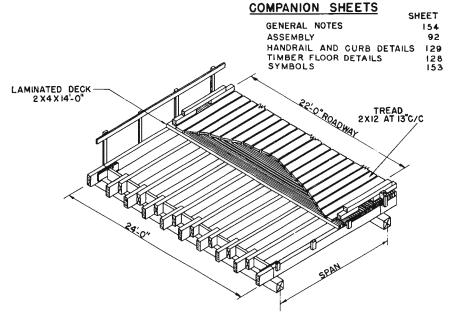




HIGHWAY CLASS 25, DOUBLE-LANE

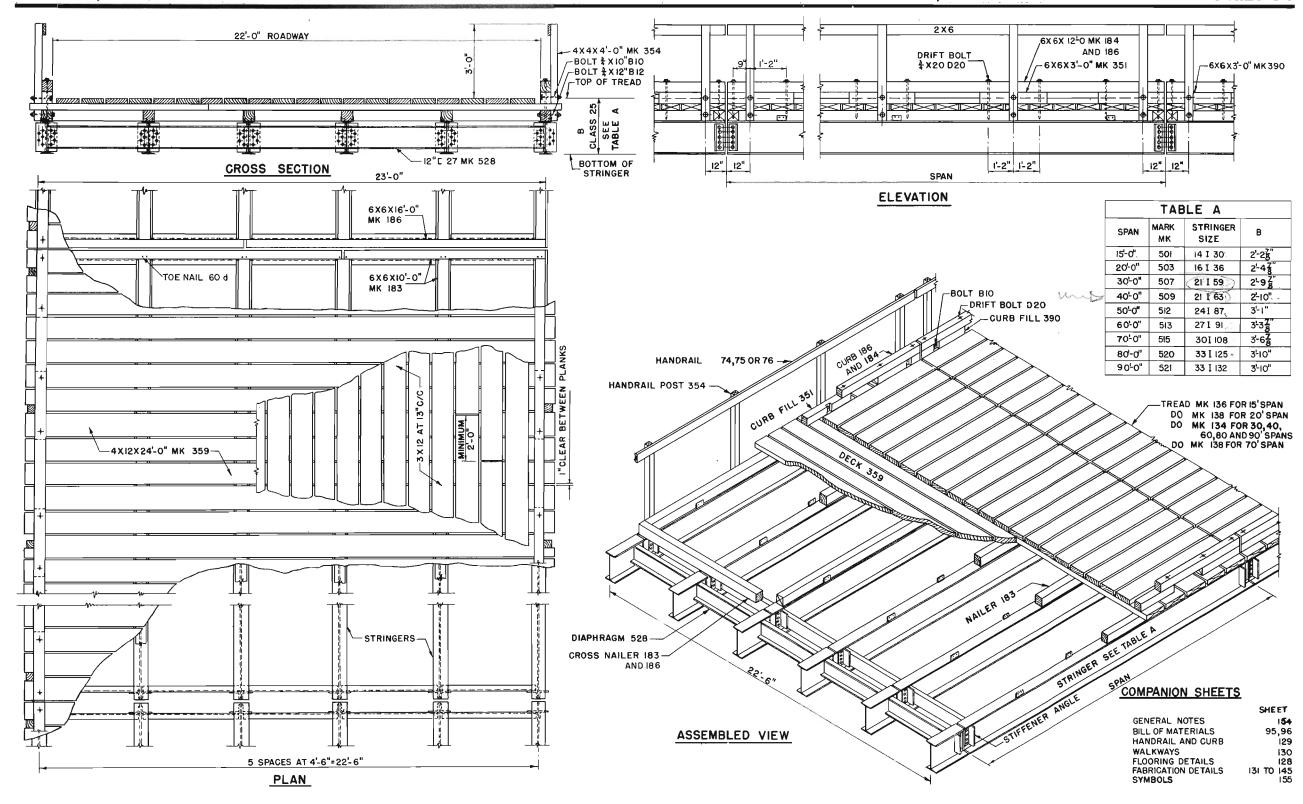






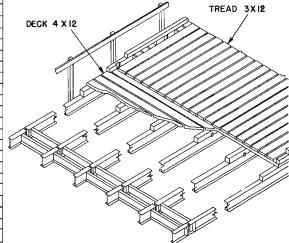
							11'0"	SP4N	13'0'	SP4N	15'0"	SPAH
.INE	DESCRIPTION	STOCK NUMBER	SIZE (INCHES)	LENGTH	Mark	WEIGHT (POUNDS)	QUANTI IY	FBM	QUANTITY	FBM	COUNTLITA	FBM
	LUMBER, SOFTWOOD											
	STRUNGERS		6 X 16	16'0"	51C	480					8	1024
.2	00		6 X 16	16'0"	52C	490					2	256
3	<u> </u>		6 X 16	1410*	51B	420			8	896		
4	20		6 X 16	14'0"	528	420			2	224		
5	∞		6 X 16	12'0"	514	360	8	768				
6	∞		6 x 16	12'0"	522	360	2	192				
7	SPACER (STRINGER)	39-3330.08	5 x 8	14'0"	115	105	2	55	2	56	2	56
8	SCAB	39-3330.08	3 × 8	310-	373	23	4	24	4	24	4	24
9	DECK	39-3952.12	3 X 12	24'0=	357	270	고 10	720	л 15	864	ш ₁₄	1008
10	TREAD	39-3330.12-16	3 x 12	16'0"	136						20	960
11	DO	39-3330.12	3 X 12	14'0*	135	158			20	840		
12	DO	39-3952.12-12	3 X 12	12'0"	134	135	20	720				
13	CURS	39-3360.05-16	6 x 6	16'0"	186	180					2	96
14	DO	39-5560.06-14	6 4 5	14'0"	185	158			2	84		
15	DO	39-3360.06-12	6 X 6	12'0"	134	135	2	72				
16	CURB FILL	39-5360.06	6 (6	3'0"	351	34	4	36	4	36	6	54
17	HANDRAIL POST	39-3340.04	4 x 4	4"0"	354	20	4	22	4	22	6	32
18	POST FILL	39-3360.06	6 x 6	0'9"	352	8	4	9	4	9	6	14
19	HANDRAIL	39-3880.06-16	2 X 6	16'0"	76	60					2	32
20		39-3880.06-14	2 × 6	14'0"	75	52			2	28		
21	DO	39-3880.06-12	2 X 6	12'0"	74	45	2	24				
	-					•						
	STEEL HARDWARE, BLACK		1									
22	MACHINE BOLT WITH SOUARE	43-2325.07-16	3/4	16"	816	2.52	12		12		18	
	NUT AND THO WASHERS					<u> </u>						
23		45-2325.07-144	3/4	14*	B14	2.27	2_		2	_	2	
24	00	43-2325.07-124	3/4	12"	B12	2.02	2		2		4	
25		43-2325.07-1	3/4	10"	B10	1.77	14_		14		14	
26	DRIFT BOLTS	43-1636.07-22	3/4	224	D22	3.0	20		20		20	
27	WIRE SPIKE	42-8488.035-07-	5/16 X 7			. 15	100		120		140	
28 29	WIRE NAIL	42-6028.3-5 42-6028.3-2	50 d			.10	200		240		280 32	
	PROVIDE TWO ADDITIONAL HAN TWO POST FILLS FOR EACH BR			WO SPACER	S AND				1			

							11'0	SPAN	13'0'	SPAN	15'0"	SPAN
.INE	DESCRIPTION	STOOK NUMBER	SIZE (INCHES)	LENGTH	MARK	WEIGHT (POUNDS)	QUANTITY	FBM	QUANTI (Y	F84	QUANTITY	F814
	LUMBER, SOFTWOOD											
_1	STRINGERS		6 X 16	15'0"	51C	480					8	1024
2	∞	A-3471 - 1-042 - 110	6 X 16	16'0"	52C	480					2	256
3	∞		6 X 16	14'0=	518	420			8	896		
4	∞		6 X 15	14'0"	528	420			2	224		
5	<u> </u>		6 X 16	12'0"	514	360	8	768				
6	00		6 X 16	12'0"	524	360	2_	192				
7	SPACER (STRINGER)	39-3330.03	3 X S	14'0-	115	105	2_	56	2	56	2	56
В	SCAB	39-3330.08	3 x 8	3'0"	373	25	4	24	4	24	4	24
9	DECK	39-3880.04	2 X 4	24'0"	360	60	82	1312	96	1535	111	1773
10	TREAD	39-3228.12-12	2 X 12	12'0"	104	90	20	480				
11.	00	39-3228.12-14	2 X 12	14'0"	105	105			20	560		
12	DO	39-3228.12-16	2 X 12	15'0"	106	120					20	640
13	CURB	39-3360.06-12	6 X 6	12'0"	134	135	2	72				
14	00	39-3360.06-14	6 X 6	14'0"	185	158			2	84		
15	00	39-3350.06-16	6 4 6	16'0"	186	180					2	96
16	CURBFILL	39-3560.06	5 x 5	3'0"	351	34	4	36	4	36	6	54
17	HANDRAIL POST	39-3340.04-08	4 × 4	4'0=	354	20	ц	22 .	4	22	4	22
18	POST FILL	39-3360.06	6 X 5	0'9"	352	8	ц	9	4	9	6	14
19	HANDRATL	39-3880.06-12	2 x 6	12'0"	74	45	2	24				
20	00	39-3880.06-14	2 x 6	14'0"	75	52			2	28		
21	20	39-3890.06-16	2 X 6	16'0"	76	60					2	32
	STEEL HAROWARE, BLACK											
22	MACHINE BOLT WITH SOURCE	43-2325.07-16	3/4	16*	B16	2.52	12		12		18	
	NUT AND 2 WASHERS											
23	DO	43-2325.07-144	5/4	14*	814	2.27	2		2		2	
24	00	43-2325.07-124	3/4	12*	B12	2.02	2		2		и	
25	DO	43-2325,07-1	3/4	10 "	B10	1.77	14		14		14	
26	ORIFT BOLT	43-1636.07-22	3/4	22*	D22	3.00	20		20		20	
27	WIRE NAIL	42-6028.3-5	50 d			. 11	1800		2100		2400	
28	WIRE NAIL	42-6028.3-2	20 d			.0#	12		12		16	

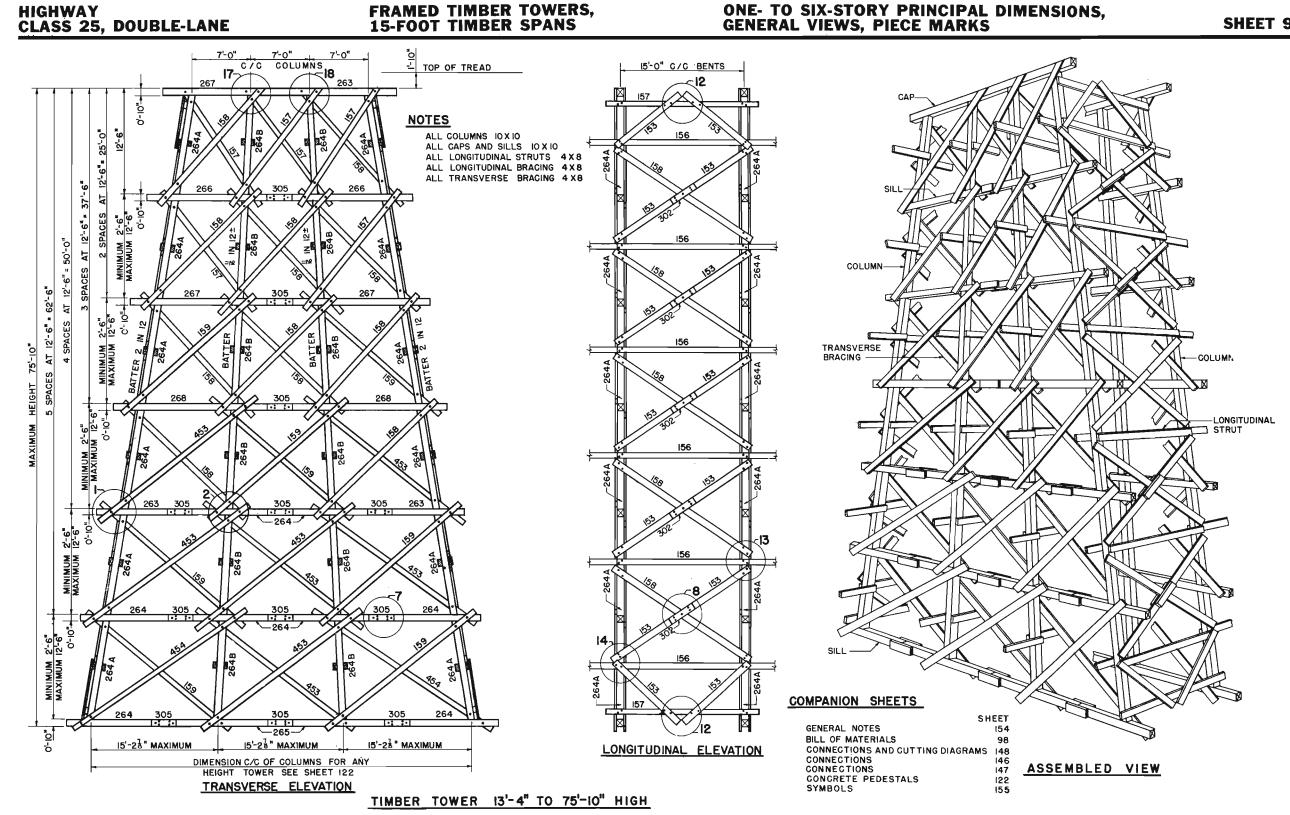


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Marches Services 1985 19	THE	DESCRIPTION	STOCK NO	MARK	SIZE		UNIT			1				i i												11945
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1 100, 1991-191-191 11 11 11 17 17 17 17	2							20	960	1	1200					- 70	3000		4200	10,	4200	100	4800			-
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2 Georgia	5	HAILER	39-3360.06-16	186	.6 X 6	16'-0"	180	2	96	2	96	2	96	2		2	96	2		 		2				_
Second Content	6	DO	39-3360.06-1	183	6 X 6	10'-0"	113	11	330	14	420	20	600	26	780	32	960	38	1140	44	1320	60	1500	56	1680	6
1-	7	CURB	39-3360.06-16	186	6 X 6	16'-0"	180	2	96	3	144	1	48	6	288	4_	192	٩	432	11	538	12	576	14	672	7
Machine Mach	8	DO	39-3360.06-12	184	6 X 6	12'-0"	135					4	144			4	144									В
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11			1							8	43	12	64	14	75	18	96	20	107	24	128	26	155	30	150	
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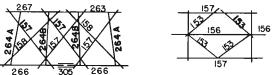
																										SHEE
6	BILL OF MATERIALS FOR C	NE SPAN																								STEEL SPANS, 15-TO 90-FOOT 9
					SPAN LENGT	TH	15	51	20	'	-	101	44			0'	+	60'		0'	-	0'	90	יי		BILL OF MATERIALS, RIVETED 9
<u> </u>		Т		_	STRINGER S		14 1	30	16	36	21	I 59	21	63	24	I 67	27	I 91	30	I 108	33	L 125	33	132		TIMBER FLOOR DETAILS 12 HANDRAIL AND CURB DETAILS 12
LINE	DESCRIPTION	этоск но	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	CHANTITY	FBM	QUANTITY	FBM	ÓTIMO TI J	r FBM	QUANTITY	FBM	QUARTET	Y FBM	QUANTITY	FBM	QUANTETY	FBM	CHANTELLA	FBM	*URITY	F8M	LINE	WALKWAYS FOR HIGHWAY BRIDGES 13
Н.	LUMBER, SOFT WOOD					(FOLINGS)	1	l .	I.	<u> </u>	1				Ш		Ш							l		FABRICATION DRAWINGS 131 T
	FLOOR, TREAD	39-3228.12-2	108	2 X 12	20'-0"	150			20	800															1	JUNCTIONS, TIMBER, AND STEEL-STRINGER SPANS 14
2	00	39-3228, 12-16	106	2 X 12	16'-0"	120	20	640							\bot		ļ				100	3200			2	GENERAL NOTES 15
3	DO	39-3228, 12-14	105	2 X 12	14'-0"	105				<u> </u>	50	1200	67	1608	72	2016	100	2400	100	2800			150	3600	3 4	SYMBOLS 15
3	FLOOR DECK	39-3228.12-12 39-3228.06-14	104	2 X 12 2 X 6	12'-0"	90 53	111	1554	148	2072	221	3094	295	4130	369	5166	443	5202	516	7224	590	8260	664	9296	3	
6	DO	39-3228.06-1	73	2 X 6	10'-0"	38	111	1110	148	1480	221	2210	295	2950	369	3690	443	4430	516	5160	590	5900	664	6640	6	
	NAILER	59-3360.06-16	186	6 X 6	16'-0"	180	2	96	2	96	2	96	2	96	2	96	2	96	2	96	2	96	2	96	7	
	00	39-3360,06-1	183	6 X 6	16'-0"	113	2	330 96	14	420 144	20	600 48	26	780 288	32	960 192	38	1140 432	11	1320	50	1500		1680	6 q	
10	DO .	39-3360.06-16 39-3360.06-12	184	6 X 6	12'-0"	_	 	90	^	144	4	144	│	200	+ :	144	 '	432	1 11	528	12	576	14	672	10	
11	CURB FILL	39-3360.06	390	6 X 6	31-0*	34	4	36	4	36	4	36	4	36	4	36	4	36	4	36	4	36	4	. 36	11_	
12	<u>DO</u>	39~3360.06	351	6 X 6	3'-0*	34	2	18	4	36	8	72	70	90	14	126	16	144	20	180	22	198	26	234	12	
	HANDRAIL POST	39-3340.04 39-3880.06-16	354 76	2 X 6	16'-0"	20 60	6 2	32 32	8	43	12	64	14	75	18	96	20	107	24	128	26	139	30	160	13	
15	DO DO	39-3880.06-14	75	2 X 6	14'-0"	53			5	42	5	70	6	84	8	113	9	126	11	154	12	168	14	196	15	
5	STEEL, STRUCTURAL			_	_				п				,		-		,									
$\overline{}$	STRINGER	48-2900, 33-152	521W	33 I 132	9'-10 1/2"		<u> </u>		1					ļ <u>.</u>	₩	ļ						_	12		16	
17	00 00	 	 		39'-10 1/2" 39'-10 1/2"				-		1		1		#				$\parallel \parallel$	-	6	-	6		17	
19	DO	46-2900.33-125	520W	33 I 125	40'-0"	_															6	Ī			19	
20	DO	45-2900.3-108	515W	30 I 108	40'-0=	4320													6						20	TREAD 2 X 12
21		45 275517 255		X 1 100	29'-10 1/2*		├		!				-	-	#	-	 		5			_			21	DECK 2 X 6
22	DO	48-2900.27-091	513W	27 1 91	19'-10 1/2"		-		 				╂	-	+		6			-		-			28	ON EDGE
24	00	** *** ****	512W	24 1 87	40'-0"		 	Ι.	<u> </u>				1		6							\neg			23	
25	00	48-2900.24-087	312M		9'-10 1/2"										6										25	
26	DO	46-2900.21-063		· -	201 -101/2	_			<u> </u>				6		#										26	
27 28	DQ	48-2900.21-059 48-2900.16-036			29'-10 1/2"			-	-		6		-		+	 	<u> </u>		-			-			27 28	
29	00	48-2900.14-030	_		14'-10 1/2"	_	6								1							ı			29	
	DIAPHRAGM	48-3790.12-21	C4	12 € 20.7		85	10		10		15		15		15		20		20		25		25		30	
31 32	STIFFENTR PLATE	47-7844.04 47-7844.04	P10 P23	4 x 3/8 4 x 3/8	2'-0"	10			1				1		+		48		48		60		60		31 32	
33	00	47-7844.04	P20	4 X 3/8	1'-6"	8			 			-			36										33	
34	00	47-7644.04	P6	4 x 3/8	1'-7"	8					36		36		<u> </u>										34	
35		47-7844.04	P2	4 X 3/8	1'-2"	6	Ļ		24			ļ	-		₩							_		$-\!\!+\!\!$	35	
36 37	NEB SPEACE PLATE	47-7844.04 47-7844.04	P1 P9	4 X 3/8	1'-6"	22	24		1		<u> </u>		+		+				12		12	\dashv	24	-	36 37	
38	DO DO	47-7844.04	P19	9 X 3/8	1'-0"	11	1		1				 		12				**		**	\neg		-	38	
39	DQ .	47-7844,04	P22	9 X 3/8	1'-5"	14					_		1				12								39	
40	FLANGE SPLICE PLATE	47-7844-1	P43	9 X 1 7 X 1/2	4'-0"	122			₩				-		#								12		40	
41	DQ	47-7844,05	P8 P11	9 x 1/2	3'-0"	22 46			#				1		+					- 1	6		12	-	42	
43	00	47-7844,06	P18	7 x 5/8	4'-0"	60									. 6											BILL OF MATERIALS FOR FLOOR AND STRINGER COMBINATION
44	DQ	47-7844.04	P21	8 x 3/8	2'-0"	20											6								44	SHEET
45		47-7844.04	P26 P27	9 x 3/8	2'-4"	34 71					 	 	1		 				6	∦					45	I. STANDARD PLANK FLOOR 95 RIVETED STEEL DETAILS 95 HARDWARE 95
46	DO DO	47-7844.1	P27	9 X 1	2'-8"	82									+	\vdash			6	$-\parallel$	6		-+	\dashv	46	HARDWARE 95
48	00	47-7644.03	P30	9 X 1/2	3'-10"	59					t	 									-		12		48	
49	DO	47-7844, 3	P32	8 X 1	3'-6*	95											6								49	WELDED STEEL DETAILS 96
50	DQ	47-7844.04	P.37	7 x 3/8	2'-0"	18									6				-	$-\!$					50	HARDWARE 95
	HALLER ATTACHENT PLATE	47-7644,03	 	2 x 1/4 7/32	0'-4"	0.6	24		30		42		54		66 28 LB		78 77 LB		90 89 L8		102 138 LB		114 9 LB		52 52	3. ALTERNATE LAMINATED FLOOR 96
53		46-3772-2-7		3/16			22 LB		24 LB		40 LB		43 LB		66 LB		59 LB		71 LB		60 LB		8 LB		53	RIVETED STEEL DETAILS 95 HARDWARE 96
	STEEL HARDWARE, BLACK								11	1	1									- 1		n		n]	**
	NOTITIE BOLT, SOURCE NUT, THO WASH		B12	3/4	12"	2.1	6		8		12		14		18		20		24		26	- 6	10		54	4. ALTERNATE LAMINATED FLOOR 96 WELDED STEEL DETAILS 96 HARDWARE 98
	DO PAFT BOLT, SQUIRRE HERD, WRINER	43-2325.07-1 43-1636.07-2	B10 D20	3/4	20*	1.66 3.0	12		16		12	_	14 28		18 36	\vdash	20 40		24 48		26 52	_	50		55 56	HARDWARE 96
	TEEL WIRE HAIL	42-6028.5-6		60d		.10	14		14		14		14		14		14		14		14	_	4		57	
58	DQ	42-6028.3-5		504		.08	.344		444		710		920		1070		1400	Ţ	1510		1780	7	90		58	
59		42-6028.3+3	-	304	-	.05	1990	-	2650	ļ	3952		5271		6590		7910		9210		0530		850	-+	59	
.40.	20	42-4028, 3-2	1	204		. 04	24	Ц	56	<u> </u>	58		68		68		98		115		128	<u> </u>	148	IL	60	



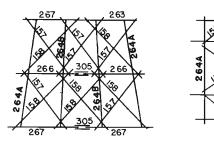
HIGHWAY

SHEET 154 97

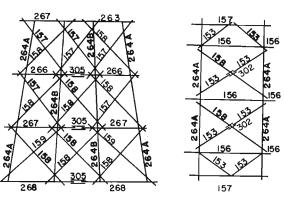
COMPANION SHEETS

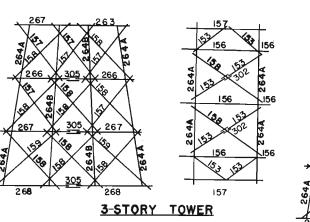


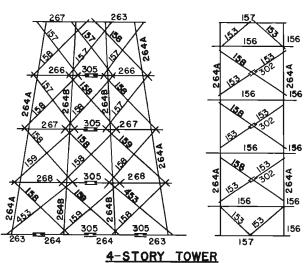
I-STORY TOWER

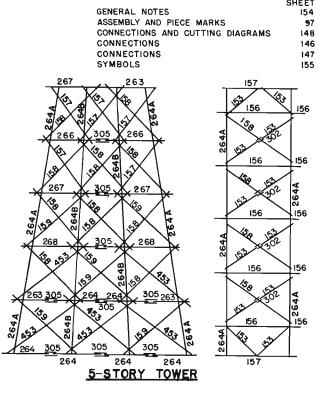


2-STORY TOWER

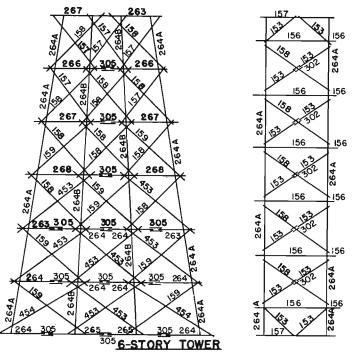








						TYPE	6-510	RY	5-31	ORY	4-S	TORY	3-57	ORY	2-510)RY	1-510)PY
		_		_	MAXIMU	M HEIGHT	75'-1	0*	631-	4-	•	-10"	38'-		25'-	_	1-31-4	
.INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENCTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	FBM	CANTIL		QUANTITY	FBM	ÚNJULI LA	FBH	COLANTITY	FBM
	LUMBER, SOFT MOOD																	
1	CAP	59-6620. 1-18	267	10 X 10	18'-0"	563	2	300	2	300	2	500	2	300	2	300	2	300
2	no	59-6620.1-1	265	10 × 10	10,-0.	313	2	157	2	157	2	167	2	1-57	2	167	2	167
3	SILL	39-6620.1-2	268	10 × 10	201-0-	625	4	667	4	657	4	667	4	557				
4	ος.	39-6620.1-18	267	10 × 19	18'-0"	563	4	600	4	600	4	600	4	າດວ	4	600		
5	BO .	39-6620.1-16	266	10 10	15'-0"	500	4	535	4	553	4	533	4	533	4	533	a l	55
6	00	39-6620, 1-14	265	10 < 10	14'-0"	438	4	467										
Z	DO	59-6620.1-12	264	10 × 10	12'-0"	375	16	1600	12	1200	4	400						
3	00	59-6620.1-1	263	10 × 10	10'-0"	313	4	333	ц	333	4	333						
,	COLUMN	39-6620.1-12	2644	10 × 10	12'-0"	375	24	2400	20	2000	16	1500	12	1200	8	800	ı,	40
,	00	39-6620.1-12	264B	10 × 10	12'-0"	375	. 24	2400	20	2000	16	1500	12	1200	8	800	i i	40
1	STRUT	39-3340.09-13	157	4 4 3	18'-0"	180	4	192	4	192	4	192	4	192	ц	192	4	19
	20	39-3340.03-15	156	4 X 3	16'-0"	160	48	.2048	40	1707	32	1365	24	1024	15	583	8	34
,	BRACING	59-5340.08-26	454	4 × 9	26'-0"	260	4	277										
	no	39-3340.08-24	453	4 x 8	24'-0	240	16	1024	12	768	4	256						
<u> </u>	00	39-3340.08-22	159	4 X 8	22'-0"	220	15	939	12	704	8	459	4	235				
S	20	39-3340.08-2	158	4 X 3	201-01	200	34	1813	32	1707	30	1600	-24	1280	14	747	4	21
7		39-3340.08-19	157	4 × 3	18'-0"	180	12	576	12	576	12	575	12	575	12	576	8	39
3	00	39-3340.08-1	153	4 x 3	10'-0"	100	23	747	24	840	20	533	16	427	12	320	8	. 21.
0	SCAB	39-3340.1	305	4 × 10	51~O*	38	48	480	a 35	360	24	240	12	120	8	80	4	40
	no	39-3228.08	502	2 X B	3'-4=		20	89	16	71	12	53	8	36	4	18		
	STEEL HARDWARE, BLOCK																	
1	MACHINE BOLT WITH SQUARE	43-2325. 1-24	E24	1	24*	6.40	16		16		16		16		16		8	
	NUT AND TWO HASHERS										<u> </u>							
2	∞	43-2325. 1-2	E20	1	20"	5.61	332		260		189		116		63		28	
3	00	45-2325.1-164	E16	1	16"	4.75	168		144		120		96		72		56	
4	200	45-2325.1-104	E10	1	10*	3.45	66		56		46	_	36		26		ا کنا	
5	DRIFT BOLT, PLAIN	43-1636.07-2	D20	3/4	20 *	2.5	146		122		93		74		50		26	



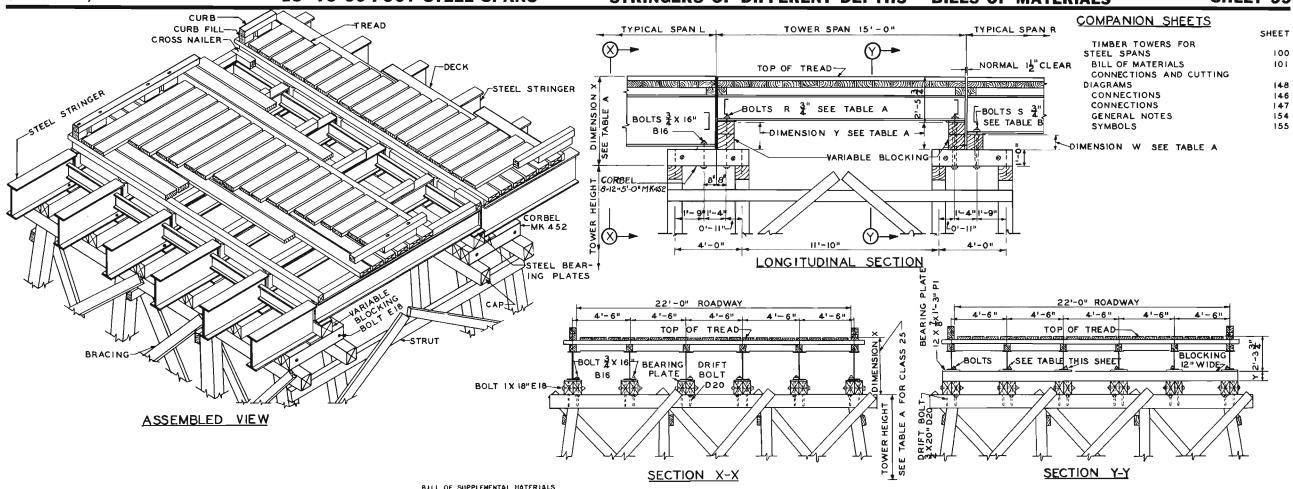
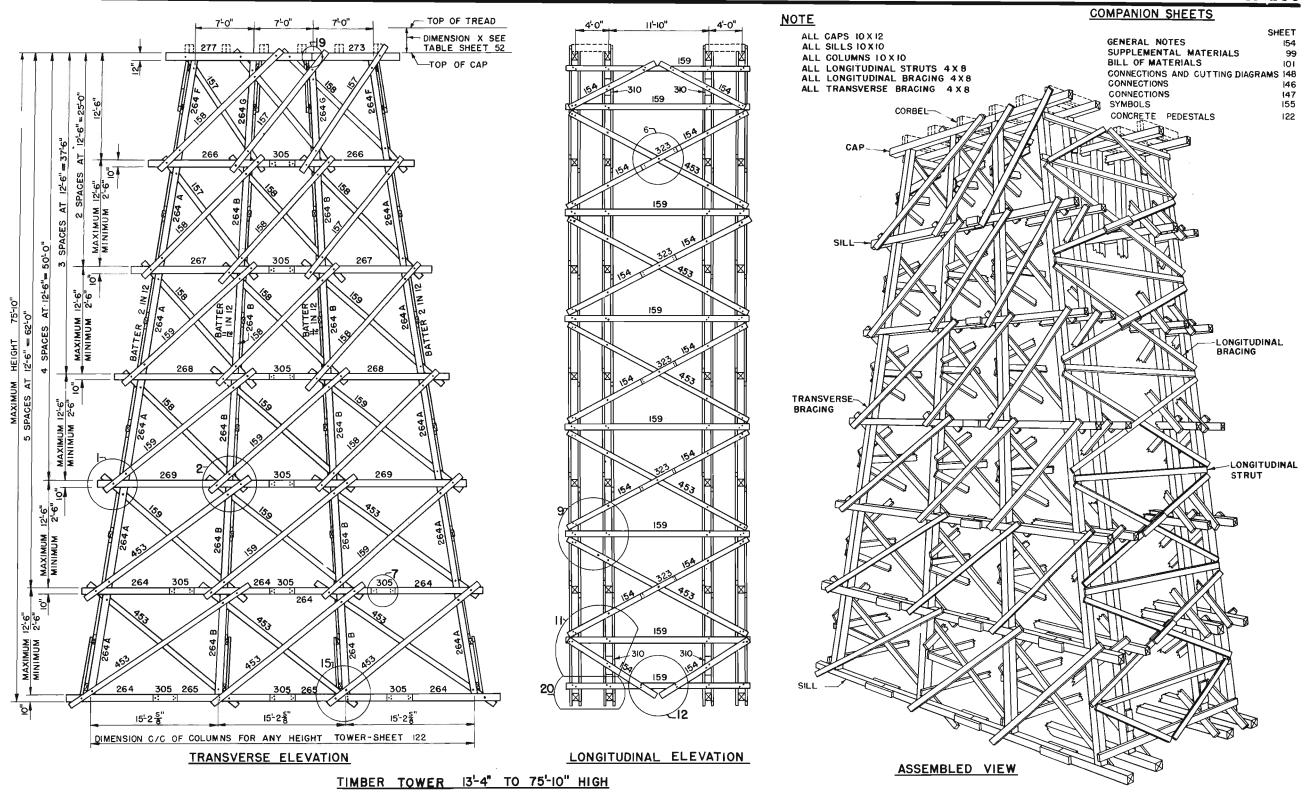
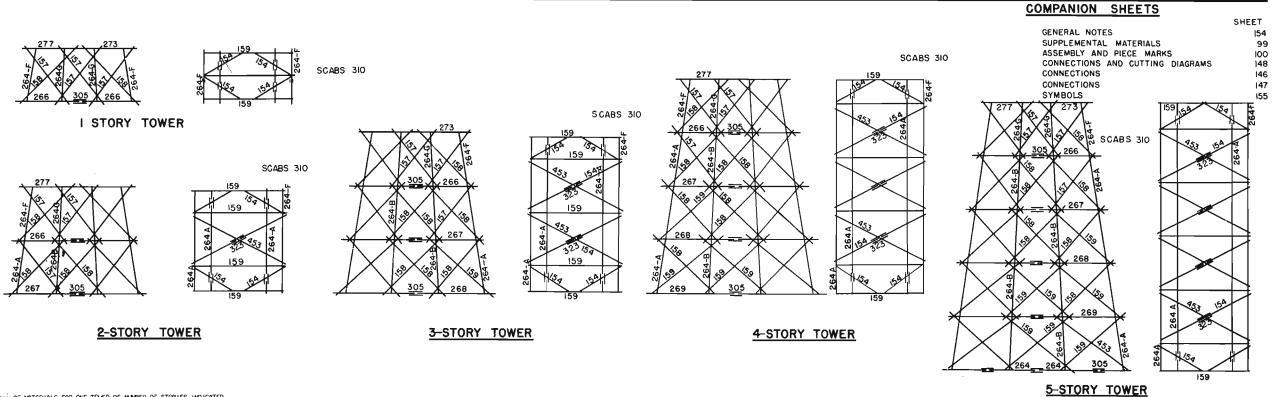


TABLE A

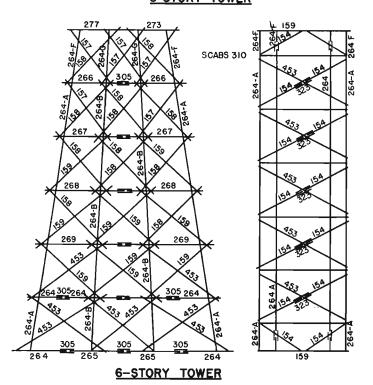
_			_		-							
S	<u>PA I</u>	A L		90'_	80'	70'	60'	5 0'	40'	30'	20'	15'
			Х	4-11	4108"	4- 73"	4-4꽃	4-2"	3-102"	3-10꽃"	3-5₹"	3-3 4
			Υ	1- 7글"	1- 7늄"	<u>'</u> 4"	1-1"	0,10 1,0	0-7등*	0-7"	Or 2.	0"
TIMBER	SPANS		w	2 <u>-</u> 1"	2 ^L 0 78"	I <u>- 9축</u> "	I ^L 6 <u>쿡</u> "	1 <u>'</u> 4"	I ^L 0중"	1-0골"	0 ^L 7 <u>국</u> *	0 ⁻ 5 <u>국</u> "
ĭ	SP	BOLT	A	38"	38"	36"	32"	30 "	26"	26"	22"	20"
	5,		W	1-74"	1-74"	1 ^L 4*	1, 1 ,	0,104,	0년7늄*	Q ^L 7*	0-2"	
	2	BOLT	Α	34"	34"	32"	28"	26"	22"	22"	18"	
	o.		W	l¹-5- <u>‡</u> "	1-5-6"	1-2"	0,11,	0'84"	0 ^L 5늄"	0 ¹ 5"		
	N	BOLT	Α	32"	32"	30"	26"	24"	20"	20"		
	30'		W	- - -	1,0 f.	Or 9.	0, 6,	0-34	아이놈			
	ñ	BOLT	Α	28"	28"	24"	22"	18"	16"			
S	40,		W	1-0-	Ir O.,	0 ¹ 8구"	0"5 7 "	O-34				
	4	BOLT	Α	28"	28"	24*	22"	18"				
SPAN	o,		W	0- 9"	0-8 7	O <u>-</u> 5₹"	22" 0-2-4"					
ď	Ŋ	BOLT	Α	24"	24"	22"	18"					
۷,	o		W	0º 6늄"	아6분	0 ^L 3"						
	9	BOLT	Α	22"	22"	18"						
	70,		W	0-34"	아 3분							
	7	BOLT	Α	18"	18"							
	90		W	O'O'								_
	Ó	BOLT	Α	16"								

				<u>S</u>	<u>FC HÖ</u>	<u>N X-</u>	<u>-X</u>					±."					<u>SEC I</u>	IOIA	1-1					
BILL	OF SUPPLEMENTAL MATER	HALS											п .	_			п .							
					AIN SPAN		+	5'	2.5		30		40		.50		60		70		80		90	•
				_	TRINGER S		 	I_30	16]		21 I		21 I		24 I	87	27 I		30 I		33 I			I 132
				۵	IMENSION	X	3'-	3 3/4*	31-5	3/4"	3'-10	3/4"	3'-10	7/8"	41-	2*	4'-4	3/4"	4'-7	3/4"	4'-16	0 7/8*	41-	-11*
				0	IMENSION		0'-0	0*	0'-2		0'-7		0'-7	1/8*	0'-1	0 1/4"	1'-1	•	1'-4'		1'-7	1/8*	1'-7	7 1/4"
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM.	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	.FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	CHANLELLA	FBM
		I	1.				0		1				0 0		1 25	· I	I 25		1 24		24		24	
_ 1	BEARING PLATE	47-7844,08	Pl	12 X 7	/8 1'-3'	1 44.6	24		24	<u> </u>	24		24		24		24		24	l	24		24	
	LUMBER, SOFT WOOD		-				п		1				,											
2	CORBEL	35-6616.12	452	_			24	960	24	960	24	960	24	960	24	960	24	960	24	960	24	960	24	960
3	BLOCKING	39-6630.12-1.	2 284	12 X 1	2 12'-0'	540	ļ	_											4	576	4	576	4	576
4	DO	39-6620.12-1	2 274	10 X 1	2 12'-0'	450	ļ		<u> </u>	ļ					4	480	4	480						
5	DÚ	39-6616.12-1	6 246	8 x 1	2 16'-0'	480			l		4	512	4	512					l		4	512	4	512
6	·DO	39-3340.12-13	2 1/4	4 X 1	2 12'-0"	180					i								4	192				
7	ooi	39-3952.12-12	2 134	3 X 1	2 12'-0"	135											4	144	i					
8	DC	39-3228.12-12	2 104	2 X 1	2 12'-0"	90		Γ	4	96														
	STEEL HARDWARE, BLACK		•														•							
9	MACHINE BOLT WITH SQUARE-		6 834	3/4	34*	4.7															12		12	
10	DO	43-2325.07-32	832	3/4	32"	4.5													12					
11	DO	43-2325,07-28	828	3/4	28"	4.0											12							
12	DC	43-2325.07-266	5 B26	3/4	26"	3.8									12									
_ 13	DO	43-2325,07-22	B22	3/4	22"	3.3					12		12											
14	DO	43-2325.07-18		3/4	18*	2.8			12															
15	DG	43-2325.07-16	B16	3/4	16*	2.6	24		12		12		12		12		12		12		12		12	
16	DG	43-2325.1-18	£18	1	18"	5.0	24		24		24		24		24		24		24		24		24	
17	DRIFT BOLT WITH SQUARE HEAD ALC WASHER	43-1636.07-2	D20	3/4	20*	3.0	48		48		48		48		48		48		48		48		48	





				NUMBER	OF STORIE	S	6-S	FORY	5-51	TORY	4-ST	QRY	3-Sī	ORY	2-51	ORY	1-8	STORY
				TOWER 1:	EIGHT		75'	-10*	63'-	4"	501-	10"	581-	4"	251-	10*	13'	-4"
INE	DESCRIPTION	STOCK NO	HARK	SIZE (Inches)	LENGTH	WE IGHT (POUNDS)	QUANTITY	FBM	PUANTITY	FBM	QUANT ITY	FBM	QUANT ITY	FBM	CALLINERY	FBM	YTITIAPUK	⊦™BM
	LUMBER, SOFT WOOD	_																
1	CAP	39-6630.12	277	10 X 12	18'-0"	675	4	720	4	720	4	720	ц	720	4	720	4	720
2	_00	39-6630.12	273	10 x 12	10'-0"	375	4	400	4	400	4	400	4	400	4	400	4	400
3	SILL	39-6620.1-22	269	10 × 10	22'-0"	688	в	1467	8	1467	8	1467						
4	00	39-6620.1-2	268	10_X_10	201-0	625	88	1333	88	1333	8	1333	8	1333				
5		39-6620,1-18	267	10 X 10	18'-0"	563	8	1200	8	1200	8	1200	8	1200	8	1200		
6	00	39-6620.1-16	266	10 X 10	16'-0"	500	8	1067	8	1067	8	1067	8	1067	8	1067	8	1067
7	200	39-6620.1-14	265	10 X 10	14'-0"	438	8	933										
8	no	39-6620.1-12	264	10 x 10	12'-0"	375	24	2400	. 16	1600								
9	COLUMN	39-6620.1-12	264A	10 x 10	12'-0"	375	40	4000	32	3200	24	2400	16	1606	8	800		
10	00	39-6620.1-12	2648	10 x 10	12'-6"	375	40	4000	32	3200	24	2400	16	1600	8	800		
11	000	39-6620.1-12	264F	10 X 10	12'-0"	375	8	800	8	800	8	800	8	800	8	800	8	800
12	∞	39-6620.1-12	264G	10 X 10	12"-0"	375	8	800	8	800	8	800	8	800_	8	800	8	800
13	STRUT	39-3340.08-22	159	4 X 8	22'-0"	220	32	1877	28	1645	24	1408	20	1173	16	939	12	704
14	BRACING	39-3340.08-24	453	4 X 8	24'-0"	240	52	3326	24	1536	12	768	8	. 512	4	256		
15_	00	39-3340.08-22	159	4 X 8	22'-0"	220	40	2347	40_	2347	24	1408	8	469				
16	no	39-3300-08-2	158	4 X B	20'-0"	200	48	2560	48	2560	48	2560	40	2153	24	1280	8	427
17	_ no	39-3340.08-18	157	4 X 8	18'-0"	180	24	1152	24	1152	24	1152	24	1152	24	1152	16	768
18	DO.	39-3340.08-12	154	.4 x B	12'-0"	120	56	1792	48	1536	40	1280	52	1024	24	768	16	512
10	SCAR	39-3340.1	505	4 X 10	5'-0"	38	80	800	56	560	32	320	.24	240	16	160	8	80
20	<u> </u>	39-3340.1	310	4 X 10	2'-0"	25	16	107	16	107	16	107	16	107	16	107	2.4	160
21	00	39~3880.08	325	2 X 8	31-8	18	40	196	32	156	24	117	16	78	8	39		
	STEEL HARDWARE, BLACK		1								1 1							
22	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.1-2	£20 .	1	20"	5.6	512		400		288		224		160		96	
23	DC)	43-2525.1-164	£16	1	16*	4.7	624		526		452		336		240		.160	
24	∞	45-2325.1-104	E10	1	10"	3.4	132		112		92		72		52		32	
25	DRIFT BOLT, PLAIN	43-1636.07-2	D20	3/4	20*	2.5	292		244		196		148		100		52	



103

NOTES

ALL DETAILS FOR CLASS 50 DOUBLE-LANE TOWERS ARE TO BE USED FOR CLASS 25 DOUBLE-LANE TOWERS, EXCEPT AS FOLLOWS:

1. USE CAP BEAM MK 615 SHOWN ON THIS SHEET INSTEAD OF CAP BEAM MK 675 SHOWN ON SHEET 59.

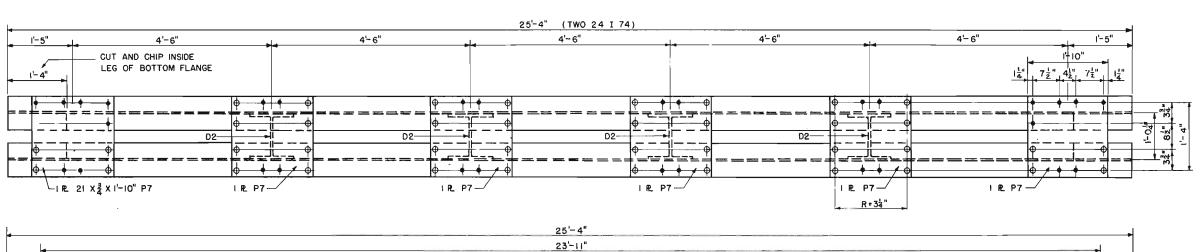
2. USE SHIMS ON SHEET 103 INSTEAD OF SHIMS ON SHEET 63.

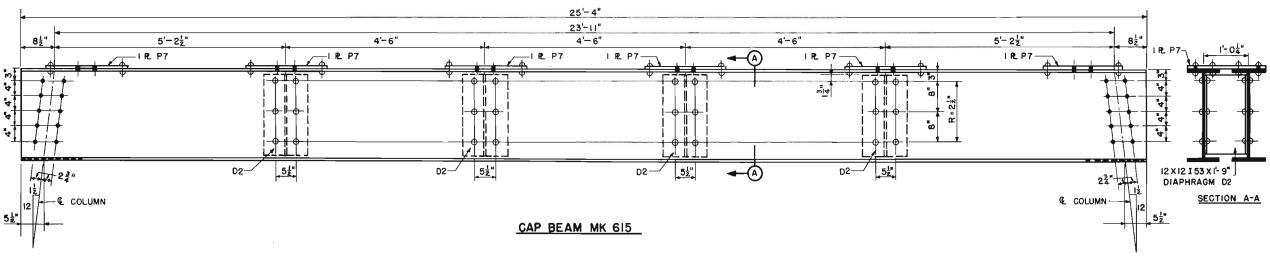
FOR BILL OF MATERIALS FOR ONE CLASS 25 DOUBLE-LANE TOWER SEE: I. SHEET 57, MATERIALS COMMON TO ALL TOWER HEIGHTS 2. SHEET 58, MATERIALS FOR PIECES WHICH VARY WITH DIFFERENT TOWER HEIGHTS

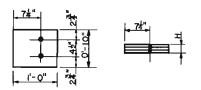
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STRUTS AND COLUMNS 61
ROD BRACING 62

COMPANION SHEETS

SHIMS



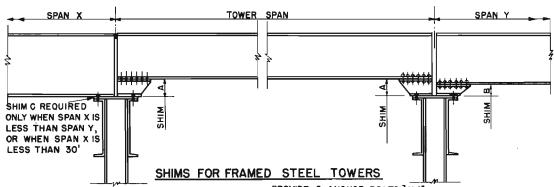




DETAIL OF PLATE SHIM

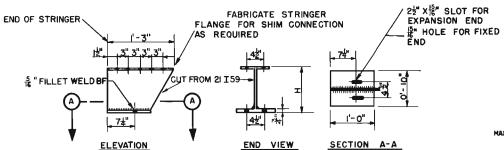
BILL OF MATERIALS FOR ONE PLATE SHIM

DESCRIPTION	STOCK NO	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)		750-2 H = 2 3/4* QUANTITY	7503 H = 3 1/8" QUANTITY	
PLATE	47-7844-07	10X3/4	1'-0"	26		1	3	
DO	47-7844.08	10x7/8	1'-0"	-30			1	
DO	47-7844.1	10 X 1	1'-0"	34	2	-2		
ANCHOR BOLT	43-2219.08-05	7/8	5.	1.2	.2			
DO	43-2219.08-07	7/8	7.	1.7		2	2	



PROVIDE 2 ANCHOR BOLTS X4"
PER STRINGER WHEN SHIMS ARE NOT

Sŀ	IIMS	FOR	FRAMED	STEEL	TOWERS	REQUIR		WHEN	SHIMS	ARE NO	т
5	PAN	x	90'	801	701	60'	50'	401	30'	20'	15'
_		А	7513	7512	7509	7505	7503				
	15	8	7518	7518	7516	7514	7510	7507	7507	7507	7507
	Ш	С								7504	7507
		А	7513	7512	7509	7505	7503				
	20	В	7517	7517	7515	7511	7508	7504	7504	7504	7504
		С								7504	7507
		A	7513	7512	7509	7505	7,503				
	30	В	7513	7512	7509	7505	7503				
		С								7504	7,507
		Α	7513	7512	7509	7505	7503				
	9	В	7.512	7512	7509	7505	7503				į .
		C								7504	7507
		А	7513	7512	7509	7505	7503	7,503	7503	7503	7503
>-	<u>5</u>	В	7509	7509	7505	7502					
SPAN	"`	С						7503	7503	7508	7510
ŝ		A	7513	7512	7509	7505	7505	7505	7505	7505	7505
	0	В	7506	7506	7503						
		c					7502	7505	7505	7511	7514
		Α	7513	7512	7509	7509	7509	7509	7509	7509	7509
	2	е	7503	7503							
	Ш	C				7503	7505	7509	7509	7515	7516
		А	7513	7512	7512	7512	7512	7512	7512	7512	7512
	8	6									
	لتّا	С			7503	7506	7509	7512	7512	7517	7518
		А	7513	7513	7513	7513	7513	7513	7513	7513	7513
	9	В									
		C			7503	7506	7509	7512	7513	7517	7518



DETAIL OF BUILT-UP SHIM

BILL OF MATER	IALS FOR ONE BU	HLT-UP S	нін	
DESCRIPTION	STOCK NO	91ZE (INCHES)	LENGTH	QUANTITY
BEAM	48-2900.21-059	21 I 59	1'-3"	1
PLATE	47-7844.07	10x3/4	1'-0"	1
RIVET	43-6353.08	7/8	2 3/4"	10
ANCHOR BOLT	45-2219.08-04	7/8	4 -	2

1-LB

ELECTRODE 46-377.2.2-7 3/16

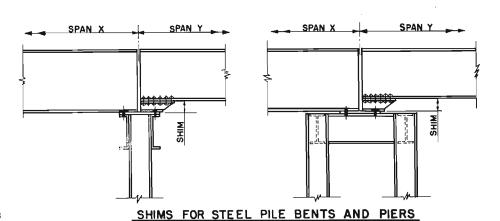
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STEEL PILE BENTS AND
PIERS, WELDED 119,120
FRAMED STEEL TOWERS 55,56

MARKS AND DIMENSIONS FOR BUILT-UP SHIMS

MARK	н	WEIGHT (POUNDS)
7504	5*	52
7505	5 7/8*	53
7506	6 1/4"	54
7507	7*	54
7508	8 1/4"	57
7509	8 7/8"	58
7510	10 1/4"	60
7511	11*	61
7512	12*	62
7513	12 1/4"	63
7514	13*	64
7515	14*	65
7516	16*	68
7517	17 1/8"	70
7518	19 1/8"	73



BILL OF MATERIALS FOR ANCHOR BOLTS ONLY WITHOUT SHIMS

DESCRIPTION	STOCK NO	SIZE (INCHES)	LENGTH	WEIGHT EACH (POUNDS)
ANCHOR BOLT	43-2219-08-04	7/8	0'-4 "	1.2

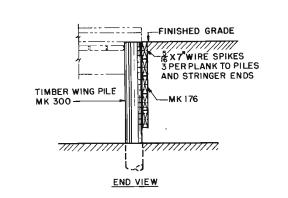
TWO BOLTS REQUIRED FOR EACH STRINGER SUPPORT CONSTRUCTION INDICATED BY BLANK SPACES IN TABLES FOR SHIMS

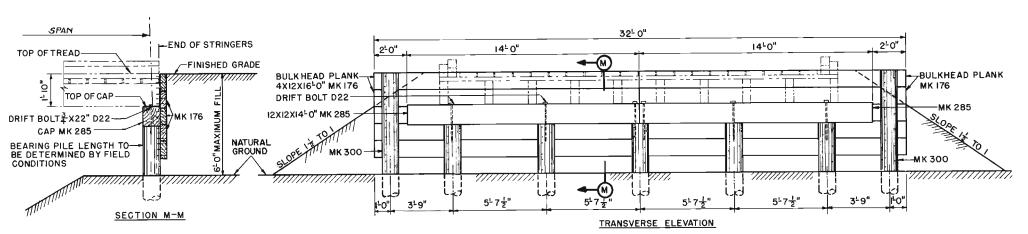
	_									
20° 30° 40° 50° 60° 70° 80°	PAN X	90'	80'	70'	601	50'	40'	30'	20'	151
\top	15'	7518	7518	7516	7514	7510	7507	7507	7501	
	201	7517	7517	7515	7511	7508	7504	7504		7501
	30'	7513	7512	7509	7505	7505			7504	7507
1	401	7512	7512	7509	7505	7503			7504	7507
ğ.	50'	7509	7509	7505	750∠		7503	7503	7508	7510
જ	60'	7506	75 C6	7503		7502	7505	7505	7511	7514
L	701	7503	7503		7503	7505	7509	7505	7515	7516
	801	[7503	7506	7509	7512	7512	7517	7518
Γ	90'	1		7503	7500	7569	7512	7513	7517	7518

SHEET

COMPANION SHEETS

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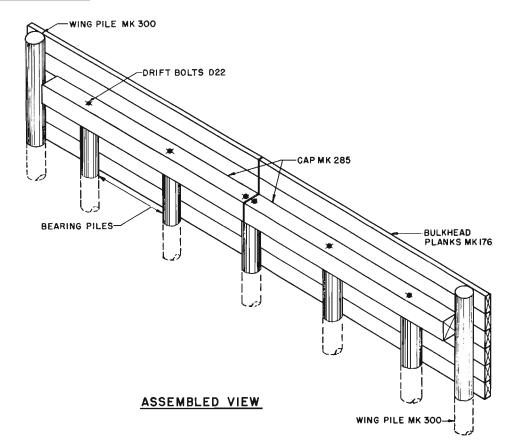


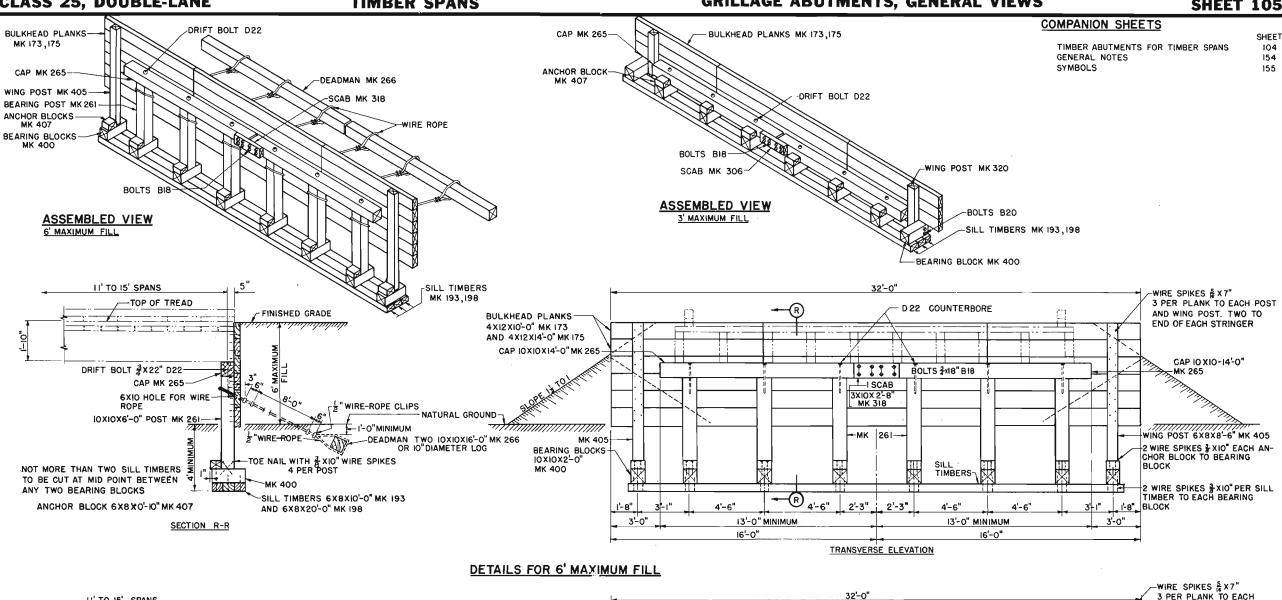
TIMBER ABUTMENTS,

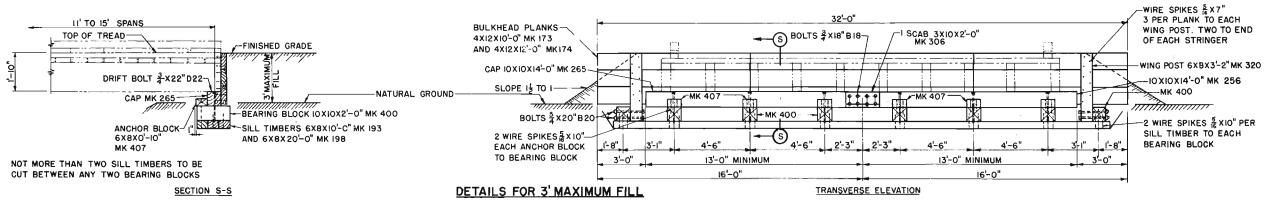
TIMBER SPANS

TIMBER PILE ABUTMENT SUPPORTING II'TO 15' TIMBER-STRINGER SPANS

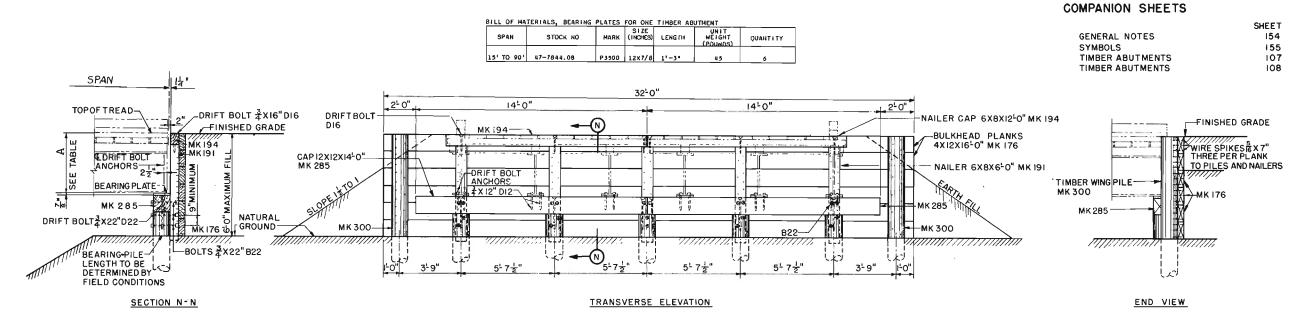
		TYPE OF ABUTMENT					TIMBER PILE	ABUTHENT	т т	IMBER GRI	LLAGE ABUTME	éT.	
		FILL HEIGHT	_			,	6' MAXIN	NUM	6' MA	CIMUM	3' MAX	MUM	
. I NE	DESCRIPTION	STOCK NO	HARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LIN
ı	BULKHEAD PLANK	39-3340.12-16	176	4 X 12	16'-0"	240	12	768					
2	3 DO	39-3340.12-14	175	4 X 12	14'-0"	210			6	336			2
3	3 00	39-3340.12-12	174	4 X 12	12'-0"	180		,			3	144	,
4	.3 DO	39-3340.12	173	4 X 12	10,-0.	150			12	480	6	240	4
5	PILE (WING)		300		15'-0"		2				1		
6	1 PILE (BEARING)				1		5		1	_			6
7	2 POST (WING)	39-3560.08	405	6 X B	8'~6"	128			2	68			7
8	2 DO	39~3360.08	320	6 × 8	3'-2"	47					2	25	e
9	2 POST (BEARING)	39-6620.1	261	10 X 10	6'-0"	188			6	300	 		و
10	CAP	39-6630.12-14	285	12 X 12	14'-0"	630	2	336	1				10
11	DO	39-6630.1-14	265	10 × 10	14'-0"	437			2	233	2	233	11
12	SCAB	39-3330.1	318	3 X 10	2'-8"	25			2	13			12
13	DO	39-3330.1	306	3 X 10	2'-0"	19					2	10	13
14	GRILLAGE TIMBERS	39-3360.08	193	6 X 8	10'-0"	150			3	120	,	120	14
15	DO	39-3360.08-2	198	6 X 8	20'-0"	300			3	240	3	240	15
16	BEARING BLOCK	39-6620.1	400	10 × 10	2'-0"	63			8	133	8	133	16
17	DEADMAN	39-6620.1-16	266	10 X 10	16'-0"	500			2	267			17
18	ANCHOR BLOCK	39-3360.08	407	6 X 8	0'-10"	13_			В	26	6	20	18
	STEEL HARDWARE, BLACK												
19	WIRE ROPE	22-4567.4-05		1/2	20'-0"	13			8				19
20	WIRE-ROPE CLIP	42-3544.5-05		1/2		0.72			32	-	1		20
21	MACHINE BOLT WITH NUT AND TWO WASHERS	43-2325.07-2	820	3/4	20-	3.06		_			4		21
22	DO	43-2325.07-183	818	3/4	18*	2.92			8		8		22
23	DRIFT POLT	43-1636.07-22	D22	5/4	22*	2.76	6		6		6		23
24	STANDARD WIRE SPIKE	42-8488.04-1		3/8	10-	0.53			96		60	_	24
25	DO	42-8488.035-07		5/16	7*	0.14	136		172		52		25
<u>1</u>	BEARING PILE LENGTHS TO	D BE DETERMINED B	Y FIELD	CONDITIONS.									T
_2	CUT TO FIT FOR FILLS L	ESS THAN A FEET.											1





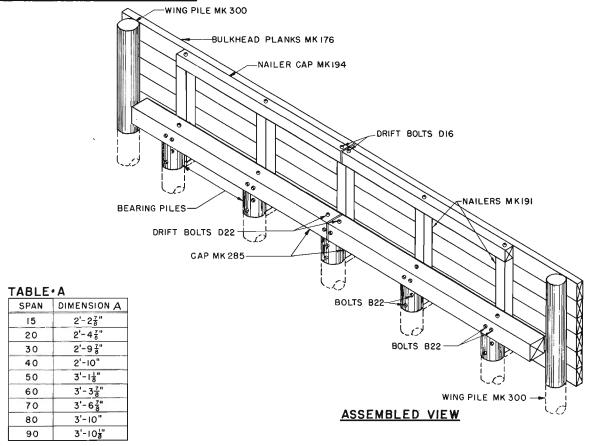


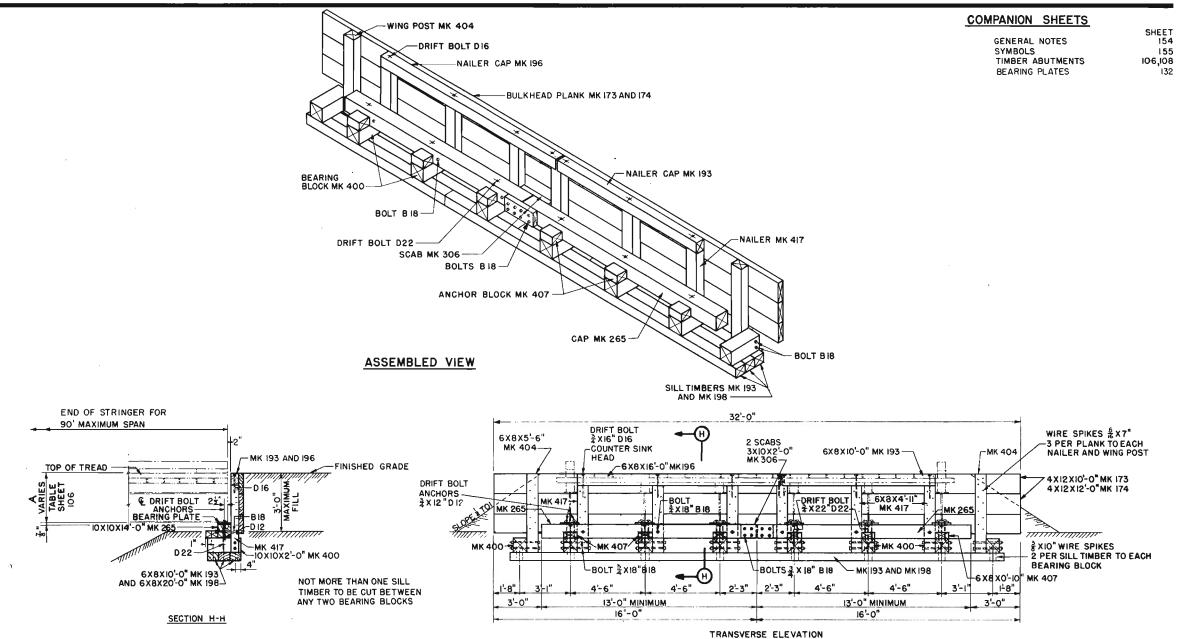
TIMBER GRILLAGE ABUTMENTS SUPPORTING II' TO 15' TIMBER-STRINGER SPAN



TIMBER PILE ABUTMENT SUPPORTING 15' TO 90' STEEL-STRINGER SPAN

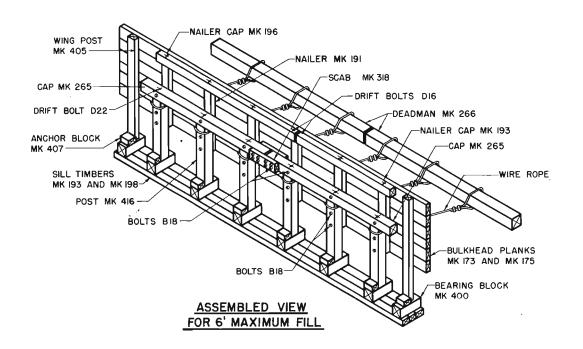
		TYPE OF ABUTMENT			-	-	T IMBER ABUTA	MENT			LAGE ABUT]
ı,		FILL HEIGHT -				-	6' MAX	IMUM	6' MA	X I MUM	3' MA	KIMUM	4
INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT (POUNDS)	QUANTITY	FBH	QUALITITY	FBM	QUANTITY	FBM	LIN
1	3 BULKHEAD PLANK	39-3540.12	173	4 X 12	10'-0-	150			12	480	8	320	1
2	00 لاـــ	39-3340.12-12	174	4 X 12	121-0"	180					4	192	2
3	<u>≯</u> 00	39-3340-12-14	175	4 X 12	14'-0"	210			6	336]		3
4	_3 DO E_	39-3340.12-16	176	4 X 12	16'-0"	240	12	768					4
5	PILE (WING)		300		15'-0"		2				ì		5
6	2 PILE (BEARING)				_2		5				1		6
7	J POST (WING)	39-3360.08	405	6 X 8	8'-6"	128			2	68	1		7
8	<u>J</u> 00	39-3360.08	404	6 X 8	5'-6"	83					2	44	8
9	POST (BEARING)	39-6620-1	416	10 × 10	5'-6 1/4"	172			6	275			9
10	CAP	39-6630-12-14	285	12 X 12	14'-0"	630	2	336					10
11	DO	39-6620.1-14	265	10 X 10	14'-0"	437			2	233	2	233	11
12	SCAB	39~5330.1	318	3 X 10	2'-8"	25			2	13.			12
13	00	39-3330.1	-306	3 X 10	2'-0"	19					2	10	1.3
14	1 NATLER	39-3360.08	191	6 X 8	6'-0"	90	5	120	6	144			14
5	DO	39-3360.08	417	6 X 8	4'-11"	74					6	118	1:
6	NATLER CAP	39-3360.08	193	6 X 8	10'-0"	150			1	40	1	40	16
7_	00	39-3360.08-12	194	6 X 8	12'-0"	180	2	96					1.7
18	DO	39-3360-08-16	196	.6 X 8	16'-0"	240			11	64	l	64	18
19	GRILLAGE TIMBERS	39-3360.08	193	6 X 8	10'-0"	150			3	120	3	120	15
20	DO	39-3360.08-2	198	6 X 8	201-01	300			3	240	3	240	20
21	BEARING BLOCK	39-6620-1	400	10 × 10	2'-0"	63			8	133	8	133	21
22	DEADMAN	39-6620-1-16	266	10 × 10	16'-0"	500			2	267	1		22
23	ANCHOR BLOCK	39-3360.08	407	6 X 8	0'-10"	13	Ì		8	26	6	20	23
	STEEL HARDWARD, BLACK					1		_	1 0 1				100
24	WIRE ROPE	22-4567.4-05		1/2	20'-0"	13	\vdash		8		1		24
25	WIRE-ROPE CLIP	42-3544-5-05		1/2		0.72			32		+		25
26	MACHINE BOLF WITH SQUARE NUT AND TWO WASHERS	45-2525.07-225	822	3/4	22"	3.30	20						26
27	00	43-2325.07-2	B20	3/4	201	3.06					16		27
28	DO .	43-2325-07-183	B18	3/4	18"	2.82			26		14		28
2.5	DRIFT BOLT	43-1636-07-22	D22	3/4	22*	2.76	6		6		6		25
10	DO	43-1636.07-16	016	3/4	16"	2.00	6		7		7		30
11	DRIFT BOLT ANCHOR	43-1636-07-12	D12	5/4	12*	1.50	12		12		12		31
12	STANDARD WIRE SPIKE	42-8488.C4-1		3/8	10"	0.33			96		60		32
13.	DO	42-8488.035-07		5/16	7-	0.143	144		180		120		33
L)	CUT TO FIT FOR FILLS UND	ER 6 FEET.											1
	LENGTH OF BEARING PILE TO	D BE DETERMINED B	Y FIELD	CONDITIONS.		_							

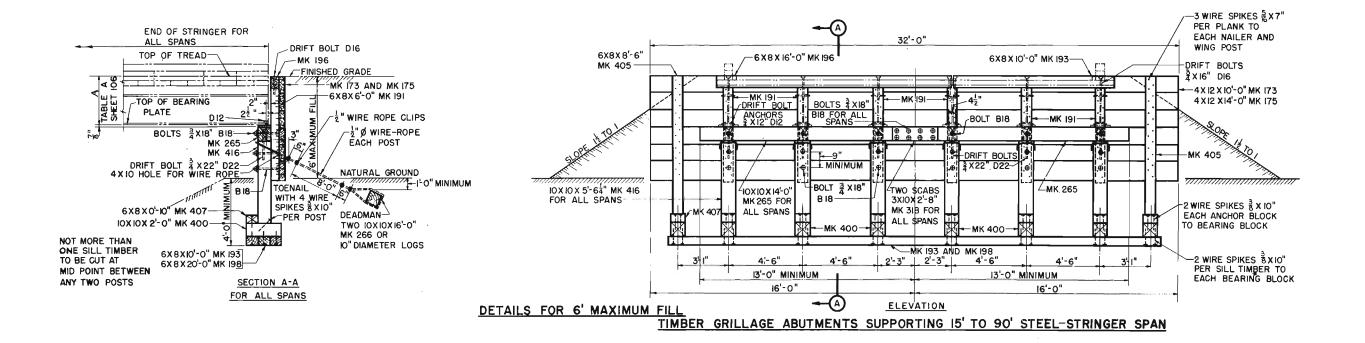




TIMBER GRILLAGE ABUTMENTS SUPPORTING 90' MAXIMUM STEEL-STRINGER SPAN

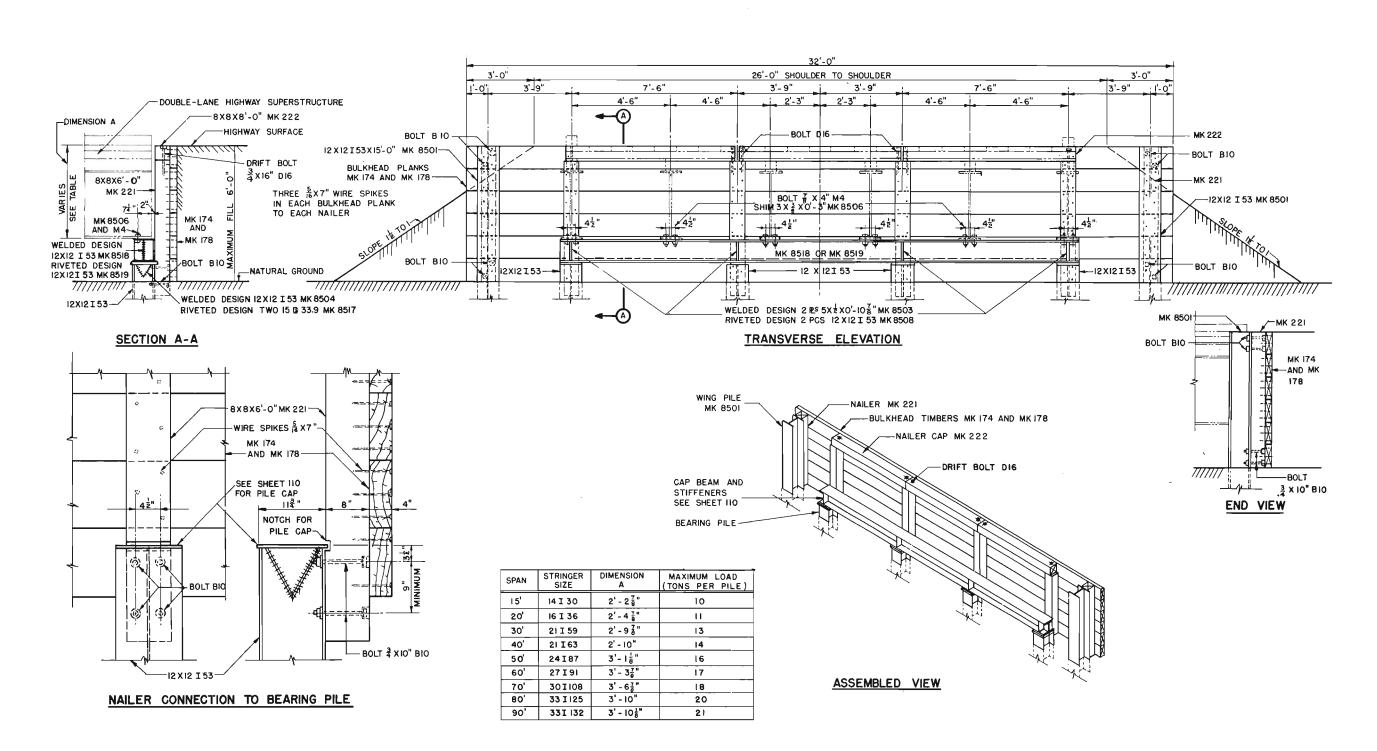
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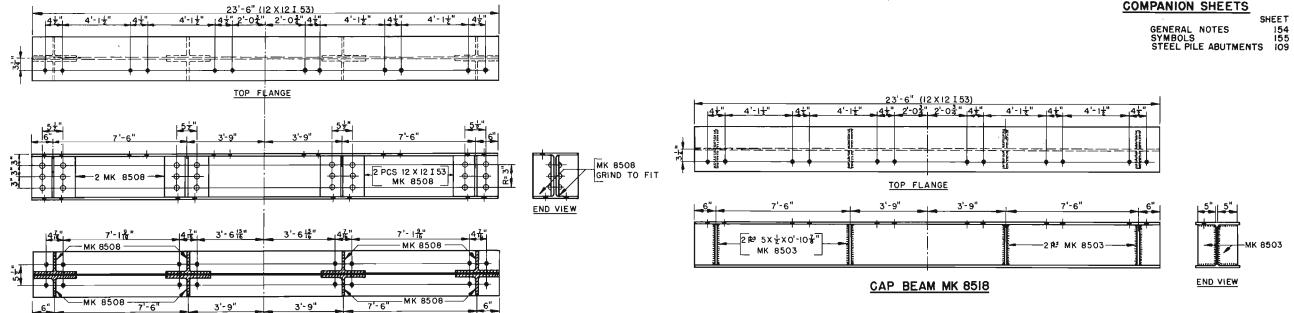


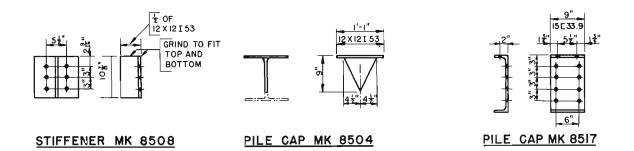


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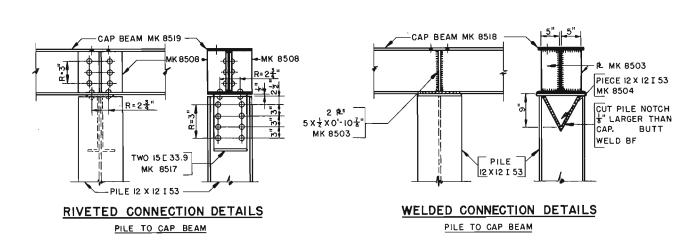
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COMPANION SHEETS	SHEET
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SYMBOLS	155
STEEL PILE ABUTMENTS	110







BOTTOM FLANGE VIEW CAP BEAM MK 8519



BILL O	F MATERIALS FOR ONE ABUTMENT							
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	QUANTITY	F8M	WEIGHT EACH (POUNDS)
ALTER	NATE NO 1 WELDED DETAILS			•	•			
1	WING PILES		8501	12X12 I 55	15'-0"	2		795
2	CAP BEAM		8518	12X12 I 55	23'-6"	1		1245
	STIFFENERS	47-7844.05	8503	PL 5 X 1/2	10 7/8	8		8
4	PILE CAP		8504	12X12 I 53	1'-1"	4		29
	_							
ALTER	MATE NO 2 RIVETED DETAILS							
ALTER	THATE NO 2 RIVETED DETAILS							
5	WING PILES		8501	12×12 I 53	15'-0"	2		795
6	CAP BEAM		8519	12X12 I 53	23'-0"	1		1245
7	STIFFENERS		8508	1/2 12X12 I 55	10 7/8*	8		24
8	PHLE CAP	48-3790-15-34	8517	15 [33.9	01-9"	8		26
				-				
LUMBE	R, SOFT WOUD ALT NOT AND NO 2							
9	NATILERS	39-6616.08	221	8 × 8	6'-0"	6	192	120
10	NATLER CAPS	39-6616.08	-222	8 × 8	8'-0"	3	128	160
11	BULKHEAD TIMBERS	39-3340.12-2	178	4 X 12	20'-0"	6	460	300
12	DO	39-3340.12-12	174	4 × 12	12'-0"	6	288	1.80
STEEL	HARDWARE, BLACK							
13	BULTS WITH NUTS AND THO WASHERS	43-2325.07-1	810	3/4	10-	24		
14	ANCHUR BOLTS WITH NUTS AND TWO WASHERS	43-2219.08-04	M4	7/8	4.	12		1 17
15	DRIFT BOLTS WITH WASHERS	45-1656.07-16	016	3/4	16.	4		<u>1</u>] 8
16	WIRE SPIKES	42-8488.035-07		5/16	7.	108		1 18
17	RIVETS	43-6353.08-25		7/8	2 1/2"	16		.62
18	00	43-6553.08		7/8	2 3/4"	56		-46
19	WELDING ROD	46-3772.2-7		3/16				18

1 TOTAL WEIGHT.

BOLT BIG 4

4-0"

SECTION

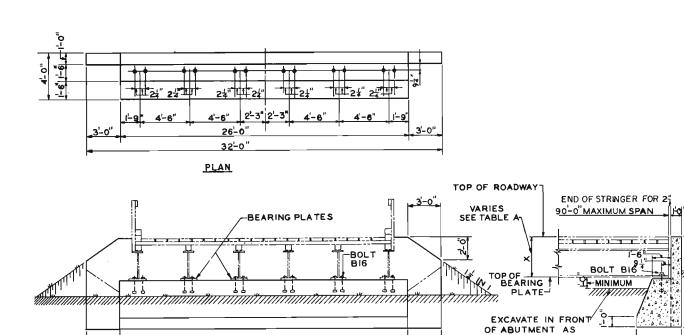
-Y-MINIMUM

REQUIRED

32-0" ELEVATION

-3'-0"MAXIMUM FILL

NATURAL GROUND



26-0"

ELEVATION

ABUTMENT 3'-0" MAXIMUM FILL

3'-0"

ANCHOR-BOLT DETAIL

ABUTMENT, 6'-0" MAXIMUM FILL

				H SQUARE NUT ER, STOCK NO	CONCRETE				
SPAN FEET	×	Y	43-23	25.07-16 6" B 16	6 MAXIMUM FILL	3' MAXIMUM			
			QUANTITY	WEIGHT EACH	CU YDS	CU YDS			
15	2-23	2-43	12	3.5	33.0	22.1			
20	2'- 4쿻"	2-6-37	12	3.5	32.5	21.8			
30	2'-97"	2-11≩	12	3.5	31.4	20.9			
40	0 2'-10" 2'-112"		12	3.5	31.4	20.9			
50	3'-1 ਜ਼ੂੰ"	3'-3"	12	3.5	30.7	20,3			
60	3'-37	3'-5≹"	12	3.5	30.1	19.8			
70	3'-68	3'-83"	12	3.5	29.5	19. 3			
80	3'-10"	3-11者"	12	3.5	28.8	18.7			
90	3-108	4'-0"	12	3.5	28.8	18.7			
(12) (13)	(&XI'-3" (REQUIRE	S (SHEE MK 3500 D FOR EA 47-7844.0	ACH ABUTM	ENT					

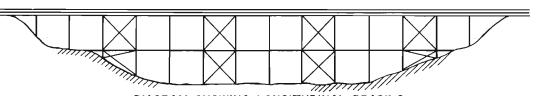
SECTION

SHEET

113

154

155



TIMBER PILE BENTS FOR TIMBER SPANS GENERAL NOTES

COMPANION SHEETS

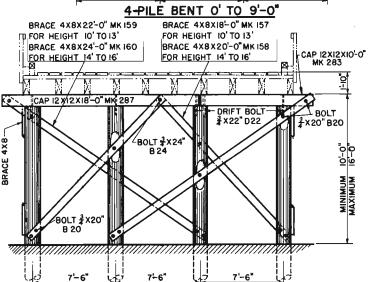
SYMBOLS

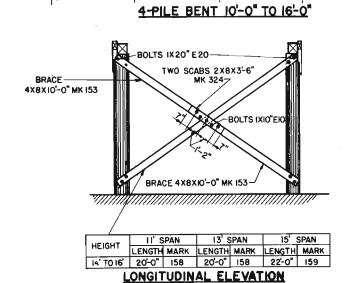
DIAGRAM SHOWING LONGITUDINAL BRACING

TRESTLES OVER 13 FEET HIGH HAVE LONGITUDINAL CROSS BRACING EVERY THIRD SPAN. LONGITUDINAL STRUTS ARE CARRIED TO BANK AND FASTENED TO BENT NEAR GROUND LINE.

DRIFT BOLT 3 ** X22" D22 7-6" 7-6" 7-6" 7-6" 81L

-CAP 12 X 12 X 18 -0" MK 287

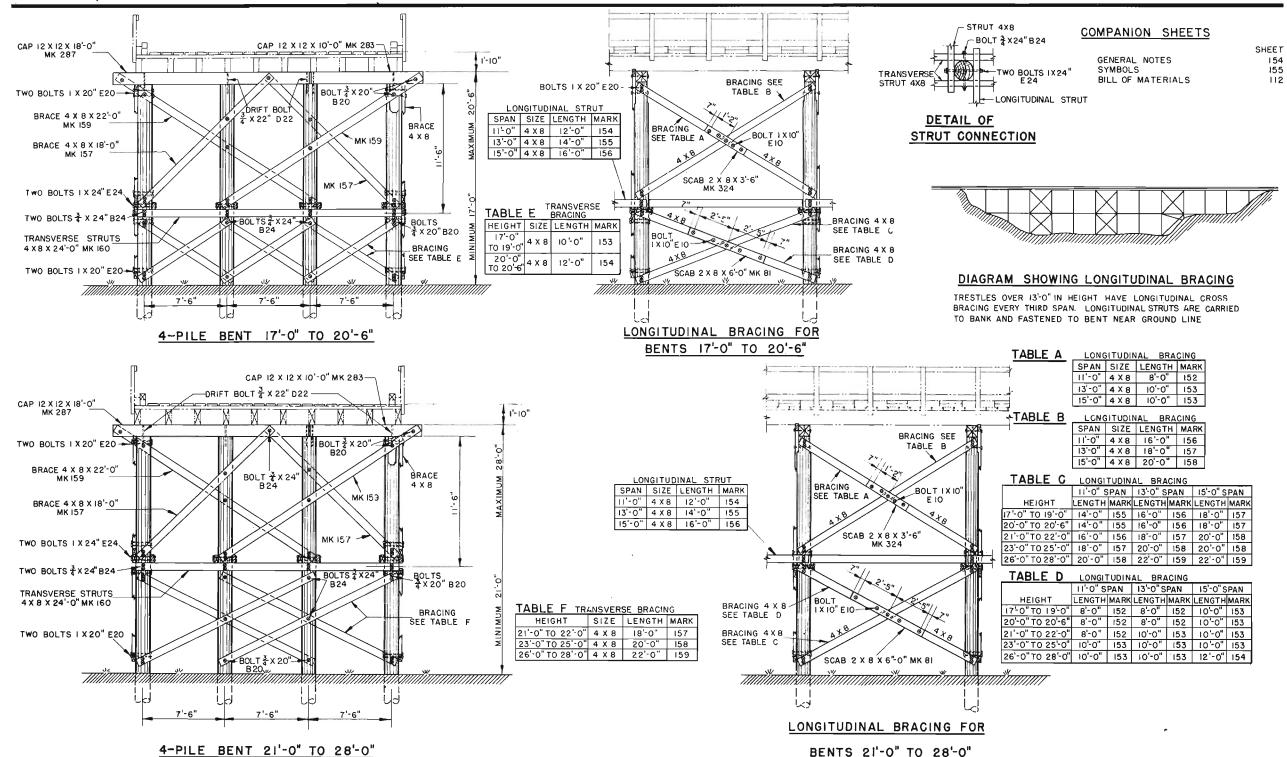




	BILL OF MATERIALS FOR LO	NGITUDINAL BRAC	ING FO	OR ONE B	ENT OR	ONE SP	PAN															
				BENT	HEIGHT		0' TO !	יפ	10' TO	13'	14' ro	16'	17' TO	19'	20' TO	201-6*	21' TO	22'	23' TO	251	26' TO	281
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	FBM	QUARTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	F8M
1	PILE						4		4		4		4		4		4		4		4	
2	CAP, LUMBER, SOFT WOOD	39-6630.12-12	283	12X12	10'-0"	450	1	120	1	120	1	120	1	120	1	120	1	120	1	120	1	120
3	DO	39-6630.12-18	287	12X12	18'-0"	810	1	216	1	216	1	216	1	216	1	216	ı	216	1	216	1	216
4	BRACE, LUMBER, SOFT WOOD	39-3340.08-1	153	4X8	10'-0"	100							6	160								
5	DO .	39-3340.08-12			12'-0"										6	192						
6	DQ	39-3340.08-18	157		18'-0"				2	96			2	96	2	96	6	288	2	96	2	96
7	00	39-3340.08-2	158		20'-0"						2	107							. 4	213		
8	DQ	39-3340.08-22	159		22'-0"				2	117			2	117	2	117	2	117	2	117	6	. 352
9	00	39-3340.08-24	160		24'-0"						2	128										
10	STRUT, LUHBER, SOFT HOOD	39-3340.08-24	160	4×8	24'-0"	240							2	128	2	128	2	128	2	128	2	128
	STEEL HARDWARE, BLACK																					
11	DRIFT BOLT WITH SQUARE HEAD AND ONE WASHER	43-1636.07-22	D22	3/4	22"	3.0	5		5		5		5		5		5		5		5	H
12	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.07-2	B20	3/4	20 *	3.0			16		16		24		24		32		32		32	
13	DO	43-2325.07-24	B24	3/4	24"	3.6			1		1		11		11		9		9		9	
. 14	00	43-2325.1-24	E24	1	24"	5.5					8		8		8		8		8		8	

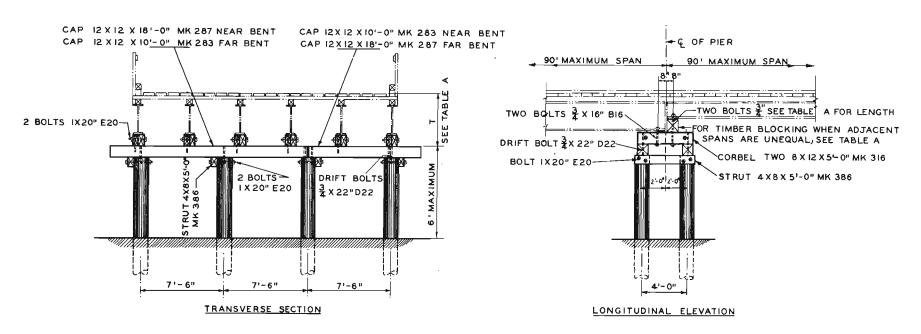
MATERIALS REQUIRED FOR LONGITUDINAL BRACING FOR VARIOUS SPANS, STRUTS ONLY				
11' SPAN				
15 STRUT, LUMBER, SOFT WOOD 39-3340.08-12 154 4X8 12'-0" 120		4 128 4	128 4 128 4	128 4 128
13' SPAN			- ,	
16 STRUT, LUMBER, 90FT WOOD 39-3340.08-14 155 4X8 14'-0" 140		4 149 4	149 4 149 4	149 4 149
15' SPAN				
17 STRUT, LUMBER, SOFT WOOD 39-3340.08-16 156 4X8 16'-0' 160		4 171 4	171 4 171 4	171 4 171
MATERIALS REQUIRED FOR LONGITUDINAL BRACING FOR VARIOUS SPANS. STRUTS AND BRACES	_			

MATERIALS REQUIRED FOR LO	NGITUDINAL BRACI	NG FO	R VARIO	US SPAN	S. STR	TS AND BRACES	 							_				
11' SPAN	_						 											
18 BRACE, LUMBER, SOFT_WOOD	39-3340.08-08	152	4X8	8'-0"					8	171	88	171	8	171	4	85	4	
19: 00	39-3340.08-1	153	4X8	10'-0"	100		4	107							4	107	4	\perp
20 00	39-3340.08-14	155	4X8	14'-0"	140				2	75	2	7.5						
21 00	39~3340.08-16	155	4X8	15'-0"	160				2	85	2	85	4	171	2	8.5	2	
22 00	39-3340.08-18	157	4X8	18'-0"	180										2	96		
23 DO	39-3340.08-2	158	4×8	20 ' -0 "	200		2	107									2	
4 STRUT, LUMBER, SOFT WOOD	39-3340.08-12	154	4X8	12'-0"	120		4	128	ų	128	4	128	4	128	4	128	4	\perp
13' SPAN																		
5 BRACE, LUMBER, SOFT WOOD	39-3340.08-08	152	4×3	3'-0*					4	85	4	85						
5 DO	39-3340.08-1	153	4X8	10'-0"			4	107	4	107	4	107	в	213	8	213	8	\perp
27 DO	39-3340.08-16	156	4X8	16'-0"					2	85	2	85						\perp
8 DO	39-3340.08-13	157	4X8	18'-0"					2	95	2	96	4	192	. 2	96	2	
9 00	59-3540.08-2	158	4×8	20'-0"			2	107							2	10.7		_
00 00	39-3340.08-22	159		22'-0"													2	_
STRUT, LUMBER, SOFT WOOD	<u> 59-3340.08-14</u>	155	4X8	14'-0"	140		 	149	ц	149	4	149	4	149	4	149	4	L
15' SPAN			_				 											_
2 BRACE, LUMBER, SOFT WOOD	39-3540.08-1	153	4X8	10'-0"			4	107	8	213	8	213	8	213	8	213	4	┸
5 00	39-3340.03-12	154	4X8	12'-0"						ļ							4	╄
4 00	39-3340.08-18	157	4X8	18'-0-			 		2	96	2	96						+
5 00	39-3340.08-2	158	4X8	20'-0"					2	107	2	107	4	213	4	213	2	┸
56 DO	39-3540.08-22	159	4X8	22'-0"			2	117										_
37 STRUT, LUMBER, SOFF HOOD	39-3540.08-16	155	4X8	15'-0"	160		1 4	171	4	171	4	171	4	171	4	171	4	Ц,
ALL SPANS				,			 											_
58 SCAB, LUMBER, SOFT WOOD	39-3880.08	324	2×8	3'-5"			 4	19	4	19	4	19	4	19	4	19	4	\perp
9 00	39-3880.08	81	2×8	6'-0"	30				4	32	4	32	4	32	4	32	4	L
STEEL HARDWARE, BLACK							 											
MACHINE BOLT WITH SQUARE		I		l		1 1					l			[
10 NUT 4HD THO WASHERS	43-2325.1-104	E10	1	10 *	3.5		 10		20		20		20		20 .		20	+
41 00	45-2525.1-2	£20	1	20 •	5.5		16	1	32	1	32	i i	32	i l	32	1	32	



COMPANION SHEETS





8-PILE PIER 0'-0" TO 6'-0"

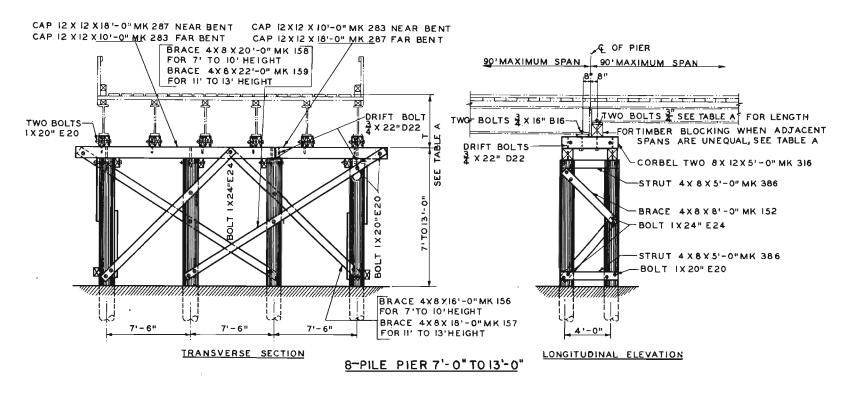
REQUIRED PILE CAPACITY

TOTAL LENGTH OF TWO ADJACENT SPANS	301	40'	601	80'	100,	120'	1401	1601	1801
TONS PER PILE	10	10	12	13	15	16	18	18	18

TABLE A

DEPTH OF BLOCKING AND LENGTH OF ANCHOR BOLT
WHEN ADJACENT SPANS ARE NOT FOUND.

IADL	<u>L A</u>		WHEN A	DJACEN	<u>IT SPA</u>	NS ARI	E NOT	EQUAL		
SPAN	_		TIMBER SPAN				STEEL	. SPAN		
31 714	'		151	151	20'	30'	40'	50'	6 0'	701
00	41 110	BLOCKING	2'-1"	יי7יו	1' - 5"	1'-0"	1'-0"	0'-9"	0'-6"	0'-3"
90	4' -11"	BOLT	40"	36"	34"	28"	28º	26"	22"	20"
80'	4'-107"	BLOCKING	2'-1"	17-7"	1'-5"	1'-0"	11-0"	0'-9"	0'-6"	0'-3"
8 0.	41-108	BOLT	40"	36"	34"	28"	28"	26"	22"	20"
701	4'-73"	BLOCKING	1'-10"	1'-4"	1'-2"	0,-8,	0'-9"	0'-6"	0'-3"	
70'	4'-/4	BOLT	36"	32"	30"	26"	26"	22"	20"	
60¹	4'-43"	BLOCKING	1'-7"	11-10	01-11"	0'-6"	0'-6"	Ou-3n		
•0	4-44	BOLT	34"	30"	28"	22"	22"	20°		
50'	4'-2"	BLOCKING	l'- 4"	0'-10"	0'-8"	0'-3"	0'-3"			
50	4-2-	BOLT	30"	26"	24"	20"	20"			
40'	3'-107"	BLOCKING	11-10	0'-7"	0'-5"					
40	3,7108	BOLT	28"	24"	22"					
30,	3'-10 3"	BLOCKING	יין – יוּ	0'-7"	0'-5"					
30	3 104	BOLT	28"	24"	22"					
20'	3'-5 3"	BLOCKING	0'-8"	0'-2"	[
20	3-37	BOLT	22"	″18#						
151	31-33" BLOCKIN		0'-6"							
13	3 3 T	BOLT	22"							



SPECIAL BLOCKING AT JUNCTION OF STEEL AND TIMBER SPANS

CLI	ASS 25-DOUBLE LANE					,			PIER	HEIGHT			
LINE	DESCRIPTION	STOCK NO	MARK	SIZE	ILE LEDGER	WEIGHT	0' TO	6'	7' TO 10'		11' TO 13'		LINE
				(INCHES) LENGTH WEIGHT OU (POUNDS) QU		QUANTITY	FBH	QUANTITY	FBM	QUANTITY	FBH		
1	PILE						8		8	1	8		1
	LUMBER, SOFT WOOD						•			1000	•		
.2	CAP	39-6630.12-1	-283	12 X 12	10'-0"	450	2	240	2	240	2	240	2
3	DO.	39-6630.12-18	.287	12 X 12	18'-0"	810	2	432	-2	.432	2	432	3
4	CORBEL	39-6616-12	316	8 X 12	51-0*	150	12	480	12	480	1.2	480] 4
5	STRUT	39-3340.08	386	4 X 6	51-0	50	4	53	6	80	6	80	5
6	BRACE	39-3340.08-08	152	4 X 8	8'-0"	80			4	86	4	86	6
7	DO	39-3340.08-16	156	.4 X 8	16'-0"	160			4	171			7
6	DO	39-3340.08-18	157	4 X 8	18'-0"	180					4	192	В
9	DO	39-3340.08-2	158	4 × 8	201-0	200			.4	213			.9
10	DO .	39-3340.08-22	159	4 X 8	22'-0"	220					4	235	10
	STEEL HARDHARE, BLACK												
11	DRIFT BOLT WITH SQUARE HEAD AND ONE WASHER	45-1636.07-22	D22	3/.4	22*	3.0	22		22		22		11
12	MACHINE BOLT WITH SQUARE NUT AND THO WASHERS	45-2525.1-2	E20	1	20.	5.6	28		68		68		12
13	DO	45-2325.1-24	E24	1	24"	6.5		, i	10		10		13
14	DO	43-2325.07-16	B16	3/4	16"	2.6	24		24		-24		14

COMPANION SHEETS

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TIMBER PILE PIERS FOR STEEL SPANS	114

TABLE A

INDEL	~	
STEEL SPAN	DIMENSION	BOLT R
15'	0'-53"	20"
20'	0'-73"	22*
30'	l'−0¾"	26*
40'	ı'−0≩"	26"
50'	1'-4"	30"
60'	I'-63#	32"
70'	l'-9≹"	36*
80'	2'-0}"	38"
90	2'-1"	38"

3/4" ANCHOR BOLT HITH SQUARE NUT AND TWO MASHERS FOR REQUIRED LENGTH SEE TABLE A SHEET 114 SIX REQUIRED AT ELNGTH SEE TABLE A SHEET 114 SIX REQUIRED AT EACH SUPPORT FOR EACH STEEL SPAN TWELVE REQUIRED AT EACH SUPPORT FOR EACH STEEL SPAN BOLT LENGTH STOCK NUMBER 18" 49-2325.07-185 20" 43-2325.07-25 22" 43-2325.07-25 24" 43-2325.07-26 28" 43-2325.07-26 28" 43-2325.07-28

BILL OF MATERIALS FOR ANCHOR BOLTS AND BEARING PLATES

26° 43-2325,07-266
28° 43-2325,07-28
30° 43-2325,07-506
32° 43-2325,07-32
34° 43-2325,07-346
35° 43-2325,07-366
40° 43-2325,07-405

BEARING PLATE 12 X 7/8 X 1'-5" MK P3500 (SHEET 132) STRUCTURAL STEEL SIX REQUIRED FOR EACH STEEL SPAN AT EACH SUPPORT STOCK NUMBER 49-7844,00

RIABLE BLOCKING 12" WIDE X 12'-0" LONG O

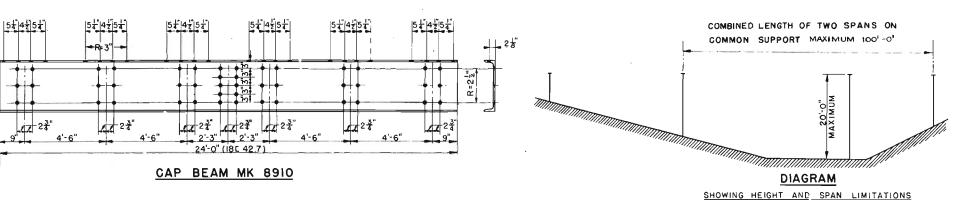
HIGHWAY

CLASS 25, DOUBLE-LANE

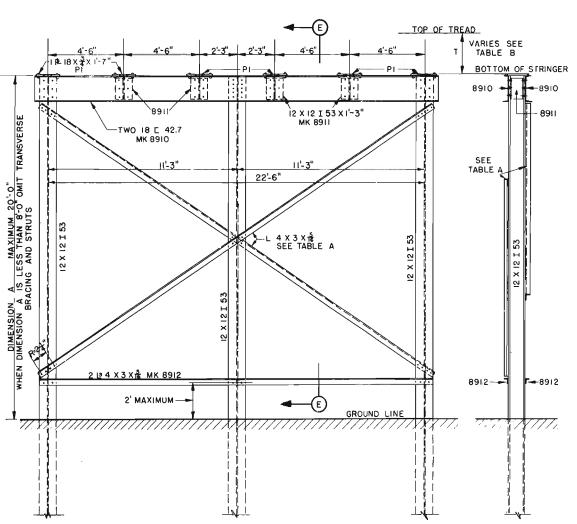
SHEET

154 155

150 118



SECTION E-E

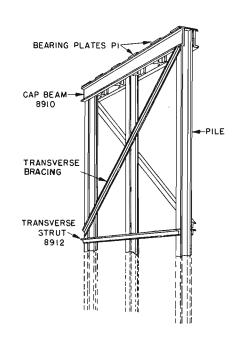


THREE PILE BENT

MAXIMUM PILE LOAD						
TOTAL LOADED LENGTH	TONS PER PILE					
30'	15					
40'	18					
5 0	20					
60,	22					
70'	24					
80,	27					
90'	29					
100'	31					

TABLE A BENT TRANSVERSE HEIGHT A BRACE MARK 8'-0" 8950 10'-0" 8949 12'-0" 8948 14'-0" 8947 16'-0" 894C 18'-0" 8945 20'-0" 8944

	TABLE B						
I	DISTANCE FROM TOP OF TREAD TO BOTTOM OF STRINGERS FOR VARIOUS SPANS						
SPAN	STEEL— STRINGER SIZE	TOP OF TREAD TO BOTTOM OF STRINGER T					
15'-0"	14 I 30	2'-27"					
20'-0"	16 I 36	2'-47"					
30'-0"	21 I 59	2'-97					
40'-0"	21 I 63	2'-10"					
50'-0"	24 I 87	3'-1 ਛੇ "					
60'-0"	27 I 91	3' -3 7 "					
70'-0"	30 I I08	3'- 6 7 "					
80'-0"	33 I I25	3'-10"					
90'-0"	33 I 132	3,-10₽,					



COMPANION SHEETS

FABRICATION DRAWING

BILL OF MATERIALS

GENERAL NOTES

SYMBOLS

ASSEMBLED VIEW

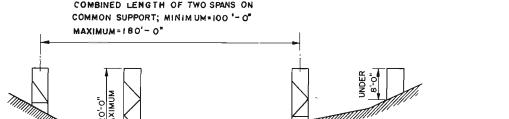
8909

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COMPANION SHEETS

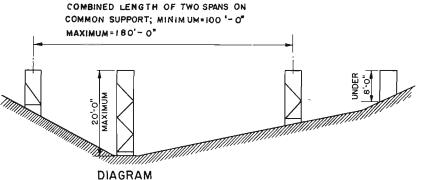
GENERAL NOTES SYMBOLS BILL OF MATERIALS FABRICATION DRAWING

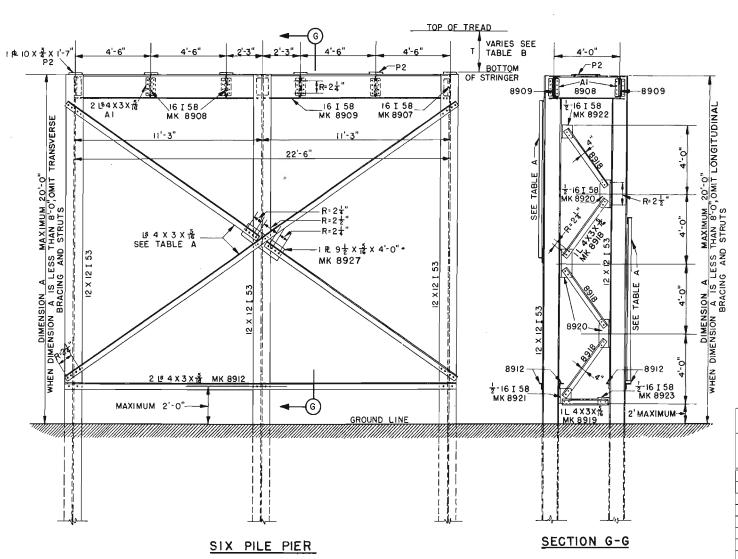
SHIMS



8909 TOP PLAN

SHOWING HEIGHT AND SPAN LIMITATIONS

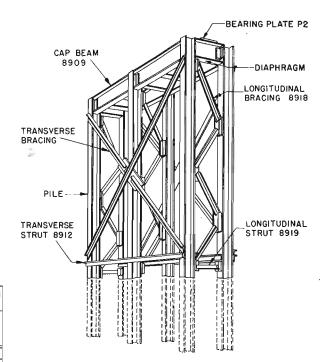




MAXIMUM					
PILE LOAD					
TOTAL	TONS				
LOADED	PER				
LENGTH	PILE				
110'	20				
120'	22				
130'	23				
140'	24				
150'	25				
160	26				
170	27				
180'	28				

<u>I AB</u>	LL	<u>A</u>					
BENT	TRANSVERSE						
HEIGHT A	BRACE	MARK					
8'-0"	8950	8951					
10'-0"	8949	8952					
12'-0"	8948	8953					
14'-0"	8947	8954					
16'-0"	8946	8955					
18'-0"	8945	8956					
20'-0"	8944	8957					

TABLE B DISTANCE FROM TOP OF TREAD TO BOTTOM OF STRINGERS. FOR VARIOUS SPANS TOP OF TREAD TO BOTTOM OF STEEL STRINGER SPAN SIZE STRINGER T 15'-0" 14 I 30 2'-2 20'-0" 16 I 36 2'-4 30'-0" 21 I 59 2'- 9 40'-0" 21 I 63 2'-10 50'-0" 24 I 87 3'-18 60'-0" 3'-38 27 I 91 3'- 6 g 70-0" 30 I 108 80'-0" 33 1125 3'-10' 90'-0" 3'-10 ਢ 33 I 132



ASSEMBLED VIEW

SHEET

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COMPANION SHEETS

STEEL PILE BENTS AND PIERS

GENERAL NOTES

SYMBOLS

BILL OF MATERIALS FOR ONE RIVETED STEEL BENT OR PIER STEEL PILE BENT HEIGHT STEEL PILE PIER HEIGHT 20' 18' 16' 14' 12' 10' 8' UNDER 8' 20' 18' QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY QUANTITY MARK LENGTH LINE USE STOCK NO (INCHES) 48-2900.16-058 8909 16 I 58 11'-2' 548 48-3790.18-43 8910 18 [42.7 24'-0' 1025 8911 12X12 I 53 1'-3' 66 1 CAP BEAM 2 DO 3 DIAPHRAGM 4 4 4 4 8911 12X12 1 55 1 -57 00 48-2900.16-058 8907 16 I 58 2!-11 58 172 48-2900.16-058 8908 16 I 58 3'-11 227 48-2550.4-035 41 4X3 X 5/16 1'-0 7 48-2900.16-058 8920 1/2 16 I 59 1'-6 1/2' 45 # DO 5 DO 6 CONNECTION ANGLE 4 4 4 4 4 4 - 5 40 40 40 5 3 3 3 3 3 40 40 6 40 40 7 CONNECTOR 3 3 8 _8 DO 3 3 9 00 3 3 10 10 11 100 2 2 -11 12 BEARING PLATE 13 DO P1 PL 18 x 3/4 1'-7" 73 P2 PL 10 x 3/4 1'-7" 40 47-7844.07 47-7844.07 12 13 48-2550,4-035 8919 L4X3X5/16 2'-91/4" 20 14 STRUTS AND BRACES 2 2 2 2 4 4 4 4 4 14 15 DO 9 9 12 6 6 3 15 16 DO 3 16 17 3 3 3 3 3 48-2550, 4-035 8919 L4X3X5/16 2"-9 1/4" 20 48-2550, 4-035 8948 L4X3X5/16 26"-5" 205 48-2550, 4-035 8945 L4X3X5/16 26"-4" 197 48-2550, 4-035 8946 L4X3X5/16 26"-4" 190 48-2550, 4-035 8947 L4X3X5/16 26"-6" 184 48-2550, 4-035 8948 L4X3X5/16 24"-10" 179 48-2550, 4-035 8948 L4X3X5/16 24"-10" 179 48-2550, 4-035 8950 L4X3X5/16 24"-5" 175 48-2550, 4-035 8950 L4X3X5/16 11"-0" 79 48-2550, 4-035 8951 L4X3X5/16 11"-0" 79 48-2550, 4-035 8952 L4X3X5/16 11"-4" 82 48-2550, 4-035 8953 L4X3X5/16 11"-4" 82 17 DO 18 DO 19 DO 18 19 20 20 DO 21 DO 21 22 23 22 DO 23 00 24 DO 24 25 26 25 DO 48-250.4-035 8955 L4X3X5/16 11'-10' 86 48-250.4-035 8955 L4X3X5/16 12'-10' 89 48-250.4-035 8956 L4X3X5/16 12'-10' 93 48-250.4-035 8956 L4X3X5/16 13'-4' 96 48-250.4-035 8957 L4X3X5/16 13'-4' 96 26 DO 27 28 DO 28 29 29 00 DO 30 24 24 24 24 24 24 24 24 24 24 24 24 24 24 24 24 24 24 23 232 220 220 128 176 164 164 152 152 140 140 96 31 RIVETS 43-6353.08-2 7/8 2" .53 32 DO 33 DO 43~6353.08-23 32 43-6353.08-25 92 33 34 00 43-6355.08-3 35 PILE

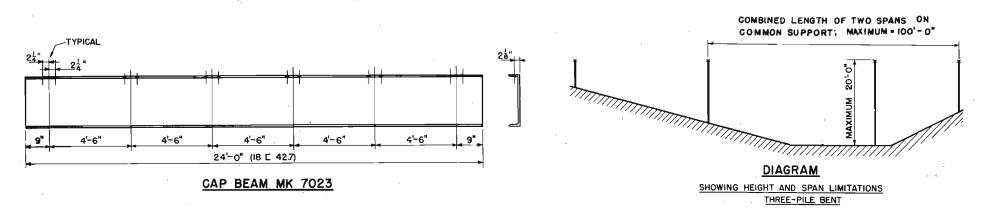
PILE LENGTH TO BE DETERMINED BY FIELD CONDITIONS.

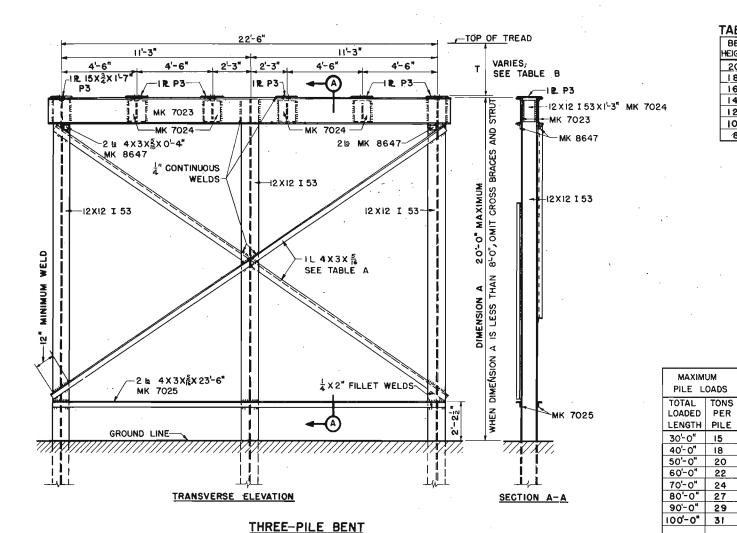
								STEEL	PILE BE	NT HEIGH	IT				_	STEEL P	ILE PIE	R HEIGHT				
		DESCRIPT	ION			20'	18'	16'	14'	12'	10'	8'	UNDER 6'	20'	18'	161	14'	12'	10'	8'	UNDER 81	4
INE USE	STOCK ,NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTI TY	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTITY	QUANTIT	YQUANTITY	QUANTITY	QUANTITY	QUANTITY	LINE
1 CAP BEAM	48-3790.18-43	7023	18 □ 42.7	24'-0"	1025	2	2	2	2	2	2	2	2									1
2 DO	48-2900.21-059	7033	21 I 59	25'-2 1/4"	1368									2	2	2	2	2	2	2	2	2
3 DIAPHRAGM	48-2900.21-059	7034	21 I 59	3'-11 1/2"	234									6	6	6	6	6	6	6	6	
4 DO		7024	12X12 I 53	1'-3"	66	4	4	Ħ	4	4	4	4	4									4
5 CONNECTOR	47-7844.04	7045	PL 5 1/2 X 3/8	3'-9"	26									2	2	2	2	2	2	2		5
6 DO	47-7844.05	8659	PL 8 X 1/2	1'-6"	20									9	6	6	3	3				6
7 00	47-7844.05	8660	PL 8 X 1/2	1'-0"	14	1								6	6	6	6	6	6	6		7
8 DO	47-7844.05	8651	PL 8 X 1/2	0'-6"	7						ر د			3	3	3	3	3	3	3		8
9 BOLTING CLIPS	47-7844.04	Ρ7	PL 3 X 3/8	0'-4 ע/אי	1									24	24	24	24	24	24	24	24	9
O SHELF ANGLE	48-2550.4-035	8647	L 4X3X5/16	0,-4.	2	4	4	4	4	4	4	4	4									10
1 BEARING PLATE	47-7844.07	Ρ3 -	PL 15 X 3/4	1'-7"	60	6	6	6	6	6	6	6	6									lu
2 00	47-7844.07	Ρ4	PL 10 X 3/4	1'-7"	40									6	6	6	6	6	6	6	6	12
3 STRUTS AND BRACES	48-2550.4-035	7025	L 4X3X5/16	23'-6"	169	2	2_	2	2	2	2	2		3	3	3	3	3	3	3		13
4 DO	48-2550.4-035	7026	L 4X5X5/16	28'-5"	205	2								2								14
5. DO	48-2550.4-035	7027	L 4X3X5/16	271-4"	197		2								2							1:
6 DO	48-2550.4-035	7028	L 4X3X5/16	26'-4"	190			2								2						16
7 00	48-2550.4-035	7029	L 4X3X5/16	25'-6*	184				2								2					11
8 DO	48-2550.4-035	70 30	L 4X3X5/16	24'-10"	179					2								2			, !	18
9 DO	48-2550.4-035	7051	L 4X5X5/16	24'-3"	175						2								2			15
0 DO	48-2550.4-035	7032	L 4X3X5/16	23'-10*	172							2								2		20
1 00	48-2550.4-035	7035	L 4X3X5/16	15'-9"	99	ï								4								21
2 00	48-2550.4-035	7036	L 4X3X5/16	15'-4"	96										đ							22
3 DO	43-2550.4-035	7037	L 4x3x5/16	12'-10"	93											4						23
4 DO	48-2550.4-035	70 38	L 4X3X5/16	12'-4"	89									!			4					24
.5 DO	48-2550.4-035	7039	L 4X3X5/16	11'-10"	86													4				25
6 DO	48-2550.4-035	7040	L 4X3X5/15	11'-4"	82														4			26
7. DO	48-2550.4-035	7041	L 4X3X5/16	11'-0"	79															4		27
8 DO	48-2550.4-035	8613		4'-1 15/16"	30									12	9	9	6	6	3	3		28
9 DO	48-2550.4-035	8622	L 4X3X5/16	2'-9 1/4"	20	L	L .							3	,	3	3	3	3	3		25
WELDING ROD (POUNDS)	46-3772.2-7		3/16	L		15	15	15	15	15	15	15	-11	40	37	37	34	34	31	31	20	30
PILE			12X12 I 53	Ī		3	3	3	3	3	3	3	3	6	6	6	6	6	6	6	- 6	31
2 PILE CAP						1				I				6	6	6	6	6	6	6	6	32

¹ PILE LENGTH TO BE DETERMINED BY FIELD CONDITIONS

COMPANION SHEETS

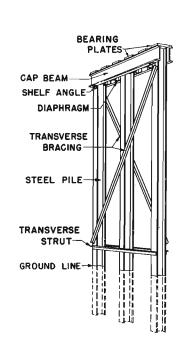
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SHIMS	





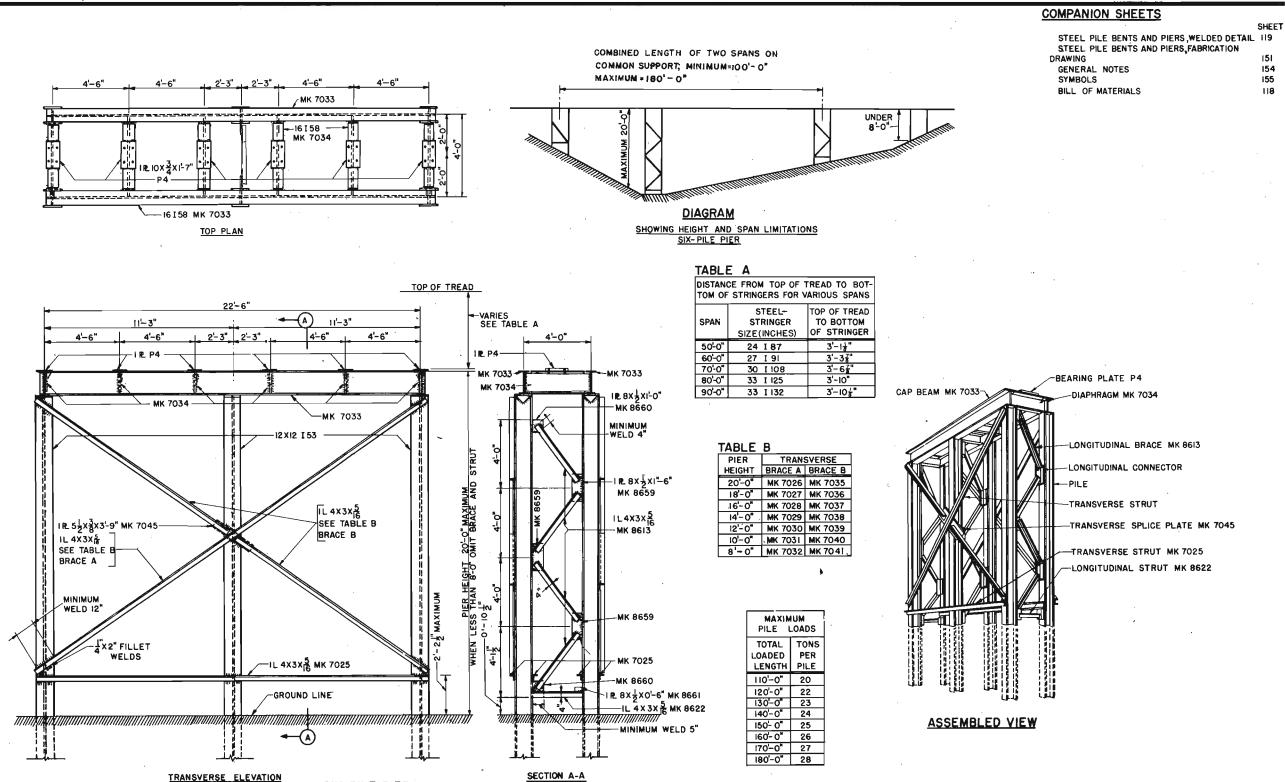
<u>TABLE</u>	<u>A</u>
BENT	TRANSVERSE
HEIGHT A	BRACING
20'-0"	MK 7026
18'-0"	MK 7027
16'-0"	MK 7028
14'-0"	MK 7029
12'-0"	MK 7030
10'-0"	MK 7031
8'-0"	MK 7032

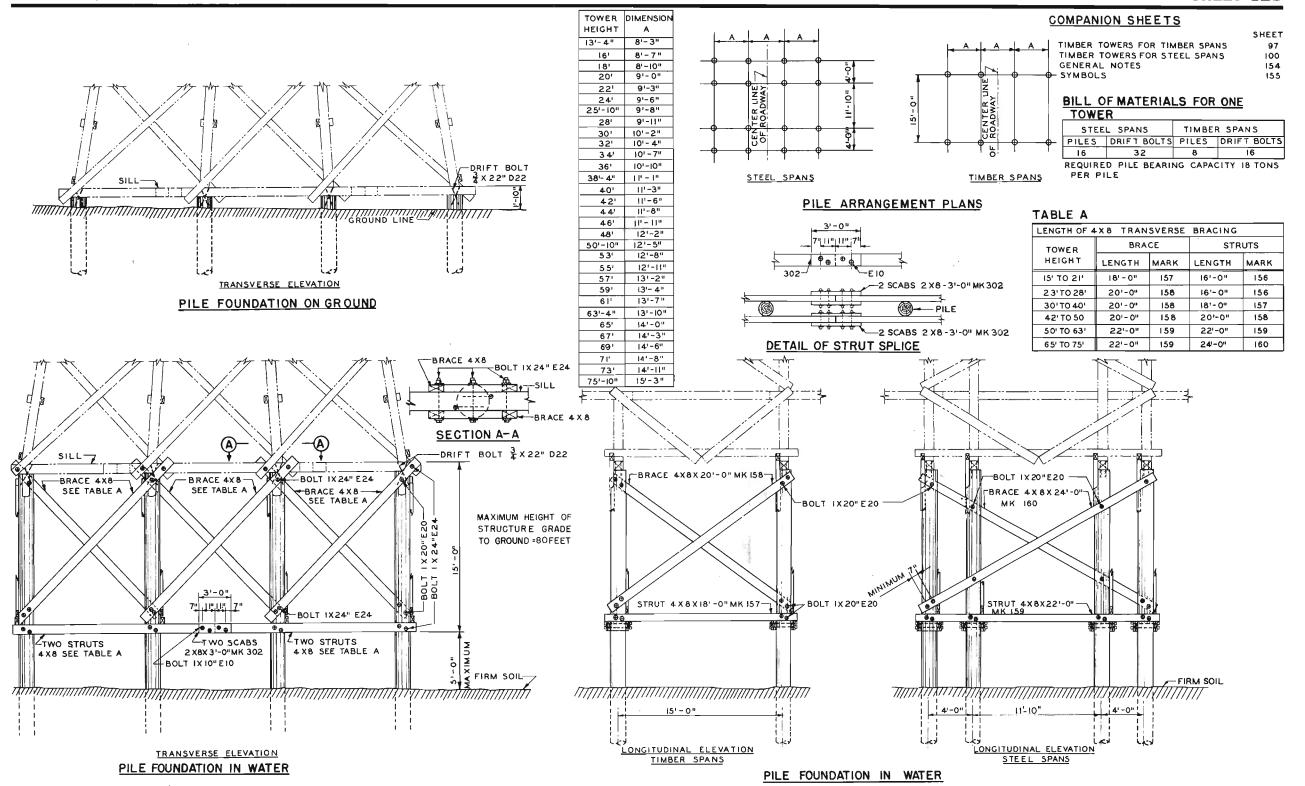
TABLE- B DISTANCE FROM TOP OF TREAD TO BOTTOM OF STRINGER FOR VARIOUS SPANS TOP OF TREAD STEEL-SPAN TO BOTTOM OF STRINGER SIZE STRINGER T 15'-0" 14 I 30 2'-28 20'-0" 16 I 36 2'-48 30'-0" 21 I 59 2'-97 40'-0" 21 I 63 2'-10" 50'-0" 24 I 87 3-18 60'-0" 27 I 91 3'-3å 70'-0" 30 I 108 3-62 80^L0" 90'-0" 33 I 125 33 I 132



ASSEMBLED VIEW

SIX-PILE PIER





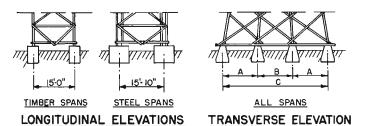
TIMBER SPANS

SHEET 154 155

© ROADWAY

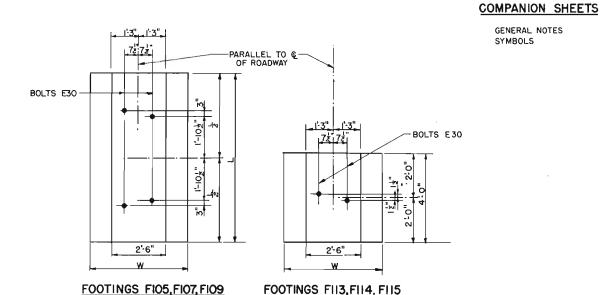
PLAN OF CONCRETE PEDESTALS

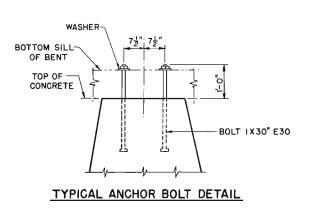
STEEL SPANS

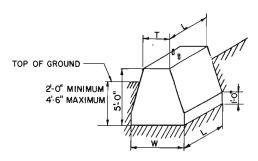


CONCRETE PEDESTALS

		STE	EL SPA	NS	TIMI	BER SPA	NS	FOOTIN	G MARK
	TOWER HEIGHT	Α	В	С	Α	В	С	TIMBER SPAN 15-0"	STEEL SPAN 15'-0" TO 90'-0
Ī	13'-4"	8-31	8-38	24-10	8'-3 ½"	8'- 3늘"	24'-10½"	FII5	FI09
	16'-0"	8'-7"	8'-7"	25'-9"	8'-7"	8'-7"	25'-9"	FI15	FI09
	18,0,	8'-10"	8'-10"	26-6	8'-10"	8,-10 _n	26'-6"	FII5	F109
2	20'-0"	9.0,	9'-0"	27:0"	9, 0,	9'-0"	27'-0"	F115	F109
	22:0"	9-3	9'- 3"	27'- 9"	9'-3"	9'-3"	27'-9"	FII5	F107
	24'0"	9'-6"	9'-6"	28'- 6"	9'-6"	9,-6"	28'-6"	F115	F107
	25'-10"	9'- 8"	9'- 8"	29'-0"	9-84	9'-84"	29 03	FII5	F107
-	28'-0"	9'-11"	9'-11"	29-9"	9'-11"	9'-11"	29'-9"	FII5	F107
	30'-0"	10'-2"	10'- 2"	30'-6"	10'-2"	10,5"	30'-6"	FI15	F107
3	32'-0"	10'-4"	10'-4"	31'-0"	10'-4"	10'-4"	31-0"	F114	F107
3	34'-0"	10'-7"	10'-7"	31-9"	10'-7"	10-7"	31-9"	FII4	F107
	36'-0"	10'10"	10'-10"	32'-6"		10'-10"	32'-6"	FII4	F107
	38'-4"	11'-0g	11'-0§"	33-12	11,0%,	11.0%	33'-2{8"	FII4	F107
	40-0"	11'-3"	11'-3"	33-9"	11'-3"	11'-3"	33'-9"	FII4	F107
	42'-0"	11-6"	11'-6"	34'- 6"	11'-6"	11'-6"	34'-6"	FII4	F107
_	44-0"	11-8"	11'-8"	35'-0"	11'-8"	11'-8"	35'-0"	FII4	FIO7
4	46'·0"	11, 11,		35'-9"	11,11,	44'-44"	35'-9"	FII4	F107
	48'-0"	12'-2"	12-2"	36'-6"	12,-5,	12'-2"	36'-6"	FII4	F107
	50-10	12-58	12-58°	37-48	12·5z	12'-5½	37-4½"	FII4	F105
	53'-0"	12'-8"	12'-8"	38'-0"	12'-8"	12'-8"	38'-0"	F113	F105
	55 ¹ 0'	12'-11"	12'-11"	38'-9"	12 [!] 11"	12'-11"	38'-9"	FII3	F105
	57:0"	13'-2"	13'-2"	39'-6"	13'-2"	13'-2"	39-6"	FII3	F105
5	59'-0"	13'-4"	13'-4"	40'-0"	13'-4"	13'-4"	40-0"	FII3	F105
	61-0"	13'-7"	13'-7"	40'-9"	13'-7"	13'-7"	40'-9"	F113	F105
	63-4"	1 3'-10"	13'-10"	41-6"	13-101	13,107,	41-6	FII3	F105
	65:0"	14'-0"	14-0"	42'-0 ^{ll}	14'-0"	14'-0"	42'-0"	FII3	F105
	67'0'	14-3	14'-3"	42'-9"	14'-3"	14'-3"	42'-9"	F113	FIO5
	69;0"	14'-6"		43'- 6"	14'-6"	14'-6"	43-6"	FII3	F105
6	71'-0"	14'-8"	14-8"	44'-0"	14'-8"	14'-8"	44'-0"	F113	F105
	73'-0"	14'-11"	14-11	44'-9"		14:11"	44'-9"	F113	F105
	75'-10"	15'-2 ⁵	15-28	45-78	15.2%	15'.2 2	45-85	F113	F105



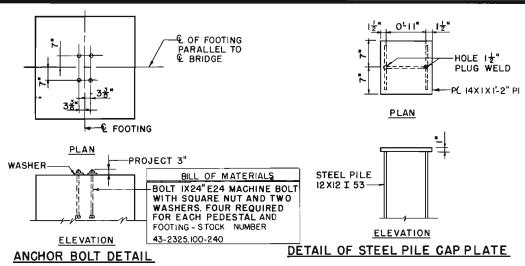




CONCRETE PEDESTAL
FOR FRAMED TIMBER TOWERS

CONCRETE PEDESTALS FOR FRAMED TIMBER TOWERS

	$\overline{}$					
MARK	WIDTH (W)	TOP (T)	LENGTH	CONCRETE CUBIC YARDS	MACHINE BOLT SQUARE I AND TWO W STOCK NO 43-	NUT, E 30, ASHERS
					QUANTITY	POUNDS
F105	5'-6"	2'-6"	7'-6"	6.0	4	31
F107	5'-0"	2'-6"	7'-0"	5.2	4	31
F109	4'-6"	2'-6"	6'-6"	4.5	4	31
F113	5'-0"	2'-6"	4'-0"	3.0	2	16
F114	4'-6"	2'-6"	4'-0"	2.7	2	16
F115	4'-0"	2'-6"	4'-0"	2.5	2	16



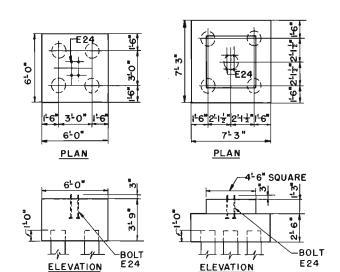


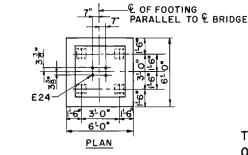
TABLE OF DIMENSIONS AND BILL OF MATERIALS FOR ONE PEDESTAL WITH TIMBER PILES

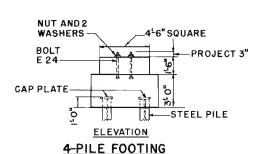
4-PILE FOOTING

<u>F135</u>

5-PILE FOOTING

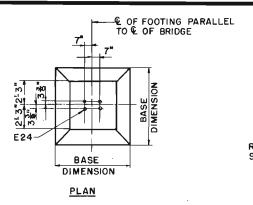
ADJACENT SPAN	HEIGHT OF TOWER	FOOTING MARK	NUMBER OF PILES PER FOOTING	CONCRETE (CUBIC YARDS)
15'	77'OR LOWER	F134	4	5.0
20'	77' OR LOWER	F134	4	5.0
30'	77'OR LOWER	F134	4	5.0
40'	77 OR LOWER	F134	4	5.0
50'	77'OR LOWER	F134	4	5. 0
60'	77'OR LOWER	F134	4	5.0
70'	77'OR LOWER	F134	4	5.0
80'	57'OR LOWER	f 134	4	5.0
	59' TO 77'	F135	5	5.8
90'	57'OR LOWER	F 134	4	5.0
	59' TO 77'	F135	5	5.8

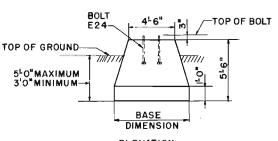




REQUIRED BEARING CAPACITY OF PILES, TONS PER PILE 4-PILE FOOTING

		_							
	HEIG	HT OF	TOWE	R					
ADJACENT SPAN	21' OR LOWER	23' TO 39'	41' TO 57'	59' TO 77'					
15'	12	13	14	16					
20'	12	13	15	17					
30'	13	14	16	18					
40'	14	15	17	19					
50'	14	16	18	20					
60'	15	17	19	21					
70'	16	18	20	22					
80'	17	19	21	23					
90'	18	20	22	24 긔					
II 5-PIL									





ELEVATION
CONCRETE PEDESTALS WITHOUT PILES

TABLE OF DIMENSIONS AND BILL OF MATERIALS FOR ONE PEDESTAL WITHOUT PILES

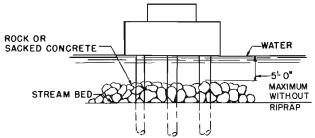
ADJACENT	HEIGHT OF	FOOTING	BASE	CONCRETE
SPAN	TOWER	MARK	DIMENSION	(CUBIC YARDS)
15'	39'OR LOWER	F 120	6 <u>-</u> 0,	6.0
	41' TO 77'	F_121	7 ' -0"	7. 4
20'	21 OR LOWER	F 120	6 <u>-</u> 0	6.0
	23'TO 77'	F 121	7 ' 0"	7. 4
30'	21' OR LOWER	F 120	6 <u>-</u> 0*	6.0
	23'TO 77'	F 121	7-0"	7. 4
40'	57 OR LOWER	F 121	7 <u>'</u> 0"	7. 4
	59'TO 77'	F 122	8 <u>'</u> 0"	9.1
50'	39' OR LOWER	F 121	_7 <u>'</u> -0"	7, 4
	41' TO 77'	F 122	8 <u>-</u> 0,	9. 1
60'	39' OR LOWER	F 121	7 <u>'</u> 0"	7.4
	41' TO 77'	F 122	8 <u>'</u> -0"	9. i
70'	21'OR LOWER	F 121	750	7. 4
	23'TO 77'	F 122	8 <u>-</u> 0,	9. 1
80'	21' OR LOWER	F 12 I	7 ⁴ 0"	7. 4
	23' TO 77'	F 122	8 <u>'</u> 0"	9.1
90,	57' OR LOWER	F 122	8 <u>r</u> O _"	9. 1
	59'TO 77'	F 123	9 <u>-</u> 0,	10.8

BILL OF MATERIALS FOR ONE FOOTING WITH STEEL PILES

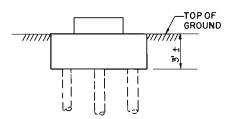
DESCRIPTION	STOCK NUMBER	MARK	SIZE (INCHES)	LENGTH	WEIGHT EACH	QUANTITY
CONCRETE						5. I CU YD
PILE			12X12I53			4
CAP PLATE	47-7844.1	PΙ	14X I	l ⁻ 2"	55LB	4
WELDING ELECTRODE	46-3772.25-5		<u>7</u> 32			4 POUNDS

COMPANION SHEETS

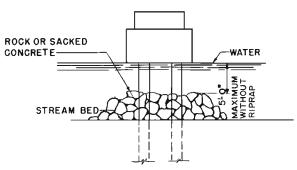
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FRAMED STEEL TOWERS	56



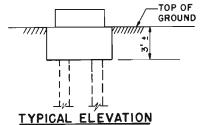
TYPICAL ELEVATION TIMBER PILE FOOTINGS IN WATER



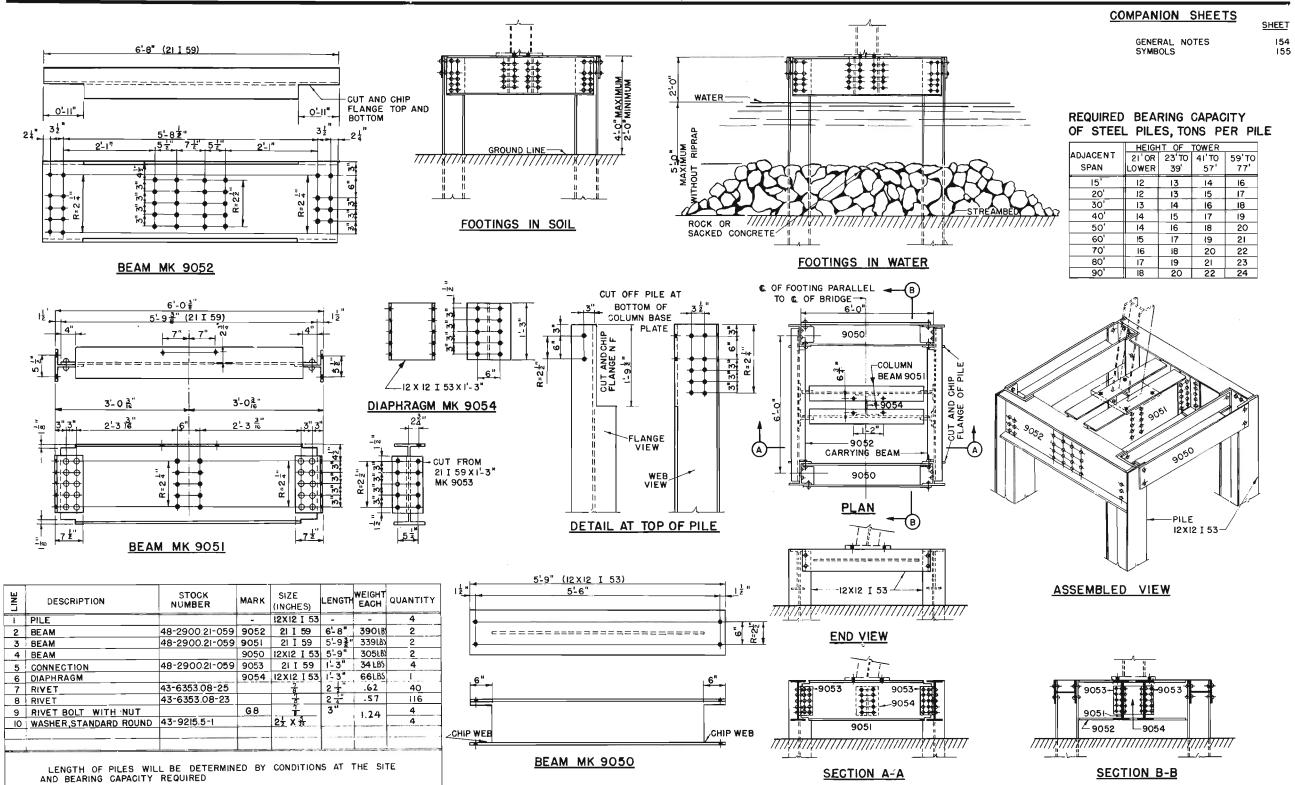
TYPICAL ELEVATION TIMBER PILE FOOTINGS IN SOIL

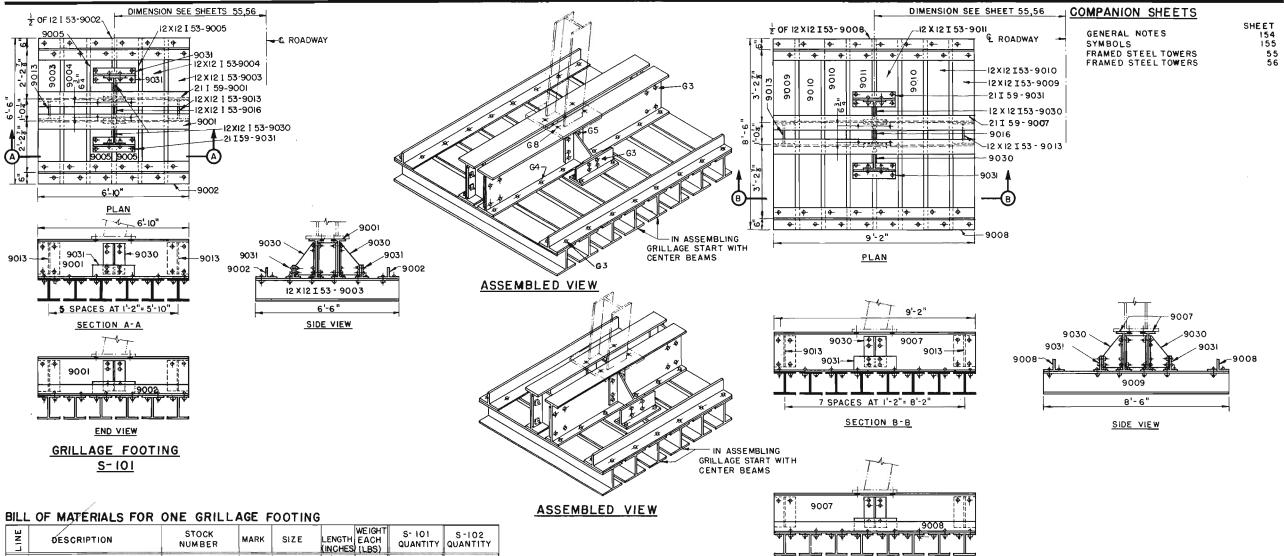


TYPICAL ELEVATION STEEL PILE FOOTINGS IN WATER



TYPICAL ELEVATION
STEEL PILE FOOTINGS IN SOIL





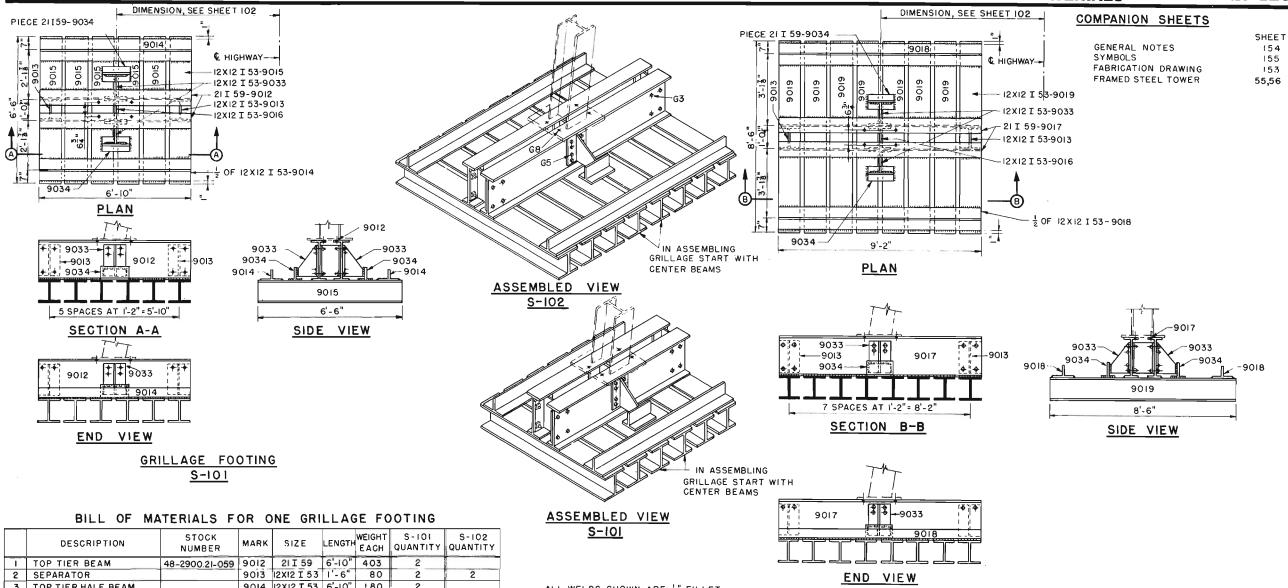
LINE	DESCRIPTION	STOCK NUMBER	MARK	SIZE	LENGTH (INCHES		S- 101 QUANTITY	S-102 QUANTITY
1	TOP TIER BEAM	48-2900.21-059	9001	21 I 59	6'-10"	403	2	
2	TOP TIER HALF BEAM		9002	12 X 12 153	6'-10"	180	2	_
3	BOTTOM TIER BEAM	20 0000000	9003	12 X 12 I 53	6'-6"	345	2	
4	BOTTOM TIER BEAM		9004	12 X 12 I53	6'-6"	345	2	
5	BOTTOM TIER BEAM		9005	12 X 12 I53	6'-6"	345	2	
6	TOP TIER BEAM	48-2900.21-059	9007	21 I 59	9'-2"	541		2
7	TOP TIER HALF BEAM	P.	9008	12X12I53	9'-2"	243		2
8	BOTTOM TIER BEAM		9009	12X12I53	8'-6"	450		2
9	BOTTOM TIER BEAM		9010	12 X 12 I 53	8'-6"	450		4
10	BOTTOM TIER BEAM		9011	12 X 12 I 53	8'-6"	450		2
Ш.	SEPARATOR		9013	12 X 12 I 53	1'-6"	80	2	2
12	SEPARATOR		9016	12 X 12 I 53	1'-6"	80	i i	I I
13	BRACE		9030	12 X 12 I 53	1'-6"	53	2	2
14	BRACE	48-2900.21-059	9031	21159	1,-11,	50	2	2
						UNIT		
	}					WEIGHT	19.189	
15	RIVET BOLT		G3	7	2 16"	.94	48	56
16	RIVET BOLT		G 4	7 8	2 1 "	.97	24	28
17	RIVET BOLT		G5	7 8	27 "	1.00	16	16
18	RIVET BOLT AND WASHER		G8	1	3 "	1. 09	4	4

GRILLAGE FOOTING <u>S-102</u>

SCHEDULE FOR SELECTION OF GRILLAGE FOOTING FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

END VIEW

OIL MIGHT OF AIL	- LITOIT AIN	<i>U</i> 1 4	W - IV			
	SPAN		OTINGS EIGHT O	FOOTINGS ON		
DESCRIPTION	BETWEEN	UP	23 '	41'	59'	ROCK
	TOWERS	TO	TO	TO	TO	ALL TOWER
		21	39'	57'	77'	HEIGHTS
DOUBLE LANE CLASS 25	15' TO 40'	5-101	S-101	5-101	S-101	S-101
DO	50'	5-101	\$-101	S-101	S-102	S-101
DO	60'	5-101	5-101	S-101	S-102	S-101
DO	70'	S-101	S-101	S-101	S-102	S-101
DO	80'	S-101	\$-101	S-102	S-102	S-101
DO	90'	S-101	S-101	S-102	S-102	S-101

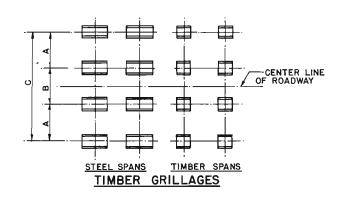


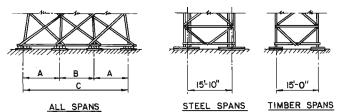
	END VIEW
ALL WELDS SHOWN ARE $\frac{1}{4}$ " FILLET WELDS UNLESS OTHERWISE NOTED	GRILLAGE FOOTING
	<u>S-102</u>

3 TOP TIER HALF BEAM 9014 |2XI2 I 53 | 6'-10" | 180 4 BOTTOM TIER BEAM 9015 12X12I53 6'-6" 345 9016 |2X12I53 |1'-6" 80 5 SEPARATOR 6 TOP TIER BEAM
7 TOP TIER HALF BEAM 48-2900.21-059 9017 21 1 59 9'-2" 541 9018 | 12X12 I 53 | 9'-2" | 243 9019 12X12I53 8'-6" 450 9033 12X12I53 1'-6" 53 8 BOTTOM TIER BEAM 9 BRACE 48-2900.21-059 9034 21159 1'-2" 35 IO BRACE 2 TOTAL WEIGHT 15 II RIVET BOLT 16 G5 12 RIVET BOLT 16 16 16 13 RIVET BOLT AND WASHER G8 5 14 WELDING ELECTRODE 46-3772.2-7 9 LBS I2 LBS.

SCHEDULE FOR SELECTION OF GRILLAGE FOOTINGS FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

	F	FOOTINGS			
SPAN	H	ON ROCK			
BETWEEN	UP TO	23' TO	41' TO	59' TO	ALL TOWER
TOWERS	21'	39'	57'	77'	HEIGHTS
15' TO 40'	S-101	S-101	S-101	S-101	S-101
5 0'	S-101	5-101	S-101	S-102	S-101
60'	101-2	S-101	S-101	5-102	S-101
70'	S-101	S-I 0I	S-101	S-I 02	S-101
80'	S-101	S-101	S-102	S-I 02	S-101
90'	S-101	S-101	5-102	S-102	5-101



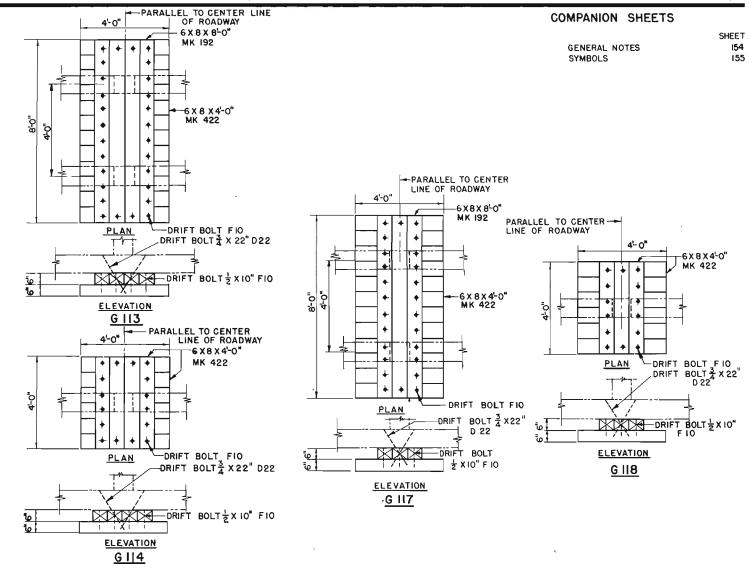


TRANSVERSE ELEVATION

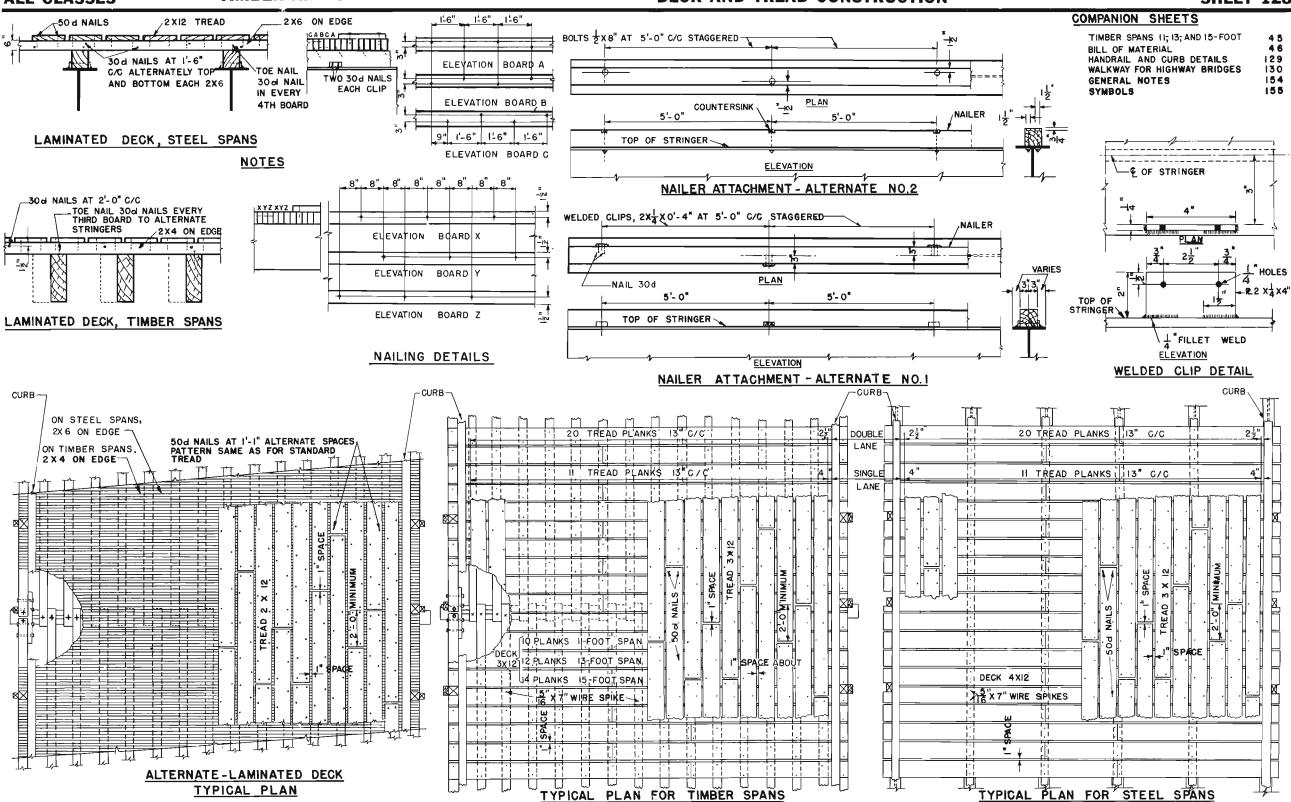
LONGITUDINAL ELEVATIONS

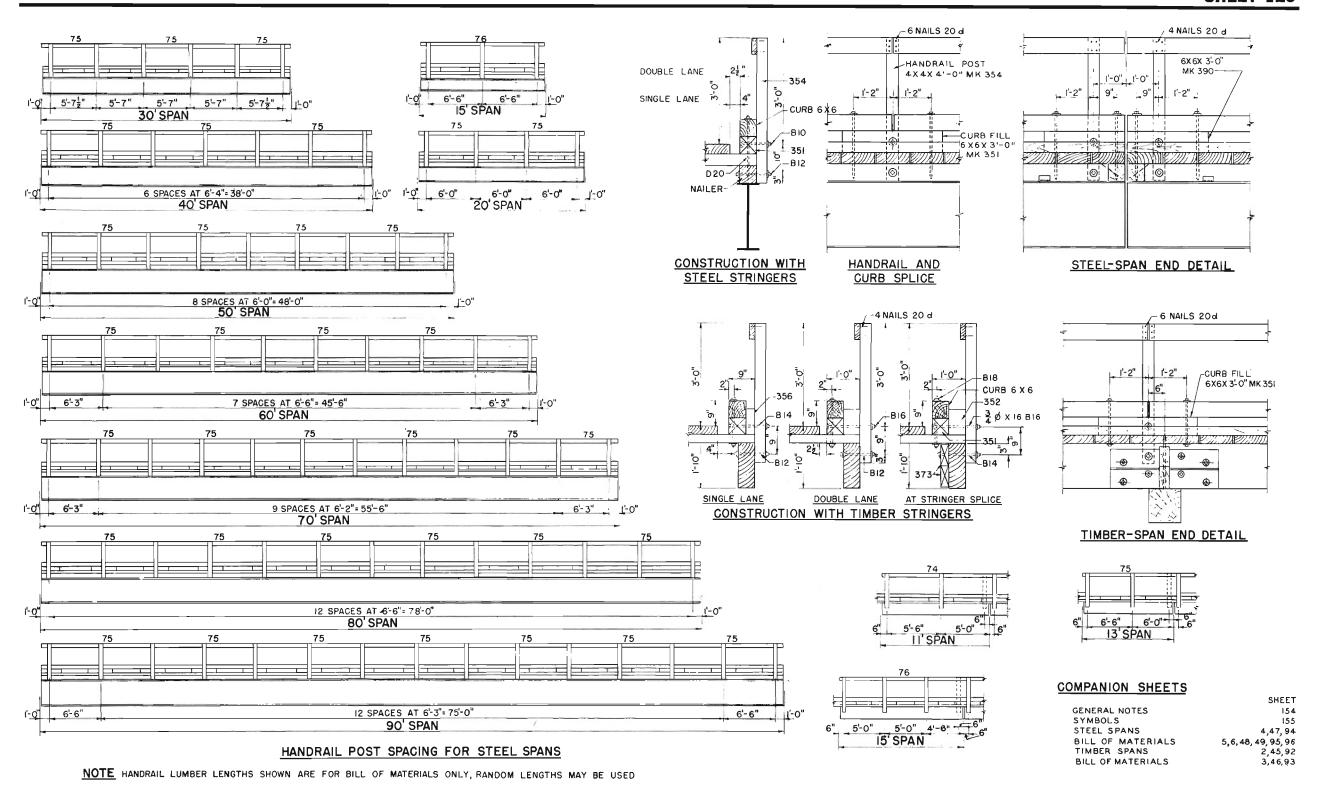
15'-0"

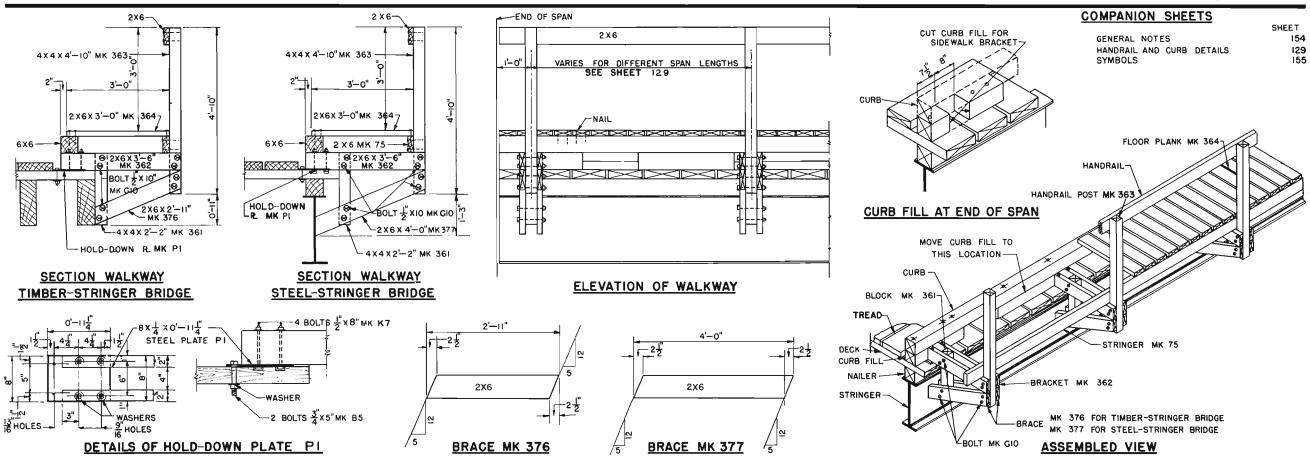
TIMBER		LLAGE STEE		VS	TIMBER SPANS			FOOTING MARK		
	TOWER		1		1 1141					
STORIES	HEIGHT	Α	В	C	A	В	С	TIMBER SPANS 15	STEEL SPANS 15' TO 90'	
1	13'-4"	8-3 } "	8-3출	24-10 g	8 <u>'</u> -3₺"	8-3½"	24-10분	G 118	GII7	
	16'	8'-7"	8'-7"	25'-9"	8-7"	8'-7"	25'-9"	G I I 8	G117	
	18'	8'-10"	8'-10"	26'- 6"	8'-10"	8'-10"	26-6"	G 118	G117	
_	20'	9-0"	9'-0"	27-0"	9'-0"	9-0"	27'-0"	G 118	GII7	
2	22'	9'-3"	9'-3"	27-9"	9'-3"	9'-3"	27-9"	G 118	G 117	
	24	9'-6"	9'-6"	28'-6"	9'-6"	9,-6,	28'-6"	G 118	G 117	
	25'-10"	9'-8"	9'-8"	29'-0"	9'-84"	9-84	29'-04"	G 118	G117	
	28'	9'-11"	9'-11"	29'-9"	9'-11"	9'-11"	29'-9"	G 118	G117	
	30'	10'-2"	10'-2"	30'-6"	10-2"	10-2"	30'-6"	G 118	G 117	
7	32'	10-4"	10'-4"	31'-0"	10'-4"	10'-4"	31-0"	G 118	G 117	
3	34'	10'-7"	10'-7"	31-9"	10'-7"	10'-7"	31'-9"	G 118	G 117	
	36'	10,-10,	10'-10"	32'-6"	10'-10"	10,-10,	32'-6"	G II8	G 117	
	38'-4"	11'-05	11,08,	33-17	11'-07"	11'-0 2	33-2 ⁵	G 118	G 117	
	40'	11'-3"	11-3"	33'-9"	11'-3"	11'-3"	33, 9,,	G 118	G 117	
	42'	11'-6"	11'-6'	34'-6"	11'-6"	11 ^L 6"	34'-6"	G118	- G 117	
	44'	11'-8"	11'-8"	35'-0"	11,-8,	11'-8"	35'-0"	G 118	G 117	
4	46'	11'-11"	14'-11"	35'-9"	11,-11 _a	11'-11"	35'-9"	G 118	G 117	
	48'	12'-2"	12'-2"	36'-6"	12'-2"	12'-2"	36-6"	G118	G 117	
<u> </u>	50'-10"	12-5	12-58	37 ^L 4 8"	12-5분	12'-5날	37-42"	G 118	G 117	
	53'	12'-8"	12'-8"	38'-0"	12'-8"	12-8"	38-0"	G114	G 113	
	55'	12'-11"	12'-11"	38'-9"	12'-11"	12'-11"	38'-9"	G 114	G 113	
_	57'	1352"	13-2	39'-6"	13'-2"	13'-2"	39'-6"	G114	- G 113	
5	59'	13'-4"	13-4"	40-0"	13'-4"	13'-4"	40-0"	G114	G 113	
	61'	13'-7"	13'-7"	40'-9"	13 ^L 7"	13-7"	40'-9"	G 114	G 113	
	63'-4"	13-10"	13-10"	41-6"	13'-104"	13404"	41-63"	G 114	G 113	
	65'	14-0"	14'-0"	42-0"	14'-0"	14'-0"	42'-0"	G 114	G 113	
	67'	14'-3"	14'-3"	42'-9"	14'-3"	14'-3"	42'-9"	G 114	G 113	
6	69'	14'-6"	14'-6"	43'-6"	14'-6"	14'-6"	43'-6"	G 114	G 113	
U	71'	14'-8"	14-8"	44'-0"	14'-8"	14'-8"	44'-0"	G 114	G 113	
	73'	14'-11"	4'-1 "	44'-9"	14'-11"	14'-11"	44'-9"	G 114	G 113	
	75'-10"	15'- 2g	15-25	45'-7 2 "	15¹-2₹"	15'-27	45'-85"	G 114	G 113	



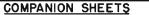
BILL OF MATERIALS FOR ONE TIMBER GRILLAGE G 118 G 113 G 117 G 114 WEIGHT STOCK QUANTITY FBM QUANTITY FBM QUANTITY FBM QUANTITY FBM MARK SIZE LENGTH EACH DESCRIPTION LINE NUMBER (INCHES) (LBS) LUMBER, SOFT WOOD I GRILLAGE 192 6X8 8^L0" | 120 128 39-3360.08 4 422 6X8 4'-0" 60 2 GRILLAGE 39-3360.08 12 192 192 144 STEEL HARDWARE, BLACK D22 22" 2.75 DRIFT BOLT 43-16 36.07-22 10" 0.6 4 DRIFT BOLT 43-1636.05-I FIO 26 14 28



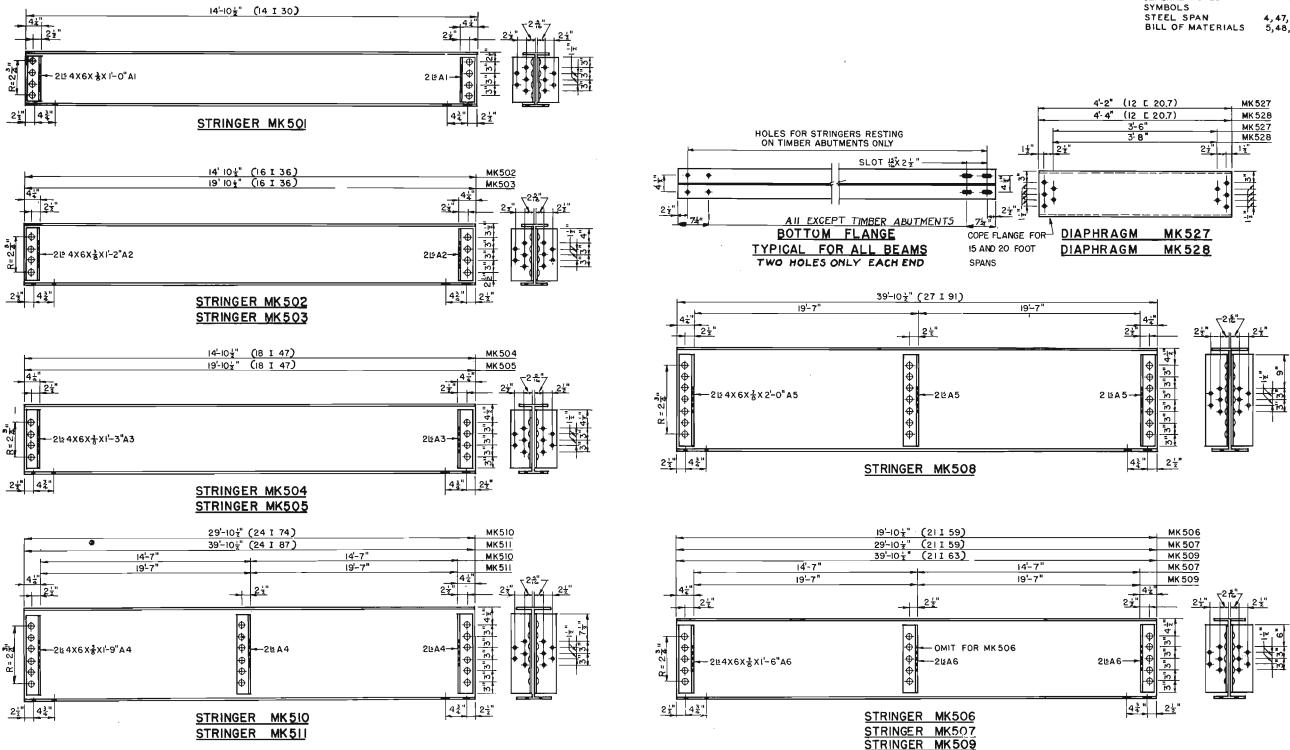




	BILLS OF MATERIALS FOR ONE WALKHAY R	OR 11-, 13-, AND 15-FOOT	TIMBER SPANS	AND FOR	5-TO 90-	ROOT ST	EEL SPAN	s																						
							WALKWAY FOR BRIDGE WITH TIMBER STRINGERS							Walknay for Bridge with Steel Stringers																
	DESCRIPTION	STOCK NUMBER		SIZE (INCHES)			11'-0" SPAN		13'-0" SPAN		15'-0" SPAN		15'-0	15'-0" SPAN		201-0# SPAN		30'-0" SPAN		SPAN	501 -01	SPAN	SPAN 601-		70'-0" SPAN		80'-0" SPAN		901-	O* SPAN
прм			MARK		;) \ \	UNIT WEIGHT (POUNDS)		FBM	CUANTITY	(ABM	CUANTIT	Y F8M	QUARTITY	FBM	CUANTIT	n FBM	CNANTITY	FBM	QUANTITY	FBM	QUANTITY	' FBM	DUANTITY	FBM	QUANTITY	FBM	QUANTITY	РВ М	QUANTIT	Y FEN
	LUMBER SOFT WOOD								_					·											•					
1	BLOCK	39-3340.04	361	4 X 4	21-24	11	2	6	2	6	3	9	3	9	4	12_	6	18	7	21	9	_26	10	29	12	35	13	38	15	44
2	PRACKET	39-3228.06	362	2 X 6	3'-6"	13	4	14	4	14	6	-21	6	21	8	28	12	.42	14	40	18	63	20	70	24	84	26	91	30	105
3	HANDRAIL POST	39-3340.04	363	4 X 4	4'-10"	24	2	13	2	13	3_	20	3	20	4	26	6	39	. 7	45	و ا	58	10	65	12	78	13	Au	15	97
4	FLOOR PLANK	39-3228.06	364	2 X 6	31-04	11	19	57	23	69	26	78	26	78	35	105	52	156	69	207	87	261	104	312	121	363	138	414	155	465
5	BRACE	39-3228.06	576	2 x 6	2'-11"	11	•	12	4	12	3	18																<u> </u>		
6	BRACE	39-3228.06	377	2 X 6	4'-0"	15							6	24	8	32	12	48	14	56	18	72	20	80	24	96	26	104	30	120_
	STRINGER	39-3228.06-14	75		141~0#				1	14									3	42	4	56	5 -	70	6	84	6	84	7	98
8	STRINGER	39-3228.06-12	74	2 x 6	12'-0*	45	1	12							2	24	3	36												
	STRINGER	39-3880,04-16	76	2 X 6	16,-0.	60			1		1	16	1	16																
	STEEL HARDWARE, BLACK																						•		'		•			
_10	HOLD-DOWN PLATE	47-7844.03		8 X ‡	114.	64	2		2		3		3		<u>ų</u>		6		7		9		ro		12		13		15	
11	BOLT WITH SOUARE NUT AND WASHER	43-2325.07-05	85	3/4	51	1.0	4		4		6		6		В		12		14		18		20		24		26		30	
12	BOLT, SQUARE HEAD WITH SQUARE NUT AND WASHER	43-2325.05-08	к7	Ł	8*	0.5	8		8		12		12		16		24		28		36		40		48		52		60	
13	BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.05-1	GIO	÷	10*	0.7	16		16		24		24		32		48		50		72		80		96		104	, ¬	120	
14	MAILS	42-6028.3-2		20 d		0.04	84		100		116		116		156		232		304		364		456		532		604		680	
																												-	1	

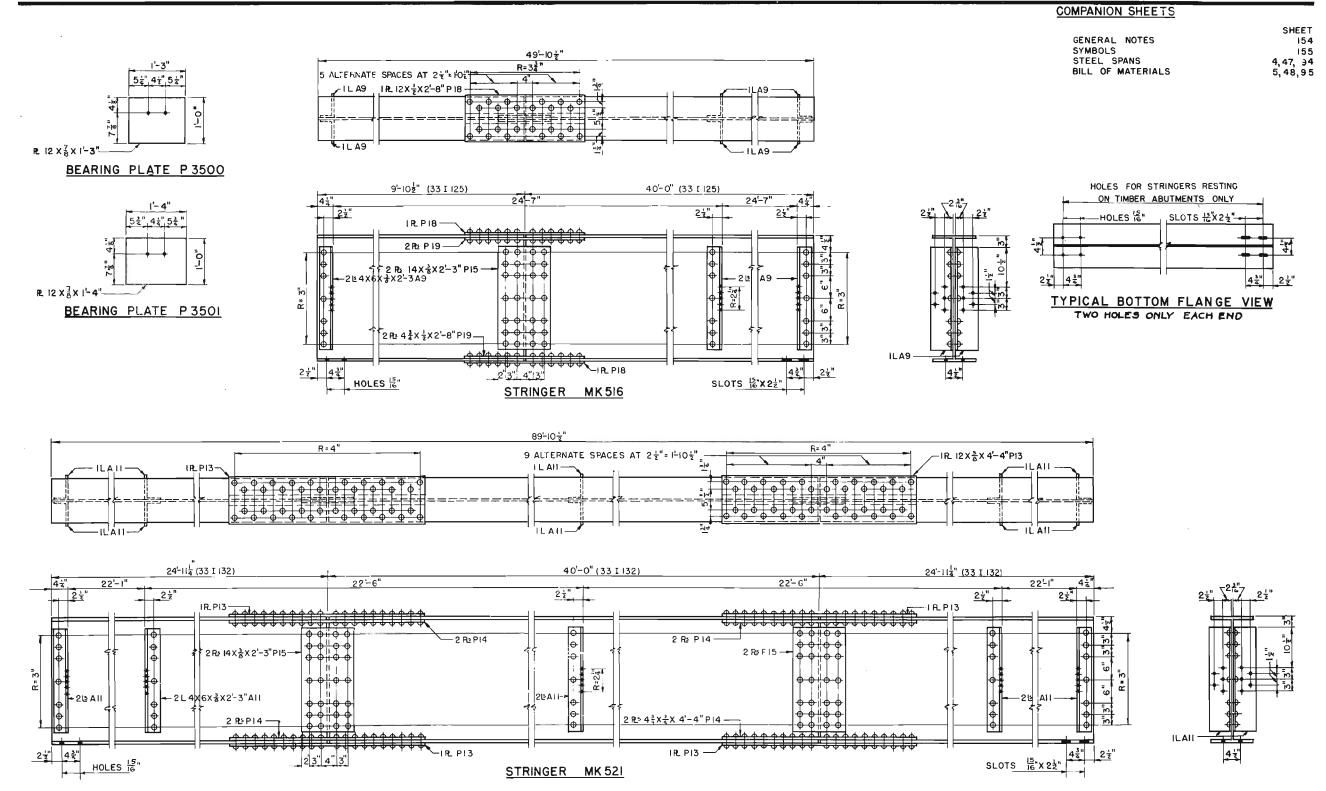


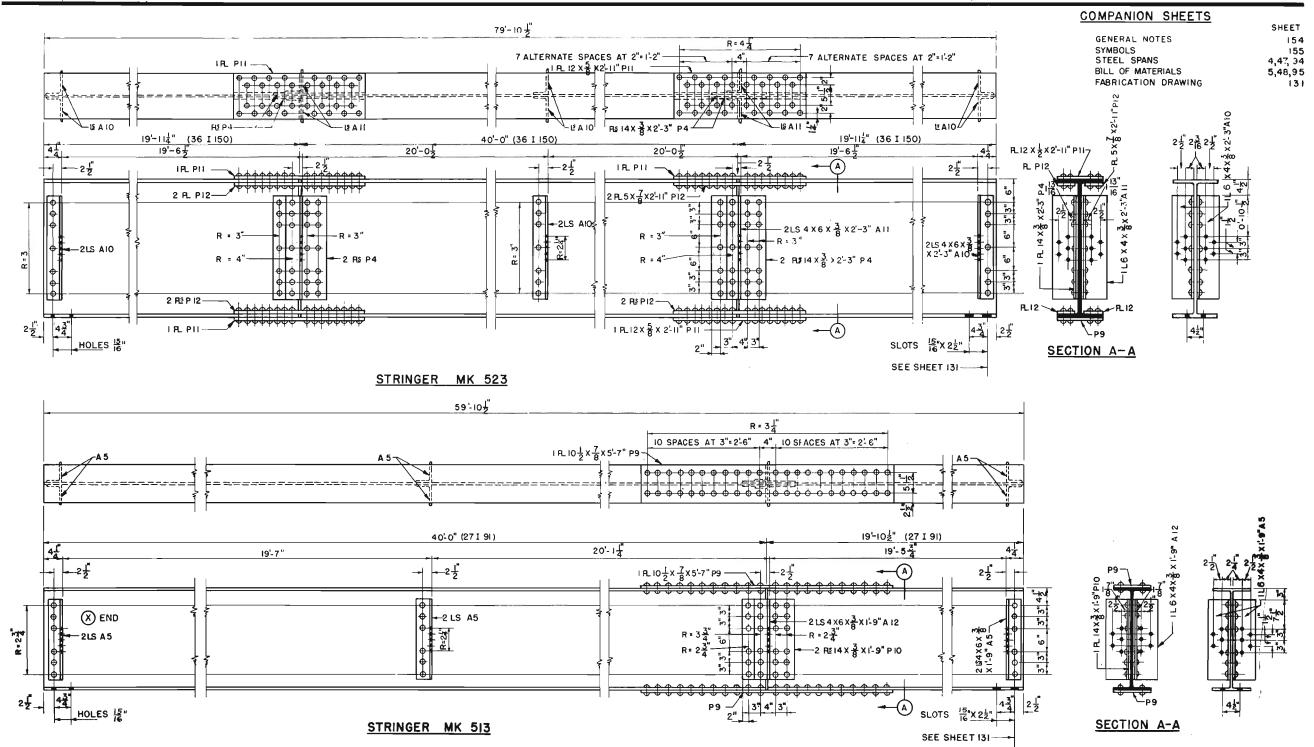




SUPERSTRUCTURE,

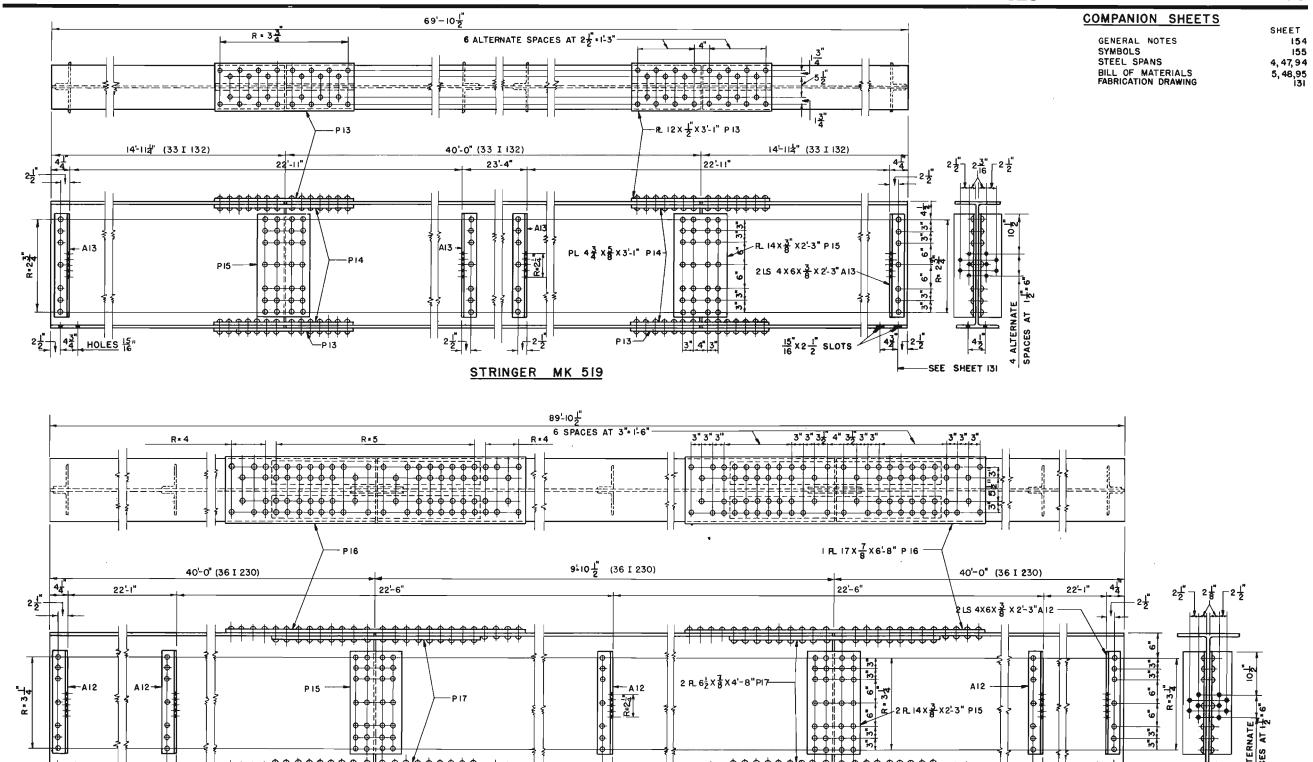
STEEL SPANS





HIGHWAY ALL CLASSES

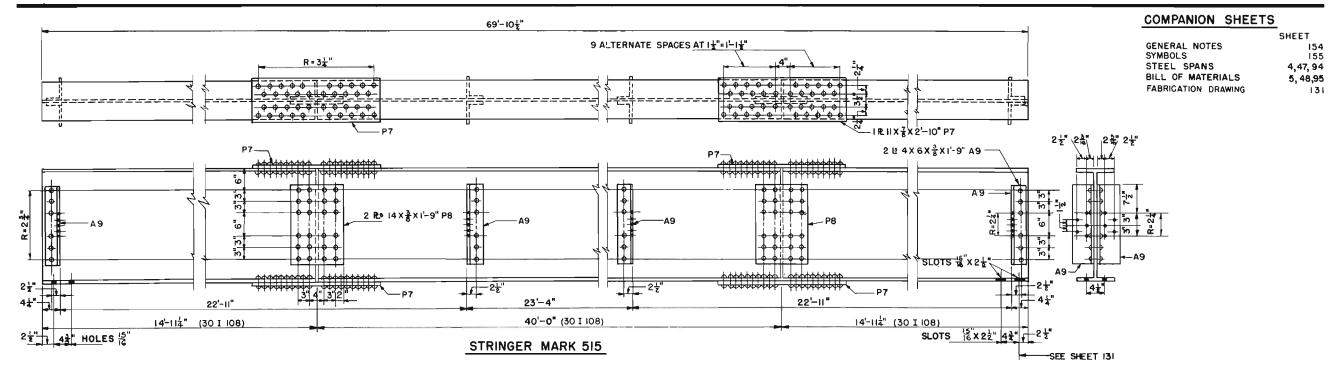
22 HOLES

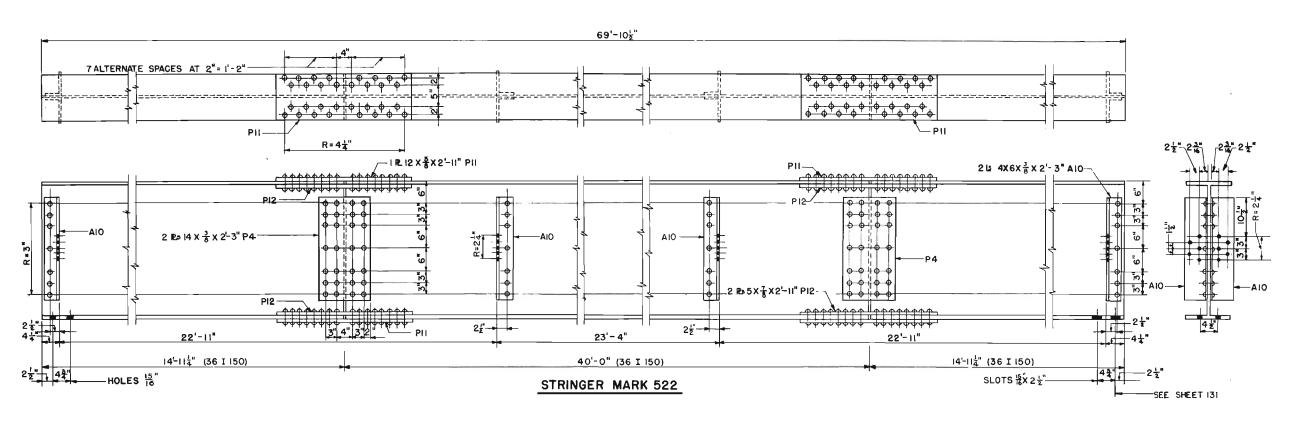


STRINGER MK 526

2 1 SLOTS 15 12 43

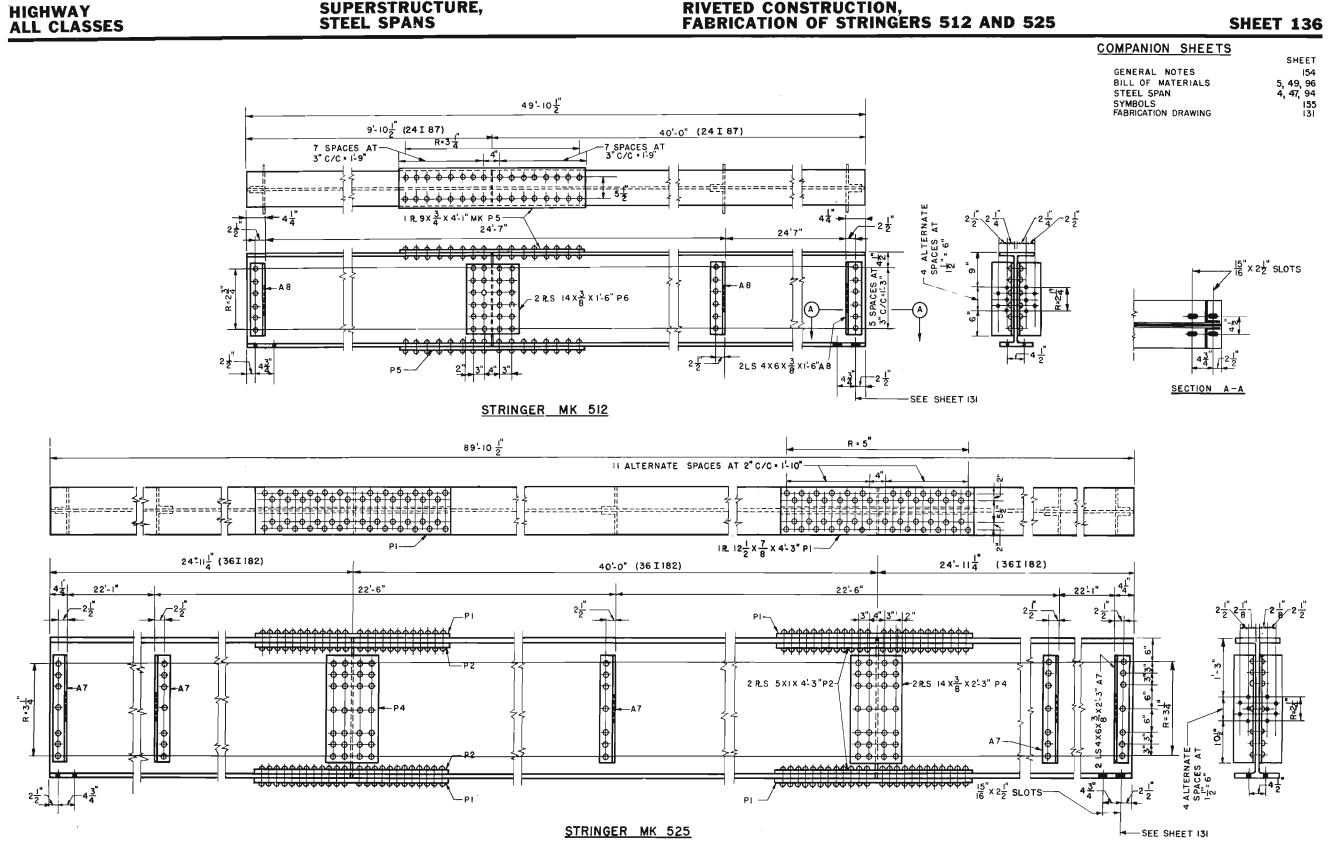
SEE SHEET 131

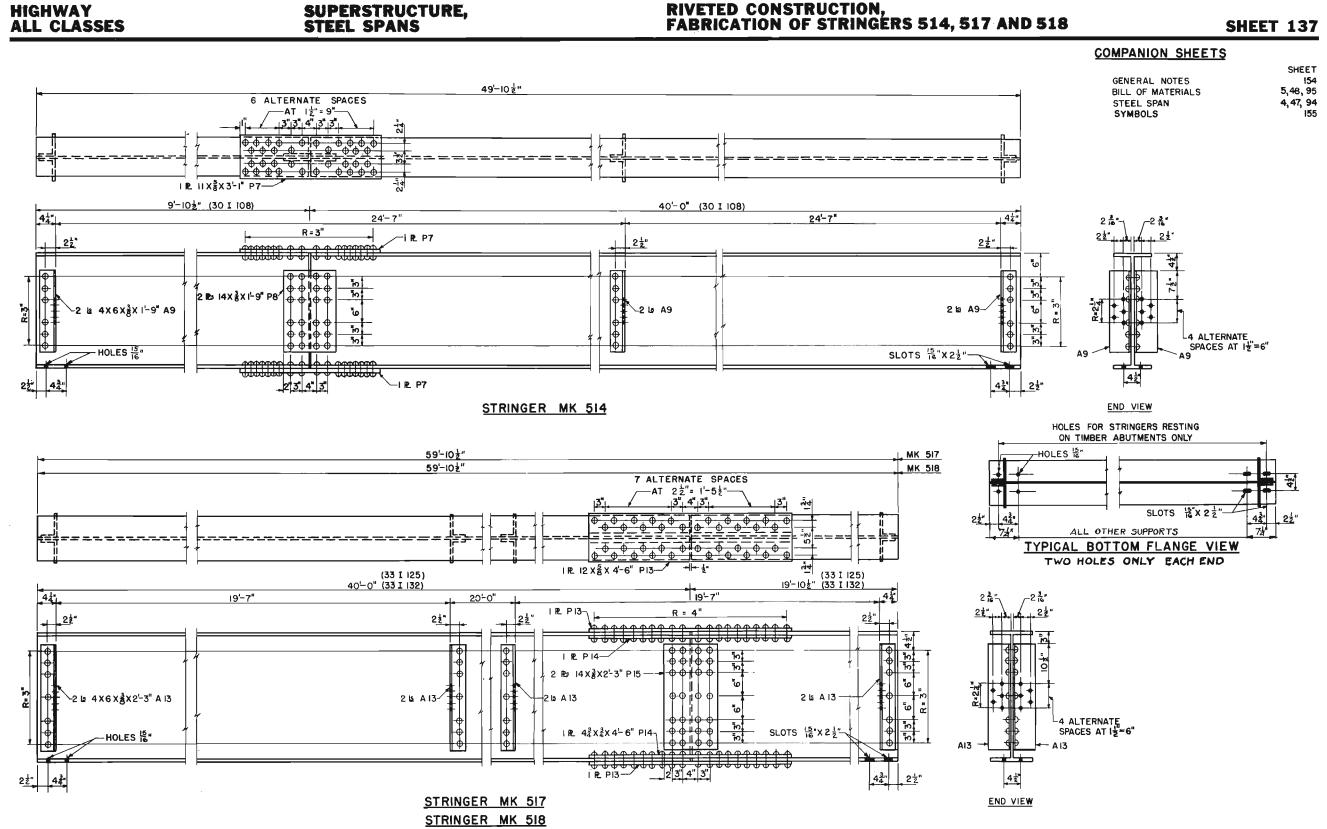




HIGHWAY

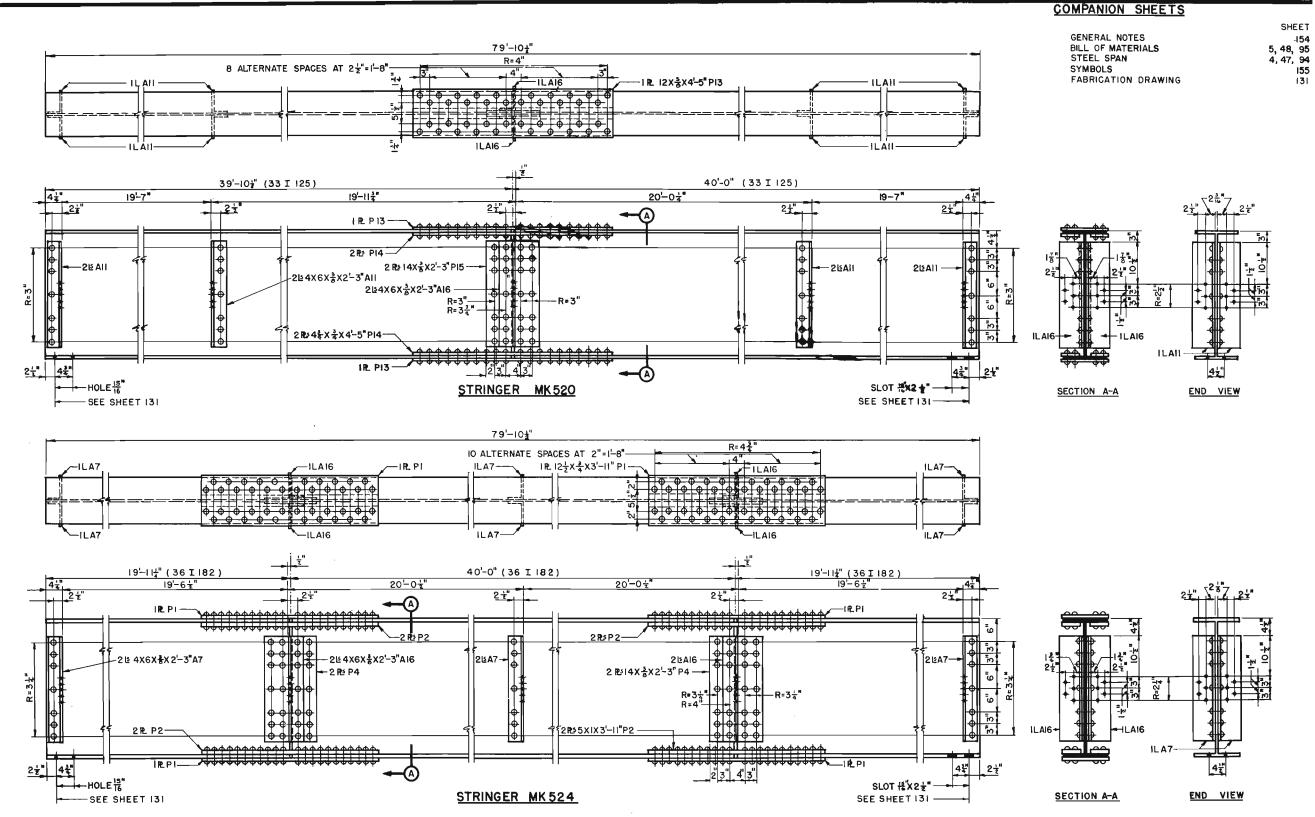
ALL CLASSES

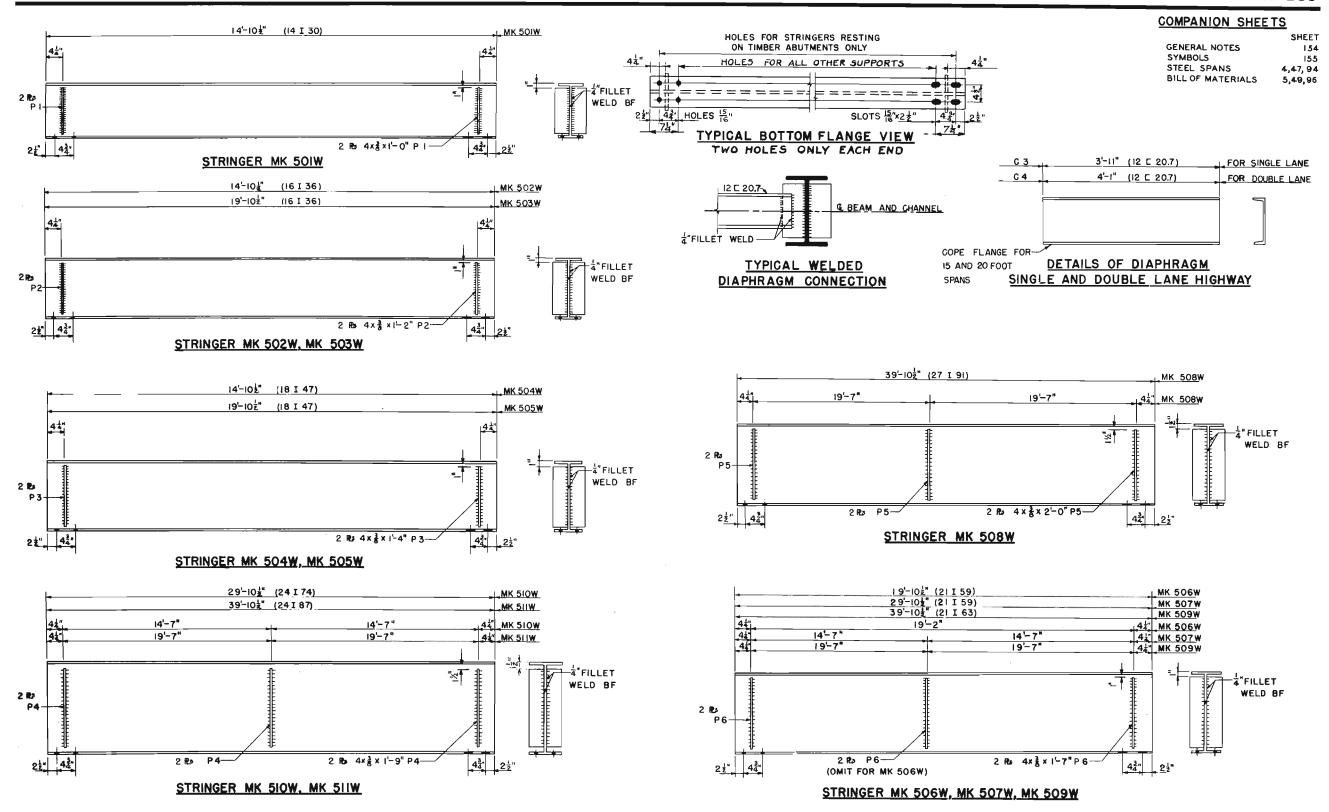


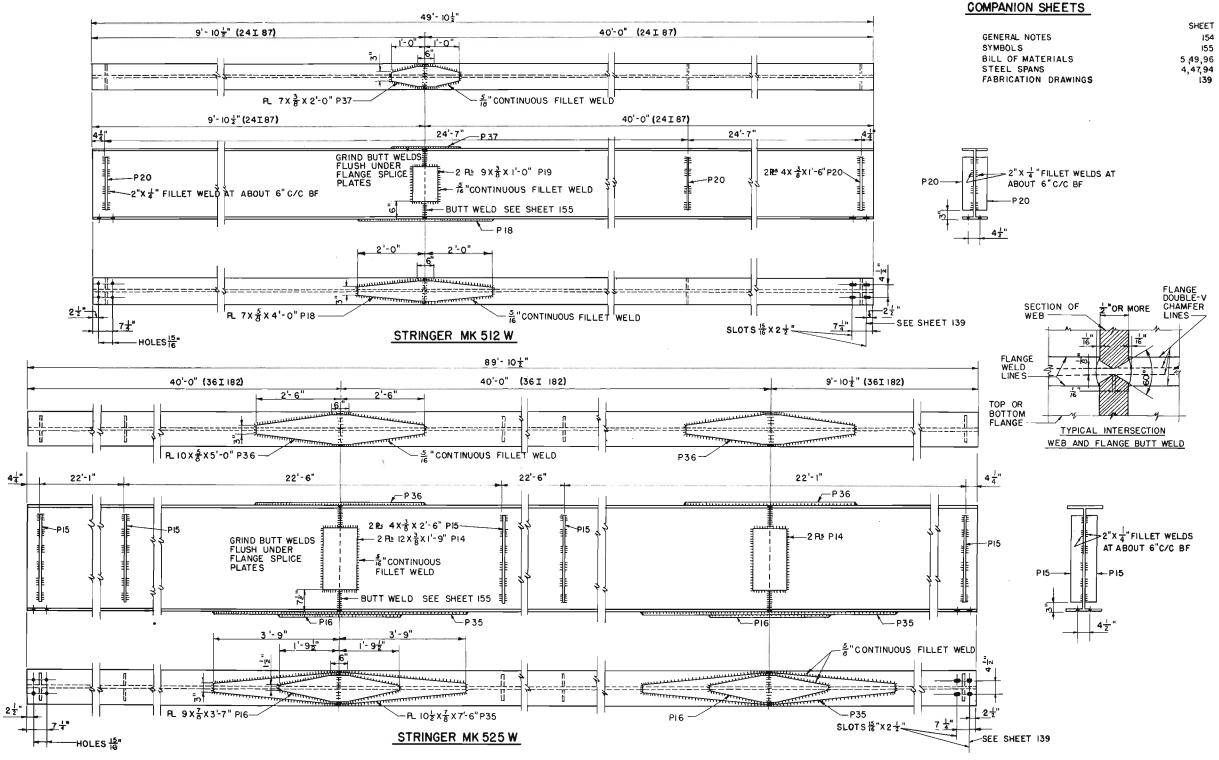


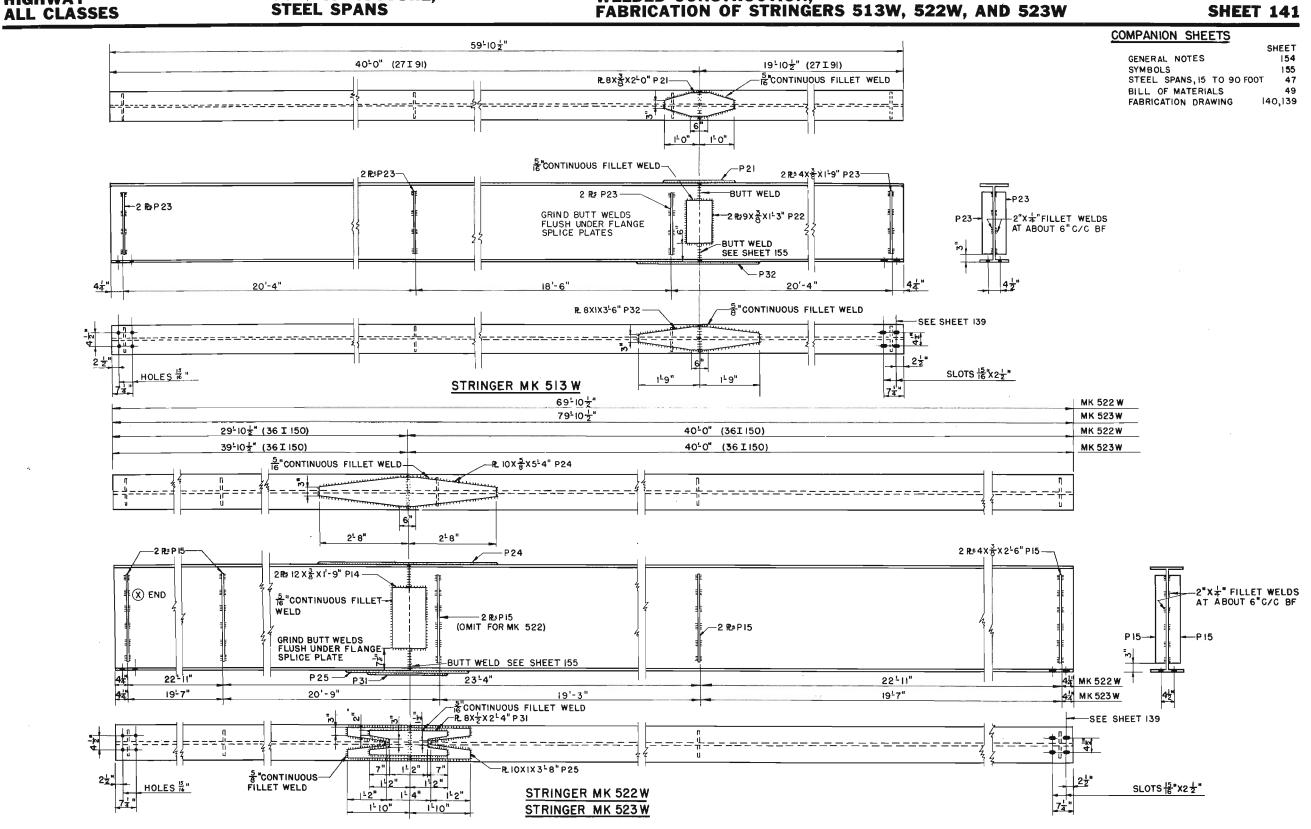
SUPERSTRUCTURE,

STEEL SPANS

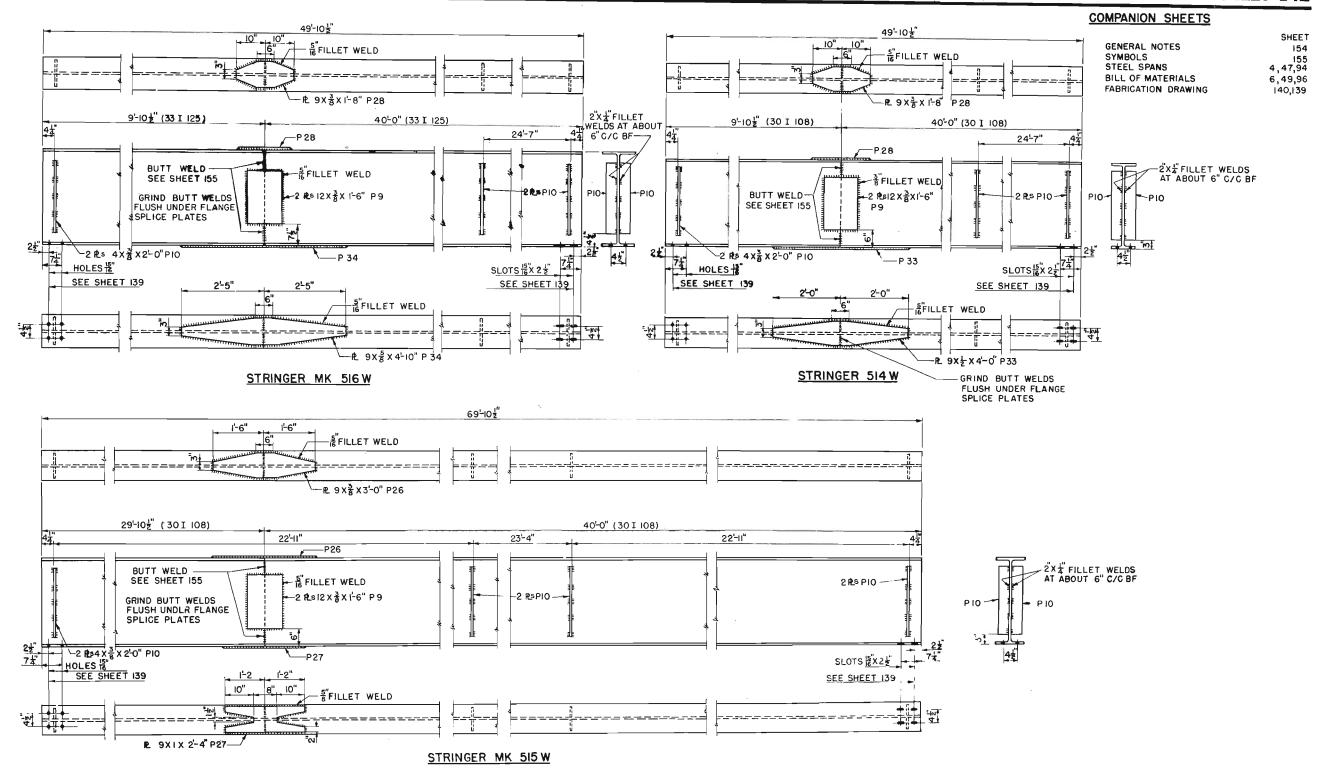


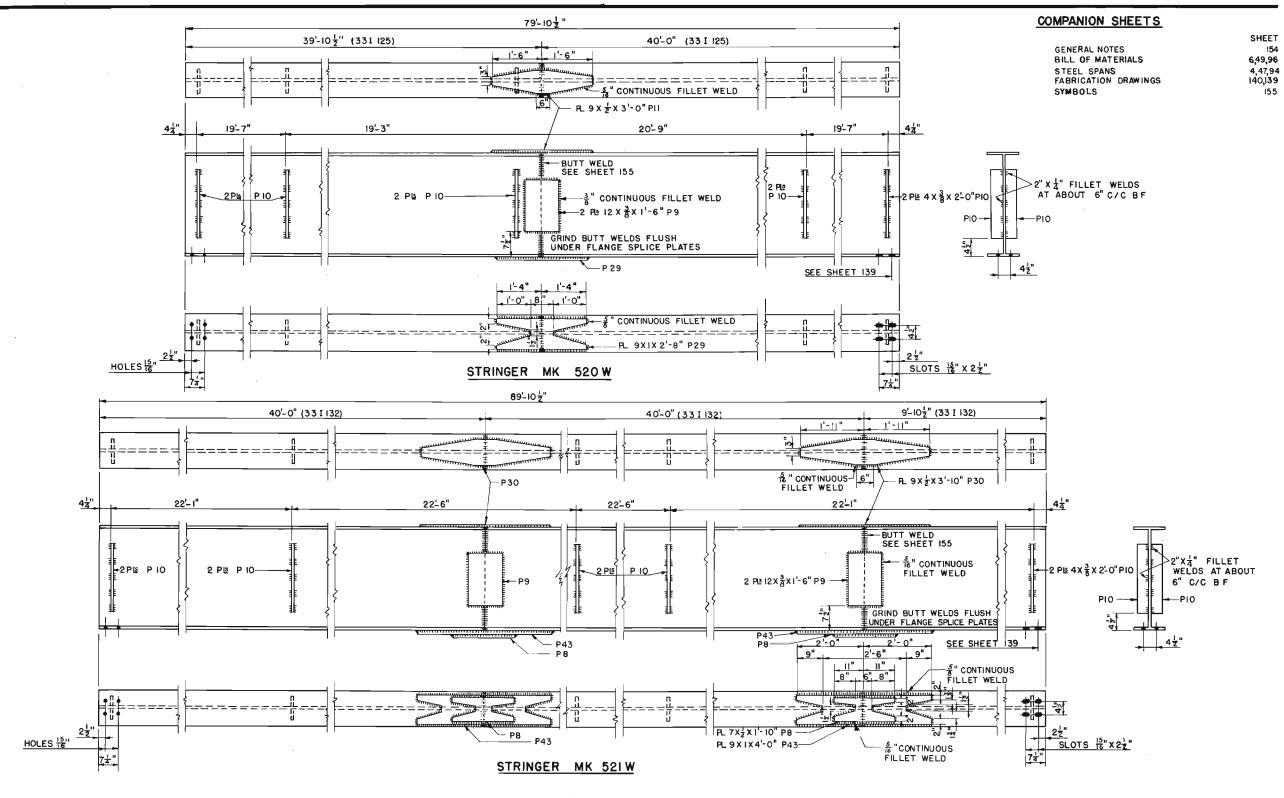


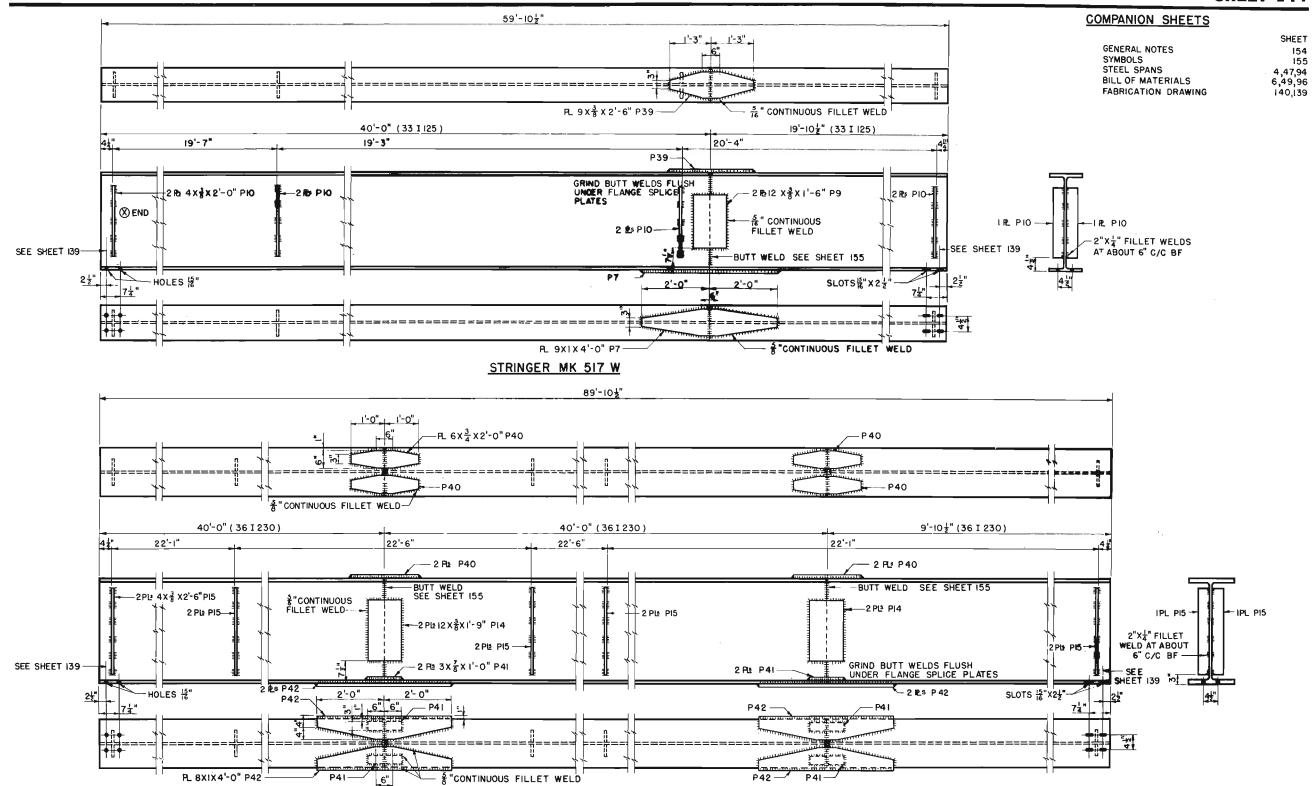




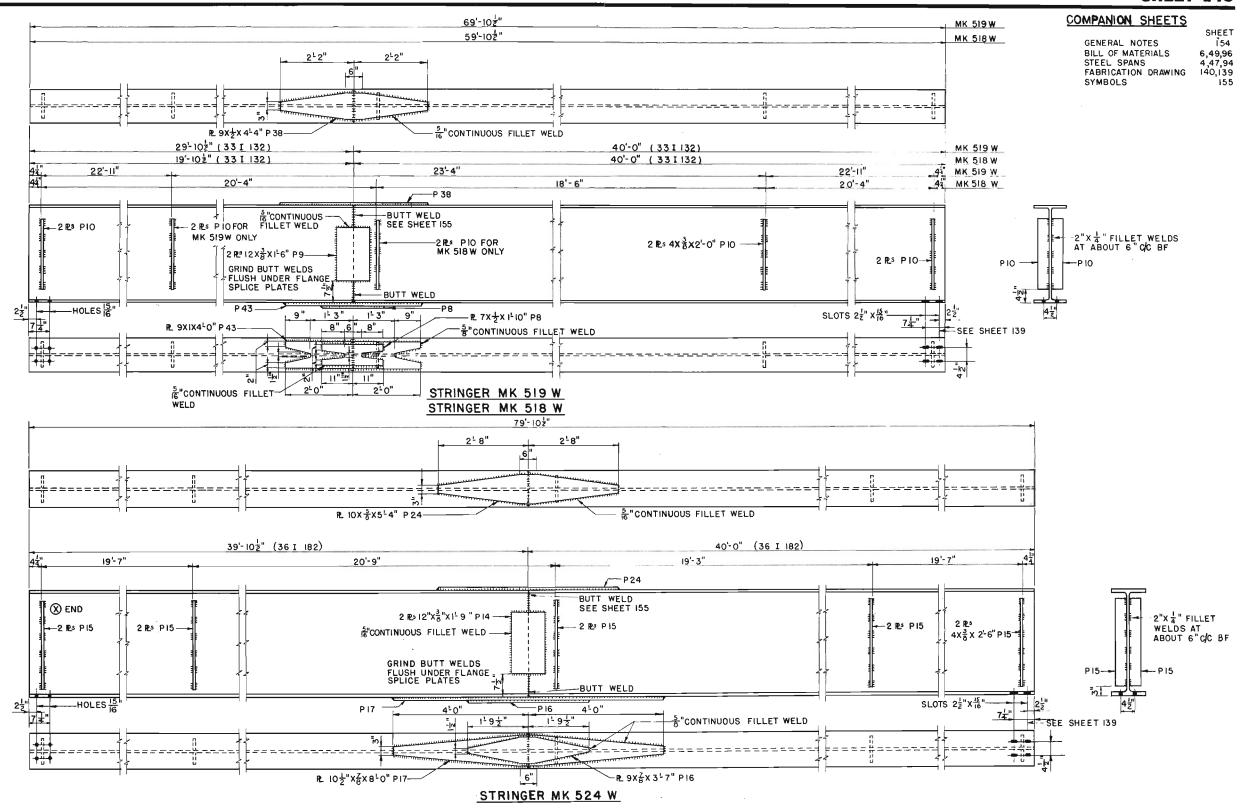
HIGHWAY







STRINGER MK 526 W



BOLT IX16"

3 DRIFT BOLTS X 20 D20

BOLT | X | 6" E | 6

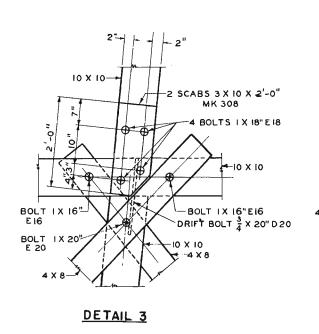
E 16

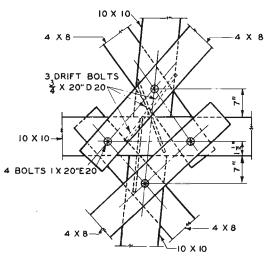
10 X 10-

10 X 10 -

COMPANION SHEETS

TIMBER TOWERS FOR TIMBER SPANS 7,50,97
BILLS OF MATERIAL 8,51,98
GENERAL NOTES 154
SYMBOLS 155





DETAIL 2

10 X 10

1 BOLT 1X 16"E16

1 BOLT 1X 20"E20

1 BOLT 1X 16"E16

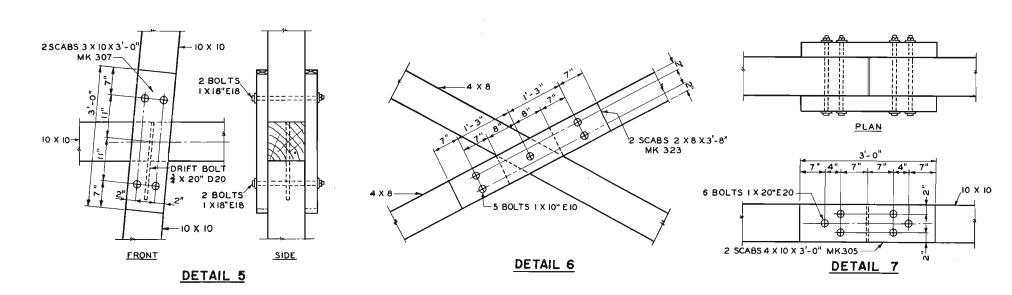
DETAIL 4

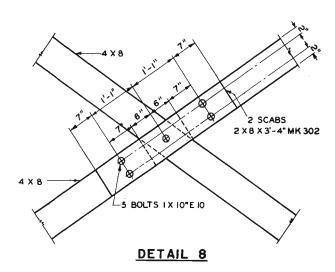
2 BOLTS | X 20" E 20

2 BOLTS | X 20"

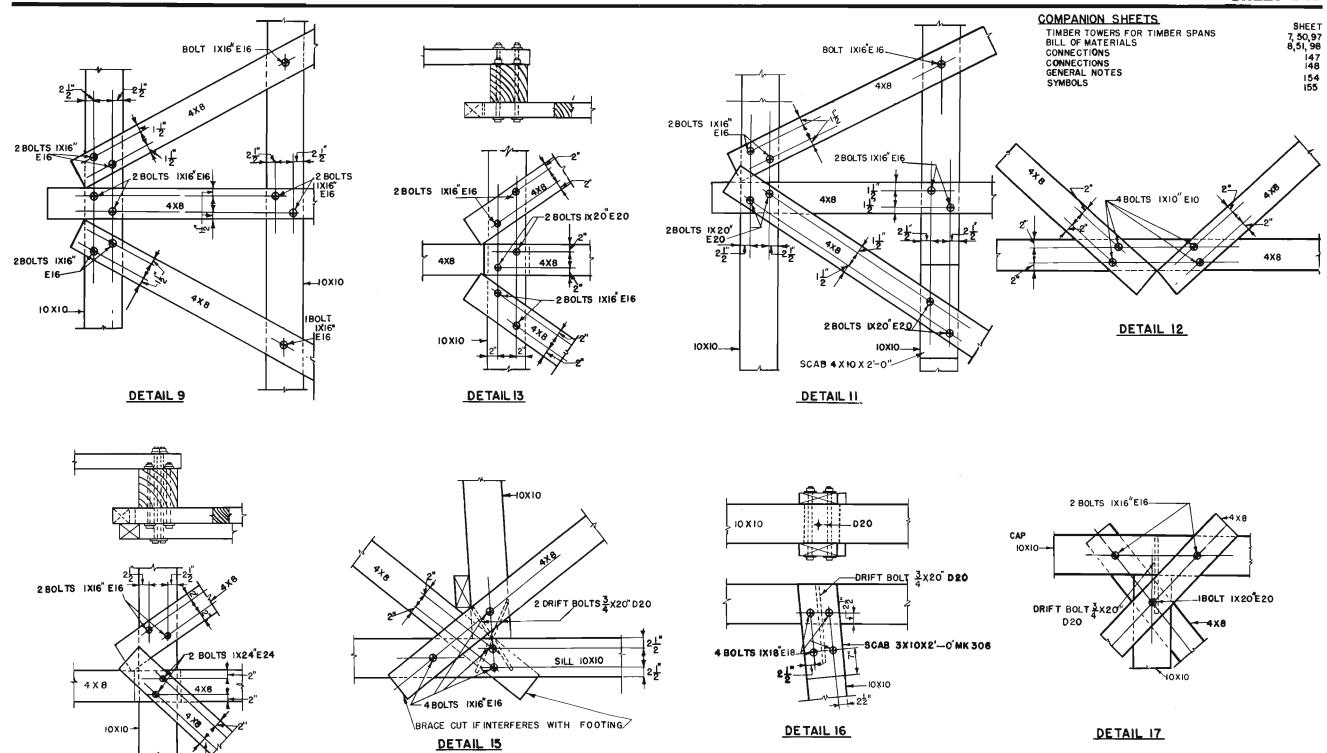
E 20

- 2 BOLTS | X 20" E 20





DETAIL I



DETAIL 14

0'-11

4X8

155A

10'-0"

4 X8

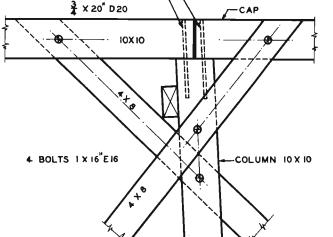
2 DRIFT BOLTS-

3 × 20" D20

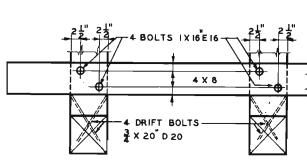
- 8 돌. 0'-11 분"

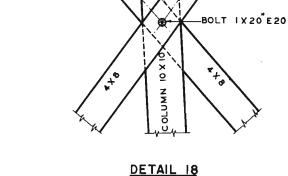


TIMBER TOWER FOR TIMBER SPANS 7,50,97
BILL OF MATERIALS 8,51,98
GENERAL NOTES 154
SYMBOLS 155



2 DRIFT BOLTS-





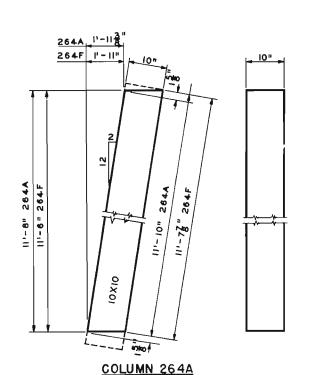
_2 BOLTS

1 X 16" E16

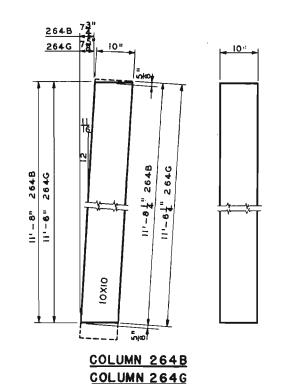
10 X 10

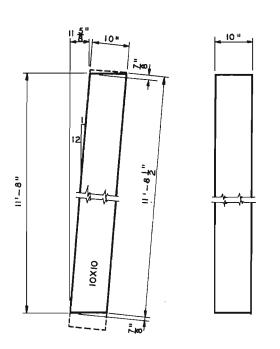
DE TAIL 19

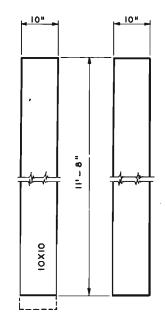
DETAIL 20



COLUMN 264F

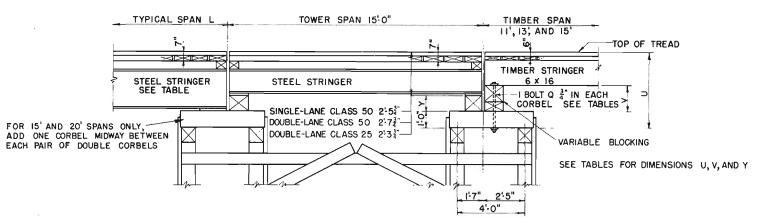






10, 53, 100

COMPANION SHEETS SHEET 154 155 GENERAL NOTES SYMBOLS STEEL SPANS 15' TO 90' SUPPLEMENTAL MATERIALS, 4,47,94 TIMBER TOWERS 9, 52,99 TIMBER TOWER FOR STEEL SPANS



LONGITUDINAL ELEVATION SHOWING JUNCTION OF TIMBER-AND STEEL-STRINGER SPANS ON TOWER

TABLE A SINGLE-LANE CLASS 50

TYPICAL	STEEL	DIMENSIONS										
SPAN L	STRINGER	U	Y	٧	BOLT Q							
15'	16 I 36	3'-53"	0,-0,,	0.7 3.	22"							
20'	18 I 47	3'-73'	0'- 2"	0,93,	24"							
30'	24174	4.13.	0'-8"	1'.3 3"	30"							
40'	24 I 87	4'-2"	0'- 84"	l'- 4"	30"							
50'	301 108	4'-73"	1'- 2"	1-93"	36"							
60'	331 25	4-10 7:	1-58	2.0 2"	40"							
70'	331 132	4'-11"	1-54"	2'-1"	40"							
80'	361150	5-13"	I'-8"	2'-3¾"	42"							
90'	361 182	5-24"	l'-8½"	2'.44"	42"							

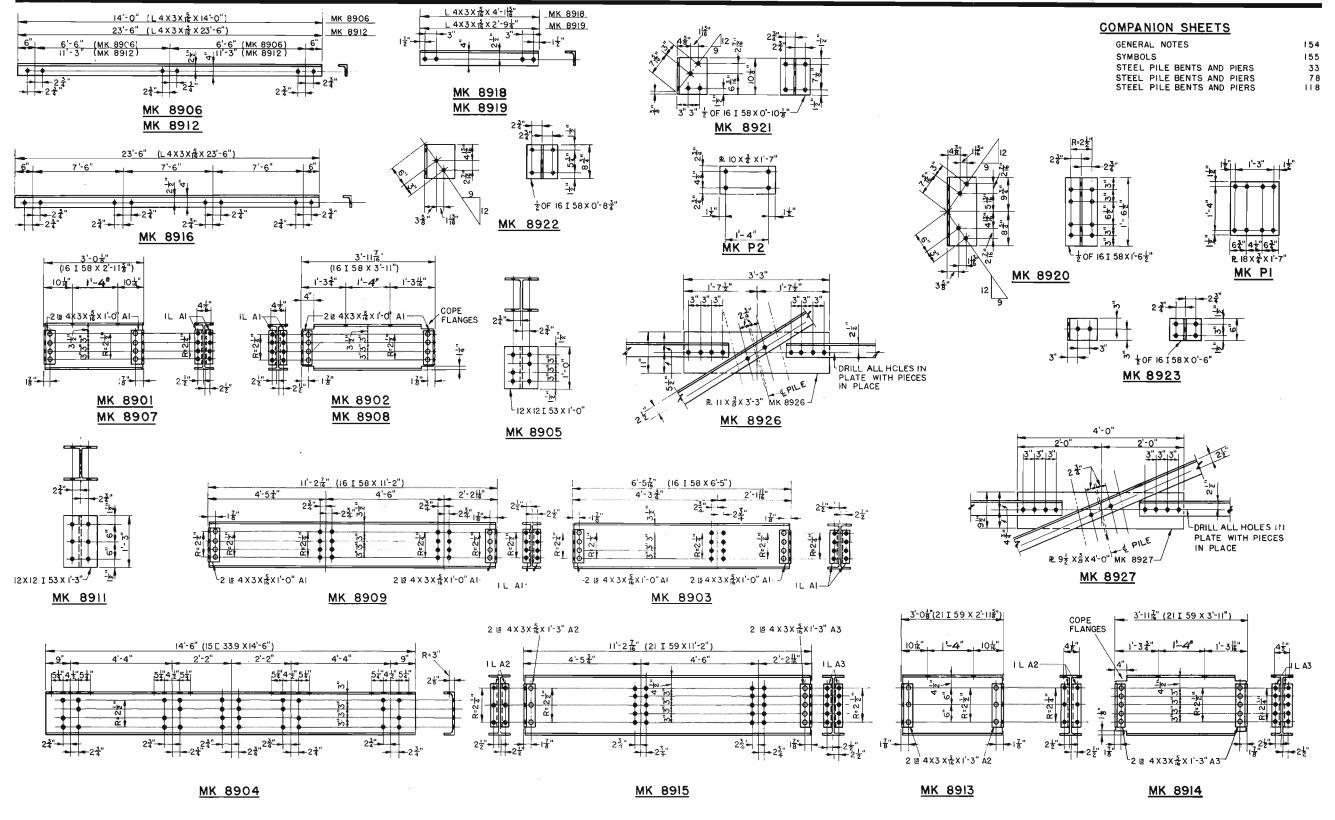
TARLE B DOUBLE-LANE CLASS 50

IADLE	ם טטטם	LE-LA	NE OL	433 30								
TYPICAL	STEEL	DIMENSIONS										
SPAN L	STRINGER	U	Y	V	BOLT Q							
15'	18 I 47	3'-74"	0'-0"	0'-94"	24"							
20'	211 59	3'-104"	0'-3"	1'-03"	28"							
30'	24 I 74	4'-13"	0'-6"	1'- 33"	30"							
40'	27 I 91	4'-43"	0'-9"	1'· 6 3"	34"							
50'	33 I 125	4'-107"	1'- 3\frac{1}{6}"	2-07"	40"							
60'	331 132	4'-11"	1'- 34"	2'-1"	40"							
70'	361 150	5'- 13"	1'-6"	2'-33"	42"							
80'	361182	5'-24	1'-6 ½"	2-44"	42"							
90'	36 I 230	5'•1 ³ / ₄ "	I'- 6"	2'-34"	42"							

TABLE C DOUBLE-LANE CLASS 25

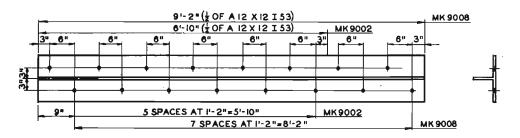
TYPICAL	STEEL				
SPAN L	STRINGER	U	Y	٧	BOLT Q
15'	14130	3'-33"	0,-0,	0'-5 3 "	20"
20'	16 I 36	3'-5\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	o'- 2'	0-73	22"
30'	21159	3'-10∄"	0'-7"	1'- 0 ³	28"
40'	21163	3'-10 2°	0'-7 ¹ 8'	1'-0g"	28"
50'	24187	4'-2"	0'-104	1'- 4"	30"
60'	27 I 9I	4-43	#_ 	I¹-6∄"	34"
70'	301108	4'-74"	- 4" - 1"	1'-94"	36"
80'	33 I 125	4-107"	1'-78"	2'-0 8"	40"
90'	331 132	4'-11"	1 - 7 - 7	2'-1"	40"

WHEN LAMINATED FLOOR IS USED IN PLACE OF STANDARD FLOOR, ADD ONE INCH TO DIMENSIONS U AND V GIVEN IN TABLES A, B AND C

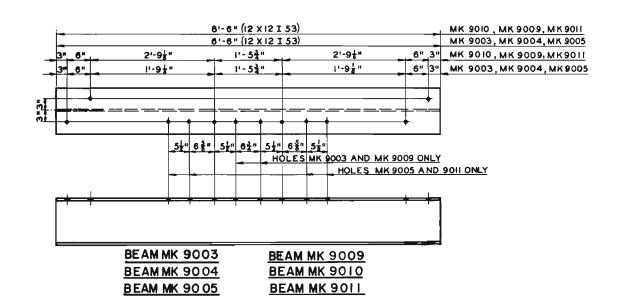


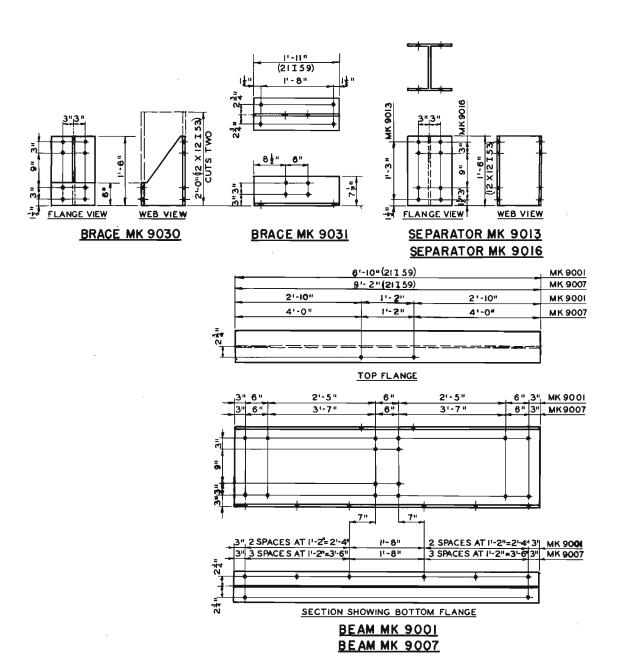
COMPANION SHEETS

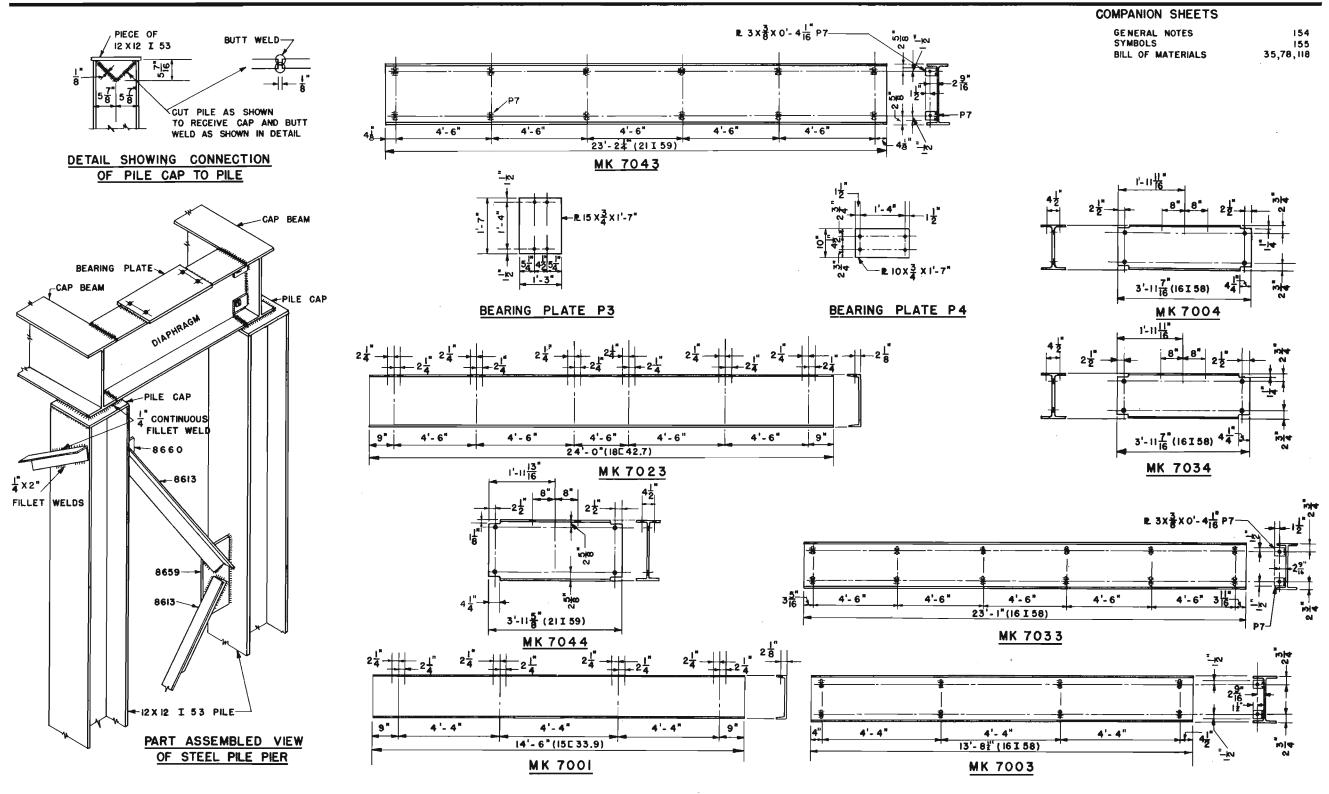
	SHEET
GENERAL NOTES	154
SYMBOLS	155
STEEL GRILL AGES, BOLTED	41
STEEL GRILLAGES, BOLTED	87
STEEL GRILLAGES, BOLTED	125



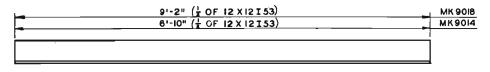
HALF BEAM MK 9002 HALF BEAM MK 9008





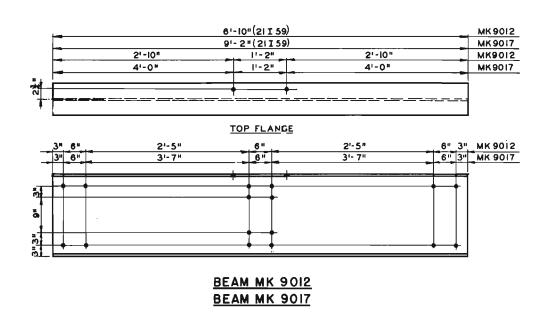


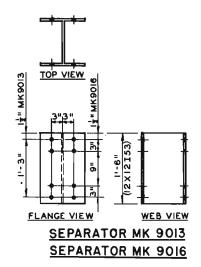
COMPANION SHEETS GENERAL NOTES 154 SYMBOLS 155 STEEL GRILLAGES, WELDED 42 STEEL GRILLAGES, WELDED 88 STEEL GRILLAGES, WELDED 126

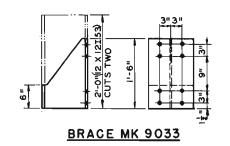


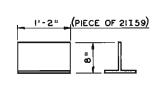
END VIEW

HALF BEAM MK 9014 HALF BEAM MK 9018







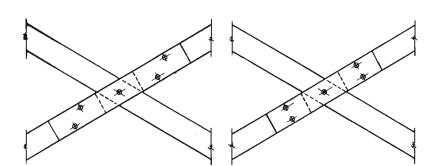


BRACE MK 9034

PREFERRED

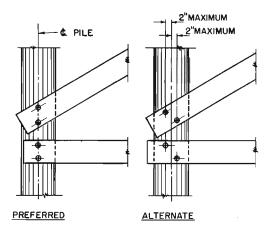
SHEET

155



BOLT PATTERN FOR TIMBER BRACING SPLICES

ALTERNATE



BRACING CONNECTION TO TIMBER PILES

STEEL FABRICATION WITH RIVETS AND BOLTS

All rivets are %-inch diameter. Structural ribbed %-inch bolts may be substituted for any %-inch rivet. The rivet length R in inches is shown on fabrication drawings for all riveted connections. Table XLIV shows corresponding lengths of structural ribbed bolts substituted for rivets.

All holes in steel are 15/16-inch diameter unless otherwise shown on drawings.

The distance from any hole to sheared edge is $1\frac{1}{2}$ inches unless otherwise shown on the drawings. This end distance is used in marking hole centers not otherwise dimensioned.

The minimum distance from center of any hole to edge of steel is 1¼ inches for 15/16-inch holes.

The minimum distance between centers of 15/16-inch holes is 3 inches.

All holes in steel may be drilled full size. If necessary to obtain accurate fit, 15/16-inch holes may be subdrilled to 13/16-inch diameter and reamed to 15/16-inch size with taper bridge reamer.

All holes must be clean, with even edges, cylindrical, and perpendicular to the steel surface.

The location of all open holes for field connections should be within 1/32 inch of the position shown on drawings.

Reaming is done after the steel members are positioned in correct alignment with the steel surfaces held in close contact.

Temporary field connections made before riveting or bolting must have at least half of the holes filled with driftpins or machine bolts.

Slotted holes shown in the bottom flanges of stringers and in bearing plates, and 1-9/16-inch holes in steel-tower-column base plates for %-inch or 1-inch anchor bolt are flame-cut.

Machine bolts may be used instead of structural ribbed bolts as anchor bolts between steel grillages and steel tower columns.

WELDING

GENERAL NOTES

Welds are ½-inch fillet welds unless otherwise indicated. Welds 5/16 inch and smaller may be made with a single pass of the electrode. Welds over 5/16 inch are made in two or more passes, each depositing an approximately equal volume of weld.

Butt welds between steel edges not over ¼ inch thick may be deposited between square-cut edges. Edges of steel from \$/6 to \$/6 inch thick are beveled for butt welding on one side at an angle of 60° to the metal surface. Edges of metal over %6 inch thick are beveled for butt welding on both sides at an angle of 60° to the metal surface.

Steel edges to be welded may be flame-cut and beveled and are cleaned to remove mill scale, corrosion, and other foreign matter within ½ inch of the edge.

TIMBER

Timber may be furnished rough, sawn to full dimension, or dressed dimension. The nominal size is shown on the drawings.

 $\mbox{\sc Holes}$ for driftbolts and machine bolts are bored the same diameter as the bolt.

Threaded bolts used for timber connections are steel machine bolts threaded with American standard coarse threads (NCTS-formerly USS thread) class 2 fit, finished black with square nuts. Two standard round iron or steel washers must be provided with each machine bolt.

For 1-inch bolts, diameter 2½ inches, thickness 5/32 inch, stock number 43-9215.5-100.

For %-inch bolts, diameter 2 inches, thickness ½ inch, stock number 43-9215.5-07.

For 1/2-inch bolts, diameter 1% inches, thickness 3/32 inch, stock number 43-9215.5-05.

The minimum distance from the center of any bolt to edge of timber is one and one-half times the diameter of the bolt. The minimum distance from the center of any bolt to end of timber is seven times the diameter of the bolt.

Standard methods of bolting scabs at timber bracing splices are shown on sketches on this sheet. Standard methods of connecting braces to timber piles are shown in sketches on this sheet.

MISCELLANEOUS

All I-beams are wide-flange sections, no American-standard I-beams being used in the designs in this manual. Plates and channels with skew cuts are cut from long lengths to save cutting work and material.

Open holes are shown in bearing plates and beams of cap beam at top of steel towers. These connections are made after erection so the beams may be spread to enter over the tower columns.

Steel stringers are so placed on supports that slotted holes in the stringers are all at one end of the span. Expansion ends and fixed ends alternate.

Steel-stringer splices are designed on the basis of actual moments and shear at the point of splice. Location of splices should be changed only on direction of officers experienced in design.

Driftbolts without heads may be used where plain driftbolts are indicated to avoid counterboring for heads to obtain unobstructed timber surface.

Stock numbers shown in bills of materials are those contained in Engineer Supply Catalog issued March, 1944. The stock number subdecimal indicating length of timber, or size of plate, has been omitted for pieces which may be cut from random length timber or from different sizes of plates. Items for which no stock number is given were not class IV material at the time these drawings were prepared.

The quantities listed in bills of materials are net requirements for finished structures; they include no allowance for waste or loss.

Fabrication drawings for steel stringers show total lengths of individual stringer sections. No deduction is shown for clearance between ends of sections at splices.

At riveted splices, clearance between ends of stringers should not exceed $\frac{1}{2}$ inch. Stringer sections, except 40-foot lengths, are listed in the bills of materials $\frac{1}{2}$ inch shorter than shown on fabrication drawings, providing plus $\frac{1}{2}$ inch cutting tolerance without trimming.

At welded splices, clearance between ends of stringers should not exceed ½ inch. Stringer sections are listed in the bills of materials the same length as shown on fabrication drawings, providing minus ½ inch cutting tolerance without frimming. If 40-foot stringer sections are not of exact length, dimensions of adjacent sections must be adjusted accordingly.

Bills of materials for timber piers for highway steel spans include anchor bolts for attaching uniform-depth spans. Only one-half the listed quantity of anchor bolts is used for each span where steel and timber spans or steel stringers of different depths meet on one pier. Timber blocking and anchor bolts for steel stringers of different depths are shown on sheets 30, 74, and 114 showing supplemental materials for highway piers and pilled on sheet 203 for railway piers.

Riprap is shown on drawings of foundation piles with concrete pedestals or steel frames. See text for information and directions as to use of riprup.

Fabrication drawings for highway steel stringers show four holes in the bottom flange at each end of the stringer. However, only two holes are needed at each end.

The holes are 2½ inches from the end on stringers resting on timber abutments.

Holes are 7½ inches from the end on beams resting on any other support.

COMPANION SHEET

SYMBOLS

Sheets 20, 63, 103, and 192 show fabricated shims for steel stringers of nonuniform depth. When these shims are required, holes must be provided for bolts connecting them to steel-stringer bottom flanges unless welded connections are used.

BEARING PLATES, BLOCKING, AND SHIMS

No bearing plates are used under timber stringers or under steel stringers on steel pile abutments. Bearing plates on steel towers are detailed and listed with other tower material.

Bearing plates on steel pile bents and piers are detailed and listed with other bent and pier materials.

Bearing plates under steel stringers on timber towers, timber pile piers, timber abutments, and concrete abutments are listed on the same sheets as tower, pier, or abutment materials, and are detailed on sheet 132 for highway and on sheet 178 for railway bridges.

Blocking under bearing plates supporting steel stringers of nonuniform-depth spans on timber towers is dimensioned and listed on sheets listing supplemental tower materials.

Sheet 9	Class 50, single-lane
Sheet 52	Class 50, double-lane
Sheet 99	Class 25, double-lane
Sheet 178	Railway

Blocking under bearing plates supporting stringers of nonuniform-depth spans on timber pile piers is dimensioned on pier drawings. Bills of materials must be prepared in the field, except for blocking under 15-foot standard railway spans between braced piers which is listed with other pier materials.

Shims under steel stringers of nonuniform-depth spans on steel towers, bents, and piers are detailed and listed on:

Sheet 20	Class 50, single-lane
Sheet 63	Class 50, double-lane
Sheet 103	Class 25, double-lane
Sheet 192	Railway

ANCHOR BOLTS

Anchor driftbolts for timber stringers are shown and listed with superstructure materials.

Anchor bolts for steel stringers are shown and listed with substructure materials:

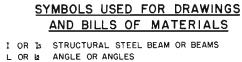
On steel towers: on drawings of shims for support of maximum depth spans.

On abutments, and for uniform-depth steel-stringer spans on timber towers, timber pile piers, and steel pile bents and piers: on drawings with abutment, tower, and pier material.

On steel pile bents and piers, for nonuniform-depth steelstringer spans: on drawings of shims for support of nonuniform-depth spans.

Anchor bolts for support of nonuniform depth steel-stringer spans on timber towers and timber pile piers are dimensioned on drawings showing supplemental tower materials and blocking on piers, but are not listed. Bills of materials for these anchor bolts must be prepared in the field; the anchor bolts which are not used but are listed in bills of materials on these drawings may be deducted.

STRUCTURAL SYMBOLS



C OR & STRUCTURAL STEEL CHANNEL OR CHANNELS

L OR & STRUCTURAL STEEL TEE OR TEES

R OR & STRUCTURAL STEEL PLATE OR PLATES

BOLT THREADS

Ø ROUND ROD, BOLT, ETC

□ SQUARE ROD, ETC

⊕ BOLT, NUT, AND WASHERS IN TIMBER

++ DRIFT BOLT

⋈ HOOK BOLT, NUT, AND WASHER

FABRICATION RIVET OR RIBBED BOLT
OPEN HOLE, FIELD BOLT, OR FIELD RIVET

MK IDENTIFIES MARK NUMBER ON DRAWING

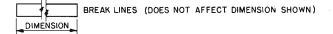
X BY, (2 X 4), 2" BY 4"

CENTERLINE

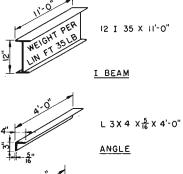
BF BOTH FACES
NF NEAR FACE

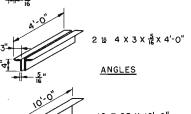
FF FAR FACE
R RIVET LENGTH

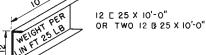
SECTION REFERENCE
ARROWS INDICATE DIRECTION OF SIGHT



METHODS OF INDICATION OF STRUCTURAL SHAPES

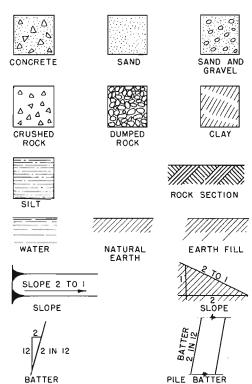




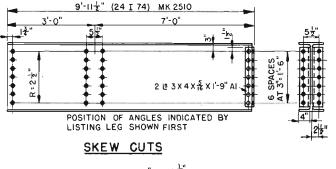


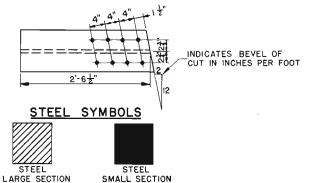
CHANNEL

STANDARD SYMBOLS

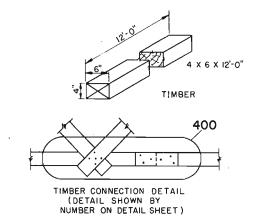


STEEL I BEAM DRAWING

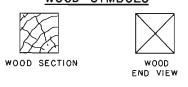




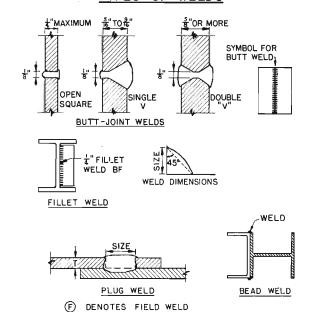
TIMBER DRAWINGS



WOOD SYMBOLS



TYPES OF WELDS



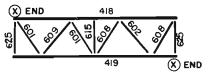
SETS OF DRAWINGS FOR DIFFERENT CONSTRUCTION UNITS

SHEET 156

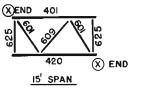
	SET NUMBER RR-1	SHEET		SHEET	
	JEI HOMOEK KK-I	186	Bill of materials common to all towers	209	Welded construction: general views of bents
	TIMBER SPANS	187	Bill of materials which vary with tower height	210	Welded construction: general views of piers
	(12 to 16 feet long)	188	Riveted construction: fabrication of cap beam, strut, and pin	211	Welded construction: fabrication of cap beams, corbels, and bracing connec-
SHEET	,	189	Riveted construction: fabrication of columns		tions
		190	Riveted construction: fabrication of columns and struts	154	General notes
157	General views and bill of materials	191	Fabrication of rod bracing	155	Structural symbols
174	General views and bill of materials for refuge bay and walkway	192	Details and bill of materials for shims under stringers of different depths; super- structure anchor bolts		SET NUMBER RR-11
154	General notes	226	Welded construction with rod bracing: cap beams and column splices welded		OLI HOMBER RR-11
155	Structural symbols	220	in fabrication and erection		TIMBER SILL AND PILE FOUNDATIONS FOR TIMBER TOWERS
	SET NUMBER RR-2	227	Welded construction with welded angle bracing: cap beams and column splices		
		/	welded in fabrication and erection	212	General views and bill of materials
	STEEL SPANS	154	General notes	213	General views
	(15 to 50 feet long)	155	Structural symbols	154	General notes
			NOTE: When welded construction is used in accordance with sheets 226	155	Structural symbols
158	General views of 15- and 45-foot spans; assembly diagrams for riveted con-		or 227, bills of materials on sheets 186 and 187, and fabrication		
	struction		details on sheets 188, 189, and 190 must be adjusted in the field.		SET NUMBER RR-12
159	General views of 50-foot span		When sheet 227 is used sheet 191 does not apply.		CONCRETE REDECTAGE FOR THURSE TOURS
160	Bill of materials: structural steel for riveted construction				CONCRETE PEDESTALS FOR TIMBER TOWERS
161	Bill of materials: structural steel for welded construction, lumber, and deck		SET NUMBER RR-6		
162	hardware Riveted construction: fabrication of lateral braces			214	General views and bill of materials
163	Riveted construction: fabrication of stringers 401, 402, 403, and 420, and of		TIMBER ABUTMENTS FOR TIMBER SPANS	154	General notes
103	diaphragms			155	Structural symbols
164	Riveted construction: fabrication of stringers 404, 405, 406, and 407				CET NUMBED DD 10
165	Riveted construction: fabrication of stringers 408, 409, 410, and 411	193	General views of pile abutments; bill of materials for pile and grillage abut-		SET NUMBER RR-13
166	Riveted construction: fabrication of stringers 412, 413, 418, and 419	704	ments		CONCRETE PEDESTALS FOR STEEL TOWERS
167	Riveted construction: fabrication of stringers 414, 415, 416, and 417	194	General views of grillage abutments General notes		CONCRETE TEDESTALS FOR STELL TOWERS
168	Welded construction: assembly diagrams and fabrication of lateral bruces	154 155	Structural symbols		
169	Welded construction: fabrication of stringers 401W, 402W, 403W, and	133	•	215	General views and bill of materials for pedestals on timber piles
	420W, and of diaphragms		SET NUMBER RR-7	216 184	General views and bill of materials for pedestals on ground and on steel piles
170	Welded construction: fabrication of stringers 404W, 405W, 406W, and 407W		A DATE OF A STEEL OF A	185	General views of 69- to 77-foot towers General views of 15- to 67-foot towers
171	Welded construction: fabrication of stringers 408W, 409W, 410W, and 411W		ABUTMENTS FOR STEEL SPANS	154	General notes
172	Welded construction: fabrication of stringers 412W, 413W, 414W, and 415W			155	Structural symbols
173 174	Welded construction: fabrication of stringers 416W, 417W, 418W, and 419W General views and bill of materials for refuge bay and walkway	195	General views of timber pile abutments	100	on octoral symbols
154	General notes	196	Bill of materials for timber abutments; general views of timber grillage abut-		SET NUMBER RR-14
155	Structural symbols		ments		
.00	,	197	General views of steel pile abutments		STEEL FRAME ON STEEL PILE FOUNDATIONS FOR STEEL TOWERS
	SET NUMBER RR-3	198 199	Fabrication details and bill of materials for steel pile abutments General views and bill of materials for concrete abutments		
	THERE TOWERS FOR THURSD SPANIS	154	General notes		
	TIMBER TOWERS FOR TIMBER SPANS	155	Structural symbols	217	General views and bill of materials
	(15 to 76 feet high)		•	184	General views of 69- to 77-foot towers
			SET NUMBER RR-8	185	General views of 15- to 67-foot towers
175	General views		TIMBER PILE BENTS FOR TIMBER SPANS	154	General notes
176	Bill of materials		(1 to 28 feet high)	155	Structural symbols
181	Details of bracing connections		(1 to 20 teet tilgti)		
182	Details of bracing connections				SET NUMBER RR-15
183	Details of bracing connections and of columns; column dimensions	200	General views		
154	General notes	201 1 <i>5</i> 4	Additional views and bill of materials General notes		STEEL GRILLAGE FOUNDATIONS FOR STEEL TOWERS
155	Structural symbols	155	Structural symbols		
	SET NUMBER RR-4	133	,	218	Bolted construction: general views and bill of materials for grillages \$101 and
	····································		SET NUMBER RR-9	-·•	\$102
	TIMBER TOWERS FOR STEEL SPANS		TIMBER PILE PIERS FOR STEEL SPANS	219	Bolted construction: general views and bill of materials for grillage \$103
	(15 to 76 feet high)		(1 to 11 feet high)	220	Welded construction: general views and bill of materials for grillage \$103 (\$101
			(1 to 11 tool mgm)		and S102 are similar)
177	Details of connection of spans to towers	0.55		221	Bolted construction: fabrication
178	Details and bill of materials for conection of spans to towers	202	General views	222	Welded construction: fabrication
179	General views	203	Bill of materials	184	General views of 69- to 77-foot towers
180	Bill of materials	154 155	General notes Structural symbols	185 154	General views of 15- to 67-foot towers General notes
181	Details of bracing connections	100	•	154	Structural symbols
182	Details of bracing connections		SET NUMBER RR-10	100	on outside symbols
183	Details of bracing connections and of columns; column dimensions		CYCEL DILE BENTC AND DIEDE FOR CYCEL CRANG		
154	General notes		STEEL PILE BENTS AND PIERS FOR STEEL SPANS		SET NUMBER RR-16
155	Structural symbols		(1 to 20 feet high)		
	SET NUMBER RR-5		:		TIMBER GRILLAGE FOUNDATIONS FOR TIMBER TOWERS
	CTELL TOWERS FOR STEEL OF THE	204	Riveted construction: general views of bents		
	STEEL TOWERS FOR STEEL SPANS	204	Riveted construction: general views of piers	223	General views
	(15 to 77 feet high)	206	Riveted construction: fabrication of cap beams, corbels, and bracing connec-	224	Additional views and bill of materials
			tions	225	Additional views
184	General views of 69- to 77-foot towers	207	Riveted construction: bill of materials	154	General notes
18 <i>5</i>	General views of 15- and 67-foot towers	208	Welded construction: bill of materials	155	Structural symbols

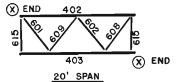
COMPANION SHEETS

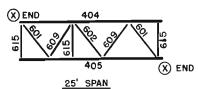


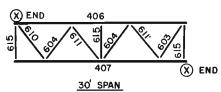


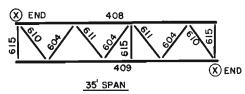
SPECIAL 30' SPAN WITH CENTER SUPPORT

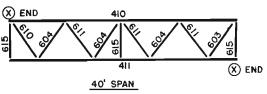


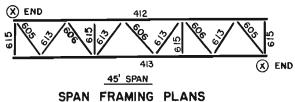












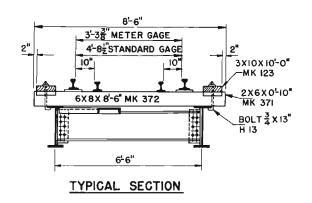
GX8X8'-6" TIES MK 372 AT 1'-0" C/C
WIRE SPIKES MK 51

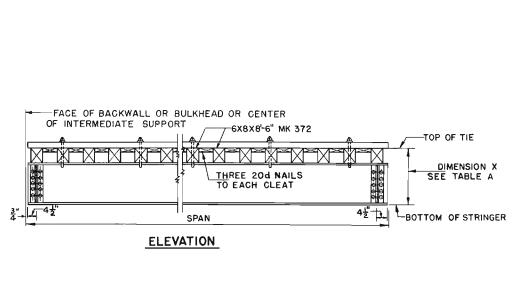
OC 15.3
SEE FRAMING PLANS

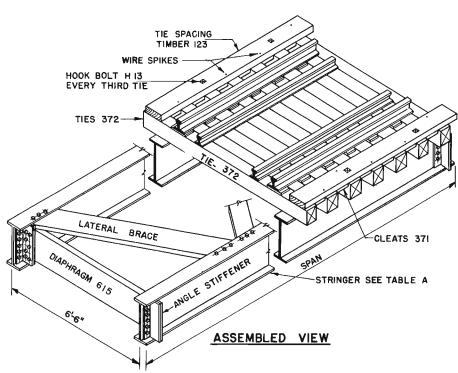
SEE FRAMING PLANS

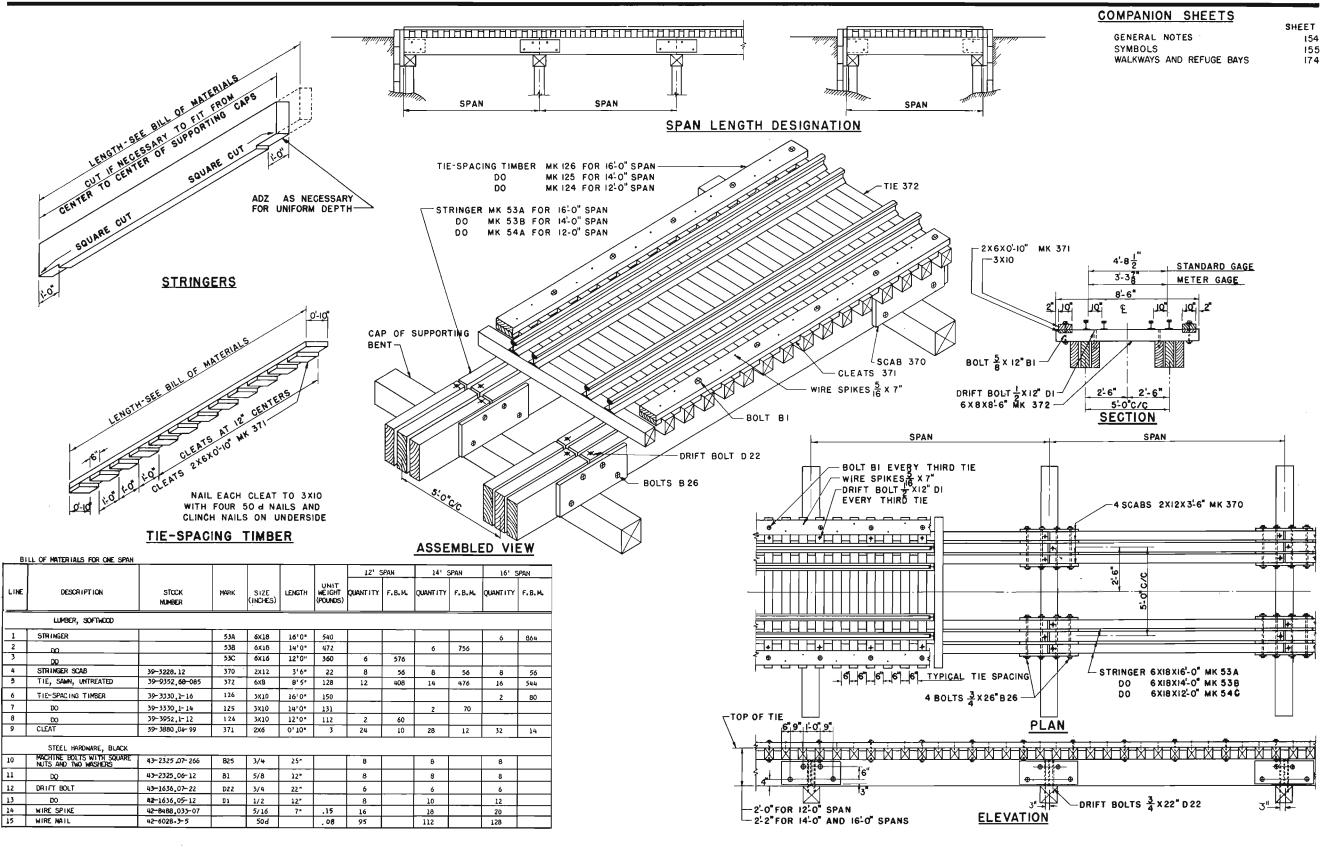
PLAN

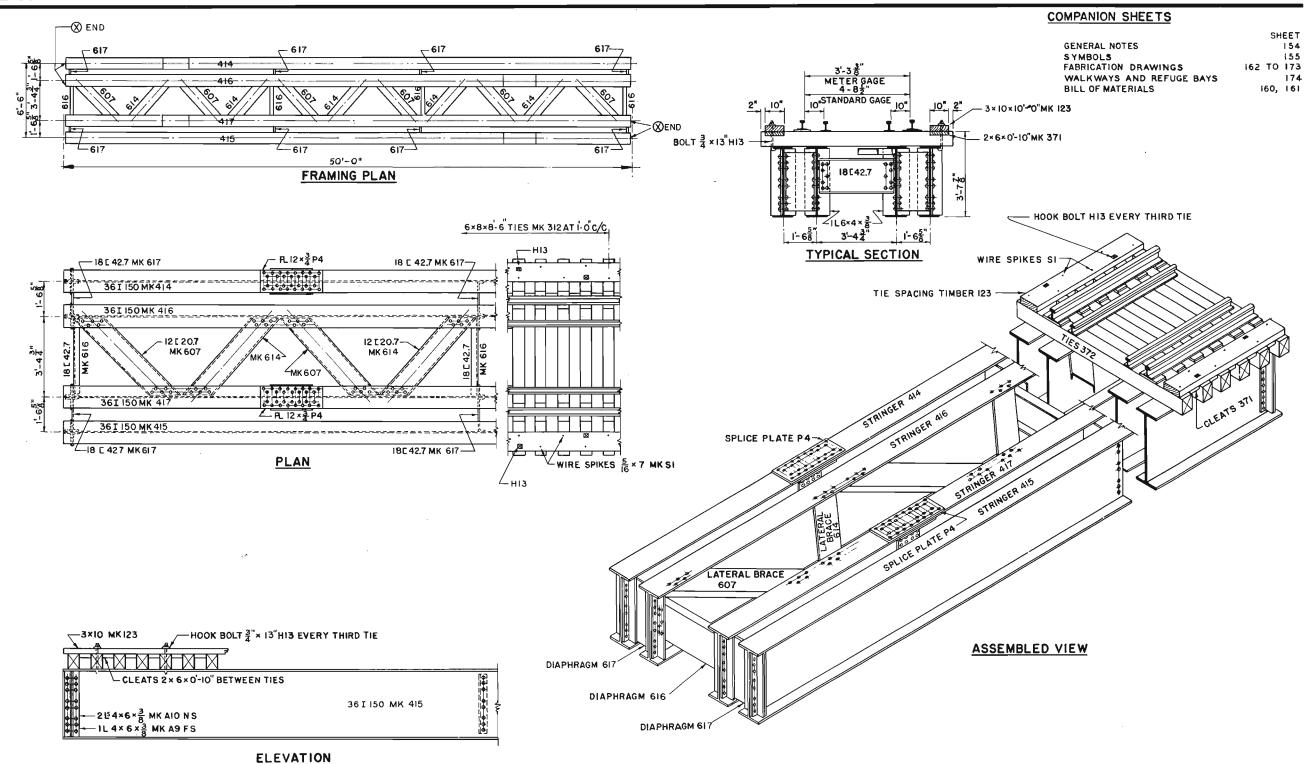
TABLE A STEEL STRINGER DIMENSION SPAN SIZE MARK Х 15'-0" 21 I 63 401 420 2'-5" 2-107 20'-0" 27 I 91 402 403 25'-0" 30 I 108 404 405 3'-17 30'-0" 33 I 132 406 407 SPECIAL 30'-0" 21 1 63 418 419 35^L-0" **36** I 150 408 409 40'-0" 36 I 182 410 411 45'-0" 36 I 230 412 413











COMPANION	SHEETS
	O' ILL C

	SHEET
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STEEL SPANS 15 TO 45 FOOT	158
STEEL SPANS 50 FOOT	159
BILL OF MATERIALS	161
FABRICATION DRAWINGS	162 TO 173

	BILL OF MATERIALS FOR ONE	RIVETED STEEL S SPAN LENGTH	STRINGER	SPAN			15	5'	,	0,	25	; t	31	0'	30' S	PECIAL	3	5'	40'		45'		501		Т
INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY		QUANTITY		QUANTITY		QUANTITY	1	QUANTITY		QUANTITY		QUANTITY		QUANTITY		QUANTITY	FBM	LINE
	STRUCTURAL STEEL	_																							
$\overline{}$	STRINGER	48-2900.36-23	413	36 I 230	40'-0"	9186															1				1
2	DO		412												-						1				3
4	DO	48-2900.36-23	422	36 I 230	4'-10"	1143															1				4
5	DO DO	1	411	36 I 182	39'-10 1/2"	7256			 					1			-		1		 				5
7	DO		417																				1		7
8	DO DO	48-2900.36-15	416	36 I 150	40'-0"	5991	 					_			 		-						1		9
10	00	<u> </u>	414																				1		10
11	DO	_	427 426		al 1=7															-			1		11
12	ĎΟ	48-2900.36-15	425	36 I 150	9'-10"	1496																	1		13
14	DO DO		424	** T 150	181-10 1/2E	5222	-								 		1						1	_	14
16	_ DO	48-2900.36-15	408	36 I 150	34'-10 1/2"	5222											1								16
17		48-2900.53-132	407	33 I 132	29'-10 1/2"	3943							1		1									-	17
19	DO	48-2900.3-108	405	30 I 108	24'-10 1/2*	2686			,		1													-	19
20 21	DO DO	·	404						1		1			 			-				-				20 21
22	00	48-2900.27-091	402	27 I 91	19'-10 1/2"	1808			1			_													22
23	DO DO	48-2900.21-053	418	21 I 63	25'-10 1/2"	1882.									1 1							_			23
25	00	48-2900.21-063	420	21 I 63	14'-10 1/2"	937	_1													-					25
26	DO	40 2940.21 007	401				1																5		26 27
27 28	TOP LATERAL BRACE DO	48-3790.12-21	614	12 [20.7	5'-3 7/16'	110																	6		28
29	DO	48-3790.1-15	613	10 [15.3	7'-11 1/2"	122															4				29
30 31	DO		606 604	10 [15.3	21-11 1/10	122							2		1		١		3	-					30 31
32	DO	48-3790.1-15	611	10 [15.5	7'-11 1/4"	122			Ι.,				2		\vdash		2		3						32
33	90	48-3790.1-15	609	10 [15.5	7'-11"	121			1		2				1					-					33 34
35	DO	48-3790.1-15	605	10 [15.3	7'-8 7/16"	118															2				35
36 37	00	48-3790.1-15	610	10 [15.3	7'-8"	117							1				2		$\frac{1}{1}$						36 37
38	00	48-3790.1-15	608	10 [15.3	7'-6 1/8-	115			1						2										36
39	DI APHRAGM		601 615 625		6'-4"	270	2		2		3		3		3		3		3		4				39 40
40 41	00	48-3790, 18-43	616	18 [42.7	3'-2 3/4*	138															·		ц		41
42	DO STIFFENER	48-3790.18-43	617 A16	18 [42.7	2'-6"	107																	8		42
94	DO	48-2240.64-04	415	L 6X4X3/8	2'-10*	35																	16		44
46	DQ	- 2240.04 04	A12 A11	2 0,47,57,0	,	, ,,			1								8		8 .						45 46
47	DO	##-22#0 A#-0#	A14	L 6X4X3/8	2'-9 3/8"	34															8				47
48	00	48-2240.64-04	A13										A	-							8				48
50	DQ DQ	48-2240.64-04	A8	L 6X4X3/8	2'-7 3/8"	32							8												50
51	00	48-2240.64-04	A10	L 6X4X3/8	2'-6"	31					A		2		-		2		2		4		4		51 52
52 53	DO DO	48-2240.64-04	A6 A5	L 6X4X3/8	2'-4 1/4"	29					8														53
54	00	48-2240.64-04	A7 A4	L 6X4X3/8	2'-3"	28	ļ		8		2			-											54 55
55 56	DO DO	48-2240.64-04	A3	L 6X4X3/8	2'-1 1/2"	26			8																56
57	DO	48-2240.64-04	A2	L 6X4X3/8	1'-7 3/4"	20	8		-					-	12										57 58
58 59	PLATE	47-7844.05	A1 P1	17 X 1/2	2'-1"	60	8								12						ц				59
60	DO	47-7844.05	P4	12 × 1/2	2'-9"	56															8		6		60 61
61 62	DO DO	47-7344.05 47-7844.05	P2 P5	6 X 1/2 5 X 1/2	1'-11"	16 16											.				•		16		62
63	DO	47-7844.04	Р3	13 X 3/8	2'-6"	42								-			14		14		4 28		8 28		63 64
64	DO	43-6353.08-23 43-6353.08-25	-	7/8 7/8	2 1/4"	0.57	18		_24		14 46		14		36		14								65
55	DO	43-6353.08		7/8	2 3/4"	0.66	76		92		28		76		114		84		44		60		170		66
67	DO DO	43-6353.08-3 43-6353.08	-	7/8 7/8	3 1/4"	0.70					64		64				64		64°		248		352		68
68	00	43-6353.08		7/8	3 3/4"	0,83																	160		69
70	DO	43-6353.08		7/8	4.	0.87									1						96				70

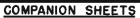
SUPERSTRUCTURE, 15- TO 50-FOOT STEEL SPANS

	BILL OF MATERIALS FOR ONE SPAN WITH WELDED STEEL DETAILS																								
	SILL OF MATERIALS FOR ONE	SPAN WITH WELDEL	J SIEEL I		N LENGTH		15	1	20	1	25	t .	30'		30' SP	ECIAL	35	,	40	1	45	1	50'		
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTI IY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LINE
	LUMBER, SOFT WOOD																					_			
	TIE TIE SPACER	39-9352.68-085 39-3952.1	372 123	6 X 8 3 X 10	8'-6*	128 94	15	270 75	20	360 100	25 5	450 125	30 6	540 150	30 6	540 150	35 7	630 175	40 8	720 200	45 9	810 225	50 10	900 250	1 2
	CLEAT	39-3880.06	371	2 X 6	0'-10"	3	28	23	38	32	48	40	58	48	58	48	68	57	78	65	88	73	98	82	3
	DECK, HARDWARE																								
	HOOK BOLT WITH		H13	3/4	1'-1"	2.1	10		14		16		20		20		24		26		30		34		
5	WASHER AND NUT WIRE SPIKE	42-8488,035-07	51	5/16	0'-7"	0.15	20		26		34		20 40		40		46		54		60		66		5_
6	NAILS	42-6028, 3-2		201	0'-4"	0.032	84		114		144		174		174		204		234		264		294		6
$\overline{}$	STEEL, STRUCTURAL						_																	000000	9
8	STRINGER DO	48-2900.36-23	412W	36 I 230	4'-10 1/2	9200	-		1												1				7
9	00	48-2900, 36-23	413H	36 I 230	40'-0"	9200															i				9
10	00	40 2900,90 29	413W		4'-10 1/2'		 		+								_		,		1		 		10
12	DO		411W	36 I 182	39'-10 1/2"	7257			1										i						12
13	00		414W		9'-10 1/2"	6000 1481			#										 				1 1		13 14
1.5	DO		415W		40'-0"	6000																	1		15
17	DQ	48-2900.36-15	415W	36 I 150	9'-10 1/2" 40'-0"	1481 6000			-		1				 	!							1		16
18	DQ		416₩		9'-10 1/2"	1481																	1		18
19 20	DO		417W		9'-10 1/2"	1481	-		1							ļ							1		19 20
2:	DO		409W		34°-10 1/2°												1_								21
22	00		408W						╂								1		<u> </u>				1		22
24	00	48-2900.33-132	406W	33 I 132	29"-10 1/2"	3943							i												24
25 26	DO DO	48-2900.3-108	40.5W	30 I 108	241-10 1/2*	2686			1		1														25 26
27	DO	48-2900.27-091	40 3W	27 I 91	19"-10 1/2"	1808			1																27
28	DQ	-	402W		201 10 1/02	1000			1						1										28
30	DO	48-2900.21-063	419H	21 I 63	29'-10 1/2"	1882									1										30
31 32	DO		420W		14'~10 1/2"	937	1		+				-	-											3 <u>1</u> 32
33	TOP LATERAL BRACES	48-3790.12-21	440W	12 [20.7	4'-9"	98																	5		33
34	00 00	-0.1700 1.15	435W 437W		7'-7 1/2"	117	1		1		2		3		1		3		4				6		34 35
36	DO	48-3790.1-15	432W 436W				<u> </u>		1 1		1		2		1		2		3						36 37
37 38	DO DO	48-3790.1-15	431W	10 □ 15.3	7'-1 5/8*	109	2		1		2		1		2		2		1						38
39	DO		439W		7'-0 1/8"	107	l		1												3				39 40
41	00	48-3790.1-15	433W		. 0 2/0	10.															2				41
42	DIAPHRAGM	48~3790.18~43	421 W _{422 W}	18 [42.7	6'-0 1/2" 2'-11 1/4"	258 126	2		2		3		3		3		3		3		` a		4		42
44		47-7844,05		PL 13 1/8 X 1/2	2'-8"	60																	8		44
45	TOP LATERAL BRACE PLATES	47-7844.04 47-7844.04	P21W P1W	10 x 3/8 9 x 3/8	1'-5"	18	6		8		10		12		12		14		16		18		22		45 46
46 47	STIFFENER PLATES	47-7844.06	Plaw	5 1/2 X 5/8	2'-10"	33	Ľ						**		^-		4		4				4		47
48	DO DO		P13W P17W						<u> </u>				 				4		4		4		12		48
50	DO	47-7844.06	P16W	5 1/2 X 5/8	2'-9 3/8"	33			1												4				50
51 52	DO	47-7844-06	P11W P10W	5 1/2 x 5/8	21-7 1/2*	31							4								-				51 52
53	. 00	47-7844.06	P8W	5 1/2 x 5/8	2'-4 3/6"	28					4														53
54 55			P7W P6W				├		1 4		4														54 55
56	DO	47-7844.06	P5W	5 1/2 x 5/8	2'-1 1/2"	25			4																56
57 58		47-7844.06	P4H P3H	5 1/2 x 5/8	1'-7 3/4"	19	4		+																57 58
59	00	47-7844.05	PISW	5 1/2 X 1/2	2'-8"	25											2		2				12		59
60		47-7644,05 47-7844.05	P18W	5 1/2 X 1/2 5 1/2 X 1/2	2'-7"	24					<u> </u>		2								4				60
52	DQ	47-7844,05	P9W	5 1/2 X 1/2	2'-2"	20					2														62
63		47-7844.04 47-7844.07	P28W P25W	21 X 3/8 10 X 3/4	1'-9"	77	-		 												4		4		63
65	00	47-7844,05	P24₩	10 X 1/2	2'-6"	43																	4		65
66		47-7844.07	P27W P26W	12 X 3/4 12 X 3/8	3'-6" 2'-0"	107 51			 				+								2				66
68	DO HEB SPLICE PLATE	47-7844.04 47-7844.04	P20W	18 X 3/8	1'-9"	40			╫						 	 					2		8		68
69	WELDING ELECTRODE	46-3772.2-7	1	3/16	<u> </u>		13 LB		16 LB		20 LB		23 LB		25 LB		27 LB		29 LB		58 LB		84 L8		69

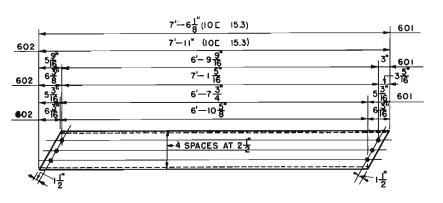
COMPANION SHEETS

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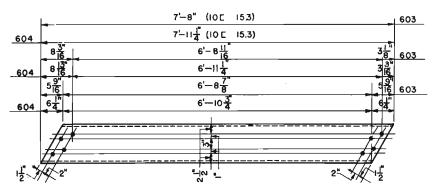
155



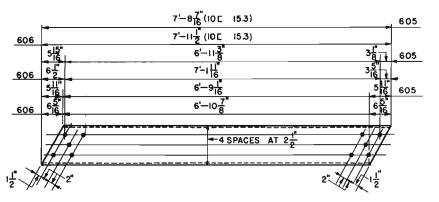
SHEET GENERAL NOTES ASSEMBLY DRAWING BILL OF MATERIALS 158,159 160 SYMBOLS



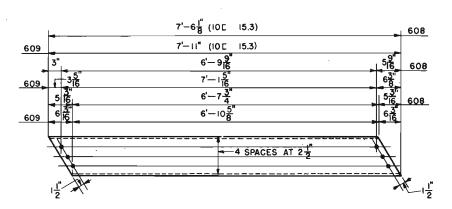
TOP LATERAL BRACE MK 601 TOP LATERAL BRACE MK 602



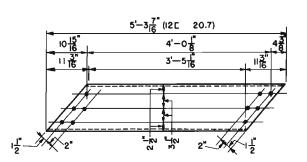
TOP LATERAL BRACE MK 603 TOP LATERAL BRACE MK 604



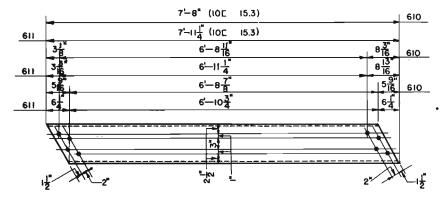
TOP LATERAL BRACE MK 605 TOP LATERAL BRACE MK 606



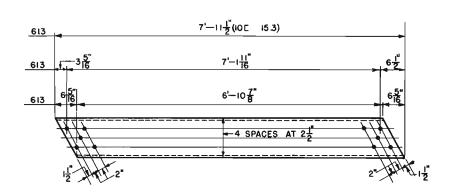
TOP LATERAL BRACE MK 608 TOP LATERAL BRACE MK 609



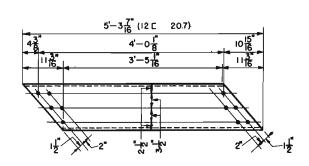
TOP LATERAL BRACE MK 607



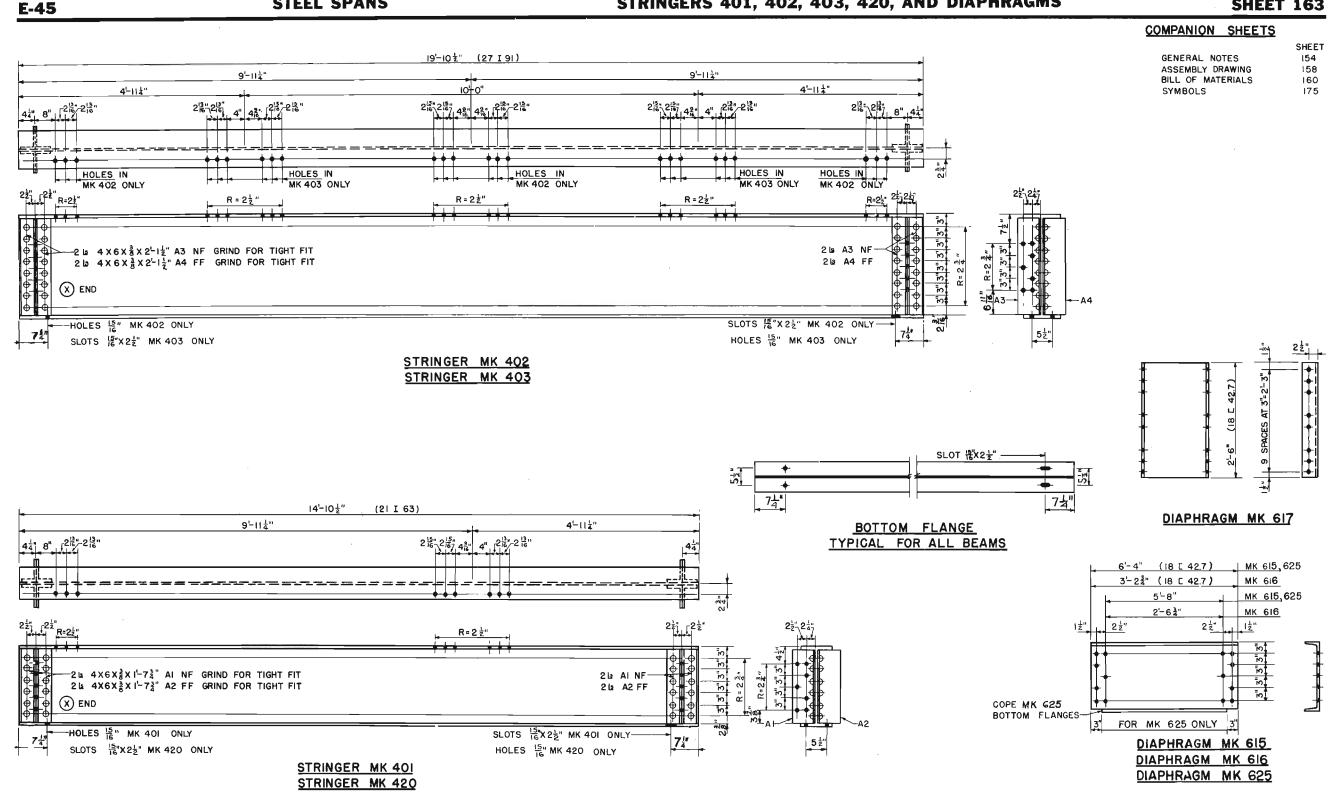
TOP LATERAL BRACE MK 610 TOP LATERAL BRACE MK 611

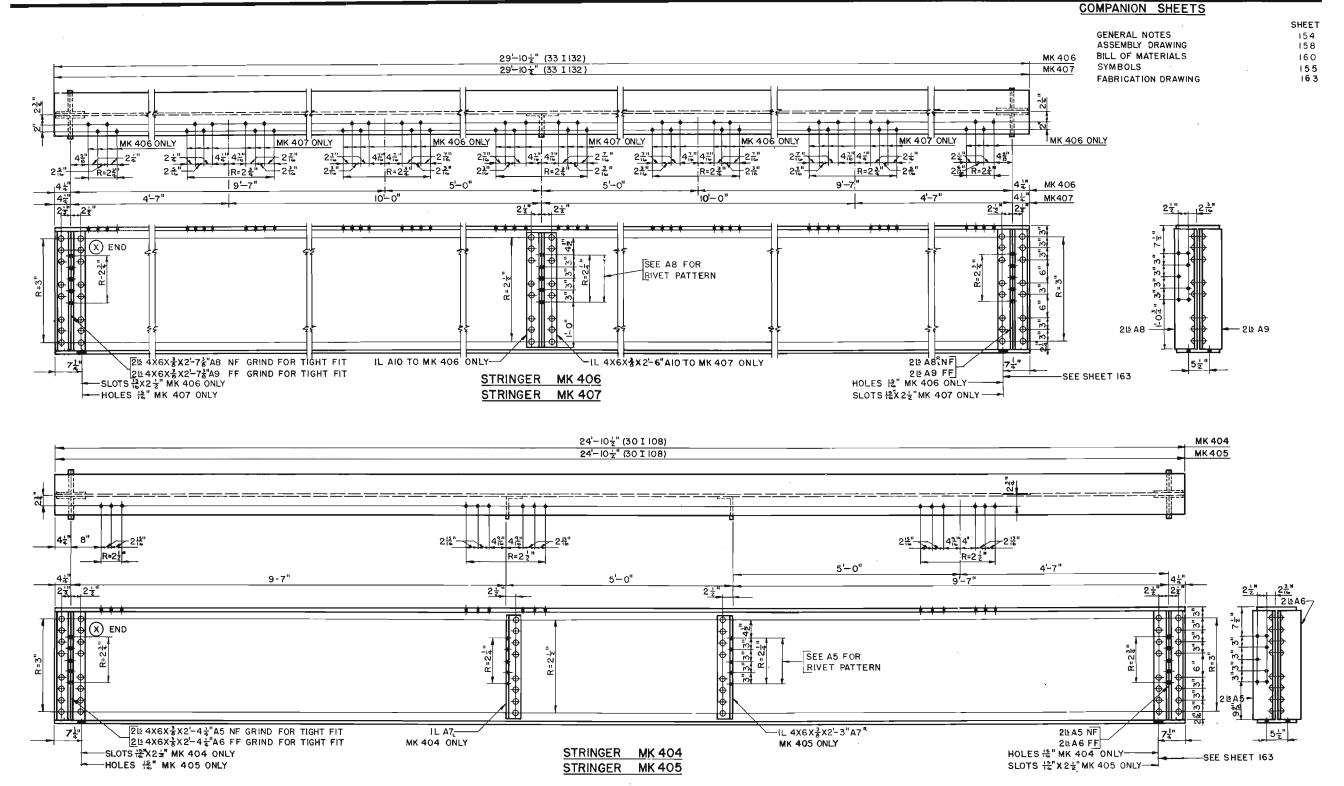


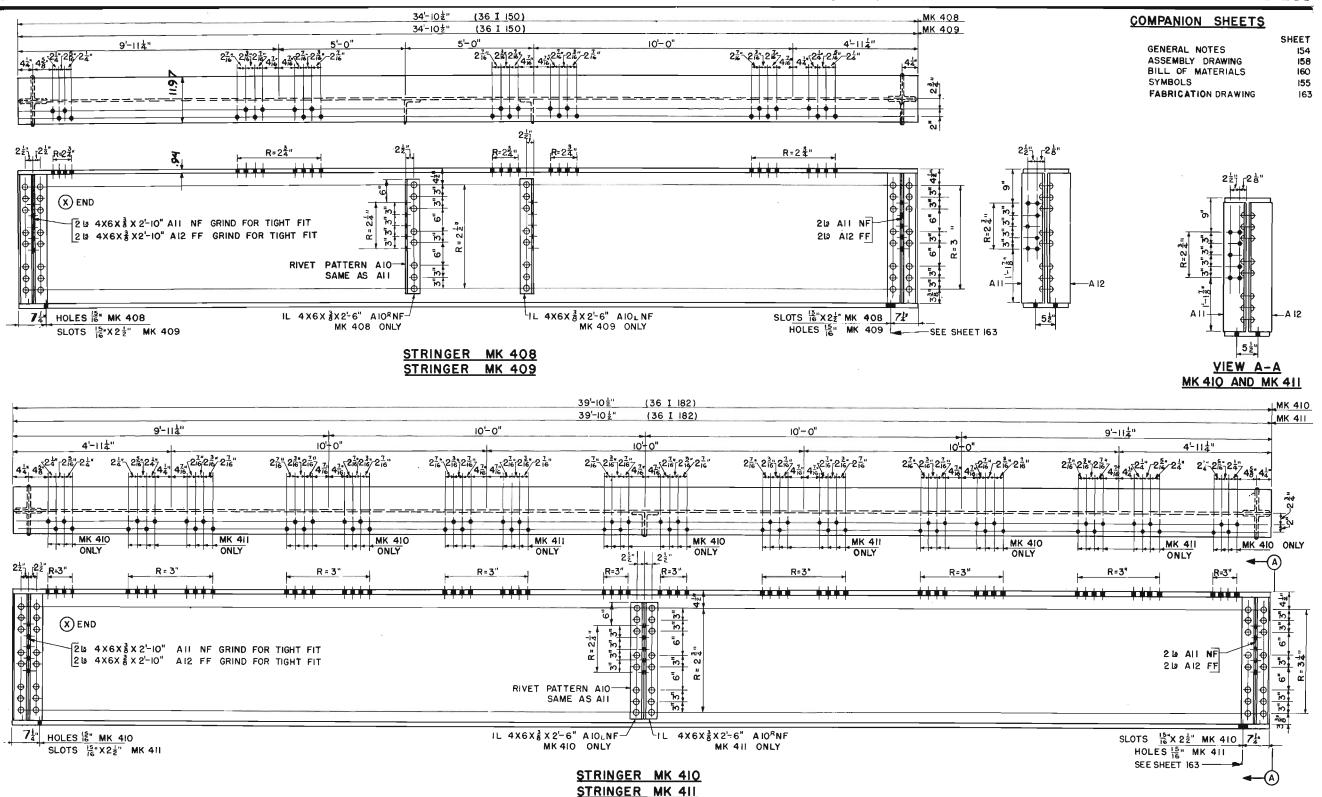
TOP LATERAL BRACE MK 613

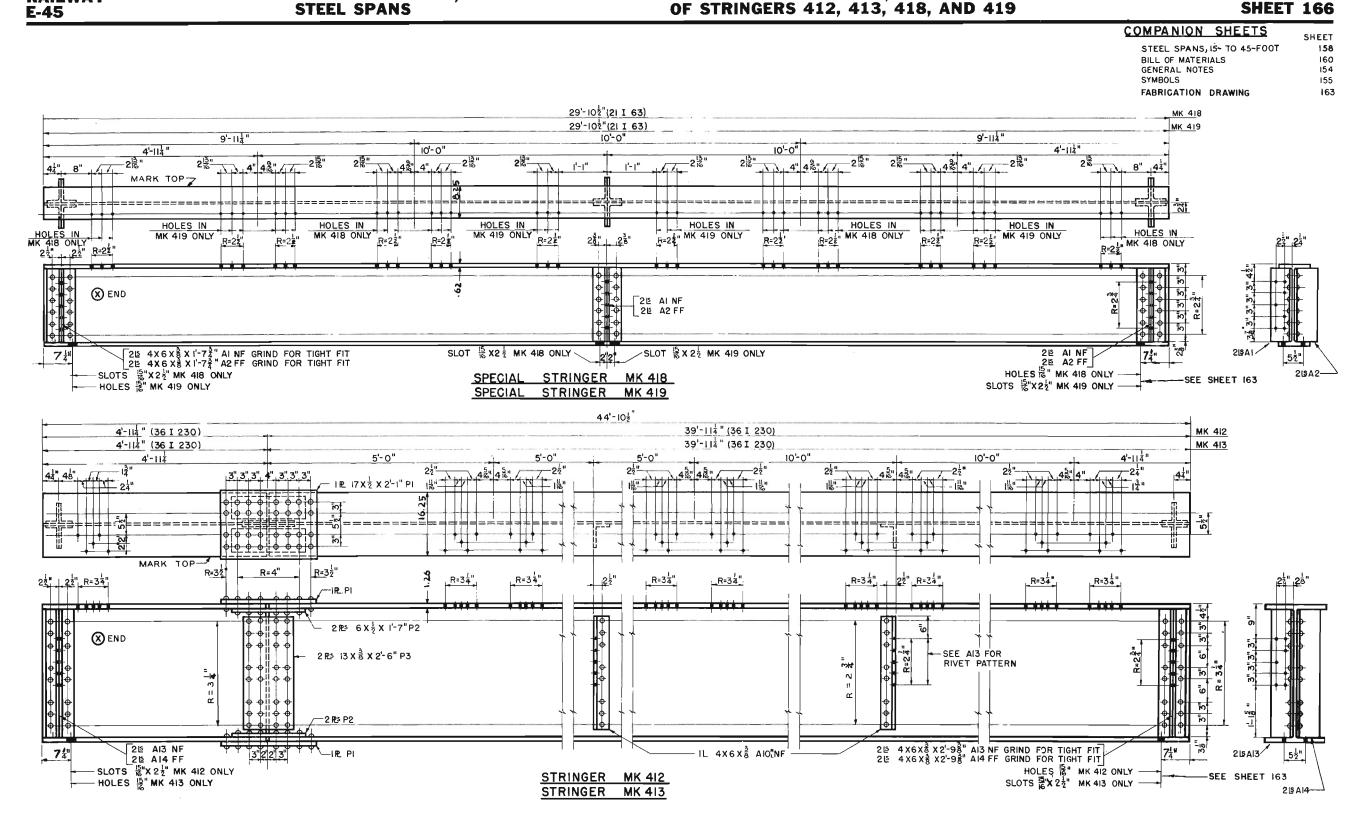


TOP LATERAL BRACE MK 614

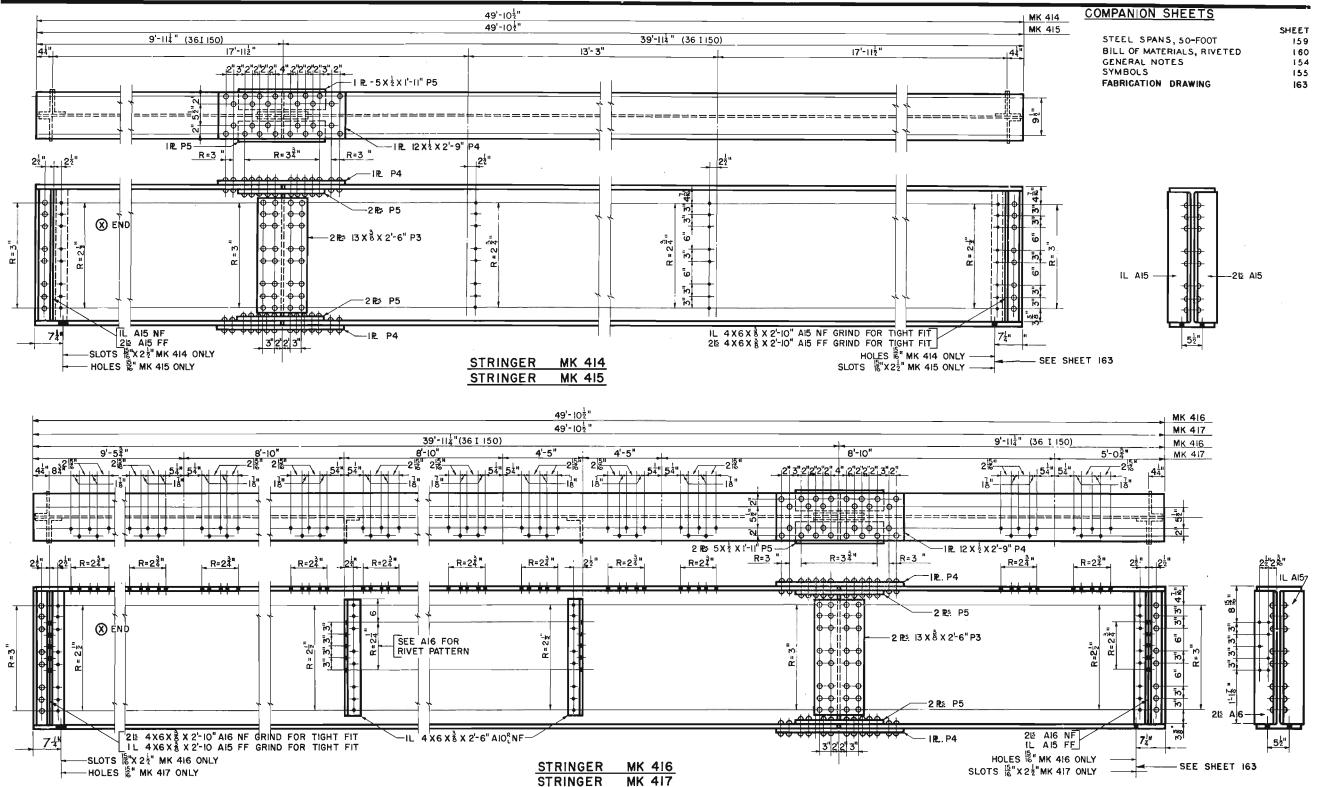








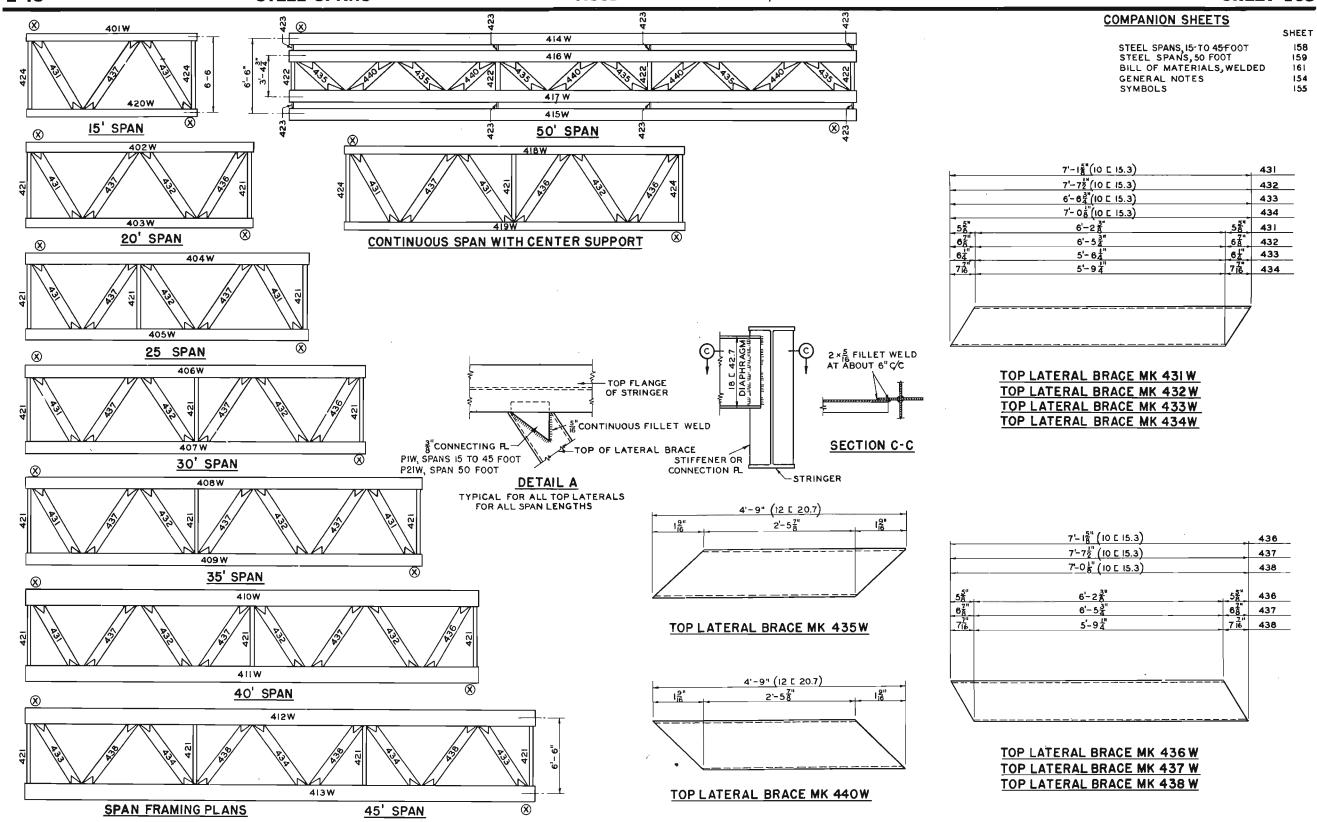
RIVETED CONSTRUCTION, FABRICATION

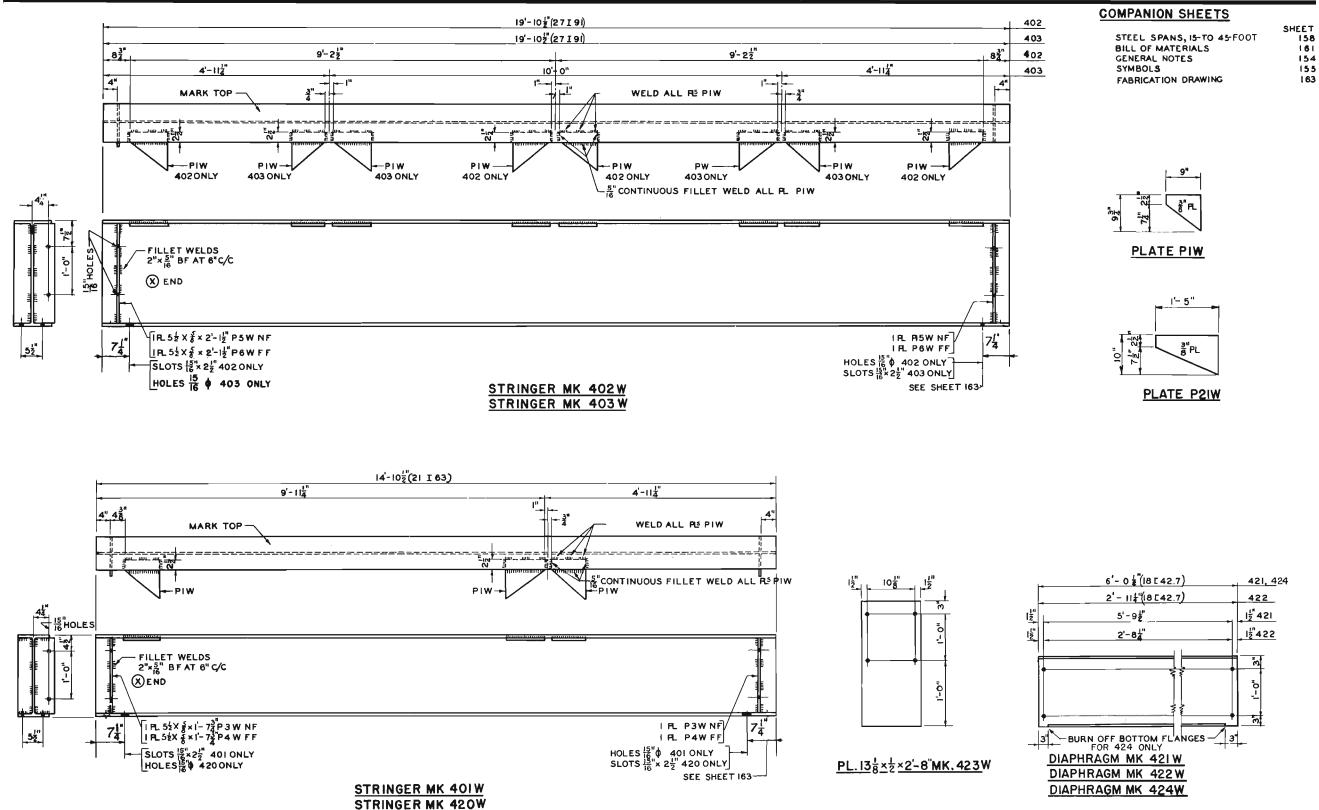


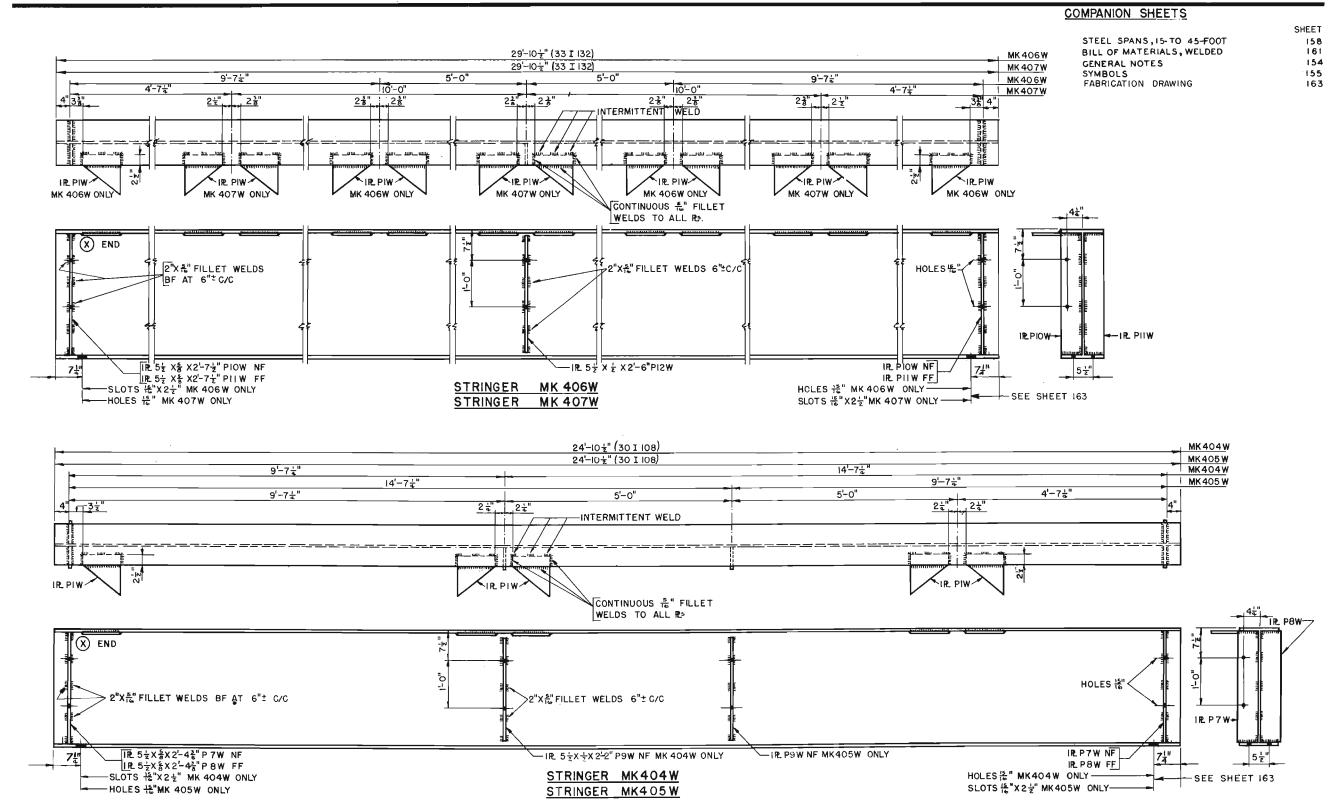
SUPERSTRUCTURE, STEEL SPANS

WELDED CONSTRUCTION, STRINGER AND BRACING ASSEMBLY DIAGRAMS, FABRICATION OF LATERAL BRACES

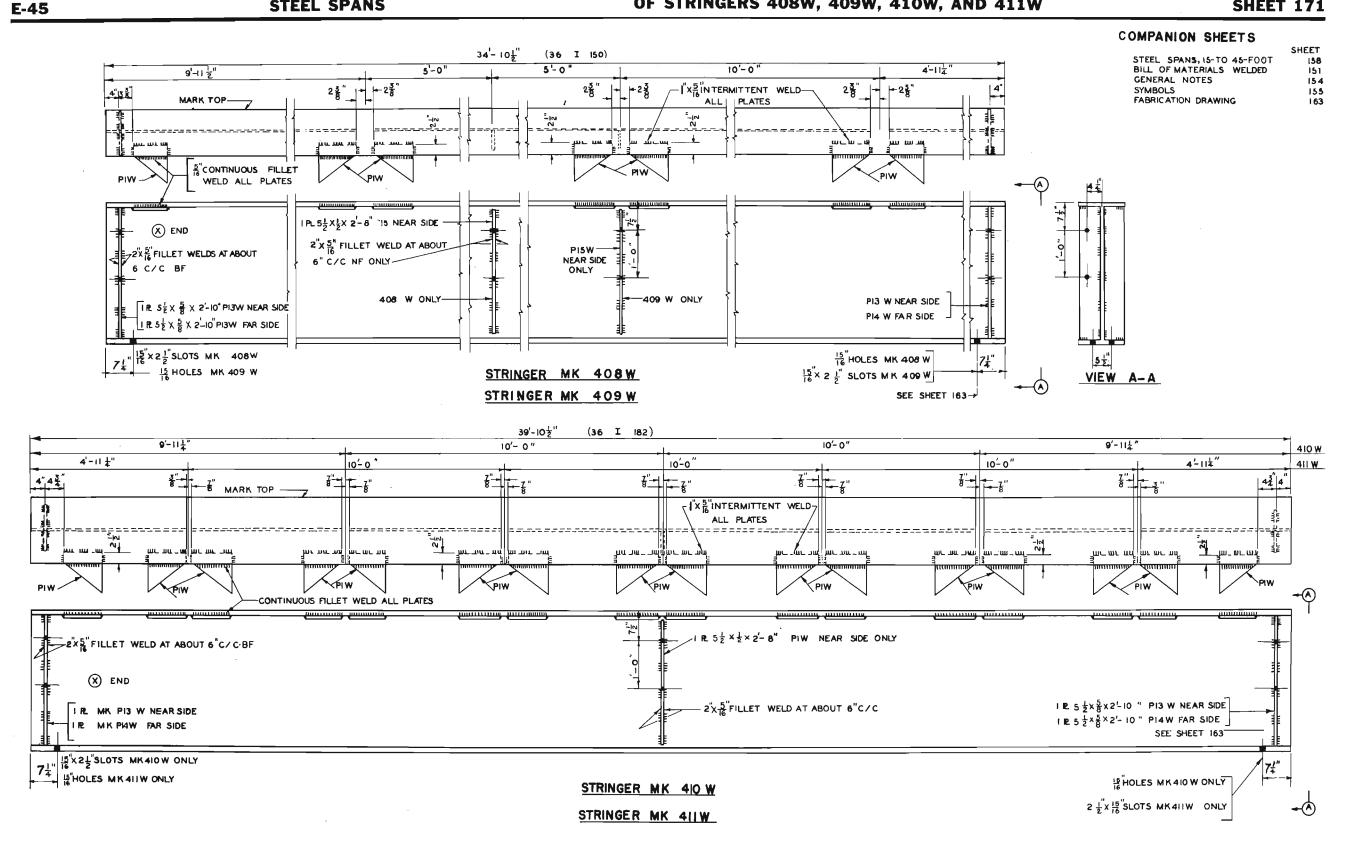
SHEET 168

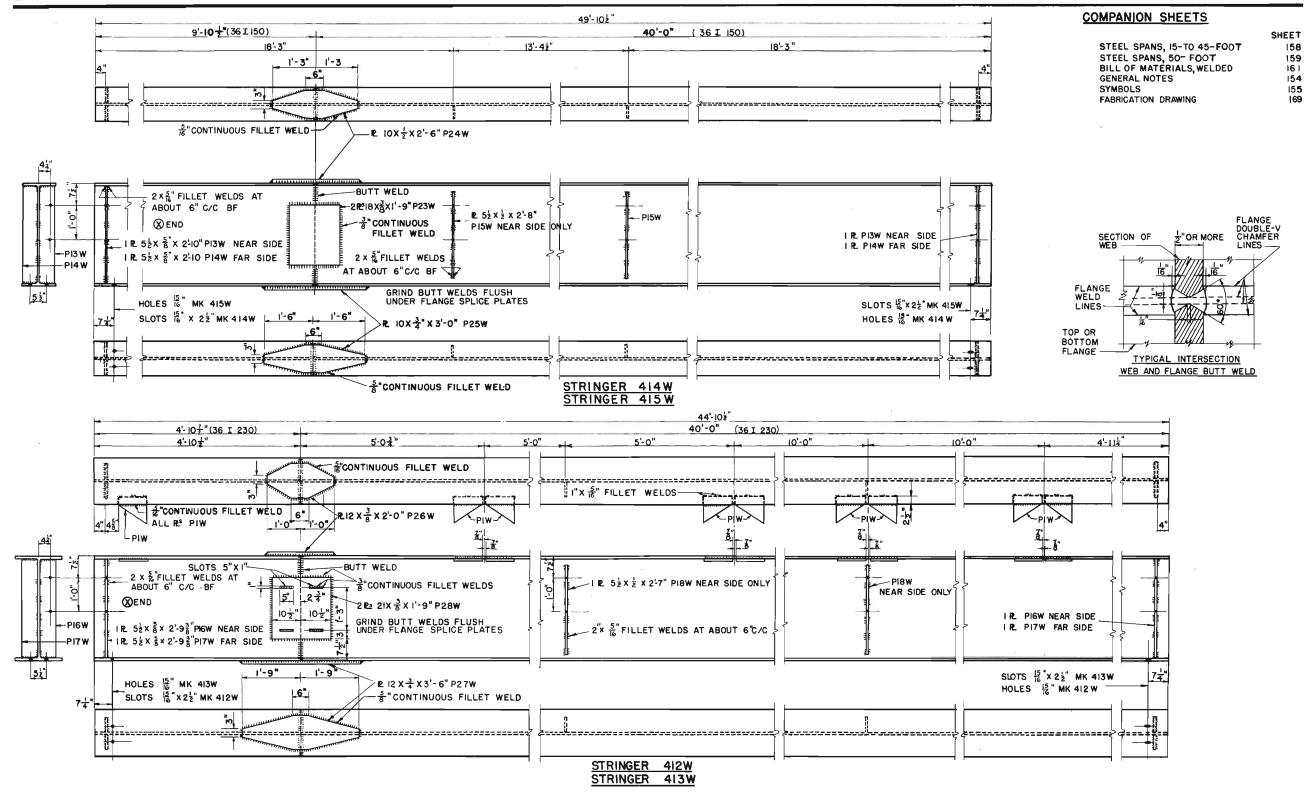






E-45

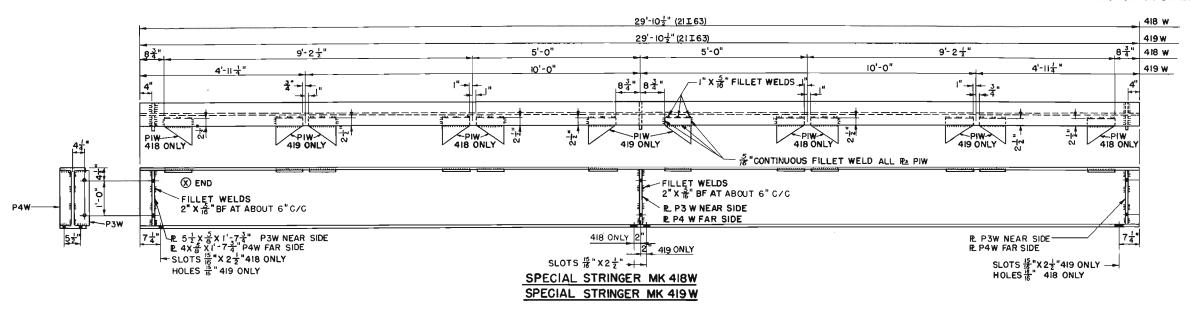


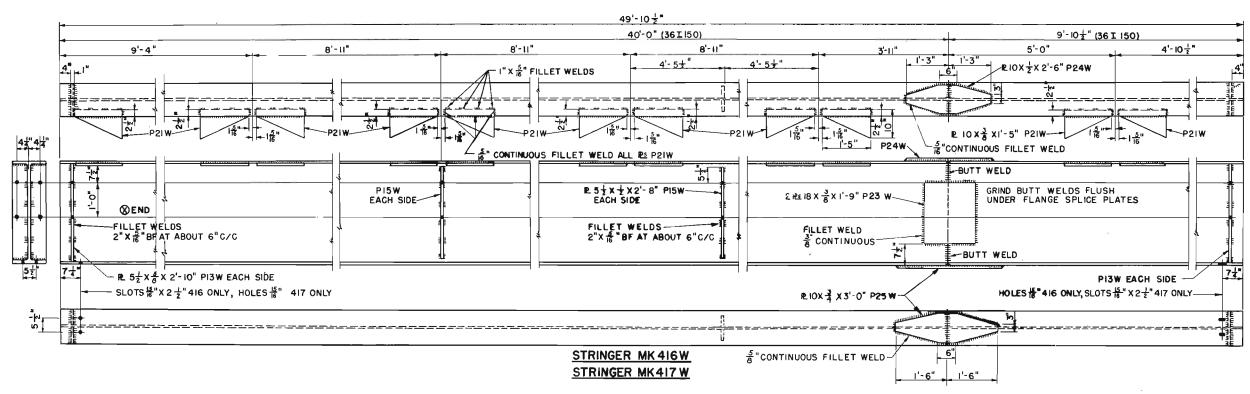


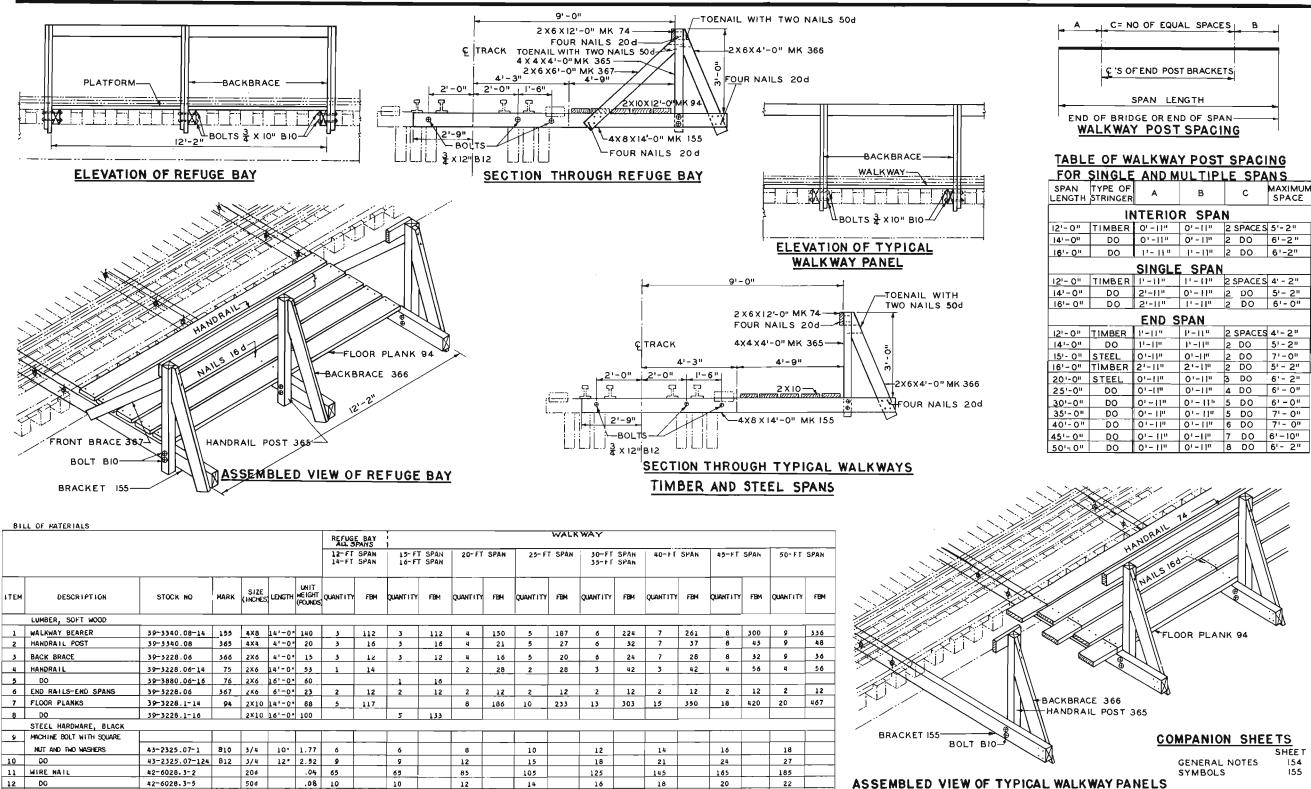
E-45

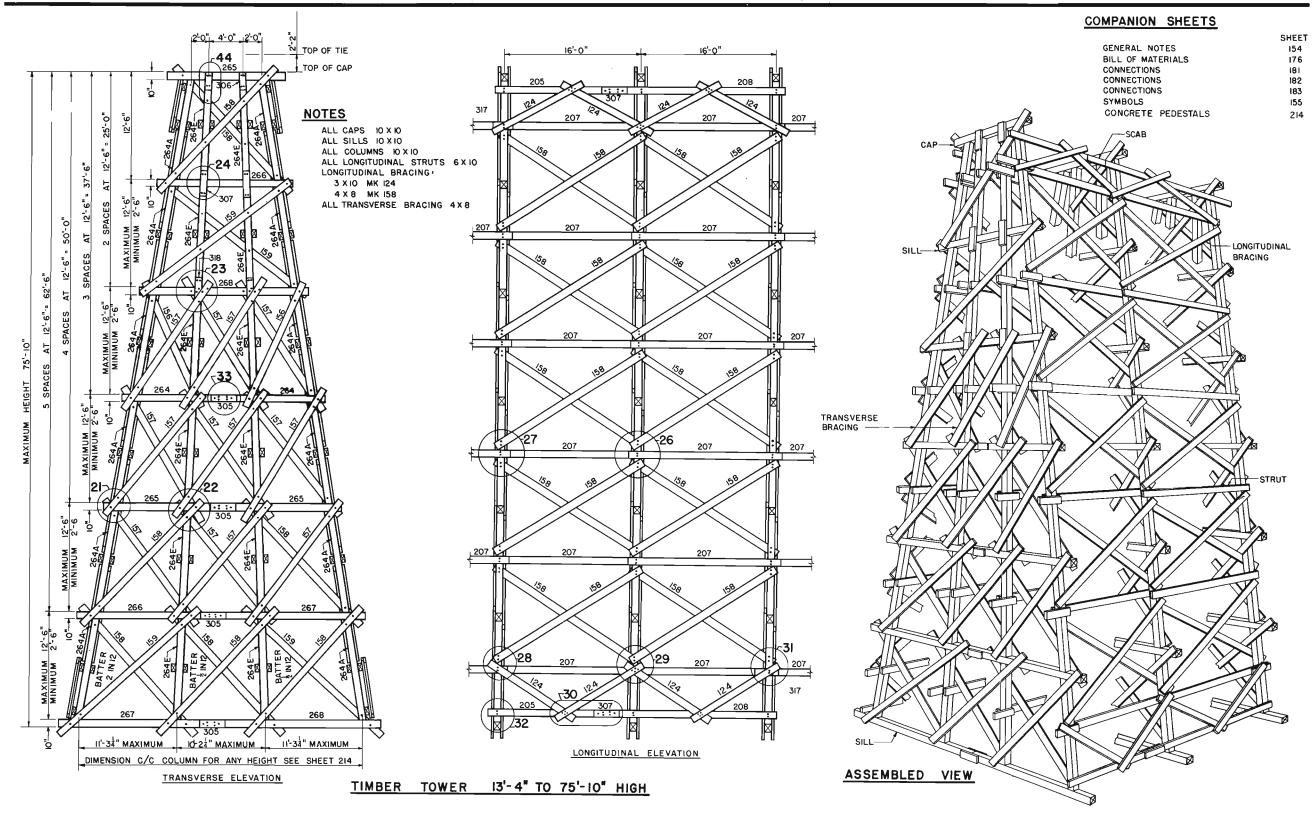
COMPANION SHEETS

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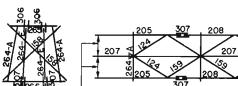






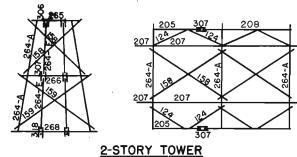
SHEET

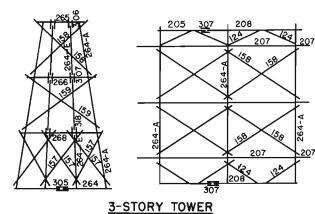
154 175

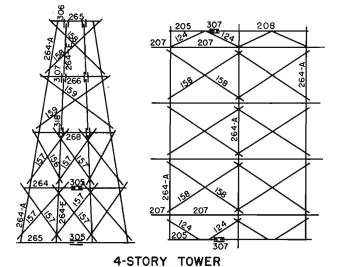


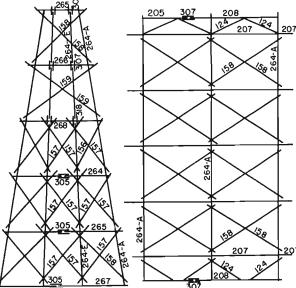
RAILWAY E-45











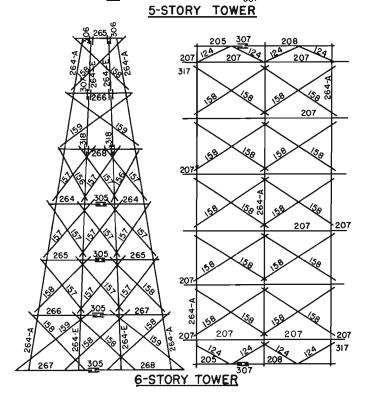
COMPANION SHEETS

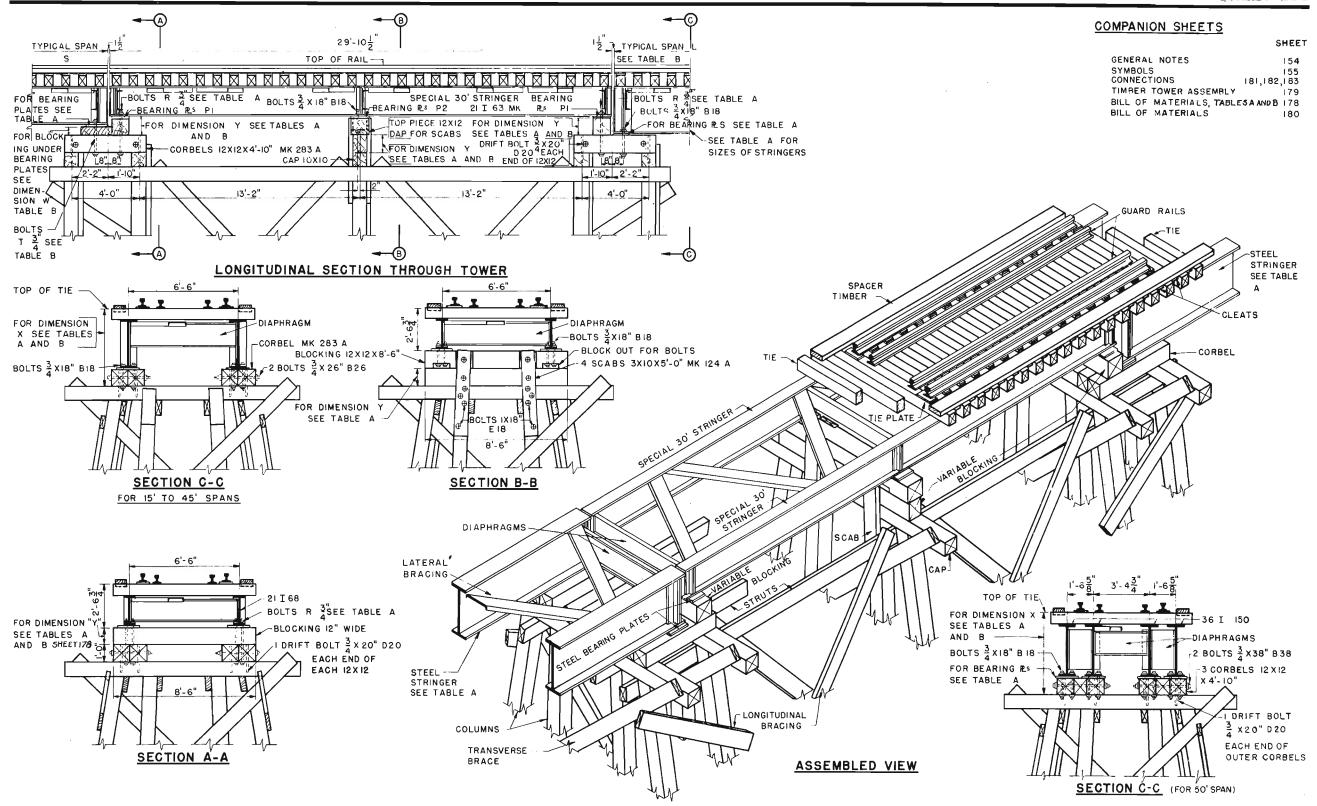
CONNECTIONS

CONNECTIONS CONNECTIONS SYMBOLS

GENERAL NOTES ASSEMBLY AND PIECE MARKS

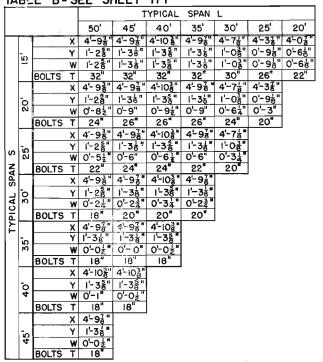
8	ILL OF MATERIAL FOR ONE TO		OF STOP	RIES INDICATE	_D		т		II		II		1				Π	
	N.	IMBER OF STORIES						STORY	5-ST		1	TORY	3-S1			TORY	П	STORY
		TOWER HEIGHT				111117	75'	-10 "	63'-	4 =	50'	-10"	38'-	-4"	25'	-10-	13'	-4"
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	F814	QUANTITY	FBM
	LUMBER, SOFT WOOD																	
1	CAP	39-6620.1-14	265	10 X 10	14'-0"	438	3	350	3	350	3	3 5 0	3	350	3	350	3	350
2	SILL	39-6620.1-2	268	10 X 10	20'-0"	625	6	1000	3	500	3	500	3	500	3	500		
3	00	59-6620.1-18	267	10 X 10	18'-0*	563	6	900	3	450								
4	DO	39-6620.1-16	266	10 x 10	16'-0"	500	6	800	6	800	3	400	3	400	3	400	3	400
5	DO	39-6620.1-14	265	10 X 10	14'-0"	458	6.	700	5	700	6	700						
- 6	00	39-6620.1-12	264	10 X 10	12'-0"	375	6	600	6	600	- 5	600	6	600				
7	COLUMN	39-6620.1-12	264A	10 X 10	12'-0"	375	- 36	3600	30	3000	24	2400	18	1800	12	1200	6	600
8	00	39-6620.1-12	264E	10 X 10	12'-0"	575	35	3600	30	3000	24	2400	18	1800	12	1200	- 5	600
9	STRUT	39-3360.1-2	208	6 X 10	20'-0"	375	4	400	4	400	4	400	4	400	4	400	4	400
10	DO	39-3360.1-18	207	6 X 10	18'-0"	358	72	6480	50	5400	48	4320	36	3240	24	2160	12	1080
_11	DO	39-3360.1-14	205	6 X 10	14'-0"	263	4	280	4	280	4	280	4	280	4	280	4	280
12	BRACING	39-3340.08-22	159	4 X 8	22'-0"	220	12	704	6	352	6	352	6	352	6	352	4	235
13	DO	39-3340.08-2	158	4 X 8	20'-0"	200	64	3413	44	2347	30	1600	22	1175	14	747	6	320
14	DO	39-3540.08-18	157	4 X 8	18'-0"	180	42	2016	42	2016	30	1440	12	576				
15	00	39-3340.08-16	156	4 X 8	16'-0"	160	6	256	6	256	6	256	6	255				
16	DO	39-3952.1-12	124	3 X 10	12'-0"	113	16	480	16	480	16	480	16	480	16	480	8	240
17	SCAB	39-3340.1	305	4 X 10	3'-0"	38	24	240	18	180	12	120	6	60				
18	DO	39-3330.1	307	3 X 10	3'-0"	28	20	150	20	150	20	150	20	150	20	150	20	150
19	00	39-3952.1	318	3 X 10	2'-8-	25	12	80	12	80	12	80	12	80	12	80.		
20	DO	39-3330.1	306	3 X 10	2'-0"	19	12	60	12	60	12	60	12	60	12	60	12	60_
21	DO	39-5330.1	317	3 X 10	1'-6"	14	4	15	4	15	4	15	4	15	4	15		
	STEEL HARDWARE, BLACK			_														
20	MACHINE BOLT WITH NUT	83-2326 I-3	£30	,	30 -	7.8	24		24		24		24		24		16	
22		43-2325.1-3	E28	1	28 •	7.4	8		8		8		8		A		1	
23	00						<u> </u>				l -		48		 		12	
24	00	43-2525.1-24	E24	1	24*	6.5 5.6	120 238		96 182		72 126		70		24 14		14	
25	DO	43-2325.1-2	E20 E18	1 ,	18"	5.1	90	-	90		90		90		96		72	
26		43-2325.1-18		1	16"	4.7				-	156	-	128		76		36	
27	00	43-2325.1-164	E16	1	14"	4.7	212 56		184		56		56		56		56	
		43-2325.1-144	E14		7				156		120		84		48		24	
29	DRIFT BOLT, PLAIN	45-1636.07-2	020	3/4	20*	2.5	192		150		120		04		<u> 40 </u>		H 24	

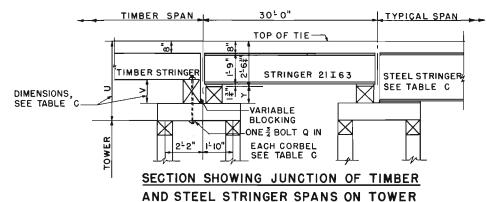




SHEET

TABLE B-SEE SHEET 177





½W ½₩

	011551
GEMERAL NOTES	154
SYMBOLS	155
SUPPLEMENTAL MATERIALS	177
TIMBER TOWERS	179,180

BEARING PLATES W L (INCHES) (INCHES) Р2 (FEET) 15,50 12 12X1X1'- 4" | 11X3X1-3" 16 20,25 12 12X IX I- 8" | 11 XI X I-7" 20 15X1X 1'-8" | 14X1X 1'-7" 30, 35 20 15 40, 45 16 21 16XIX 1-9" 15XIX 1-8"

COMPANION SHEETS

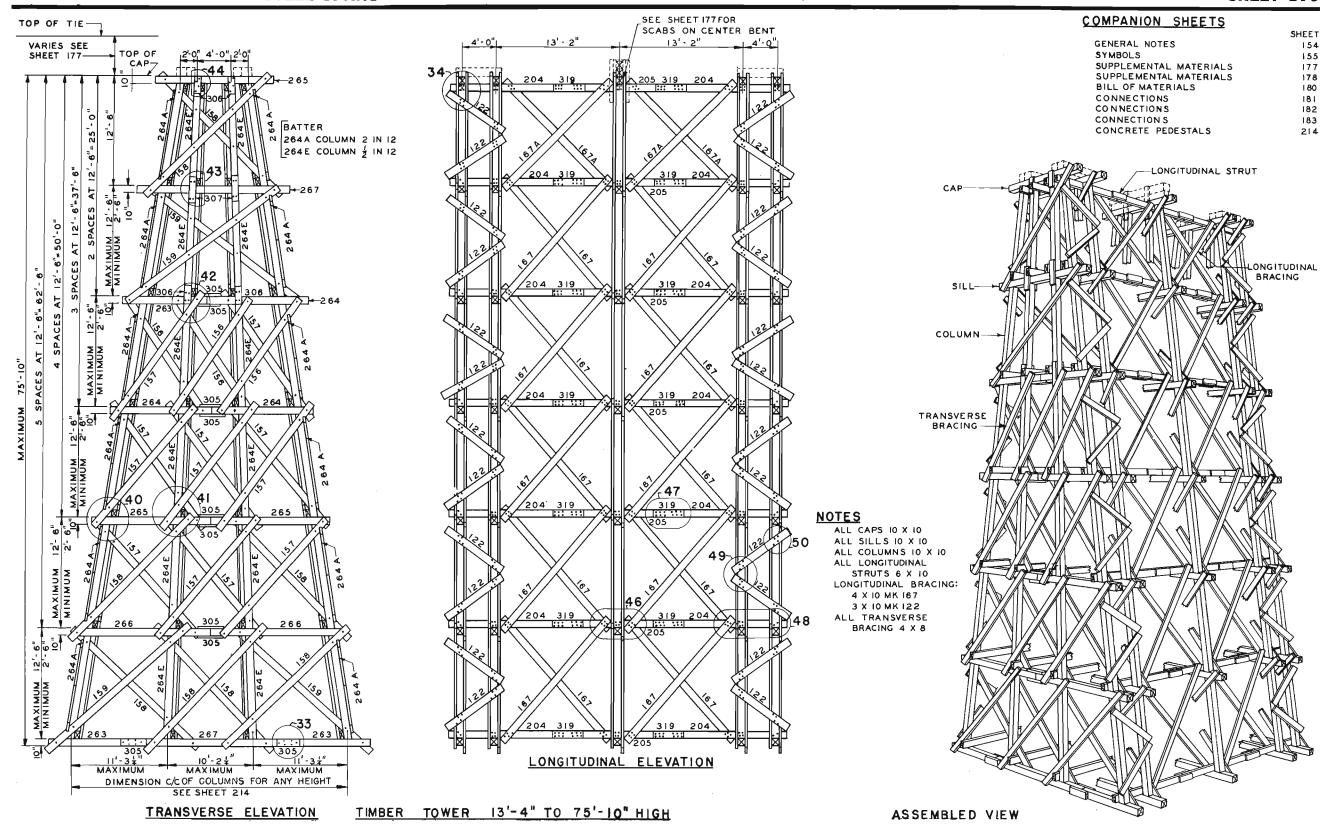
TABLE C-FOR KNOWN STEEL-STRINGER SPAN

		DIMENSIONS										
TYPICAI SPAN	STEEL STRINGERS	U	Y		MBER NGERS	I8" TIMBER STRINGERS						
				V	BOLT Q	٧	BOLT Q					
15'	21 I 63	3'-63"	0'-0"	0-63"	20"	0'-43"	18"					
20'	27 I 91	4'-07"	0,-6후		26"	0-10%	24"					
25'	30 I 108	4-37	0'-95"	1-37 "	30"	1-13"	28"					
30'	33 I 132	4'-78"	1-03"	l'−7ģ"	32"	1'- 5냚"	30"					
35'	36 I 150	4-98"	1'-34"	i'-97 "		1-7골"	34"					
40'	36 I 182	4'-108"	1'-35"	1-10흫"	36"	1'-83 "	34"					
45'	36 I 230	4-94	1-34 "	1 - 9∄"	36"	1-78"	34"					
50'	36 I I50	4-98"	1'-2출"	1-98	36"	1-7층 "	34"					

TABLE A-SEE SHEET 177

TYPICAL SPAN	STEEL STRINGERS	BEARING PLATES	DIMENS	SIONS	BOLTS R
Ĺ		MARK	υ	Y	LENGTH
15'	21 I 63		3'-63"	0'-0"	18"
20'	27 I 91		4'-0g"	0'-6 8 *	22"
25'	30 I 108		4'-3g"	0-98"	26"
30'	33 I 132		4'-78"	1'-03"	30"
35'	36 I 150		4'-9중"	1'-38 "	32"
40'	36 I 182		4'-108"	1-3종 "	32"
45'	36 I 230		4'-9g"	l'-3 ģ "	32"
50'	36 I 150		4'-98"	1'-2 § "	32"

LINE																							
LINE -			S	PAN ADJOININ	G TOWER		15		20	t .	25		30) '	3:	51	40	'	45	1	50	*	_
LINE			, ş	TRINGER SIZE			21 I	63	27 I	91	30 I	108	33 I	132	36 1	160	36 I	182	36 I	230	36 I	150	_
	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM	SNAMLLLA	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	CNWLLLA	FBM	LINE
	LUMBER, SOFT WOOD						100000000000000000000000000000000000000																
1	CORBEL	39-6630.12	283A	12 X 12	4'-10"	218	8	480	8	480	8	480	8	480	8	480	8	480	8	480	12	720	1
2	BLOCKING ON CENTER BENT	_39-6616.1	233A	8 × 10	8'-5"	210			1	67			1	67	1	67	1	57	1	67	2	134	2
3	DO	39-6620.1	263A	10 X 10	8'-5"	270					1	83			1	83	1	83	1	83			3
4	DO	39-3360.1	233A	6 X 10	81-64	180			- 3.2 15-61				ı	50									.4_
5	BLOCKING ON END BENTS	39-6616.12	2484	8 X 12	8'-6"	250			2	160			1	80	2	160	2	160	2	160	2	160	5
6	DO	39-6620.12	248A	10 X 12	8'-6"	320					2	200_			2	200	2	200	2	200	2	200	6
7	DO	39- <u>3360.12</u>	2484	6 X 12	8'-5"	190					15050000		1	1.20									7
8	TOP PIECE CENTER BENT	39-6630.12	2834	12 X 12	81-6"	580	1	120	1	120	1	120	1	120	1	120	1	120	1	120	1	120	8
9	SCAB	39-3952.1	1249	3 X 10	51-0*	50	4	60	4	60	4	60	4	60	4	60	4	60	, 4	60	4	60	وا
	STRUCTURAL STEEL																						
10	BEARING PLATE	47-7844.1	ρ1	12 X 1	11-44	50	8		6		6		6		6		6		6		10		10
11	DO	47-7844.07	P2	11 × 3/4	1'-3"	35	8		6		6		б		6		6		6		10		11
12	DO	47-7844.1	ρ1	12 X 1	1'-8"	64			2		2												12
13	DÓ	47-7844.1	ρ2	11 × 1	1'-7"	60			2		2												13
14	DO	47-7844.1	Ρ1	15 X 1	1'-8"	85							2		2								14
15	00	47-7844,1	Ρ2	14 X 1	1'-7"	75							2		2								15
16	00	47-7844.1	P1	16 X 1	1'-9"	95											2		2				16
17.	DO	47-7844.1	P2	15 X 1	1'-8"	85											2		2				17
	STEEL HARDWARE, BLACK																						
	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.07-183	818	3/4	18*	2.6	20		12		12		12		12		12		12		24		18
19	DO PRO PROJEKS	43-2325.07-223	B22	3/4	22"	3.0			8														19
20	00	43-2325.07-266		3/4	26*	3.6	8		8		16		8		8		8		8		-		20
21	DO	43-2325.07-200		3/4	30 *	4.0	0		"		1 10		a				<u> </u>		<u> </u>		8		21
22	DO	43-2325.07-32	B32	3/4	32"	4.2									8		8		8				22
23	00	43-2325.07-386		3/4	38"	5.0									1						8		23
24	DO	43-2325.1-18	E18	1	18*	4.8	10		12		12		12		12		12		12		12		24
-	DRIFT BOLT	43-1636.07-2	D20	3/4	20"	2.6	16		16		16		16		16		16		16		16	_	25

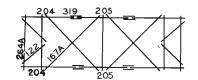


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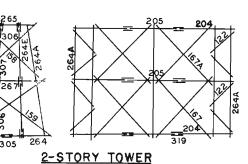
154 177, 178 179

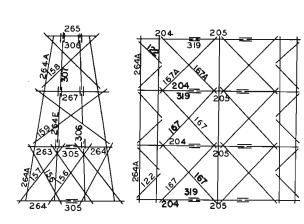


27 DRIFT BOLE, PLAIN

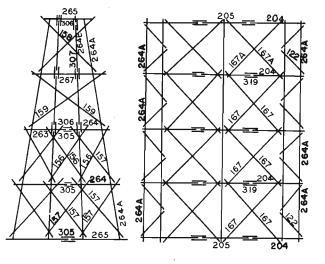


I-STORY TOWER





3-STORY TOWER



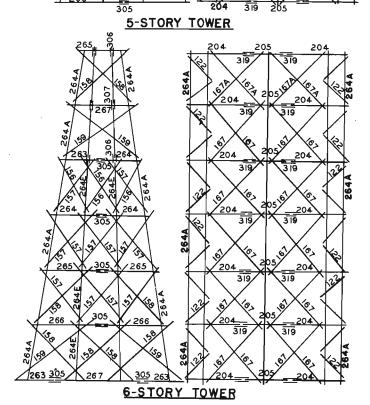
4-STORY TOWER

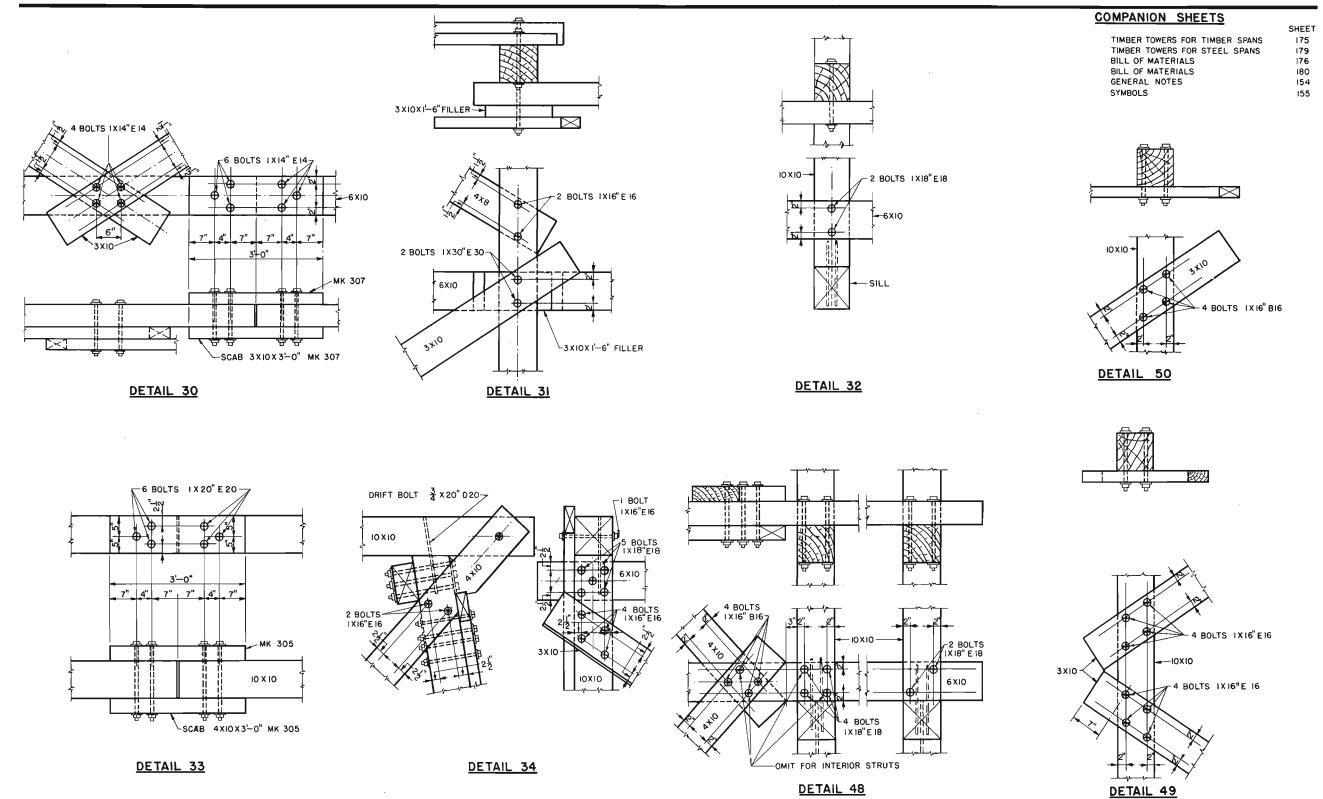
GENERAL NOTES
SUPPLEMENTAL MATERIALS
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CONNECTIONS
CONNECTIONS
SYMBOLS 181 182 183 155

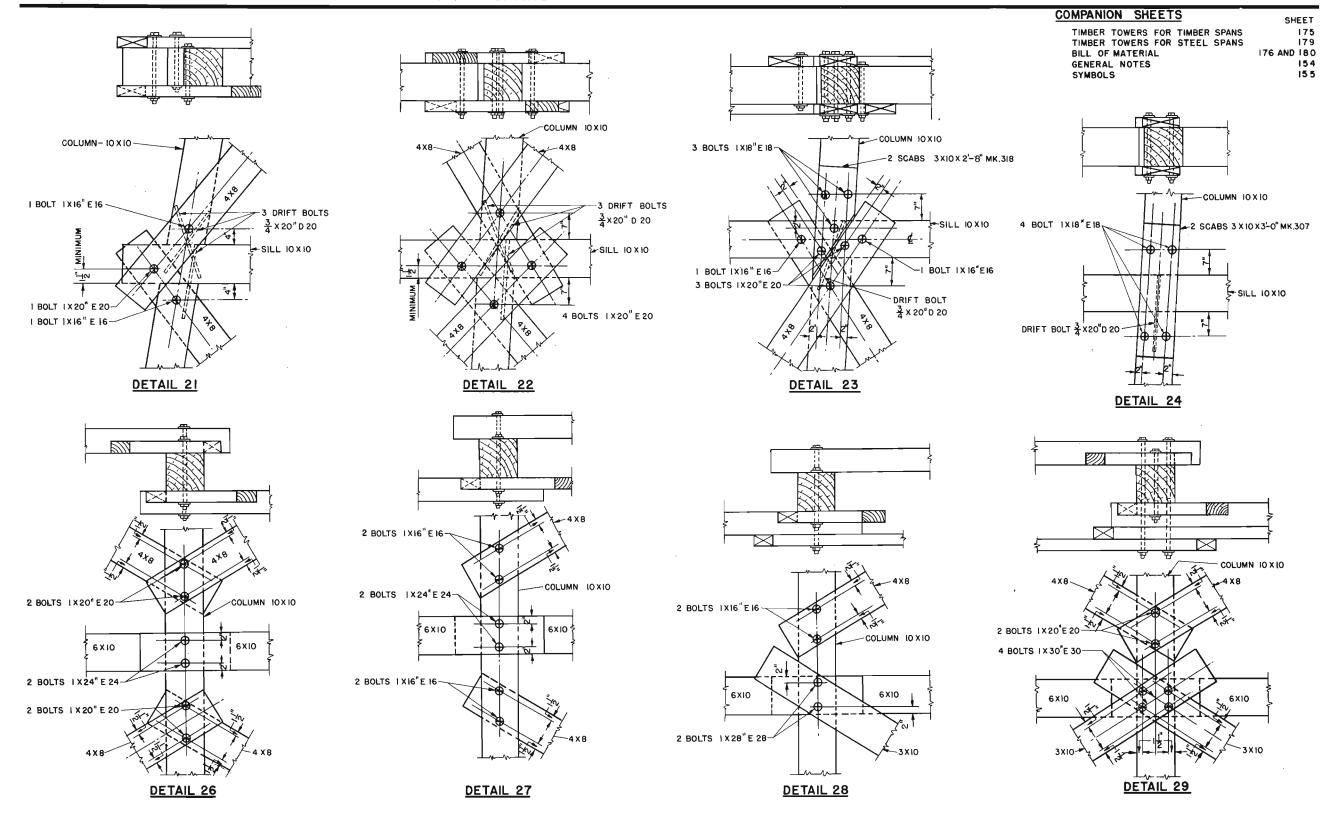
COMPANION SHEETS

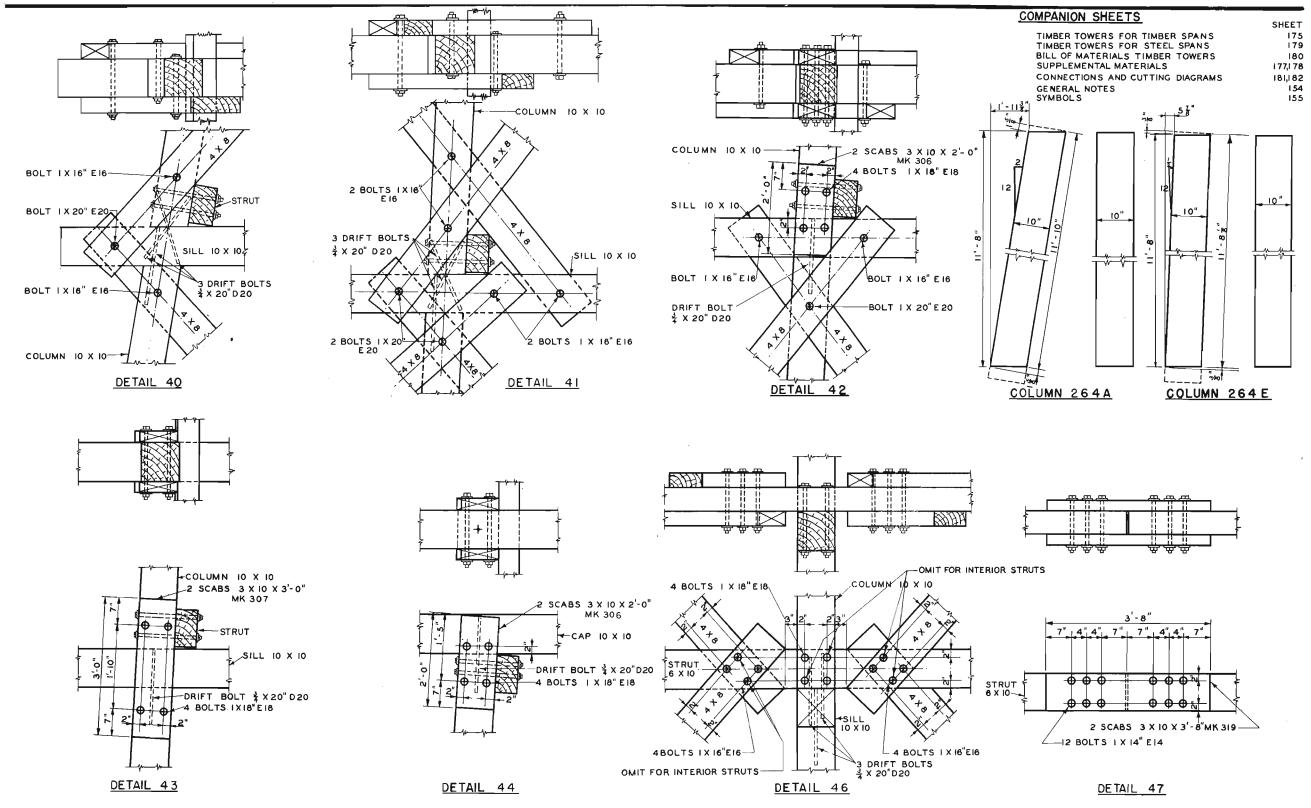
				NUMBER OF STORI	ES		6-510	RY	5-S	FORY	4-S	rory .	3 -Sr(JRY YAC	2-S	TORY .	1-5	STURY
				EIGHT UF TUWER			75'-1	0"	63'-	-4×	50'-	10"	38'-1	4.*	25'-	-10"	15'	-4"
INE	DESCRIPTION	STUCK NO	MARK	STZE (INCHES)	LENGTH	URIT WEIGHT (POUNDS)	QUANT. I TY	FBM	QUANTITY	r'BM	QUANTITY	MBH	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM
	LUMBER, SOFT WOOD	_			3/2	100000000000000000000000000000000000000											_	
	CAP	39-6620.1-14	265	10 x 10	14'-0"	438	5	583	5	583	5	583	5	583	5	583	5	593
2	SILL	39-6620.1-18	267	10 X 10	18'-0"	563	10	1500	5	750	5	750	5	750	5	750	5	750
3		39-6620.1~16	266	10 X 10	16'-0"	500	10	1555	10	1355								
4	DO	39-6620.1-14	265	10 X 10	14'-0"	438	10	1167	10	1167	10	1167						
5	DO	35-6620.1-12	264	10 × 10	12'-0"	375	15	1500	15	1500	15	1500	15	1500	5	500		
6	00	39-6620.1-1	263	10 X 10	10'-0"	313	15	1250	5	417	5	417	5	417	5	417		
یا	COLUMN	39-6620.1-12	264A	10 X 10	12'-0"	375	60	6000	50	5000	40	4000	30	3000	20	2000	10	100
8	00	39-6620.1-12	264E	10 X 10	12'-0"	375	60	6000	50	5000	40	4000	30_	3000	20	2000	10	100
٤	STRUT	39-3560.1-14	204	6 X 10	14'-0"	263	56	3920	48	3360	40	2800	32	2240	24	1680	16	112
	no	39-3360, 1-12	205	6 X 10	12!-0"	225.	.28	1680	24	1440	20	1200	16	960	12	720	8	48
Ш	BRACING	39-3350.1-08	122	3 X 10	8'-0"	7.5	48	960	40	800	32	640	24	480	16	320	8	16
2	00	39-3340.08-22	159	4 X 8	22'-0"	220	20	1173	10	587	10	587	10	587	10	587		
3	00	39-3540.08-2	158	4 X 8	20'-0"	200	40	2133	20	1067	10	533	10	533	10	553	10	53
4	00	39-3340.08-18	157	4 x 8	18'~0"	180	60	2880	60	2880	40	1920	10	480				
5	000	39-3340.08-16	156	4 X 8	161-0	160	20	853	20	853	20	853	20	853				
6.	00	39-3340,1-18	167A	4 X 10	18'-0"	225	16	960	16	960	16	<u>960</u>	16	960	16	960	16	96
7	00	.59~3340.1~18	167	4 X 10	18'-0"	225	80	4800	64	3840	.48	2880	32	1920	16	960		
8_	SCAR	39-3340.1	305	4 X 10	3!-0"	.38	60	600	40	400_	30	300	20	200	10	100		
۹	<u> </u>	39-3330.1	319	3 X 10	3'-8*	34	112	1027	96	880	80	733	64	587	48	440	32	29
┙	<u>no</u>	39-3952.1	307	3 X 10	3'-0*	28	20	150	20	150	.20	1,50	20	150	20	150	20	150
ı	Σ	39-3330,1	306	3 X 10	2'-0"	19	36	180	36	180	36	180	36	180	36	180	16	80
	STEEL HAROWARE, BLACK																	
2	MACHINE BOLT WITH SQUARE NUT AND TWO WASHERS	43-2325.1-2	E20	1	20"	5.6	300		210		150		90		40		i	
3	00	43-2325.1-18	E18	1	18"	5.1	488		436		384		332		280		186	
4	200	43-2325, 1-164	£16	1	16*	4.7	984		812		540		468		276		124	
5	ο	43-2325.1-144	E14	1	14"	4.3	672		576		480		384		288		192	
6	DO	43-2325.1-124	E12	1	12"	3.8	96		96		96		96		96		96	

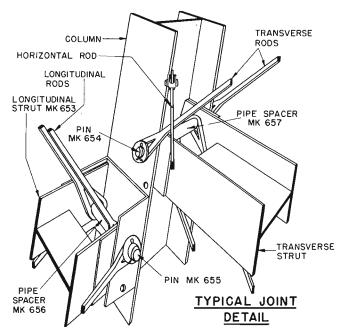
20* 2.5 320





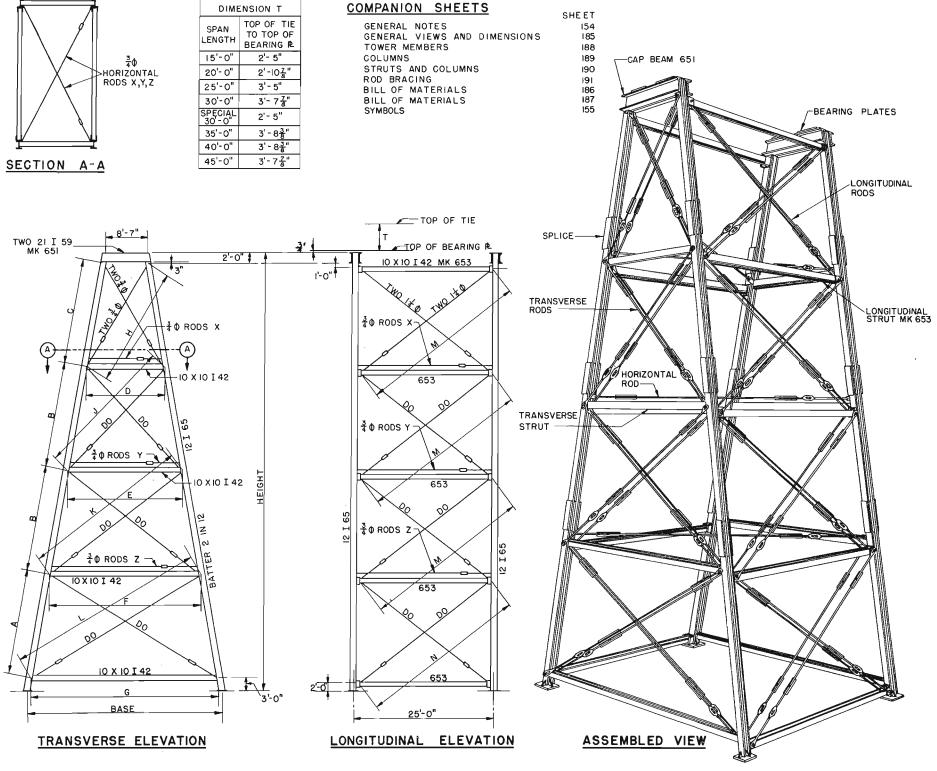


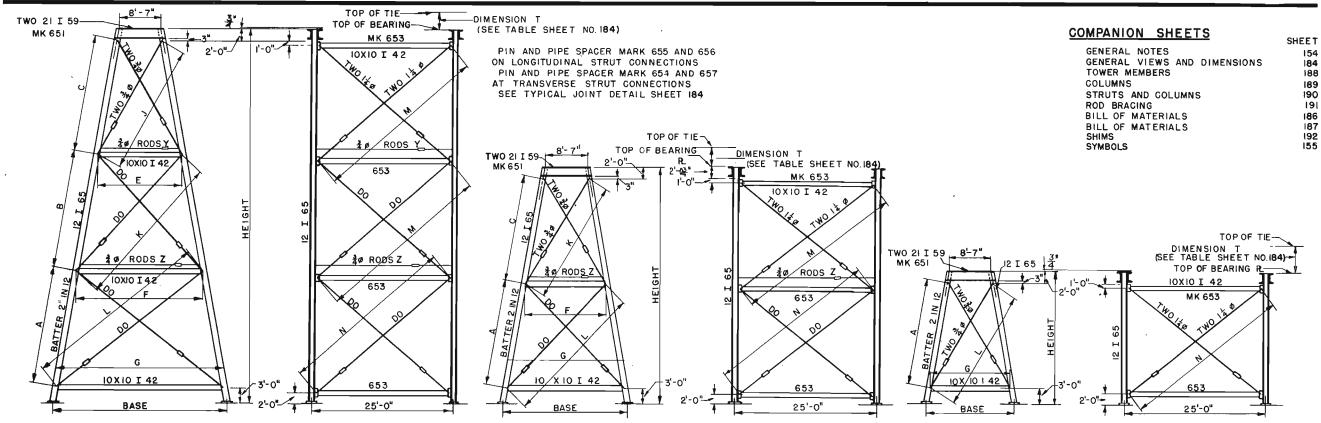




TABULATION OF TOWER DIMENSIONS AND ERECTION MARKS

			FOUR	STORY T	OWER	
HE	IGHT	77'	75′	73'	71'	69'
В	ASE	34-3"	33'-7"	32'-11"	32'-3"	31'-7"
Α	MARK	1728	1730	1729	1731	1732
	DIMENSION	18'-3"	17-8 } "	17'-2 7 "	16'-8 3 "	16'-2 \f 2"
В	MARK	1741	1742	1743	1751	1752
	DIMENSION	18 ^L -3"	17'-8 7 "	17'-2 7 "	16'-8 3 "	16'-2 5 "
С	MARK	1756	1760	1761	1757	1762
	DIMENSION	18'-3"	17'- 8 8 "	17'-2 8 "	16"-8 <u>3</u> "	16'-2 8 "
D	MARK	1709	1710	1711	1712	1713
	DIMENSION	14'-9"	1 4 '-7"	14'-5"	14'-3"	14'-1"
Ε	MARK	1694	16 95	1696	1698	1697
	DIMENSION	20'-9"	20 ^L 5"	20'-1"	19'-9"	19'-5"
F	MARK	1681	1771	1685	1686	1687
	DIMENSION	26'-9"	26'-3"	25'-9"	25'-3"	24'-9"
G	MARK	1674	1675	1676	1769	1770
	DIMENSION	32'-9"	32'-1"	31'-5"	30'-9"	30'-1"
Н	MARK	8 48	850	852	853	854
	DIMENSION	21'-6"	21'-0 ช ี"	20 '-6 7"	20-់ 1 ខ្ ងី"	19'- 7 8 "
J	MARK	83।	833	836	838	842
	DIMENSION	25'-3 ३ "	24'-9"	24'-2 5 "	23'-8 4 "	23'-2"
K	MARK	803	807	812	816	820
	DIMENSION	29 ¹ -9 8 "	29' - 2"	2ଟ-6୫ୁଁ"	27'-10 <u>7</u> "	27 ⁻ 3 ¹ / ₄ "
L	MARK	743	752	765	775	785
	DIMENSION	34'-9¼"	34'-0 8"	33'-3 8 "	32'-6"	31'-8 7 "
M	MARK	1028	1030	1031	.1032	1033
	DIMENSION	29'-8 <u>4</u> "	29'-4½"	29'-0 { "	28'-9 § "	28 '-5 {}"
N	MARK	1028	1030	1031	1032	1033
	DIMENSION	29'-8 4 "	29'-4½"	29'-0 7 "	28'-9 8 "	28'-5 8 "
X	MARK	981	982	983	984	985
	DIMENSION	27'-0 8 "	26'-11 8 "	26'-10 ⁷	26'-9 7 "	26'-9"
Y	MARK	968	969	970	971	973
	DIMENSION	30'-6 8 "	30'-3 § "	30'-1 "	29 '- 10 8 "	29'-8 "
Z	MARK	955	959	960	963	964
	DIMENSION	34'-7 3 "	34 ' -3 ‡ "	33'-11"	33'-6 8 "	33'-2 8 "





					THREE-STORY	TOMER	_							THIO-STOR	y tower									ONE-STORY TO	MER			
MEIG	нт	671	65*	63'	61'	591	57'	55"	531	51'	49'	47*	451	431	41*	391	37'	35"	331	31,	291	271	251	251	21'	19'	17'	15*
BAS	ξ	30'-11°	301-3°	291-7*	28'-11"	281-31	27'-7"	26'-11"	26'-5"	251-7"	24'-11"	24'-5"	25'-7"	22'-11"	22'-3"	21'-7"	20"-11"	20'-3"	19'-7"	18*-11*	18'-5"	17'-7"	16'-11"	16'-3"	15'-7"	14'-11"	14*-3*	15'-7"
A	MARK DIMENSION	1734 22'-3 5/8°	1735 201-341	1756 11'-3 1/8"	1728	1726 16'-3"	1729 17'-2 7/8"	1729 17'-2 7/8*	1752 16'-2 5/8*	1735 15'-2#"	1734 22*-5 5/8*	1738 21'-32"	1735 20'-54"	1739 19'-3 1/8"	1728 18'-5"	1729 17°-2 3/4°	1732 16'-2 5/8'	1733 15'-2‡*	1740 14'-2 3/8"	1719 26"-44"	1720 241-41	1721 22'-3 5/8"	1722 201-34"	1723 18'-3"	1724 16'-2 5/8".	1725 14'-2 3/8°	1726 12*-2*	1727 10*-1 5/
8	MARK DIMENSION	1746 201-341	1746	1747 19'-9±"	1748	1749	1750	1751 16'-0 3/4"	1752	1753 15'-8 5/8"																		
c	MARK DIMENSION	1767 20*-34*	1767 201-341	1758	1759 19'-3 1/8"	1756 18'-3"	1760	1757	1762	1763	1765 22'-3 5/8°	1766	1767 20'-34'	1759 19*-3 1/8*	1756 18'~3*	1761 17*~2 3/4*	1762 161-2 5/8	1764	1768 14'~2 1/8*									
E	MARK DIMENSION	1706 15'-5"	1706 151-5*	1707 15*-3*	1708 15*-1*	1709 14'-¢*	1710 14'-7"	1712 14'-3"	1713	1714 13'-11"	2 2 3,5	4.0	55 74	12 2 2 2 2		1. 2.74	10 2 370											
F	MARK DIMENSION	1691 22'-1"	1691 22'-1"	1692 21*-9*	1693 21'-5"	1694 20'-9"	1695 20'-5"	1698	1697 19'-5"	1699	1704 16*-1*	1705 15°-9°	1706 15'-5"	1708 151-14	1709 14'9*	1711 14'-5"	1715 14'-1"	1715 13'-9"	1716 13'-5"	!								
G	MARK DIMENSION	1677 29'-5"	1678 28'-9"	1679 28'-1"	1680 27'-5"	1681 26'-9"	1683 26'-1"	1684 25'-5"	1687 25'-9"	1688 24'-1"	1689 25'-5"	1690	1691 22'-1"	1693 21*-5*	1594 20 ~ 9*	1696 28*-1*	1697	1700	1701 18'-1"	1702 17'-5"	1703 16'-9*	1704	1706 15'-5"	1709 14'-9*	1713	1716 13'-54	1717 12* -9 *	1718 12*-1*
J	MARK DIMENSION	859 23'~4 3/8"	839 23'~4 3/8"	844 22°—30 3/4°	846 22'-5 1/8"	848 21'-6"	850 21'-0 3/8*	853 201-1 3/8*	854 191-7 7/8*	858 19'-2 3/8*									_									
к	MARK DIMENSION	817 27°-5 3/8°	822 27'-5"	824 261-10±	826 26'-4 1/8"	831 25'-3 3/8	833	838 25°-8±°	842 23'-2"	845 22'-7 5/8"	831 25'-3 3/8*	835 24'-3 3/4"	839 25'-4 5/8"	846 22'-5 1/8"	848 21'-6"	852 20'-6 7/8"	854 19'-7 7/8'	859 18'-9	860 17'-104"									
L	MARK DIMENSION	756 331-104"	778 32'-4 1/8"	789 31'-4"	796 30'-4"	803 291-9 5/8	810 28'-9 5/8	815 28'-34"	820 27'-3£"	827 26'-5 3/8"	804 291-6 3/4*	813 28'-5 7/8*	818 27'-5"	826 26'-4 1/8'	831 25'-5 3/8"	836 24'-2 5/8"	842 23'-2"	847 22'-1 3/8"	849 21'-0 7/8"	808 29'-14"	821 27*-2 1/8*	831 25'-3 3/8*	839 23'-4 3/8"	848 21'-6"	854 19'-7 7/8*	860 17'-104"	861 16'-1 3/8'	862 14*-54*
н	MARK DIMENSION	1025 30'-11 3/4"	1025 50'-11 3/4'	1027 30'-7 3/4"	1026 50'-3 7/8".	1028 29*-84*	1030 29'-4½"	1032 281-9 3/8*	1033 28'-5 7/8"	1035 28'-2 3/8"	1023 32°-4 1/8°	1024 321-7 3/4"	1025 50'-11 3/4	1026 30'-3 7/8°	1028 29'-84"	1031 29'-0 7/8"	1033 28'-5 7/8	1036 27'-11°	1037 27'-4 5/8"									
N	MARK DIMENSION	1023 52°-4 1/6°	1025 30°-11 3/4	1026 50'-3 7/8*	1028 29*-84*	1028 294-84*	1031 291-0 7/8	1031 29'~0 7/8"	1033 28'-5 7/8"	1036 27"-11"	1023 32*-4 1/8*	1024 31'-7 3/4"	1025 30'-11 3/4	1026 30'-3 7/8"	1028 29-84 *	1031 29'-0 7/8"	1033 28'-5 7/8'	1036 27'-11"	1037 27'-4 5/8"	1021 35'-3 1/8°	1022 33'-94"	1023 32*-4 1/6*	1025 30'-11 3/4"	1028 291-84	1033 28'-5 7/8"	1037 27'-4 5/8"	1038 26'-4 5/8*	1039 251-64"
LEVIS 160 Y	MARK DIMENSION	978 27'-5"	978 27°-5°	979 27'-3 7/8"	980 27°~2 7/8°	961 27'-0 .7/8	982 26'-11 7/8'	984 26'-10"	985 26'-9"	987 261–81										j								
2LEV1S	MARK DIMENSION	965 31' -41 "	965 31'-4½"	966 31'-1 7/8"	967 30'-114"	968 30'-6 1/8	969 30'-3 5/8"	971 29'-10 5/8"	973 291-8 1/8*	975 291-5 3/4"	976 27'-9 1/8"	977 27*-7*	978 27*-5*	980 271-2 7/8	981 27'-0 7/8*	983 26'-10 7/8"	985 26'-9"	986 251-74	988 26'-5"									

SHEET GENERAL NOTES
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									TO	MER HEIGHT G	FROUP CLAS	SIFICATION		
LINE	DESCRIPTION	STOCK NUMBER	MARK	DETAILED ON SHEET NO	SIZE (INCHES)	LENGTH		-STORY ' TO 79'		STORY TO 67'		-STORY ' TO 49'		STORY TO 31'
				G.E.F. 160	·		NUMBER	UNIT WEIGHT (POUNDS)	NUMBER	UNIT WEIGHT (POUNDS)	NUMBER	UNIT WEIGHT (POUNDS)	NUMBER	UNIT WEIGHT (POUNDS)
_1 _	CAP BEAM	48-2900.21-059	651	188	21 I 59	10'-3"	4	605	4	605	4	605	4	605
2	BEARING PLATE	47-7844.07-7	P6	188	PL 21 X 3/4	3'-4"	4	179	4	179	4	179	4	179
3	D1APHRAGIA	48-2900.12-065	Dl	188	12 I 65	1'-6"	4	98	4	98	4	98	4	98
4	RIVETS IN BEARING PLATE	43-6353.08		188	7/8	2'3/4"	32	.66	32	.66	32	.66	32.	.66
. 5	RIVETS IN WEB OF CAP	43-6353.08-25		188	7/8	2 1/2"	176	.62	176	.62	176	.62	176	.62
_6	LONGITUDINAL STRUT		653	188	10 I 42	25'-10"	10	1000	8	1000	6	1000	4	1000
_7	PIN PLATE	47-7844.04-1	P8	188	PL 9 x 3/8	0'-10*	40	10	32	10	24	10	16	10
. 8	PIN PLATE	47-7844.04-1	ρ5	190	PL 9 X 3/8	0'-10"	32	10	24	10	16	10	8	10
9	COLUMN BASE PLATE	47-7844. 1-5	Р4	189. 190	PL 24 X 1	2'-0"	ц	153	4	163	4	163	4	163
10	STIFFENERS	47-7844-04-14	P9.10.11	189	PL 6 X 3/8	1'-114"	4	15	4	15	4	15		
11	STIFFENERS	47-7844.04-14	P12.13.14	190	PL 6 X 3/8	1'-112"				•		•	4	15
12	BRACING CONNECTOR	48-2900.12-065	Cl	189.190	12 I 65	1'-1 1/4"	20	46	16	46	12	45	8	46
13	DO DO	47-7844.05-22	P3	189	PL 4 X 1/2	1'-0"	12	7	8	7	ш	7	ľ	- 40
.14	WEB SPLICE	47-7844.05-22	Pl	189	PL 10 X 1/2	3'-0 1/2"	24	52	16	52	8	52		
15	FLANGE SPLICE	47-7844.05-22	P2	189	PL 12 X 1/2	3'-6 1/2"	24	72	16	72	8	72		
16	RIVETS, WEB SPLICE	43-6353.08-3		189	7/8	3"	288	.70	192	.70	96	,70		
	RIVETS, FLANGE SPLICE	45-6353.08		189	7/8	2 3/4"	672	.66	448	.66	224	.66		
	PIN	., ., ., ., ., ., ., ., ., ., ., ., ., .	654	188	1 1/2	1'-4 1/2"	20	8	16	8	12	8	8	8
	PIN		655	188	2	1'-5 1/2"	20	16	16	16	12	16	8	16
	COTTER PIN		4,7,7	188	1/4 X 2 1/2	1) 1/2	40	.1	32	- 1	24	.1	16	.1
	COTTER PIN			188	3/8 × 3		40	.25	32	.25	24	.25	16	.25
	PIPE SPACER	44-6246.7-02	656	188	4	0'-6 1/8"	20	5.5	16	5.5	12	5, 5	8	5.5
	PIPE SPACER	44-6246.7-04	657	188	2	0'-6 5/8"	20	2	16	2	12	2	8	2
	HASHER	44 6246.7 V4	658	188	3 3/4 X 1 9/16 HOLE	33/4	72	1.24	64	1.24	56	1. 24	48	1.24
	WASHER		659	188	4 3/4 X 2 1/16 HOLE	43/4	88	1.97	80	1.97	72	1.97	64	1.97
	LOOP ROO, LONGITUDINAL, UPSET		0,55	188	1 1/8 =	4:-71	64	26	48	26	32	26	16	26
		46-6375.5-13			1 1/4 \$				96	4.5	64	4.5	32	4.5
12	SPLICE ROO	40-0373.3-13		188		J1-J*	128	4.5	1					
	UTURNBUCKLE ULOOP ROD TRANSVERSE, UPSET		677	_188 191	1 5/8 3/4 tr	4'-7#	32	5.9	24 48	5.9	16 32	5.9	8 16	5,9 11
		**********	ĺ				64	- 11	1	11		11		
	SPLICE ROD TURNBUCKLE	46-6375.5-07	678	191	3/4 %	1'-1"	128 52	1.6 2.7	96 24	2.7	16	2.7	32 8	1.6 2.7
	CLEVIS ROO, HORIZONTAL, UPSET		400						T		2	4.3	3	
	DO 00		680	191	3/4 0	11 <u>-7*</u>	6	4.3	4	4.3	2	3.7		
~~	SPLICE ROO	46-6375.5-07	678	191	3/4 ^{CI}	X_;; 3# 1'=1"	6 24	3.7	16	3.7	8	1.6		
	TURNBUCKLE	40 O)19.5-U1	070	191	1 1/8	6n 11-		1.6	4	2.7	2	2.7		
	ICLEVIS			191	IAO. 3 FOR 14 THR	5*	6	2.7	8	4.0	4	4.0	 	
-	PIN HEADED, CLEVIS,			191	1 15 P		12	4.0	8	1.5	4	1.5	 	
,							12	1.5	1		<u>u</u>	.1		
38	OTTER PIN		I	191	1/4 × 2 1/2		12	1.	8	-1	4	. (

STEEL TOWERS, STEEL SPANS

U CONNECTOR PIN ASSEMBLY, 15"

³⁾ CONNECTOR PIN ASSEMBLY, 2"
3) LOOP ROD ASSEMBLY, 1%"
3) LOOP ROD ASSEMBLY, 34"

⁵⁾ CLEVIS ROD ASSEMBLY, 34"

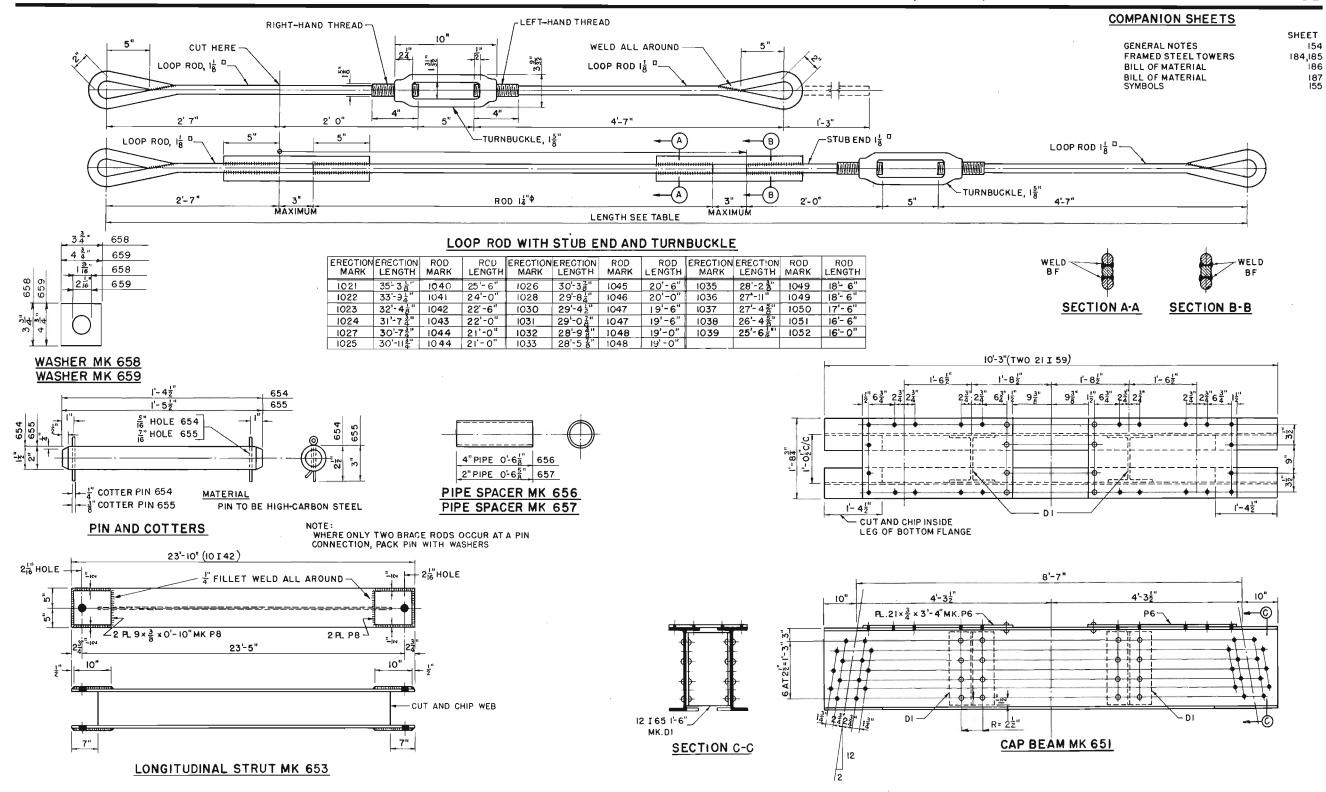
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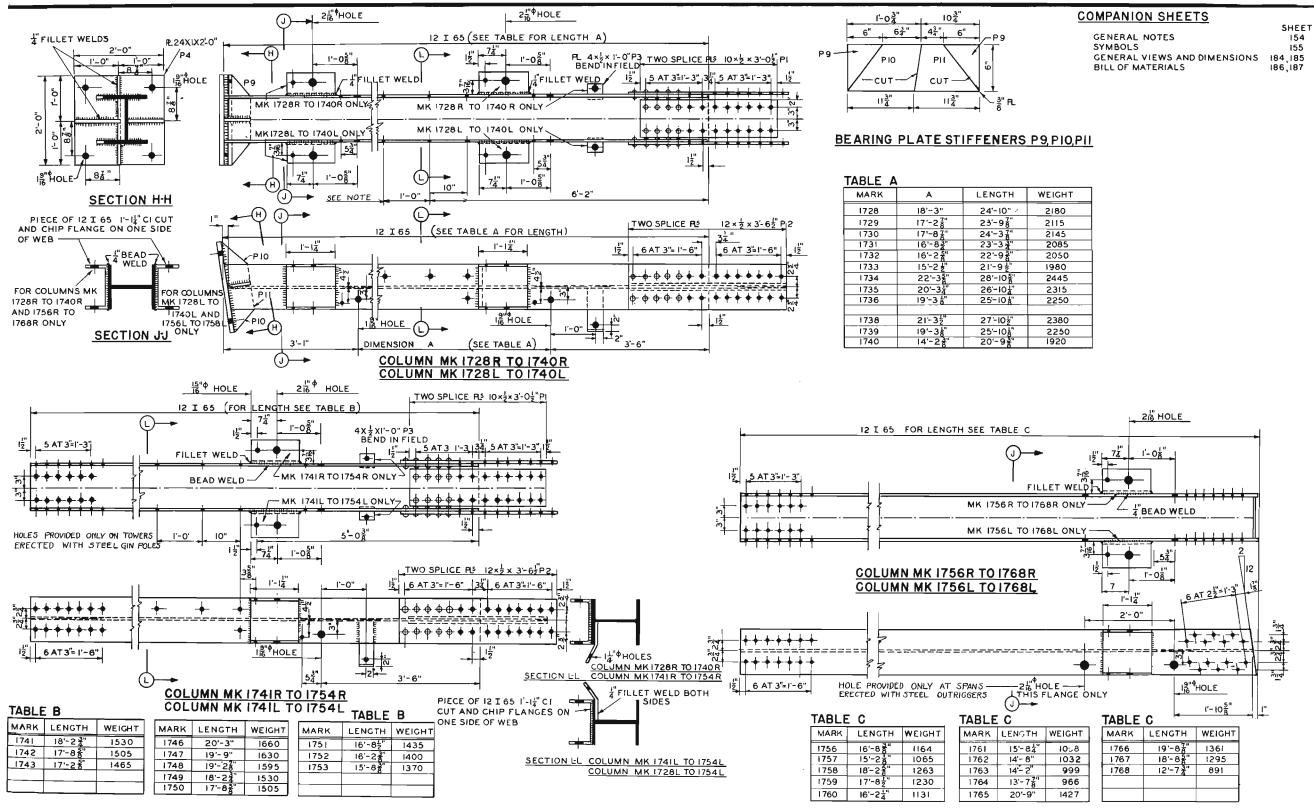
TABLE A - BILL OF MATERIALS FOR	PIŁCES				MER HEIGHTS													
		DETAILED IN SHEET	QUANTITY	MARK	REQUISITIONSD LENGTH	UNIT WEIGHT (POUNDS)	MARK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS)	MARK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS)	HASK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS)	MARK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS
DESCRIPTION	LINE	TOM	R HEIGHT		ית			75'			73'			711			198	
	_ 1		2	1729R	241-10"	1615	1730R	241-3 7/8*	1.580	1729k	231-9 7/84	1550	17316	231-3 3/4"	1615	1732R	221-9 5/8	1460
TOWER COLUMNS	2		2	17281	241-10"	1615	1730L	241-3 7/8"	1580	1729L	231-0 7/6	1550	1731L	231-3 3/4"	1515	1732L	221-9 5/8*	1490
12 I 66 STCCK NO 48-2900.12-065	3		- 4	1741R	181-2 3/4"	1185	17428	17'-8 5/8"	1150	1743R	171-2 5/8	1120	1751R	16'-8 1/2"	1090	1752R	161-2 3/8"	1050
	- 4	189	4	1741L	18'-2 3/4"	1185	17421	17'-8 5/8"	1150	1743L	17'-2 5/8"	1120	17511	16'-8 1/2"	1090	1752L	161-2 3/8"	1050
	5		2	1756R	16'-8 3/8"	1085	1760R	161-2 1/4"	1050	17616	151-8 1/4"	1020	1757R	15'-2 1/8"	985	1762R	141-8"	955
	6	+	2	1756L	16'-8 3/8"	1085	1760L	16'-2 1/4"	1050	1761L	15'-8 1/4"	1050	1757L	15'-2 1/6"	985	1762L	141-8"	955
TRANSVERSE STRUTS	7	-	2	1709	151-2*	637	1710	151-0"	630	1711	14'-10"	624	1712	141-8"	616	1713	141-6"	610
10 I 42	В	190	2	1694	211-2"	887	1695	201-10	875	1696	201-6"	861	1698	201-24	845	1697	191-10 ⁿ	634
STOCK NO	-9-	1	2	1681	271-2"	1140	1771_	261-8"	1120	1665	26'-2"	1100	1686	251-8"	1060	1687	251-2"	1060
	10		2	1674	331-2"	1390	1675	321-6"	1365	1676	31'-10"	1340	1769	311-2"	1310	1770	30"-6"	1280
TRANSVERSE RODS	ш		8	905	111-6*	17	907	111-0*	17	907	11'-0"	17	908	101-6"	16	909	10'-0"	15
3/4 Ø ROOS	12_	191	8	699	151-6"	23	900	151-0#	23	901	141-6"	22	902	141-0*	21	903	131-6"	20
STOCK NO 46-6375.5-07	13		8	690	201-0"	30	891	191-6"	29	893	181-6*	28	894	181-0#	27	895	171-6*	26
	14.	_	8	880	25'-0"	38	682	24'-0"	36	883	231-6"	35	985	221-6	34	885	221-0"	33
LONGITUDINAL RODS	_15	169	24	1046	201-0"	83	1047	191-6"	81	1047	191-6"	81	1048	191-0*	79	1048	191-0	79
1 1/4 Ø KODS STOCK NO 46-6375.0-13	16	-	- 8	1046	201-0	83	1047	16'-6"	81	1047	191-6*	81	1048	191-0"	79	1048	191-0"	79
HORIZONTAL RODS 3/4 Ø RODS	17		2	1017	231-0*	35	1017	23'-0"	35	1018	221-6"	34	1018	221-6"	34	1018	221-6"	34
STOCK NO 46-6375.5-07	18	191	2	1013	261-6"	40	1014	261-0*	39	1014	23"-0"	39	1015	25'-6"	38	1015	251-6"	36
	19		2	1007	301-6"	46	1006	30°-0*	45	1008	301-0"	45	1009	29'-6"	1414	1010	291-0"	44

STOCK NO 46-6375.5-07	18.	191	2	1013	26"-6"	40	1014	26'-0"	39	1014	231-0"	39	1015	25'-6"	38	1015	251-6	36												
	19		2	1007	301-6"	46	1006	30°-0*	45	1008	301-0"	45	1009	29'-6"		1010	291-0ª	44	MARK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS)	MARK	KEQUISTTIONED LENGTH	UNIT WEIGHT (POUNCS)	MARK	REQUISITIONED LENGTH	UNIT WEIGHT (POUNDS)	MARK	REQUISITIONED LENGTH	UNI WEIG (POUN
9.5		TOWER	HEIGHT		671			651			631			611			591			571			55'			531			511	
	_20		2	1734R	26'-10 5/8"	1880	1735R	261-10 1/4"	1750	1736R	25'-10 1/8"	1680	17286	241-10*	1620	1728R	241-10"	1620	1729R	23'-9 7/8"	1550	1729R	231-9 7/8"	1550	1732R	221-9 5/8*	1480	1733R	21'-9 1/2*	1415
TOHER OCLUMNS	21		2	1734L	26"-10 5/6"	1680	1735L	281-10 1/4"	1750	1736L	25'-10 1/8"	1680	1728L	241-10"	1620	17281	241-10"	1620	17291	23'-9 7/8"	1550	1729L	231-9 7/8*	1550	1732L	221-9 5/8"	1480	1733L	21'-9 1/2"	141
TOHER OCLUMNS 12 I 65 STOCK NO 46-2900.12-065	22		2	1748R	201-3"	1320	1746R	20'-3"	1320	1747R	191-9*	1285	1748R	191-2 7/8"	1250	1749R	18'-2 3/4"	1190	1750R	171-8 5/8*	1150	1751R	161-8 1/2"	1085	1752R	161-2 3/8"	1050	17538	151-8 3/8*	1020
310CK NO 40-2800.12-003	23	189	2	1746L	201-3"	1320	1746L	201-3"	1320	1747L	191-9*	1285	1748L	191-2 7/8"	1250	17491	18'-2 3/4"	1190	1750L	171-8 5/8"	1150	1751L	16'-8 1/2"	1085	1752L	161-2 3/8"	1050	17531	151-8 3/8"	1020
	24		2	1767R	181-8 5/8"	1220	1767R	181-8 5/8*	1220	1758R	18'-2 5/8"	1185	1759R	171-8 1/2"	1150	1.756R	161-8 3/8"	1085	1.760R	161-2 1/4*	1050	1757R	151-2 1/8"	990	1762R	141-8"	955	1763R	141-2*	820
	25		2	1767L	161-8 5/8"	1220	1767L	18'-8 5/8"	1220	1758L	181-2 5/8"	1185	1759L	17'-8 1/2"	1150	1756L	161-8 3/8*	1085	1760L	161-2 1/4"	1050	1757L	151-2 1/8*	990	1762L	141-8"	955	. 1763L	141-2*	820
TRANSVERSE STRUTS	26		2	1706	15'-10"	665	1706	151-10"	665	1707	15'-8"	660	1708	15!-6"	650	1709	151-2*	635	1710	151-0*	630	1712	141-8*	615	1713	141-6"	018	1714] 14 t = 14 M	60
10 I 42	27	190	2	1691	221-6*	945	1691	221-6"	945	1692	221-2"	930	1693	511-10m	920	1694	211-2"	885	1695	201-10"	875	1698	201-2*	845	1697	19'-10"	835	1699	191-6*	82
STOCK NO	28	50	2	1677	291-10"	1255	1678	291-2"	1220	1679	281-6"	1200	1680	27'-10"	1170	1681	27'-2"	1140	1683	261-6"	1115	1884	25'-10"	1085	1687	251-2"	1060	1638	241-6"	1030
TRANSVERSE RODS	29		8	903	131-6"	20	903	131-6"	20	904	131-0"	_20	905	121-6"	19	906	U'-6"	1.7	907	11'-0"	17	908	101-6"	16	909	101-0*	15	910	9'-6"	14
3/4 Ø ROD STOCK NO 46-6375.5-07	30	191	8.	895	171-6"	26	895	17'-6"	26	896	171-0"	26	897	16'-6"	25	899	151-6"	23	900	15'-0"	23	902	141-0"	21	903	131-8"	20	904	131-0"	20
310CK NO 40-03/3.5-0/	31		8	882	241-0"	36	885	221-6"	34	881	21'-6"	32	889	201-0"	31	890	201-0"	30	892	19"-0"	29	893	18'-6"	28	895	171-6"	26	897	161-6"	25
LONGITUDINAL RODS	32	188	16	1044	21'-0"	88	1044	21'-0"	96	1044	211-0"	68	1045	20'-6"	86	1046	201-0*	83	1047	191-6"	81	1048	181-0=	79	1048	191-0"	79	1049	181-6*	77
STOCK NO 48-6375.5-13	33		8	1042	221-6"	94	1044	21'-0"	88	1045	201-6"	86	1048	201-0#	83	1046	201-0"	83	1047	19'-6"	81	1047	191-6"	81	1048	191-0ª	79	1049	181-6"	77
HORIZONTAL ROOS	34	191	2	1017	231-0"	35	1017	231-0"		1017	23'-0"	35	1017	231-0"	35	1017	23'-0"	35	1017	231-0*	35	1018	221-6*	34	1018	221-6"	34	1018	221-6"	34
3/4 Ø ROD STOCK NO 46-6375.5-07	35		2	1012	27'-0"	41	1012	27'-0"	41	1012	27'-0"	41	1112	27'-0"	41	1013	26'-6"	40	1014	26°-0"	39	1015	251-6"	38	1015	251-6"	38	1015	251-6"	36

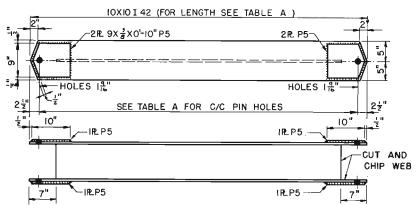
		TOWEL	HEIGHT		491			471			451			431			411			391			371			35'			331	
Y0.550 00.1500	_36_	189	2	17346	28'-10 5/8"	1880	1738R	27'-10 1/2"	1815	1735R	261-10 1/4"	1750	1739R	251-10 1/8"	1680	1728R	241-10*	1615	1729R	231-9 7/8"	1550	1732R	221-9 5/8"	1480	1733R	21'-9 1/2"	1415	17406	201-9-3/8*	1350
TOWER COLUMNS 12 I 65	37		2	1734L	281-10 5/8	1880	1738L	271-10 1/2*	1815	1735L	26'-10 1/4"	1750	1/39L	25'-10 1/8"	1680	1728L	241-10"	1615	1729L	23'-9 7/8"	1550	1732L	221-9 5/8*	1480	1733L	211-9 1/2*	1415	1740L	201-9 3/8*	_ 1350
STOCK NO 46-2900.12-065	38		2	1765R	20'-9"	1350	1766R	191-8 7/8"	1285	1767R	18'-8 5/8"	1220	1759R	17'-8 1/2"	1150	17568	161-8 3/8"	1090	1761R	151-8 1/4"	1020	1762R	141-8"	955	1764R	13'-7 7/8"	89C	17668	121-7 3/4"	825
	39		2	1765L	20!-9"	1350	1766L	191-8 7/8"	1285	1767L	18'-8 5/6"	1220	1759L	171-8 1/2*	1150	1756L	161-8 3/8"	1090	17611	151-8 1/4"	1020	1762L	14'-8"	935	1764L	13'-7 7/8*	890	1788L	12'-7 3/4"	825
TRANSVERSE STRUTS	40	190	2	1704	161-67	695	1705	161-2"	660	1706	15"-10"	665	1708	151-6"	650	1709	15'-2"	635	1711	141-10s	625	1713	141-6*	610	1715	141-2*	595	1716	131-10"	560
STOCK NO TRANSVERSE RODS	. 41.		2	1689	23'- 0"	1000	1690	231-2"	976	1691	221-6"	945	1693	211-10=	920	1694	211-2"	890	1696	201-6*	860	1697	191-10"	830	1700	191-2"	805	1701	181-6*	775
TRANSVERSE RODS	42	191	8	899	15"-6"	23	901	141-6"	22	903	131-6"	20	905	121-6*	19	906	11'-6"	17	907	111-0"	17	909	101-Q"	15	911	91-0"	14	912	8'-0"	12
3/4 \$ 600 STOCK NO 46-8375, 5-07	43		8	991	191-6"	29	893	18'-6"	28	895	171-6*	26	897	161-6"	25	899	15!-6*	23	901	14'-6"	22	903	13'-6"	20	906	12'-6"	19	906	111-6"	17
LONGITUDINAL ROOS	ith.	188	8	1042	22'-6"	94	1043	221-0"	92	1044	21'-0"	88	1045	201-6*	85	1046	201-0"	63	1047	19'-6"	81	1048	191-0"	79	1049	181-6"	77	1050	17'-6"	73
1 1/4 Ø ROD STOCK NO 48-6375.5-13	45		8	1042	22'-6"	94	1043	22'-0"	92	1044	21'-0"	88	1045	201-6*	85	1046	201-0"	83	1047	191-6"	18	1048	19'-0"	79	1049		77	1050	17'-6"	73
HORIZONTAL ROGS																														
3/4 Ø RODS STOCK NO. 46-6375.5-07	46	191	2	1016	231-6*	35	1016	23!-6"	35	1017	23'-0"	35	1017	231-0*	35	1017	231-0"	35	1018	221-6*	34	1016	221-6"	34	1018	221-6"	34	1018	22'-5"	34

		TOWER HE	EIGHTS		311			291			27'			251			231			211	7		191			17'			151	
TOWER COLUMNS	. 47	190	2	1719R	3 1-4 7/8"	2040	1720R	29'-4 5/8"	1910	1721R	271-4 1/4"	1780	1722R	251-3 7/8"	1650	1723R	23'-3 5/8"	1515	1724k	211-3 1/4"	1395	1725R	191-3"	1250	1726R	17'-2 5/8"	1120	1727R	15'-2 1/4"	985
STOCK NO 46-2900.12-065	48		1 2	17191	311-4 7/8"	2040	1720L	291-4.5/8"	1910	1721L	271-4 1/4"	1780	1722L	251-3 7/8"	1650	1723L	231-3 5/8"	1515	1724L	211-3 1/4"	1385	1725L	S1-3#	1250	17261	1/1-2 5/8"	1120	17271	15'-2 1/4"	985
TOWER COLUMNS 12 1 65 STOCK NO 46-2900.12-065 TRANSVERSE STRUTS 10 1 42 STOCK NO TRANSVERSE RODS 3/4 Ø ROD	49		2	1702	17'-10"	750	1703	17'-2"	720	1704	16*-6"	695	1706	15'-10"	685	1709	151-2*	635	1/13	14"-6"	610	1716	131-10*	580	1717	131-2*	555	1718	121-6"	525
21U.K NU 40+0345.5-07	50	191	8	891	19'-6"	29	895	17'-6"	26	899	151-6*	23	903	131-6"	20	906	111-6*	17	909	10"-0"	15	912	81-0"	12	913	61-6"	10	914	41-6*	7
LONGITUDINAL ROOS 1-1/4 Ø ROD SIOCK NO. 46-6375.5-13	51	188	8	1C40	251-6"	106	1041	241-0*	100	1042	221-6"	94	1044	211-0"	88	1046	201-0"	63	10118	191-C"	79	1050	171-6".	73	1051	161-6*	69	1052	16"-O"	67





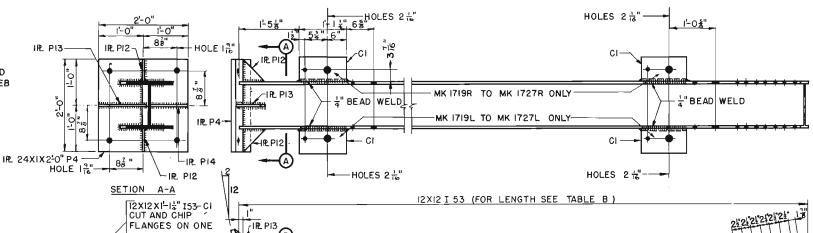
SHEET GENERAL NOTES 154 SYMBOLS 155 GENERAL VIEWS AND DIMENSIONS 184,185 BILL OF MATERIALS 186, 187



STRUTS MK 1674 TO 1681, INCLUSIVE STRUTS MK 1683 TO 1718, INCLUSIVE STRUTS MK 1769 TO 1771, INCLUSIVE

ALL WELDS SHOWN ARE TO BE 4" FILLET WELDS UNLESS OTHERWISE INDICATED

냨" BEAD WELD-



— HÖLES ાર્રું"

A (FOR LENGTH SEE TABLE 6) COLUMNS MK 1719R TO 1727R INCLUSIVE

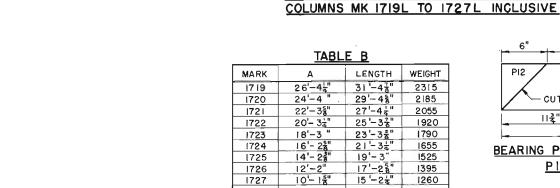
TARIF A

	IABL	<u>e a</u>	
MARK	G/G PIN HOLES		WEIGHT
1674	32'- 9"	33'-2"	1430
1675	32'- 1"	32'- 6"	1402
1676	31'-5"	31'-10"	1374
1677	29'- 5"	29'-10 "	1290
1678	28'-9"	29'-2"	1262
1679	28' 1"	28'6"	1234
1680	27'—5"	27'-10"	1206
1681	26' 9"	27'-2" 26'-6"	1178
1683	26'— I"	26'-6" 25'-10"	1150
1684	25'- 5"	25'-10"	1122
1685	25'-9"	26'- 2"	1136
1686	25'- 3"	25'- 8"	1115
1687	24' 9"	25'- 2"	1095
1688	24'- 1"	24'-6"	1066
1689_	23'5"	23'-10"	1038
1690	22'- 9"	23'- 2"	1010
1691	22'- 1"	22'- 6"	982
1692	21'-9"	22'- 2"	968
1693	21'-5"	01110"	954
1694	20'-9"	21 - 10	926
1695	20'-5"	20'-10"	912
1696	20' "	20'- 6"	898
1697	19'- 5"	19'-10" 20'-2"	870
1698	19'— 9"	20'- 2"	884

TABLE A

STEEL TOWERS, STEEL SPANS

MARK	C/C PIN HOLES	LENGTH	WEIGHT
1699	19'-1"	19'- 6"	856
1700	18'-9"	19'- 2"	842
1701	18'-1"	18'-6"	814
17 02	17 '- 5 "	17'-10"	786
1703	16'-9"	17'-2"	758
1704	16'-1"	_16'6"	730
1705	15'-9"	16'-2"	716
1706	15'-5"	15'-10"	702
1707	15'-3"	15'-8"	694
1708	15 '— 1 "	15'6"	688
1709	14'-9"	15'- 2"	674
1710	14"-7"	15'- 0"	667
1711	14'-5"	14'-10 "	660
1712_	14'-3"	14'- 8"	653
1713	14' 1"	14' 6"	646
1714	13'-11"	14'-4"	639
17 15	13' 9"	14'-2"	632
1716	13'-5"	13'-10"	618
1717	12'-9"	13'-2"	590
1718	12'-1"	12'-6"	562
1769	30'-9"	31'-2"	1346
1770	30'— I"	30'- 6"	1318
1771	26'-3"	26'- 8"	1157

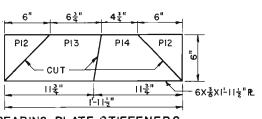


rIRL PI3

└IR_PI4 3'-1"

SIDE OF WEB

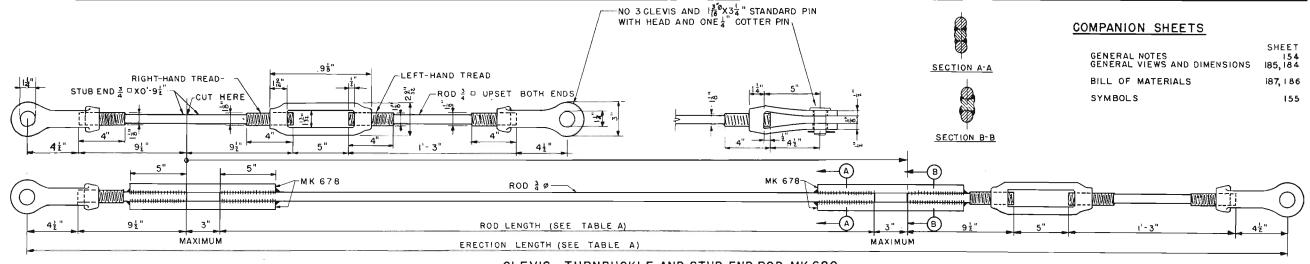
SECTION B-B



-HOLES 1큐"

1-115"

BEARING PLATE STIFFENERS P12, P13, P14,



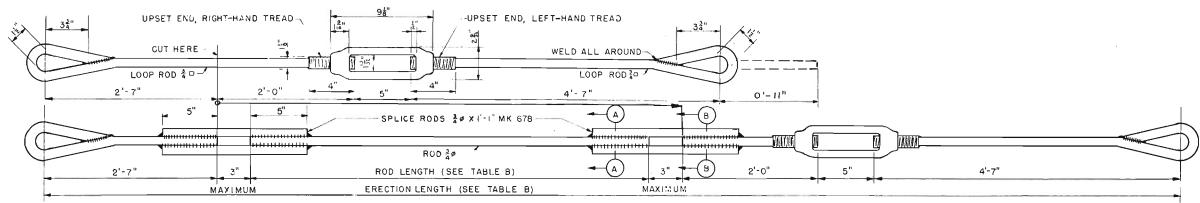
RIVETED AND WELDED CONSTRUCTION, FABRICATION OF ROD BRACING

CLEVIS, TURNBUCKLE, AND STUB-END ROD MK 680

TABLE A

RAILWAY E-45

	-																						
ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	`ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH		ROD LENGTH
955	34-73 "	1007	30'- 6"	965	31- 42"	1012	27-0"	970	_30'- IB	1014	26'-0"	977	27-7"	1016	23'-6"	982	26'-117"	1017	23-0"	987	26-8"	1018	22-6"
959	34-31	1008	30'- 0"	966	31'- 1 ₈ 7"	1012	27'-0"	97i	29'- 10}	1015	25-6"	978	27-5"	1017	23'-0"	983	26'-107"	1018	22'-6"	988	26-5"	1018	22-6"
960	33'-1'1"	1008	30'-0"	967	30-114"	1012	27-0"	973	29-8B	1015	25'-6"	979	27'- 37"	1017	23-0"	984	26'-97"	1018	22-6"				
963	33-65	1009	29'-6"	968	30-68 "	1013	26'-6"	975	29-53	1015	25-6"	980	27'- 28 ⁷	1017	23-0"	985	26'-9"	1018	22'-6"				
964	33'-2 ³ "	1010	29'-0"	969	30'-3 1 "	1014	26-0"	976	27'-9¦	1016	23-6"	981	27'-078"	1017	23'-0"	986	26'-7"	1018	22'-6"				



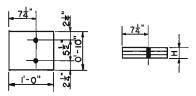
LOOP ROD WITH TURNBUCKLE MK 677

TABLE B

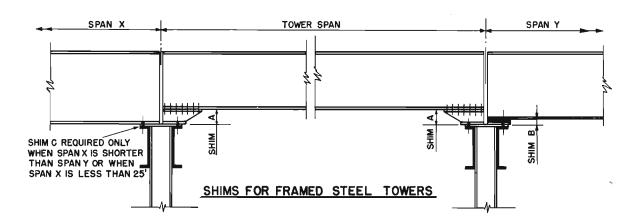
	-															11			
ERECTION MARK	ERECTION LENGTH	ROD MARK	.ROD LENGTH	.ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH	ERECTION MARK	ERECTION LENGTH	ROD MARK	ROD LENGTH
743	34'- 94"	880	25'-0"	804	29'- 6 3"	168	19'-6"	820	27'- 3 ⁱⁿ	8 9 5	17'- 6"	838	23'- 84"	902	14'-0"	852	20'-67"	907	11'-0"
752	34' - 0분"	882	24'-0"	80 7	29' - 2 "	891	19'-6"	821	27' - 28"	895	17'-6"	839	23' - 4췽"	903	13'-6"	853	20'- ਭੂੰ"	908	10'- 6"
756	33' - 104"	882	2 4'- 0"	808	29'-14"	891	19'-6"	822	27' - 5"	895	17'-6"	842	23'- 2"	903	13'-6"	854	19'-72"	909	10'-0"
765	33'- 35"	883	23'-6"	810	28'-9종"	892	19'-0"	824	26'-101"	896	17'-0"	844	22' - 103"	904	13'-0"	858	19'-23"	910	9'- 6"
775	32'-6"	885	22'-6"	812	28'-6謲"	893	;8'-6"	826	26' - 4 ¹ 6'	897	16'-6"	8 4 5	22' - 78"	904	13'-0"	859	18'-9"	116	9'- 0"
778	32'- 4洁"	885	2 2' - 6"	813	28'-5분	893	18'-6"	827	26'- 3흫"	897	16,-6,	846	22'- 5 1 "	905	12'-6"	860	17'-104"	912	8'- 0"
785	31'-87"	886	2 2'- 0"	815	28'-34"	893	18'-6"	831	25'- 3월"	899	15'-6"	847	22'- 1충''	905	12'-6"	861	16' 1출"	913	6-6"
789	31'-4"	8 8 i	21'- 6"	816	27'-108"	894	18'-0"	833	24'- 9"	900	15'-0"	848	21'-6"	906	' 1' - 6"	862	14-54	914	4-6"
796	30' - 4"	889	20,-6,	817	27'-5%"	895	17'- 6"	835	24'- 34"	901	14'-6"	849	21' - 08"	906	11' - 6"				
803	29'-95"	890	2 0' -0"	818	27' - 5"	895	17'-6"	836	24'-25	901	14'-6"	850	21 '- 08"	907	11, - 6,				



SHEET



DETAIL OF PLATE SHIM



PROVIDE 2 ANCHOR BOLTS & X4*
PER STRINGER WHEN SHIMS ARE
NOT REQUIRED

			FOR FRA			r				
5	PAN	X	50 '	45'	40'	35'	30 '	25'	201	15'
		A	7549	7549	7551	7549	7548	1		
	13	8	7555	7555	7556	7555	7554	7552	7552	7552
		С							7547	7552
	+	Α	7549	7549	7551	7549	7548			
	20	8	7552	7552	7553	7552	7550	7547	7547	7547
		С							7547	7552
	-	Α	7549	7549	7551	7549	7548			
	25	В	7549	7549	7551	7549	7548			
		O							7547	7552
		А	7549	7549	7551	7549	7548	7548	7548	7548
	30	В	7546	7546	7548	7546				
		C						7548	7550	7554
>	,	А	7549	7549	7551	7549	7549	7549	7549	7549
SPAN	35	В			7545	4				
g,		С					7546	7549	7552	7555
		Α	7551	7551	7551	7551	7551	7551	7551	7551
	40 4	В								
		С	7545	7545		7545	7548	7551	7553	7556
	-	А	7549	7549	7551	7549	7549	7549	7549	7549
	\$	В			7545					
		C					7546	7549	7552	7555
		Α	7549	7549	7551	7549	7549	7549	7549	7549
	8	В			7545					
	- 1	С					7546	7549	7552	7555

FLANGE FOR SHIM CONNECTION AS REQUIRED SIFILLET WELD BF CUT FROM 2I 159 CUT FROM 2I 159 ELEVATION END VIEW SECTION A-A

DETAIL OF BUILT-UP SHIM

BILL OF MATERIALS FOR ONE BUILT-UP SHIM

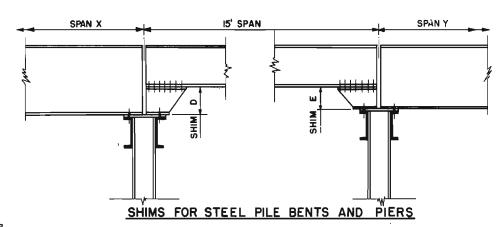
DESCRIPTION	STOCK NO	SIZE (INCHES)	LENGTH	QUANTITY
BEAM	48-2900.21-059	21 I 59	1'-9"	1
PLATE	47-7864.07	10 x 3/4	1'-0"	1
RIVET .	45-6353.08	7/8	2-3/4"	14
ANCHOR BOLT	43-2219.08-04	7/8	4 •	2
ELECTRODE	46-3772.2-7	3/16		1 LB

	SHEET
GENERAL NOTES	154
SYMBOLS	155
STEEL PILE BENTS AND	
PIERS, RIVETED	204, 205, 206
STEEL PILE BENTS AND	
PIERS, WELDED	209, 210, 211
FRAMED STEEL TOWERS	184,185

COMPANION SHEETS

MA	RKS	AND	DIMENSIONS	FOR	8U1LT-UP	SHIMS
		_		_	TOTAL	\neg

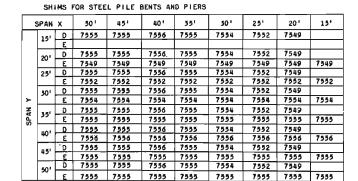
•	AND DIVIEN	STORS FOR E	JUILI OF 3
	MARK	н	(PEUNES)
	7549	5-7/8*	62
	7550	6-1/4"	63
	7551	6-1/2*	64
	7552	8-7/8"	67
	7553	9-1/2*	68
	7554	12-1/0"	73
	7555	14-7/8*	77
	7556	15-3/8"	78



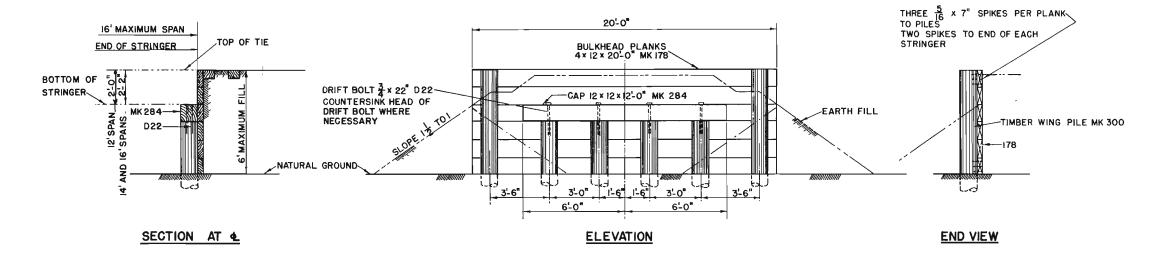
BILL OF MATERIALS FOR ANCHOR BOLTS ONLY WITHOUT SHIMS

DESCRIPTION	SSTOCK NO	SIZE (INCHES)	Lengteh	WEIGHT EACH (POUNDS)
ANCHOR BOLT	43-2219.08-04	7/8	01-411	1.2

TWO BOLTS REQUIRED FOR EACH STRINGER SUPPORT CONSTRUCTION INDICATED BY BLANK SPACES IN TABLES FOR SHIMS



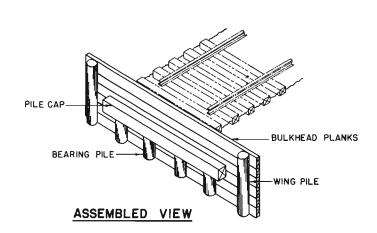
COMPANION SHEETS SHEET TIMBER ABUTMENT FOR TIMBER SPAN 194 GENERAL NOTES 154 SYMBOLS 155



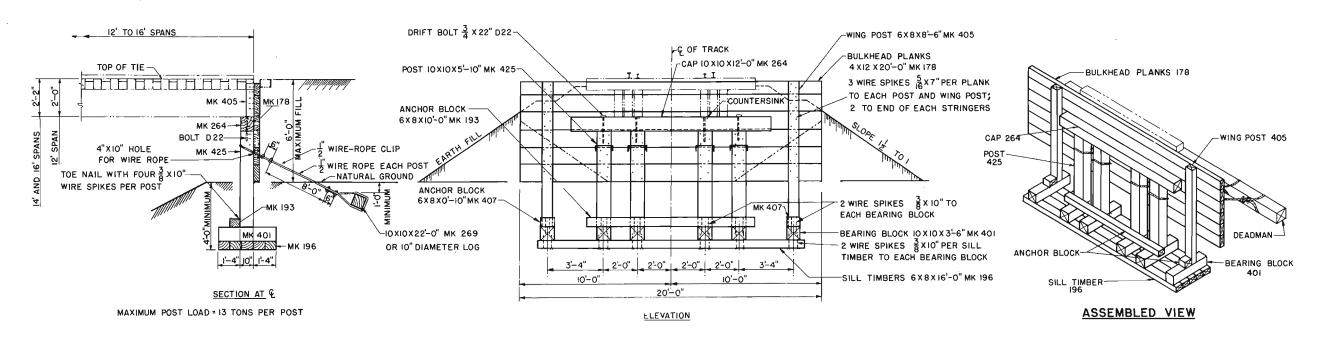
MAXIMUM PILE LOAD

SPAN LENGTH	12'	14'	16'
TONS PER PILE	13	13	13

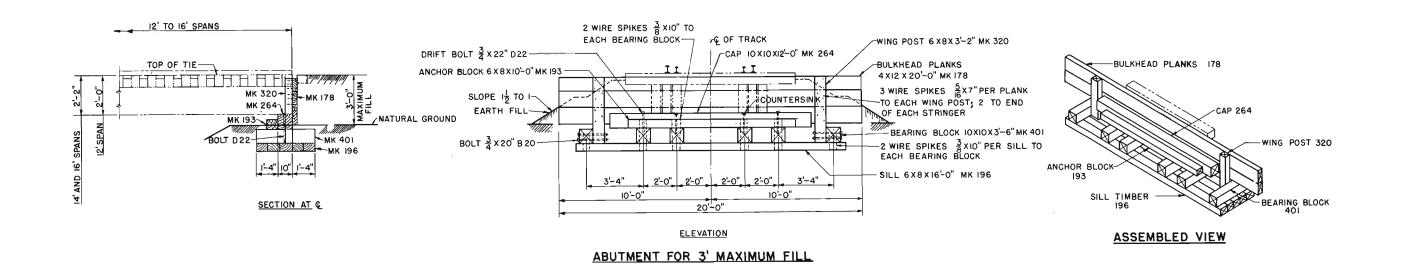
	BILL OF MATERIALS FOR ONE ABU			SIZE (INCHES)	LENGTH	UNIT		TIMBER	PILE			TIME	ER POST		
LINE	DESCRIPTION	STOCK NO	MARK			(POUNDS)	6' MAXIMUM FILL		3' MAXIMUM FILL		6' MAXIMUM FILL		3' MAXII	MUM FILL	
							QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	YTITMAUÇ	FBM	LINE
1	1 BULKHEAD PLANK	39-3340.12-2	178	4X12	20'-0"	300	6	480	5	400	6	480	2	160	1
2	CAP	39-6630.12-12	284	12×12	12'-0"	540	1 1	144	1	144					2
3	DQ	39-6620.1-12	264	10×10	12'-0"	375					1	100	1	100	3
4	PILE, WING		300		15'-0"		2		2						4
5_	2 POST, WING	39-3360.08	405	6×8	8'-6"	128					2	. 68			5
_ 6	po	39-3360.08	320	6X8	3'-2"	47							2	25	6
_7	J PILE, BEARING						4		ų						7
8	2 POST BEARING	39-6620.1	425	10×10	5'-10"	179					ц	194			8
ģ	SILL	39-3360.08-16	196	6XB	16'-0"	240					5	320	5	320	9
10	BEARING BLOCK	39-6620.1	401	10×10	31-61	109					6	175	6	175	10
11	DEADMAN	39-6620.1-22	269	10X10	22'-0*	687					1	183			11
12	ANCHOR BLOCK	39-3360.08	193	6X8	10'-0"	150					1	40	1	40	12
13		39-3360.08	407	6X8	0'-10"	13					2	7			13
14	WIRE ROPE	22-3460.4-05		1/2	20'-0"	13	_				- 6				14
15	WIRE-ROPE CLIP	42-3544.5-05		1/2							24				15
16	BOLT WITH NUT AND THO WASHERS	43-2325.07-2	820	3/4	20 *								4		16
17	DRIFT BOLT	43-6316.07-22	022	3/4	22*		4		4		4		4		17
18	WIRE SPIKE	42-8488.04-1		3/8	10 -	,33					96		68		18
19	DO	42-8488.035-07		5/16	7.	. 15	108		90		108		36		19
<u> 1</u>	NUMBER OF BULKHEAD PLANKS B	ILLED IS FOR MAXIM	UM FILL	. USE F	EWER PL	NKS FOR	SHALLOW	ER FILL.							
2	CUT TO FIT FOR FILLS UNDER	6 FEET AND FOR SPA	NS OVER	12 FEET	<u> </u>										\bot
_3	BEARING PILE LENGTH TO BE D	ETERMINED BY FIELD	CONDIT	IONS.											

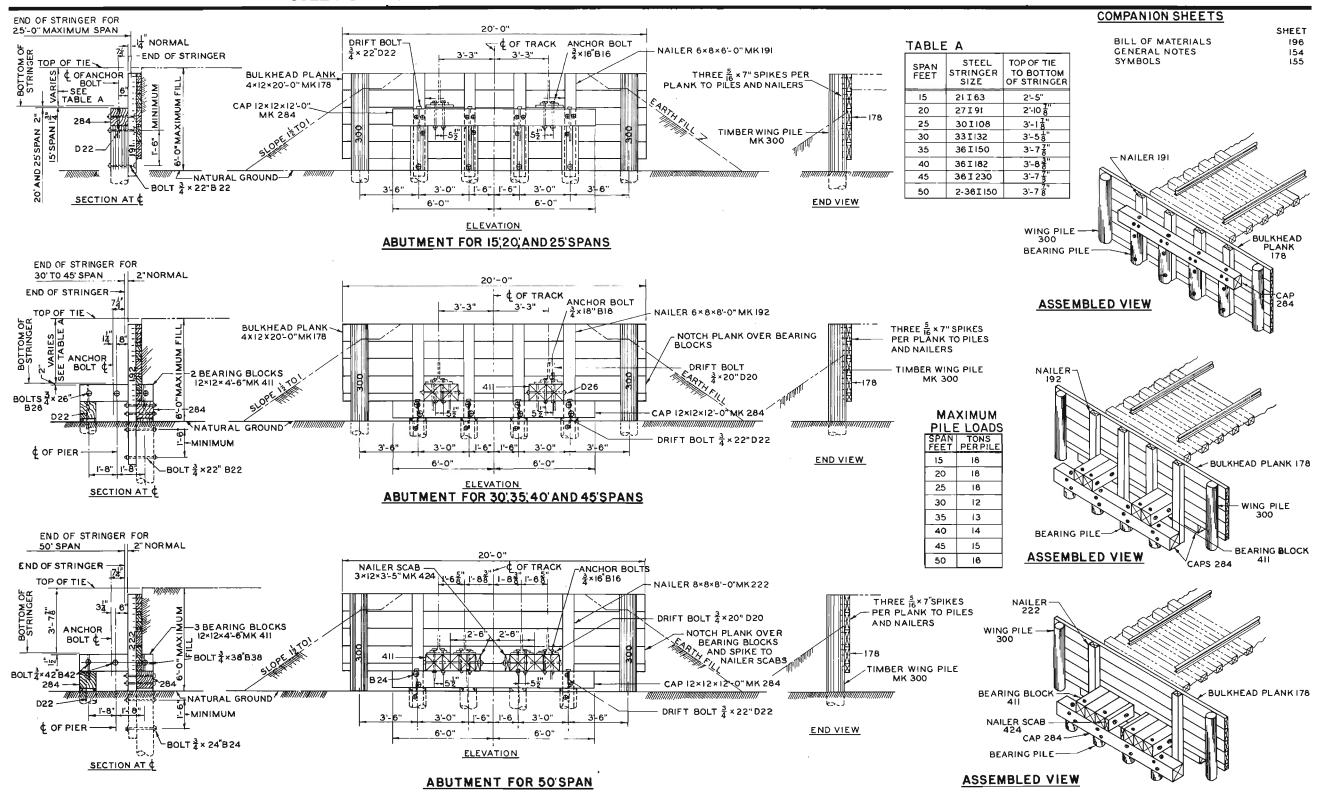


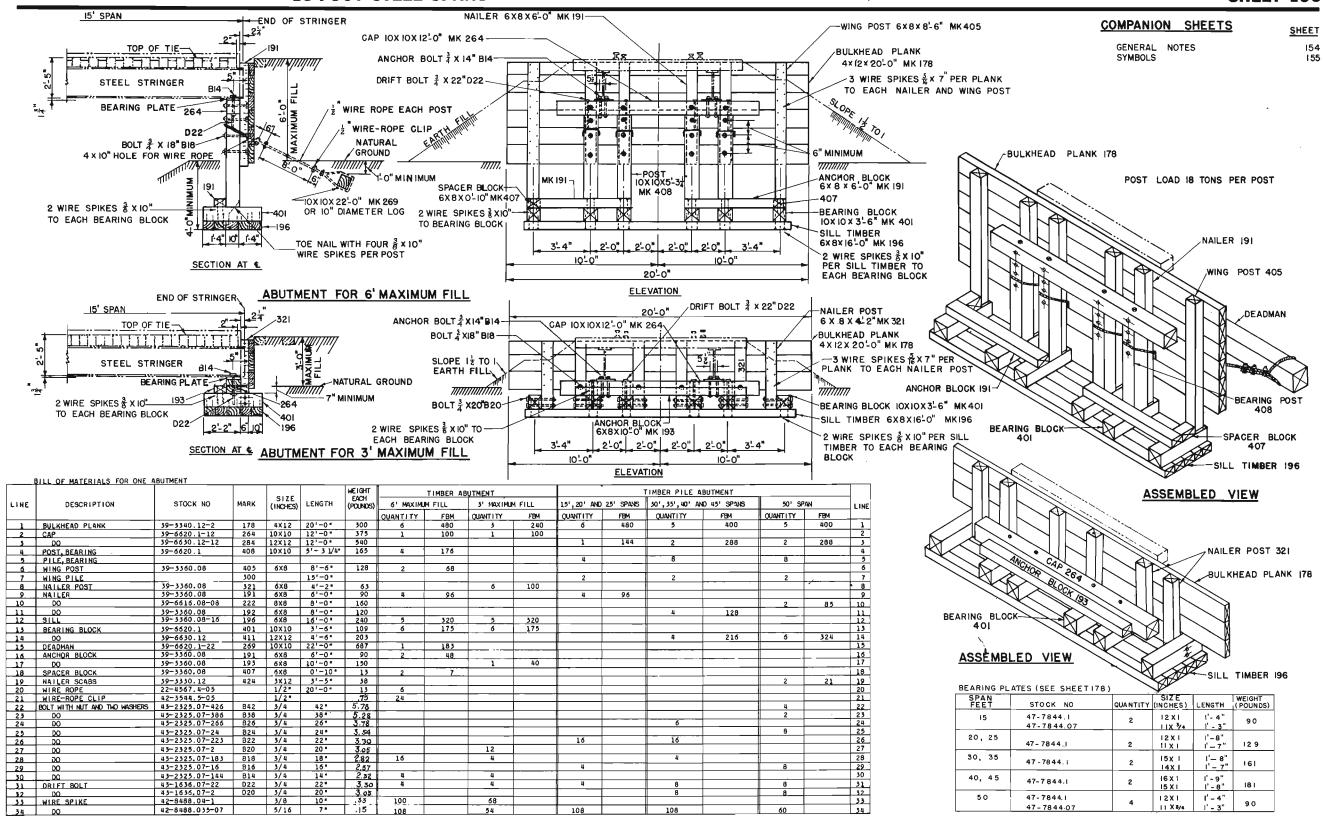
COMPANION SHEETS BILL OF MATERIALS 196 GENERAL NOTES 154 SYMBOL 155



ABUTMENT FOR 6' MAXIMUM FILL

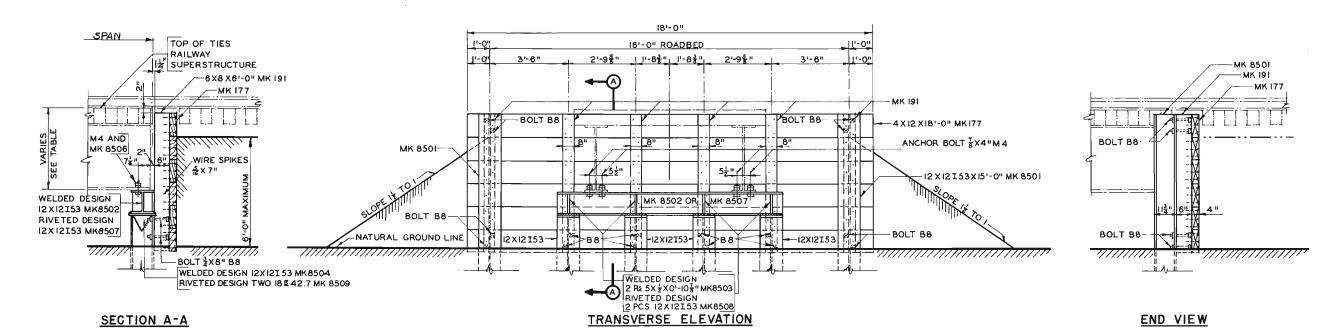


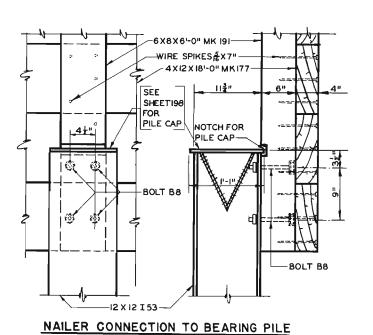




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	911661
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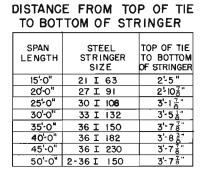
STEEL ABUTMENTS, STEEL SPANS

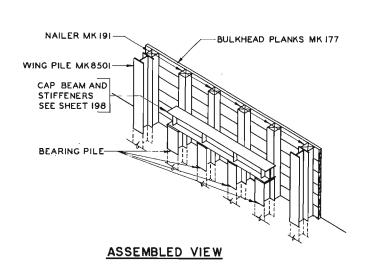
MAXIMUM
PILE LOADS

SPAN TONS PER
PILE

15'.0" 15
20'-0' 15
25'-0' 18
30'-0' 20
35'0' 22
40'.0' 24
45'.0' 26

50'-0" 28





5 X 1 X 01-10 7 1 MK 8503

TW018E42.7

MK 8509

-PILE 12 X 12 I 53 RIVETED CONNECTION DETAIL

PILE TO CAP BEAM

SHEET 198

9" 18E42.7

PILE CAP MK 8509

FBM

LENGTH OUANTITY

WETCHT EACH (POUNDS)

795

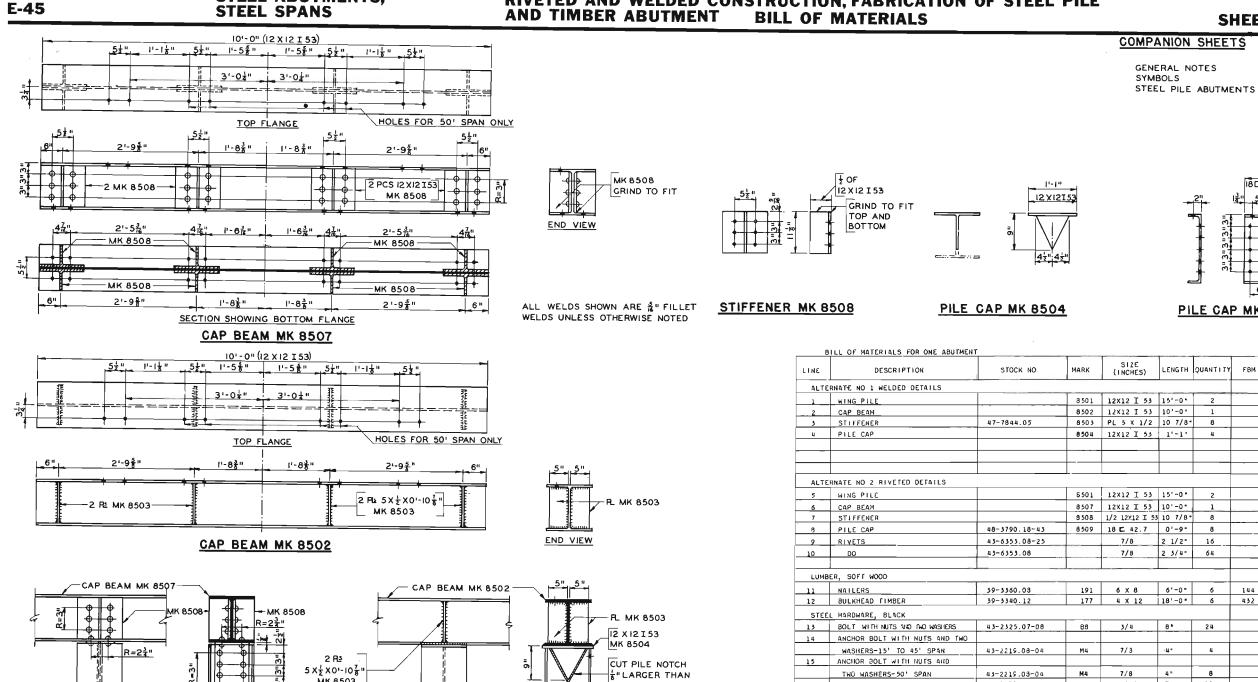
530

SHEET

154

155

197



CAP AND BUTT WELD BF

PILE

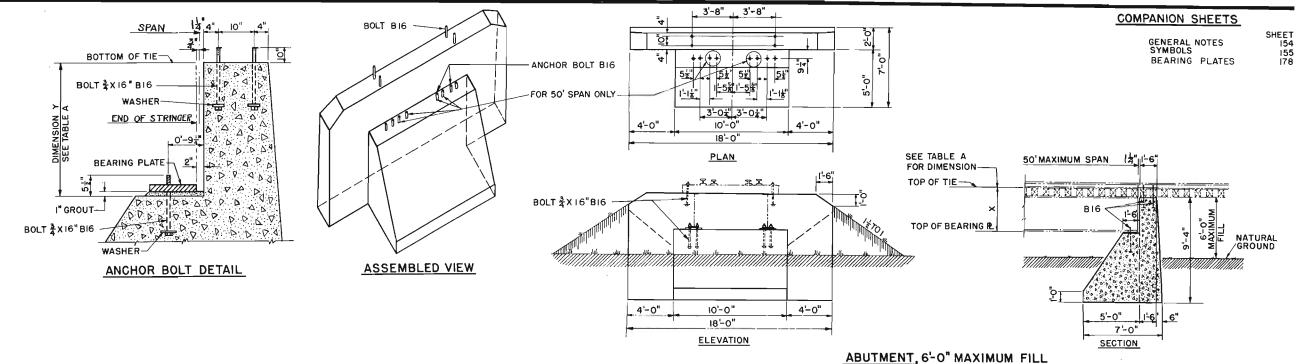
12X12T53

WELDED CONNECTION DETAIL

PILE TO CAP BEAM

ц	PILE CAP		8 50 4	12X12 I 53	1'-1"	4		29
ALTE	RNATE NO 2 RIVETED DETAILS							
5	WING PILE		6501	12×12 I 53	15'-0"	2		795
6	CAP BEAM		8507	12X12 I 53	10'-0"	1		530
7	STIFFENER		3 50 8	1/2 12X12 I 53	10 7/8	8		24
8	PILE CAP	48-3790.18-43	8509	18 € 42.7	0'-9"	8		32
9	RIVETS	43-6353.08-25	191 6 x 8 6'-0" 6 144 90 -08 68 3/4 8" 8 19 19 -04 M4 7/8 4" 8 19 16 -04 M4 7/8 4" 8 19 16 -04 M4 7/8 4" 8 19 16 -05 8501 12x12 153 10'-0" 10 10 -06 12x12 153 10'-0" 10 10 -07 12x12 153 10'-0" 10 -08 12x12 12x12 12x12 12x12 -09 12x12 12x12 12x12 -09 12x12 12x12 12x12 -09 12x12 12x12 12x12 -09 12x12 153 -09 10x12 12x12					
10	DO	43-6353.08		7/8	2 3/4"	64		.66
				1				
LUMB	ER, SOFT WOOD							
11	NAILERS	39-3360.08	191	6 X 8	6'-0"	6	144	90
12	BULKHEAD TIMBER	39-3340.12	177	4 X 12	18'-0"	6	432	270
STEE	L HARDWARE, BLACK							
13	BOLT WITH NUTS THO THO WASHERS	43-2325.07-08	88	3/4	8 *	24		1 39
14	ANCHOR BOLT WITH NUTS AND TWO							
	WASHERS-15' TO 45' SPAN	43-2219.08-04	M4	7/3	-44*	4		1 6
15	ANCHOR BOLT WITH NUTS AND							
	TWO WASHERS-50' SPAN	45-2215.03-04	M4	7/8	4"	8		1 12
16	WIRE SPIKE	42-8483.035-07		5/15	7-	108		1 16
17	WELDING ROD	46-3772.2-7		3/16				
		[1	I				

TOTAL WEIGHT



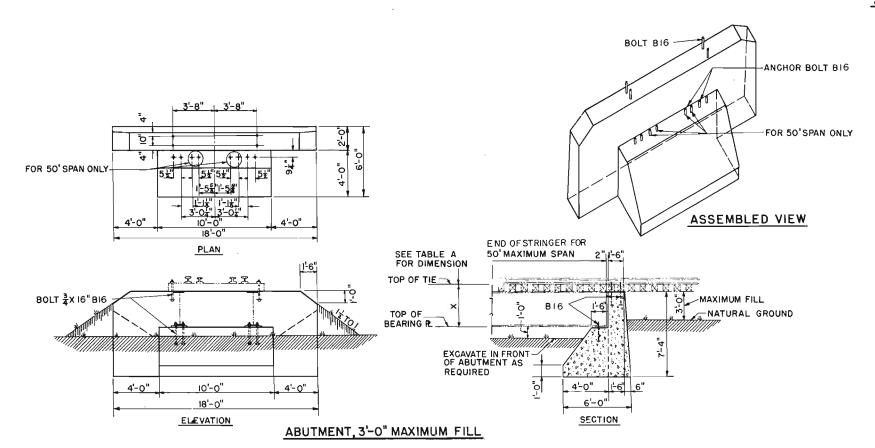
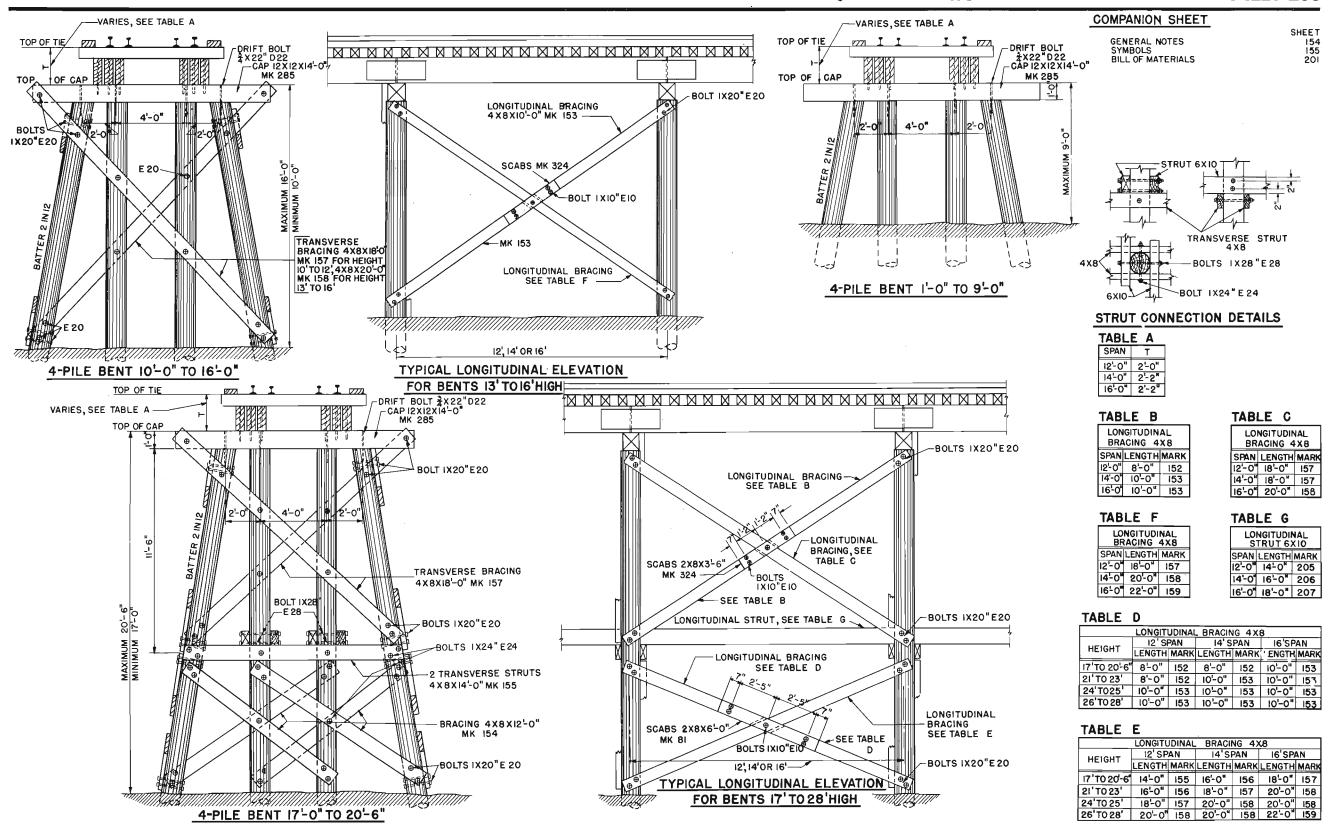


TABLE A - DIMENSIONS AND BILL OF MATERIALS

				OLTS WITH	CONCRETE				
SPAN FEET	x	Y	WASHERS STOCK NO	3 X 16" B16 43-2325.07-16	6' MAXIMUM FILL	3' MAXIMUM FILL			
			QUANTITY	WEIGHT EACH (POUNDS)	CU YDS	CU YDS			
15	2'- 5"	1'-11 2 "	8	3.5	20.4	14.4			
20	2'-10%"	2'-5#"	8	3.5	19.8	14.3			
25	3'-18"	2'-8 1 "	8	3.5	19.5	13.7			
30	3' - 5 ธู่ "	2'-115"	8	3.5	19.2	13.4			
35	3'-78"	3'-2*"	8	3.5	18.9	13.1			
40	3'-8#"	3'-3%"	8	3.5	18.8	13.1			
45	3'-74"	3'-28"	8	3.5	18.9	13.1			
50	3'-78"	3'-2**	-12	3.5	18.9	13.1			

BEARING PLATES (SEE SHEET 178)

SPAN	STOCK NO	QUANTITY	SIZE (INCHES)	LENGTH	WEIGHT (POUNDS)
15	47-7844.1 47-7844.07	2	12 X I	1'- 4" 1'-3"	90
20, 25	47-7844.1	2	12 X I	l'-8"	129
30, 35	47-7844.1	2	15 X 1 14 X I	!'-8" !'-7"	161
40, 45	47- 7844.1	2	16 X I 15 X I	l'-9" l'-8"	181
50	47-7844.1 47-7844.07	4	12 X 1 X \frac{3}{4}	'-4" '-3"	90



SHEET GENERAL NOTES 154 155 SYMBOLS TIMBER PILE BENTS 200

35 36

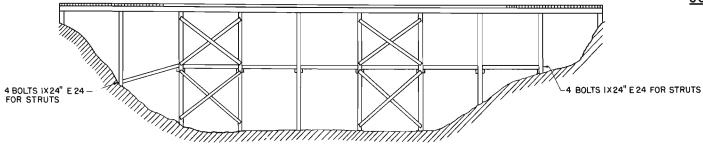
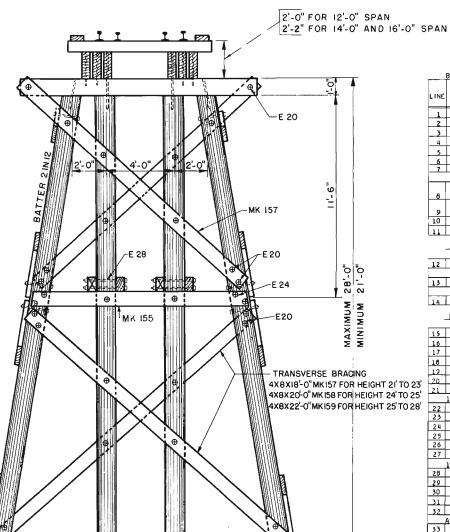


DIAGRAM SHOWING LONGITUDINAL BRACING

FOR BENTS 13 FEET HIGH OR OVER, EVERY THIRD PANEL HAS LONGITUDINAL BRACING LONGITUDINAL STRUTS ARE CARRIED TO BANK AND FASTENED TO BENT NEAR GROUND LINE.

43-2325.1-104 E10 43-2325. 1-2 E20 1

20 5.6



4-PILE BENT 21-0" TO 28'-0"

				SIZE			BENT HEIGH	יפסדים ד	BED (T HE IGHT	10' 10 12'	BENT HEIGHT	'א <u>ר כד יע</u>	BENT HEIGHT	17 TO 20'	BENT HEIGHT.	21' 10 23'	BENT HEIGHT:	24' 10 25'	BENT HEIGHT	26' 10 28'	-
LINE	DESCRIPTION	STOCK NO	MARK	(INCHES)	LENGTH		QUANTITY	FBM	QUANTITY	FBM	YTTHAUC	FBM	QUANTITY	F8M	QUANTITY	F8M	OUANTITY	FBM	QUANTITY	F814	LII
1	TIMBER PILE					-	4		ц		4		4		ц		ц		4		
2	CAP, LUMBER, SOFT WOOD	59-6530.12-14	285	12X12	14'-0"	630	1	168	1	168	1	168	1	158	1	168	1	168	ı	168	
3	BRACE, LUMBER, SOFT WOOD	39-3340.08-12	154	4x8	12'-0"	120	ĺ						4	128							Т
4	00 -	39-3340.08-18	157	4×8	18'-0"	180			2	96			2	95	ti.	192	2	96	2	96	
5	DO	39-3340.08-2	158	4×8	20'-0"	200					2	107]		2	107	ŀ		1
6	DO	39-3340.09-22	159	4X8	22'-0"	220													2	117	
7	STRUT, LUMBER, SOFT WOOD	39-3340.08-14	155	4X8	14,-0.	140							2	75	2	75	2	7.5	2	75	
	STEEL HARDWARE, BLACK																				
- 1	DRIFT BOLT WITH SQUARE		1	١.					I I										1	. '	ı
8	HEAD AND ONE WASHER	43-1636.07-22_	D22	3/4	22"	3.0	4		ц		4		_4		4		4		4		⊢
9	MACHINE BOLT WITH SQUARE HEAD, NUT AND TWO WASHERS	43-2325.1-2	E20	١,	20 "	5.6			12		12		28		24		24		1	1	
10	DO	43-2525. 1-24	E24	1	24*	5.5			1 1		12		8		6		6		24		\Box
11	DO DO	43-2325.1-28	E28	1	28*	2 11	1		 				<u>, , , , , , , , , , , , , , , , , , , </u>		- "						
4 4	100	47-2727.1-20	1620		- 20								4 1		4						.!
_	MATERIAL REQUIRED FOR LOS	NGTTUDINAL BRACT	NG FO	R VARIOL	IS SPAN	S. STR	UTS ONLY														
	12' SPAN																				
12	STRUT, LUMBER, SOFT WOOD	39-3360.1-14	205	6X10	14'-0"	262							2	140	2	140	2	140	2	140	1
	14' SPAN																				
13	STRUT, LUMBER, SOFT WOOD	39-3360.1-16	206	6X10	16'-0"	300							2_[160	2	160	2	160	2	160	Ĭ.
	16' SPAN								1				n	~~~							_
4	STRUT, LUMBER, SOFT WOOD	39-3360,1-18	207	6x10	181-0"	338							2	180	2	180	2	180	2	180	
	MATERIAL REQUIRED FOR LOP	NGITUDINAL BRACII	NG FOR	R VARIOU	S SPANS	S. BRAG	CES AND ST	TRUTS													
	12' SPAN																				
15	BRACE, LUMBER, SOFT WOOD	39-3340.08-08	152	448	8'-0"	80	11						8	171	8	171	4	85	ц	85	1 3
16	po	39-3340.08-1	153	4xB	100.	100			1		4	107					4	107	4	107	
17	00	39-3340.08-14	155	4×8	14'-0"	140			Ī				2	75							\Box
18	00	39-3340.08-16	156	4x8	16'-0"	160									2	35					П
12	00	39-3340.08-18	157	4X8	18'-3"	180					2	96	2	95	2	96	4	192	2	96	Т
20	DO	39-3340.08-2	158	4x8	20'-0"	200			i i	_			1						2	107	Т
21	STRUT, LUMBER, SOFT WOOD	39-3360.1-14	205	6×10	14'-0"	262			1				2	140	2	140	2	140	2	140	
	14' SPAN	_													•		•				
22	BRACE, LUMBER SOFT WOOD	39-3340.08-09	152	4X8	8'-0"	80							4	85							
23	DO	39-3340.08-10	153	4×8	10'-0"	100					4	107	4	107	8	213	8	213	8	213	
24	ວວ	39-3340.08-16	156	4X3	16'-0"	160							2	85							1
25	00	39-3340.05-18	157	4:48	18'-0"	180							2	96	4	192	2	. 96	2	95_	
26	DO	39-3340.08-2	158	4 x 8	20'-0*	200					2	107					2	107	2	10.7	
27	STRUT, LUMBER SOFT WOOD	39-3360. 1-16	206	6×10	16'-0"	300							2	160	2	160	2	160	2	160	<u> </u>
	6' 5PAN																				
28	BRACING, LUMBER, SOFT WOOD	39-3340.08-1	153	4X8	10'-0"	100					łį.	107	8	213	8	213	8	213	8	213	L
29	DQ	39-3340.08-18	157	4X8	13'-0"	180							2	96							┖
30	00	39-3340.08-2	158	4.48	20'-0"	200							2	107	4	213	4	213	2	107	1
31	00	39-3340.08-18	159	4x8	22'-0"	220					2	117						_	2	117	1
	STRUT, LUMBER, SOFT WOOD	39-3360. 1-18	207	6X 10	18'-0"	338							2	180	2	180	2	180	2	180	
	LL SPAN																				
	SCAB, LUMBER, SOFT WOOD	39-3228.08	81	2 48	6'-0"	30							14	32	4	32	4	32	4	32	
34	D.O	39-3228.08	324	2 ×8	3'-6"	18					- 4	19	4	19	11	19	4	19	4	19	1
	STEEL HARDWARE, BLACK																				_
	MACHINE BOLT WITH SQUARE							11							I T		aa	3	20		1.
3.5	HEAD, NUT, AND TWO WASHERS	43-2325, 1-104	£10	1	10 7	3, 5					10		20.		20		20		20		3
36	no l	43-2325.1-2	F 20	1	20.4	5.6					1.6		3.2		32		32		32		11 3

12 X 12 X 14 - 0"F

-BOLT 1X20" E 20

REQUIRED

PILE BEARING

CAPACITY

II TONS

2<u>'- 6 1 '</u>'

3 0 7 12 " 3 3 3 7 13 "

3-7 | 14 " 3-9 | 15 "

3-10 ₹ 16 "

3-93" 17 " 3-93" 18 "

DEPTH

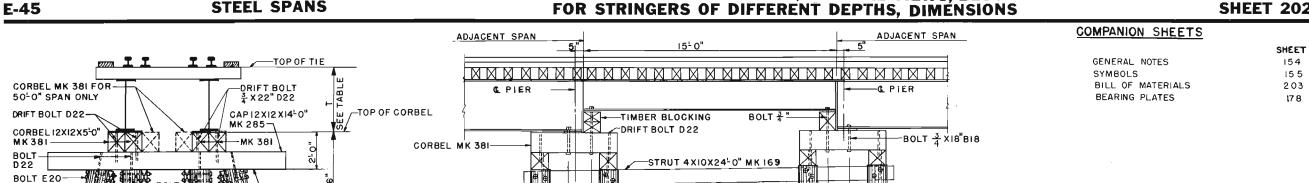
0F BLOCKING

0<u>-</u> 6 -

1-0 출

1-3 &

1 2 {



-9" I-4"0"[[

2'2'0" 2'0'-*

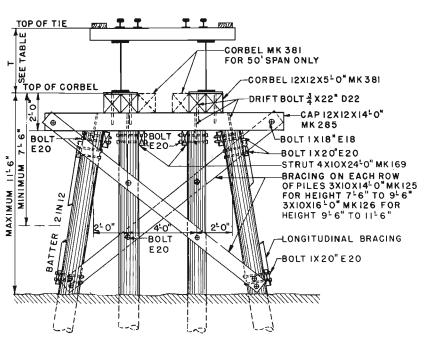
PIERS UP TO 11 FEET HIGH, GENERAL VIEWS, BLOCKING

TRANSVERSE ELEVATION 16-PILE TIMBER TOWER UNDER 716" HIGH

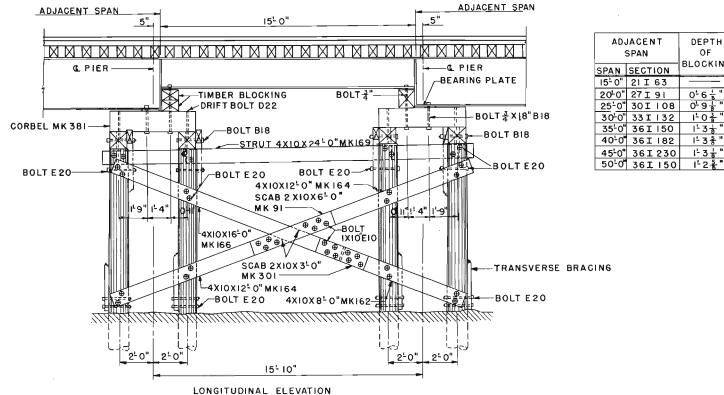
4-0"

LONGITUDINAL ELEVATION 16-PILE TIMBER TOWER UNDER 716" HIGH

15-10"



TRANSVERSE ELEVATION 16-PILE TIMBER TOWER 716" TO 11-6" HIGH



16-PILE TIMBER TOWER 7-6" TO 11-6" HIGH

RAILWAY

BOLT-

STRUT

MK169

4XIOX24-0"

	37551
GENERAL NOTES	154
SYMBOLS	155
TIMBER PILE PIERS FOR STEEL SPANS	202

BILL OF MATERIALS FOR ONE TIMBER PILE PIER 7'-6" OR LESS IN HEIGHT PIER HEIGHT 7'-6" OR UNDER SPAN 35' TO 45' SIZE (INCHES) LENGTH WEIGHT HARK FBM LINE DESCRIPTION STOCK NO QUANTITY QUANTITY F8M QUANTITY FEM QUANTITY FBM QUANTITY FBM LUMBER, SOFT WOOD 381 12 × 12 5'-0" 225 285 12 × 12 14'-0" 630 169 4 × 10 24'-0" 300 1 CORBEL 39-5630.12 480 2 CAP 3 STRUT 39-5630.12-14 39-3340.1-24 672 320 4 672 4 320 4 572 4 320 672 4 672 2 520 4 320 3 4 TIMBER PILE 5 BLOCKING 382 12 x 12 8'-6* 383 383 10 x 12 8'-6* 319 384 8 x 12 8'-6* 255 39-5630.12 1 102 5 39-6620.12 39-6616.12 6 DO 7 DO 8 DO 136 39-3350.12 385 6 X 12 8'-6" 191 STEEL HARDWARE, BLACK 9 HEAD, NUT, AND TWO WASHERS 3/4 43-2325.07-223 822 10 DO 11 DO 12 DO 13 DO 26" 3.78 30" 4.26 32" 4.50 18" 2.82 8 43-2325.07-266 B26 5/4 10 43-2325.07-306 B30 43-2325.07-32 B32 43-2325.07-183 B18 3/4 3/4 3/4 4 4 13 14 DO 43-2325.1-2 20 * 5.51 32 32 14 32 32. 32 DRIFT BOLT WITH SOUARE 15 HEAD AND WASHER 45-1636.07-22 D22

TIMBER PILE PIERS,

STEEL SPANS

	BEARING	PLATES (SEE SHEET	170)
SPAN	YT I THAUD TROPPUE HORS	SIZE (INCHES)	LENGTII	STOCK NO
15'	2	12X1 11X5/4	1'-4"	47-7844.1 47-7844.07
20',25'	2	12/1 11/1	1'-3"	47-7844.1
30', 55'	2	15X1 14X1	1'-3"	47-7844.1
40',45'	2	16X1 15X1	1,-8.	47-7844.1
50'	4	12X1	1'-4"	47-7844.1

ļ				PIER HEIGHT							71-6	5" TO 9"	-51										91	-6° TO	11'-6"					[,l
				SPAN			15	5'	20	,	25	51	30	(35' TO	45'	50)'	15!		20	1	25		30	<u>, t</u>	35' TO	45'	50		1
INE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	WEIGHT (POUNDS)	CONTITY	FBM	Cha:III LA	FBM	YTITHAUC	FEM	QUAŅT I TY	FBM	QUANTITY	FBM	OUANTI TY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	LIN
	LUMBER, SOFT WOOD			-															_												
1	CORBEL	39-6630.12	381	12 × 12	5'-0*	225	В	480	В	480	8	480	8	430	8	480	8	490	1 8 T	480	8	480	8	480	8	480	8	480	10	600	П
2	CAP	39-6530.12-14	285	12 X 12	14'-0"	630	4	672	4	672	4	672	4	672	4	672	ш	672	4	672	11	672	А	672	4	672	а .	672	и	672	\vdash
3	STRUT	39-3340.1-24	169	4 X 10	24'-0	300	4	320	4	320	4	320	4	320	4	320	4	320	4	320	4		4	320	4	320	4		4	320	
	BRACE	39-3330.1-16	126	3 X 10	16'-0"	150													8	320	8	520 520	8	320	8	320	8	320 320	8	320	
5	00	39-3330.1-14	125	3 X 10	14'-0"	131	8	280	8	280	8	280	8	280	8	280	8	280													
5	DO	39-3340.1-16	166	4 X 10	16'-0"	200	4	213	4	213	4	213	4	213	4	213	4	213	4	213	ц	213	4	213	4	213	4	213	4	213	íl –
	00	39-3540.1-12	164	4 X 10	12'-0"	150	8	320	8	320	В	320	8	320	8	320	8	320	8	320	8	320	В	320	8	320	8	320	8	320	厂
	DO	39-3340.1-08	162	4 X 10	8'-0*	100	4	107	4	107	4	107	4	107	4	107	4	107	ŭ i	107	- 4	107	4	107	4	107	4	107	4	107	đ –
	SCAB	39-3880.1	91	2 X 10	6'-0"	38	8	80	8	80	8	80	8	80	8	80	8	80	8	80	8	80	8	80	8	80	В	80	8	80	1
\perp	00	39-3880.1	301	2 X 10	3'-0"	19	8	40	8	40	8	40	8	40	8	40	8	40	8	40	8	40	8	40	8	40	8	40	8	40	1
	BLOCKING	39-6630.12	382	12 X 12	8'-6"	383	i T						1	102			1						f - 1		1	102					1
_	DO	39-6620.12	383	10 X 12	8'-6-	319					1	85					1						1	85		1					
4	00	39-6616.12	384	8 X 12	8'-6"	255									2	136	2	136									2	136	2	136	
-	DO	39-3360.12	385	6 X 12	8'-6"	191			1	51									1		1	51									1
⅃.	TIMBER PILE]	l_	1		16		16	_1	16		16		16		16		16		16		16		16		16		16		1
S	STEEL HARDWARE, BLACK										,																				
6	MACHINE BOLT WITH SQUARE HEAD, NUT, AND TWO WASHERS	43-2325.1-2	E20	1	20 •	5.51	144		144		144		144		1 = 4		144		144		144		144		144		144		144		1
7	DO	43-2325.1-104	E10	1	10 "	3.45	64		64		64		64		54		64		64		64		64		64		64		64		
	DO	43-2325.07-223	822	3/4	22.	3.30			4						/,		-		1		2										
,	00	43-2325.07-255	826	3/4	26"	3.78																	4								1
	DO	43-2325.07-306	B30	3/4	30	4.26							4										-		4			No arte di civi			
\perp	DO	43-2325.07-32	832	3/4	32*	4.50									а		п		#								4		4		
	DO	45-2325.07-183	818	3/4	16"	2.82	8		4		4		4		4		8		8		п		4		4		4		8		1 :
	DRIFT BOLT WITH SQUARE HEAD AND WASHER	43-1636.07-22	D22	3/4	22*	3.00	32		32		32		32		32		32		32		32		32		52		32		34		2

___ LENGTH OF PILES TO BE DETERMINED BY FIELD CONDITIONS.

LENGTH OF PILES TO BE DETERMINED BY FIELD CONDITIONS.

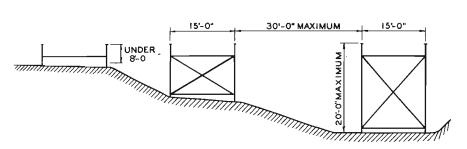


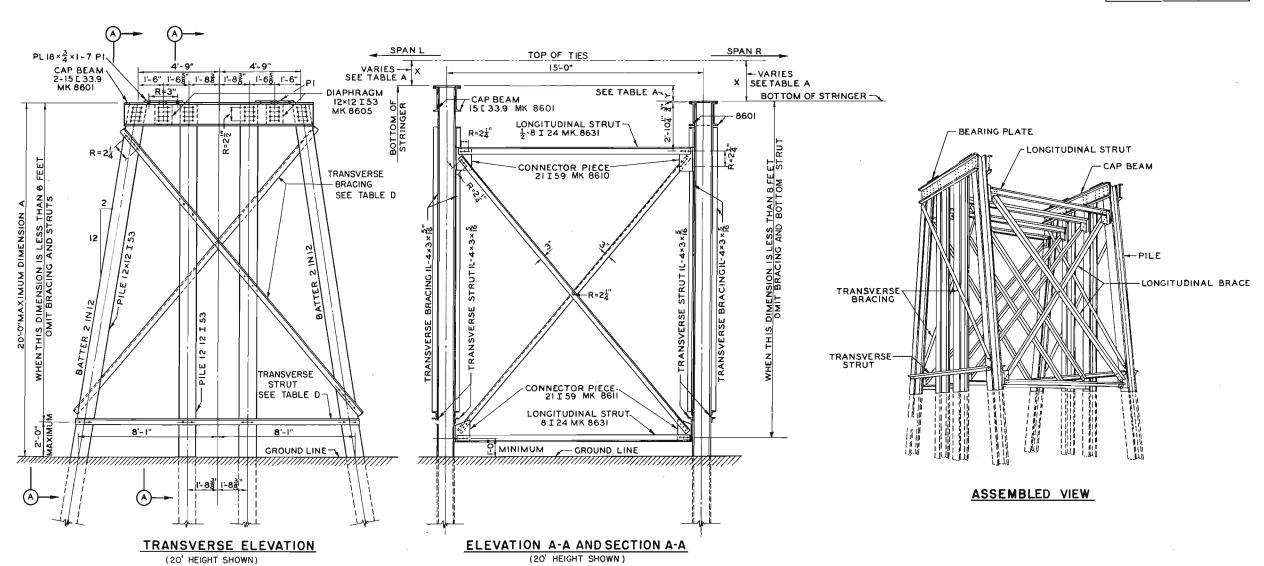
DIAGRAM SHOWING LONGITUDINAL BRACING AND HEIGHT AND SPAN LIMITATIONS OF TOWERS

TABLE	D		
TOWER		PIECE N	ARK
HEIGHT	TRANS	VERSE	LONGITUDINAL
Α	STRUT	BRACE	BRACE
8'-0 [^]	8630	8630	8632
10-0"	8632	8632	8634
12'-0"	8633	8634	8635
14'-0"	8635	8637	8637
16'-0"	8636	8641	8640
18'-0"	8638	8643	8642
20'-0"	8640	8646	8645

TABLE	Α			
SPAN R	15-0"	20'-0"	25'-0"	30'-0"
STRINGER	21163	27191	301 108	271132
х	2'- 5"	2'-107"	3'-18"	3'-5 ¹ "
SPAN L	Y	Y	Y	Y
15'-0"	0'- 0"	0'-57"	0-87"	l'-0 <u>1"</u>
20-0"	0'- 5 ⁷	0'-0"	0'-3"	0'-64"
25'-0"	0'-87"	0'-3"	0'-0"	0'-34"
30'-0"	1,-08,	0'-64"	0'-31"	0'-0"

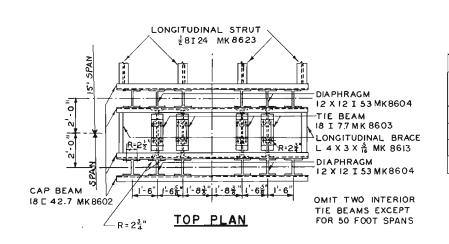
COMPANION SHEETS	
	SHEE
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SYMBOLS	155
FABRICATION DETAILS	206

MAXIMUM PILE	LOADS
SPAN BETWEEN TOWERS	TONS PER PILE
15	27
20	30
25	33
30	35







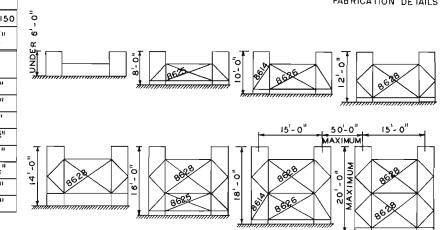


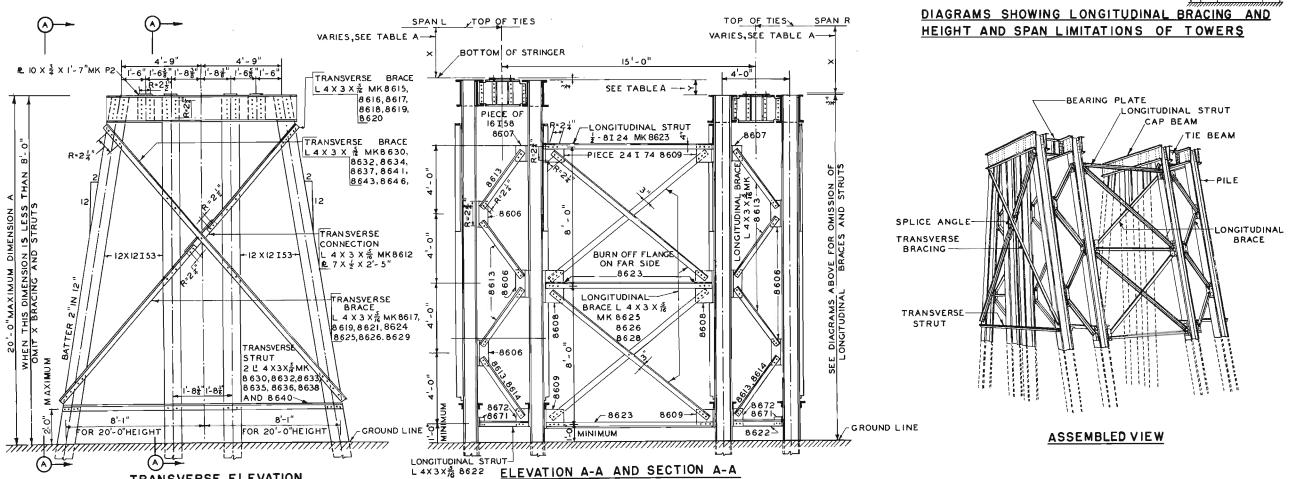
TRANSVERSE ELEVATION

(20' HEIGHT SHOWN)

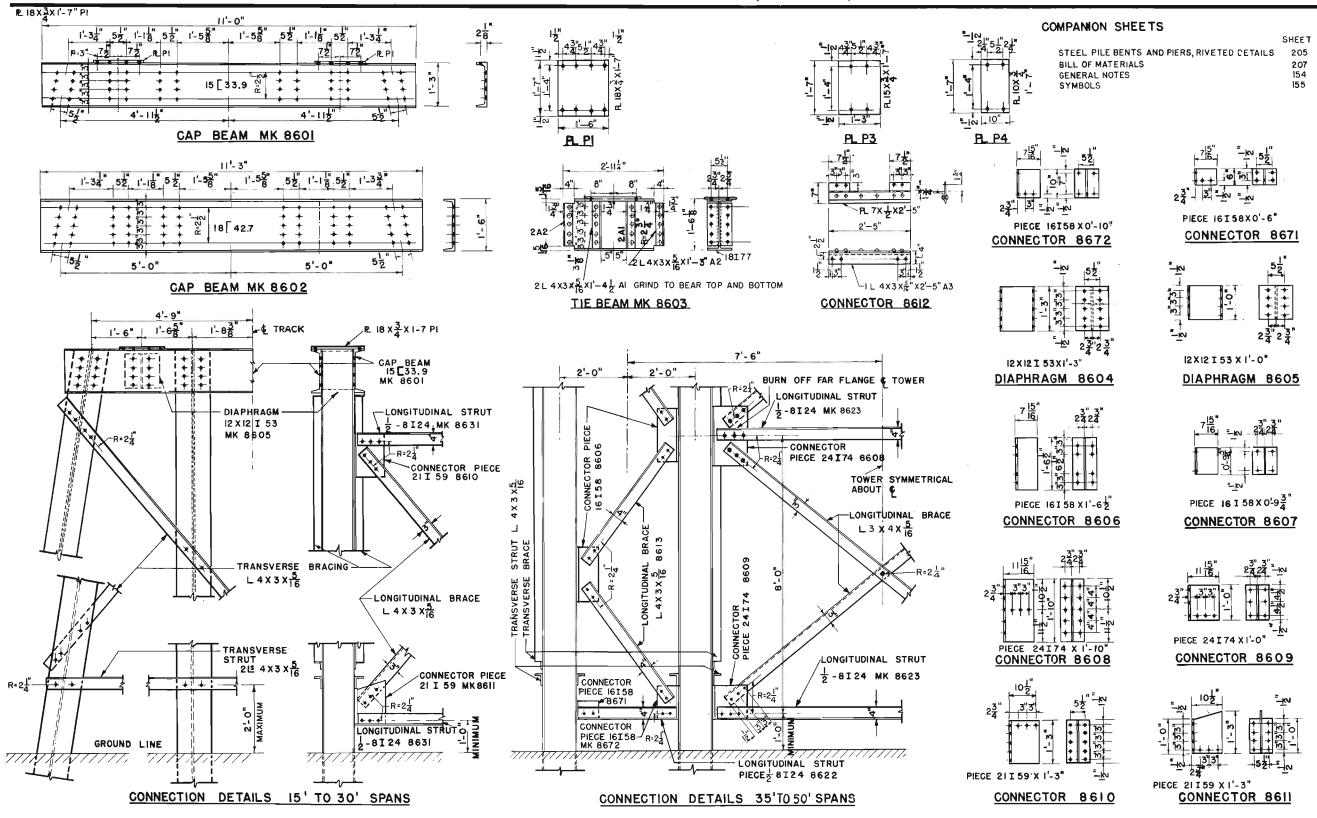
		SPAN R	35'-0"	40'-0"	45'-0"	50'-0"
		STRINGER SIZE	3€1150	361182	36 I 230	2-36 I 15
MAXIMUM PIL	E LOADS	х	3'- 7 <mark>7</mark> "	3'-8 <mark>3</mark> "	3'- 78"	3'-7 <mark>7</mark> 11
PAN BETWEEN TOWERS	TONS PER PILE	S PA N L	Y	Y	Y	Y
3.5'	20	15'-0"	1'-27"	1'-3 3 "	1'-27"	1'- 2 7"
40'	21	20'-0"	0' - 9 "	0'-9 2"	0'-9"	0, - 8 ,,
45'	23	25'-0"	0'-6"	0'-6 <mark>2</mark> "	0, - 6,,	0'-6"
50'	26	30'-0"	01-2 3 "	0'-34"	0'-23"	0'- 23"
		35'-0"	0'-0"	o'- o ¹ "	0'-0"	0, -0,,
		40'-0"	0'-02"	o¹ - o "	o'- o <u>l</u> "	o'- o 1"
		45'-0"	0'-0"	0'-02"	0'-0"	0'-0"
		50'-0"	0'- 0"	0'-0 <u>1</u> "	0'-0"	01-011

TABLE A





(20' HEIGHT SHOWN)



SHEET

COMPANION SHEETS

 GENERAL NOTES
 154

 SYMBOLS
 155

 STEEL PILE BENTS AND PIERS
 204,205,206

 -	BILL OF MATERIALS FOR	R TWO RIVETED ST	EEL PIL							0010	D 0755	0115 55	NTO CO-	151 70	101 000	10			00407	OFC:	011 5 211	CD0 505	101 00 -	al cos					554555	0.755: -					_
				88	NT OR P	IER H	EIGHT -	– <u>、</u> .ŀ	251		T	PILE BE			8' 8'	6'	4'	20'	r	16'		T -	35' TO 4				001					RS FOR 5	1 -		
H								UNIT	20'	18'	16'	14,	12'	10'	8,	6'	4.	201	18,	16'	141	12'	10'	θ'	61	41	20'	18'	16'	14'	12'	10'	8'	6'	41
.INE	DESCRIPTION	STOCK NO	MARK		IZE CHES)	LENG	:тн ₩	EIGHT (EQNUO				•	YT I THAUÇ	,							(QUANTITY	1								QUANTIT	TY			
1	CAP BEAM	48-3790.15-34	8601	15.0	33,9	111-		372-	4	ħ.	4		4	4	4		4															T	_		
2	DO DO	48-3790.18-43	8602		42.7	11'-		480			 	,	 		1	1	1	8	я	8	8	B	В	8	a	9	-	8			8				я
_	DIAPHRAGM	48-2900. 18-077			T 77	21-10	_	225										4	4	4	4	4	4	4	4	4	8	8	8	8	8	8	8	8	8
4	DO				2 I 53		-	66										8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
5	00		8605	12X12	2 I 53	11-	-0 •	55	4	4	4	4	4	4	4	4	4																_		
6	CONNECTOR	48-2900.16-058	8606	1/2 1	16 I 58	1'-6	1/2"	45										24	16	16	8	8					24	16	16	8	8				
7	DO	48-2900.16-058				_	_	24			ļ						ļ	8	8	8	8	8	8	8			8	8	88	8	8	8	8		
8	00	48-2900.24-074				_		68			ļ							8	8	8_							8	8	8						
9	DO	48-2900.24-074						37			 _	-	 		-	_	-	16_	16	16	16	16	16	16	- 8	8	16	16	16	16	16	16	16	8	8
10		48-2900.21-059				-	$\overline{}$	37	8	8	8	8	8	8	8	8	8										-			-	_				
11	DO	48-2900.21-059 47-7844.05	8612			2'-	_	37 29	8	8	8	8	8	8	8			4	4	4	4	4	4	4			4					н			
12	00	48-2900.16-058				+	_	15										8	8	8	8		8	8			8	8	8	8	8	8	8		_
14	DO	48-2900.16-058				_	_	24			T -							8	8	8	8		8	8			8	8	8	8	8	8	8		
-	SPLICE ANGLE	48-2500.4-035			5 X 5/10	_		17										4	4	4	4	ц	4	4			4	4	4	4	4	4	4		
	STIFFENER ANGLE	48-2500.4-035	Al	L4 X	3 X 5/16	5 1'-4	1/2"	10										16	16	16	16	16	16	16	16	15	32	32	32	52	32	32	32	32	32
17	CONNECTION ANGLE	48-2500.4-035	A2	L4 X	3 x 5/16	1'-	-34	9										16	16	16	16	16	16	16	16	16	32	32	32	32	32	32	32	32	32
18	BRACES AND STRUTS	48-2500.4-035	8613	L4 X 3	3 X 5/15	4'-	-2"	30										32	16	24	16	16		θ			32	16	24	16	16		8		
19	DO	48-2500.4-035			3 X 5/16			41											В				8					8		_		8			
20	00	48-2500.4-035			5 X 5/16	_	-	40			 	<u> </u>	-											4				-					4		
21	DO	48-2500.4-035			3 X 5/10	_		43			-	-											4 _					-				4			
22	DO	48-2500.4-035			3 X 5/16	+		50					_			1	-		 	4	4	4		4					4	4	4		4		
23	DO	48-2500.4-035			× 5/16	_	-	54											и и	-			и				_	4		_		4		-	-
25	00	48-2500.4-035			3 x 5/16		-	58										4	<u> </u>								- 4	7				-			
26	DO	48-2500.4-035				_		61										,				4								-	4				
27	DO	48-2500.4-035	8622	L4 X	3 x 5/16	21-	-10 4	20										8	8	8	8	8_	8	8			8	8	8	В	8	в	8		
28	00	48-2500.08-024	8623	1/2	B I 24	91-	-10 "	118										12	12	12	8	8	8	8	4	4	12	12	12	В	8	8	8	4	4
29	DO	48-2500.4-035			3 X 5/16	_	_	68													4									4		ļ			
30	DO	48-2500.4-035			3 X 5/16	_	_	76												12				8					12				8		
31	00	48-2500.4-035			3 X 5/16		_	84											12	_			8					12		_		8			
32	00	48-2500.4-035 48-2500.4-035			3 X 5/16 3 X 5/16	-	_	90 95										16	- 8	. 8	8	8			_		16	8	8	8	8				
33	DO	48-2500.4-035			3 x 5/16			97							8			•									-				_				
34 35	DO DO	48-2900.08			8 I 24	-	-	168	8	8	8	8	8	8	8	4	4							12							_		12		
36	00	48-2550, 4-035			3 × 5/16			105				_		8	8		1						12							_		12			
37	00	48-2550.4-035			3 x 5/16			108					4									8									8				
38	DO	48-2550.4-035			3 x 5/16			112			T		4	8				_				4							_	_	4				
39	00	48-2550.4-035				_		115				4	8								8									8					
40	00	48-2550.4-035			3 x 5/16	_		119			4									8									8						
41	00	48-2550.4-035			3 X 5/16	_	_	123				12			L						4									4					
42	DO	48-2550.4-035			3 x 5/16			127		4									8									8							
43	DO	48-2550, 4-035			3 x 5/16			134	4		8		-		1			8	-								в					ļ <u>.</u>			
44	00	48-2550.4-035			3 x 5/10	_		137			4	-		ļ	-				-	4			1						4			ļ			
4.5	DO	48-2550.4-035			3 X 5/16			140		8		1			1	-	 																		
46 47	00	48-2550.4-035 48-2550.4-035			3 X 5/16 3 X 5/16			148	8	4		1	-						4		L	 	+ +					4							
47 48	DO DO		8645					158	4		<u> </u>	1				-		4														 			_
_			P1					72	4	4	4	4	4	4	4	4	4	4	 				1				4	 							
50	DO PLATE		P2					40			 - 	T	<u> </u>	· ·	1	<u> </u>	T —	4	4	4	ц	4	4	4	4	4	8	8	д	я	R	8	8	В	8
-	RIVET	43-6353,08-23			7/8	2 1/		,57	324	324	324	324	324	324	324	104	104	548	516		408	408	476		24	24	543	516	516	408	408	376	376	24	24
52	00	43-6353.08-25			7/8	2 1/		.62	192	192	192	192	192	192	192		192	432	432		432	432	432	452	416	416	369	368	368	368	368	368	368	352	352
53	00	43-6353.08			7/8	2 3/		.66				1						624			416	416	352			208	784		720		576		312		368
54	DO DO	43-6353.08-3	•		7/8	3.	-	.70	16	16	16	16	16	16	16	16	16		1		1.2.2	1													200
74																																			

PILE LENGTH TO BE DETERMINED BY FIELD CONDITIONS

SHEET
GENERAL NOTES 154
SYMBOLS 155
STEEL PILE BENTS
AND PIERS 209,210,211

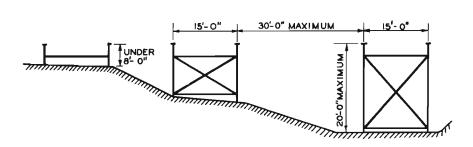
1														_		П																	
- 1					_					1	ENTS FO	R 15' TO	30' SPA			 	BRACED	STEEL PI	LE PIER	S FOR 35	' TO 45	SPANS					1	T	R FOR 50	1 1			
1				BENT OR PIE			20'	18'	16'	14"	121	10,	8'	6'	Ħ,	20'	18'	16'	141	12'	10'	81	6'	4	201	18'	16'	14'	12'	10'	8'	51	41
LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH W	UNIT EIGHT OUNDS)					QUANTIT	r								QUANTITY									QUANTIT	Υ			
1	CAP BEAM	48-2900.18-047	8649	18 I 42.7	11'-3"	480										4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	Д
2	CONNECTION PLATE	47-7844.05	Ρ5	5 1/2 x 1/2	1'-3 1/4"	13										8	9	8	8	8	8	8	8	8	16	16	16	16	16	16	16	16	16
3	CAP BEAM	48-3790.19-43	8650	18 ⊑ 42.7	11'-3"	480										ц	ц	4	4	4	4	ц	4	#	4	4	4	4	11	4	4	4	4
4	DO	49-3790.15-34	8651	15 □ 33.9	11'-0"	572	4	4	4	4	4	4	4	4	4																		
5	DIAPHRAGM		8653	12X12 I 53	1'-3"	66										8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
6	DO		8654	12X12 I 53	1'-0*	53	4	4	4	4	4	4	4	ц	4					l										<u> </u> '	<u> </u> '		
7	DO	48-2900.18-077	3652	18 I 77	2'-6 1/2"	196						•				4	4	ц	4	4	4	4	4	ц	8	8	8	8	8	8	8	8	8
8	STIFFENER PLATE	47-7844.05	P6	PL 4 X 1/2	1'-4 1/2"	9										16	16	16	16	16	16	16	16	16	32	32	32	32	32	32	32	32	32
9	SHELF ANGLE	48-2550.4-035	8647	L4 X 3 X 5/15	0'-4"	2	8	8	8	3	3	8	8	8	8	16	15	16	16	15	16	16	16	16	16	16	16	16	16	16	16	16	16
10	BEARING PLATE	47-7844.07	Р3	PL 15 X 3/4	1'-7"	60	4	4	ä	4	4	4	4	4	4							\vdash	_	igsquare		ļ				↓	<u> </u>		
11	.00	47-7844.07	Р4	PL 10 X 3/4	1'-7"	40										4	4	4	4	4	4	4	4_	4	8	8	8	8	. 8	8	8	8	8
12	SPLICE ANGLE	48-2550.4-035		L4 X 3 X 5/16	2'-0"	14					<u> </u>	-				4	ц	4	4	ц	4	4			4	4	4	4	44	4	4		-
13	CONNECTOR	47-7844.05		PL 12 X 1/2	1'-8"	54									-	3	8	8				\vdash			8	8_	8		 '	─ ──	 		-
14	00	47-7844.05	8656	PL 12 X 1/2		26	8	3	8	5	3	8	3	8	8				ļ.—										 	igwdapsilon	<u> </u>		-
15		47-7844.05		PL 12 X 1/2		26	8	8	3	8	. 3	8	8											1		-			+	$\vdash \vdash$	 '		-
16	DØ	47-7844.05	8658	PL 12 X 1/2		20				ļ						16	15	15	16	16	15	16	8	8	16	16	16	16	16	16	16	16	8
17	DO	47-7844.05		PL 8 X 1/2	1'-6"	50										24	16	16	8	8					24	16	16	8	8	$\vdash \vdash$	 '		
18.	DO	47-7844.05	8550	PL 8 X 1/2	1'-0"	14										16	15	16	15	15	16	16			16	16	16	16	16	16	16	16	—
19	00	47-7844.05	8661		0'-5"	7					 		-		-	8	8	3	9	8	8	8			8	8	8	8	8	8	8	8	ц '
20	STRUTS AND BRACES	48-2900.08-024		1/2 8 I 24		118		_				-			.	12	12	12	3	8	8	8	4	4	12	12	12_	8	8	8	8	8	1
-11-	DO	48-2900.08-024 48-2550.4-035		1/2 8 I 24		168 30	8	8	8	В	8	8	8	4	4					16		В			32	16	-	15	16	\vdash	8		
22	J <u>00</u>	48-2550.4-035	8614	L4 X 3 X 5/16		41									1	32	16	24	15	10	А			1	- 72	8	24	15_	10	8	 " -		
23	00		8622	L4 X 3 X 5/16		20									1	В	<u>3</u>	-	٠,	8	8	А			-	8	8	8	8	8	8	8	_
24	_	48-2550, 4-035	8625	L4 X 3 X 5/16		76					 					8	8	- 8	,			8	- 0		•		8	l °	\vdash		8	a	
25 26	00	48-2550.4-035		L4 X 3 X 5/16		84											8	8			8	8				8	-		┼──	8	├ ゜	-	
27	DO	48-2550.4-035		L4 X 3 X 5/16		90						 	1			16	8	8	3	8					16	8	8	В	8	٢			
28	00	48-2550.4-035				97							A			1"		<u> </u>	<u> </u>			16					⊢ •		\vdash	\vdash	16		-
29	00	48-2550.4-035		L4 X 3 X 5/16		10 <i>5</i>						8	8								15	•							\vdash	16		$\overline{}$	
30	90	48-2550.4-055		L4 X 3 X 5/16		108					4				1					8									8		1		
31	DO	48-2550.4-035		L4 X 3 X 5/16		1.2					4	9								3				T 1					3			$\overline{}$	
32	DO	48-2550.4-035				115				4	8				 				8									8					
33	DO	48-2550.4-035		L4 X 3 X 5/16		119			4									А									8	T				ī	
34	00	48-2550, 4-035		L4 X 3 X 5/16		123				12								Ĭ	а							_		9					
35	00	48-2550.4-055		L4 X 3 X 5/16	-	127		4						_			8							\vdash		8							
36	00	48-2550.4-035		L4 X 3 X 5/16	18'-6"	134	4		8							ı									8						<u></u>		
37	DO	48-2550.4-035		L4 X 3 X 5/15		157	İ		4								-	3					-				8				·	<u> </u>	
38	00	48-2550.4-035	8642	L4 X 3 X 5/15		140		8									-											Ī			<u> </u>		
39	00	48-2550.4-035		L4 X 3 X 5/15		148		Ľ.									А									А						$\overline{}$	
40	00	48-2550.4-035	8645	L4 X 3 X 5/15		155	8	-																		<u> </u>			\vdash				
41	DO	48-2550.4-035		L4 X 3 X 5/16		158	4			-						8									8				\vdash	\vdash		$\overline{}$	
			4047		"		-					-				<u> </u>		1							Ť			 		\vdash	\vdash	$\overline{}$	T
42	WELDING ROD (POUNCS)	46-3772.2-7		3/16	- 1	И	45	45	45	45	45	45	45	50	25	145	136	136	125	125	115	115	85	61	170	161	161	150	150	140	140	108	86

 $^{^{1\!\!1\!\!1}}$ PILE LENGTH TO BE DEFERMINED BY FIELD CONDITIONS.

COMPANION SHEETS

SYMBOLS BILL OF MATERIALS FABRICATION DRAWING

GENERAL NOTES



TRANSVERSE ELEVATION

DIAGRAM SHOWING LONGITUDINAL BRACING AND HEIGHT AND SPAN LIMITATIONS OF BENTS

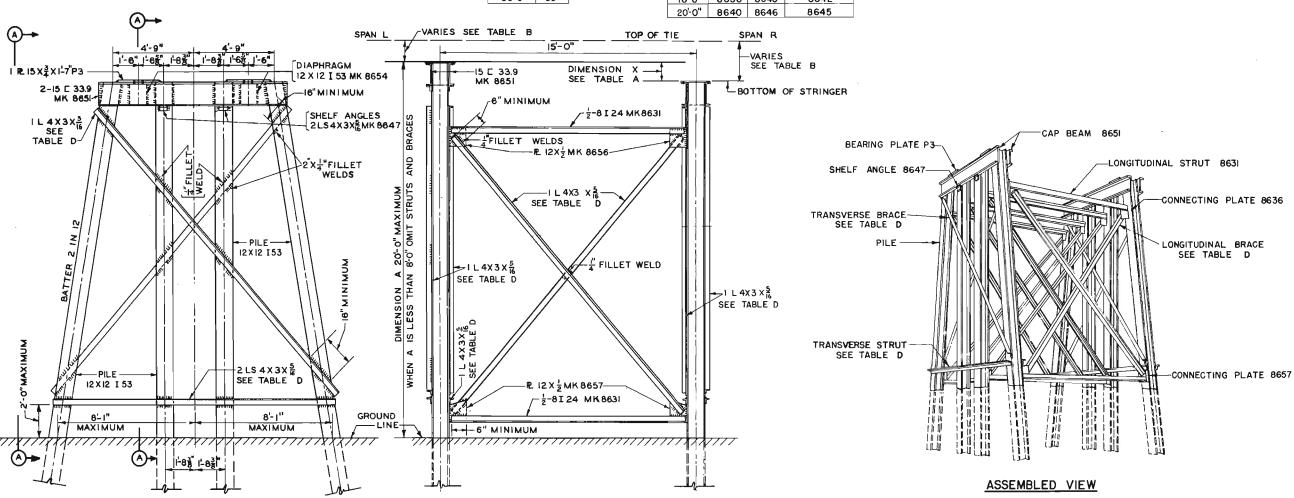
<u>.e a</u>	1		
DIM	IENSIO	N X	
	SPAN	R	
15 ¹ -0"	20'-0"	25 ' 0'	30'-0"
0"	57"	8 <mark>7</mark> "	1-08 1-08
5g"	0*	3"	6 <mark>计</mark> "
87"	3"	0"	3 4
1-0 g	6½"	3 ¹ 4	0"
	DIM 15-0" 0" 58" 87"	DIMENSION SPAN 15'-0" 20'-0" 0" 57'' 0" 57'' 0" 87'' 3"	DIMENSION X

	C	
MAXIMUM		
LOA	D	
SPAN BETWEEN	TONS PER	
TOWERS	PILE	
15-0"	27	
20'-0"	30	
25 <u>'</u> 0"	33	
30'-0"	35	

ELEVATION A-A

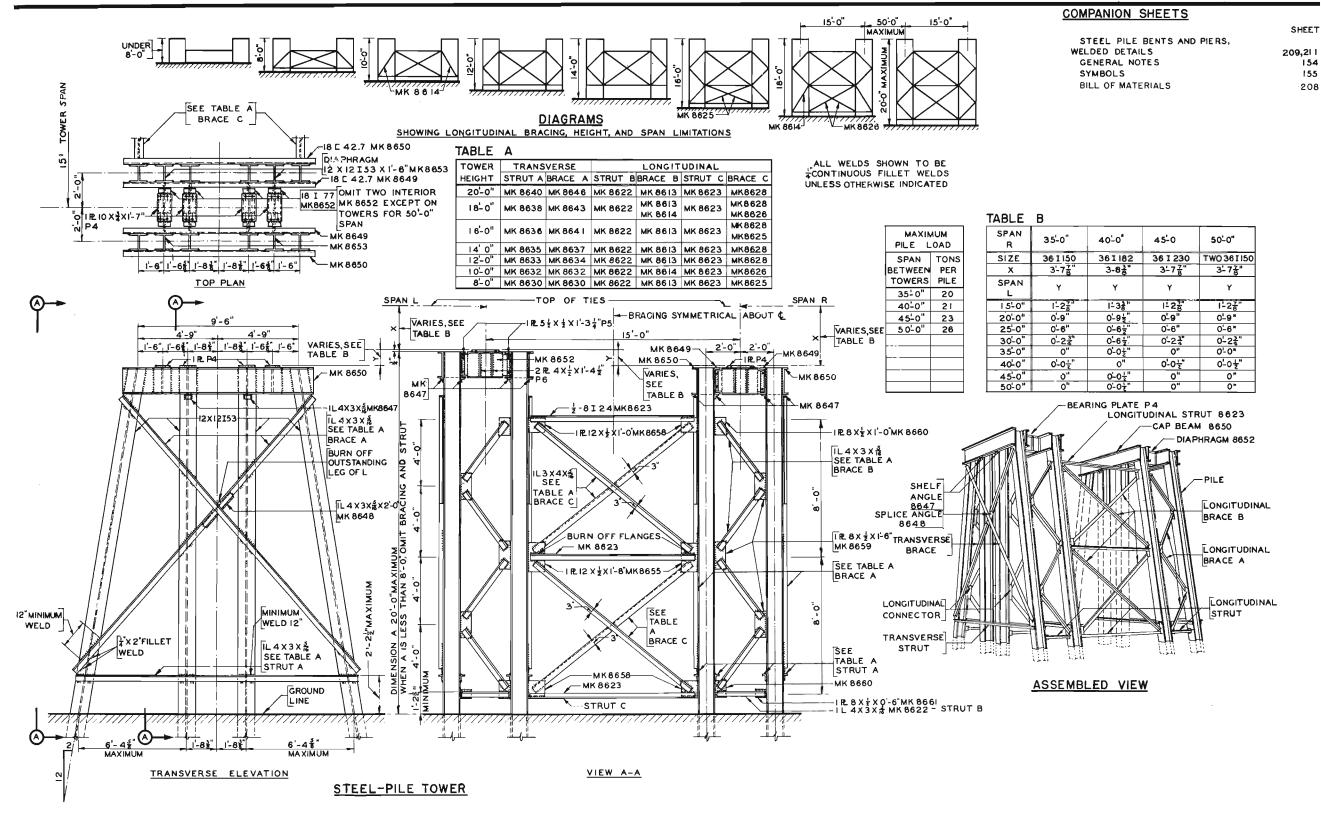
TABLE	8									
DISTANCE	FROM TOP OF	TIE TO BOTTOM								
OF STRINGER FOR VARIOUS SPANS										
SPAN	STEEL-	TOP OF TIE								
LENGTH	STRINGER	TO BOTTOM								
	SIZE	OF STRINGER								
15-0"	21 I 63	2'-5"								
20'-0"	27 I 91	2 <u>'</u> -10g"								
25-0"	30 I 108	3'-1 7 "								
30 ' -0"	33 I 132	3'-5 h**								

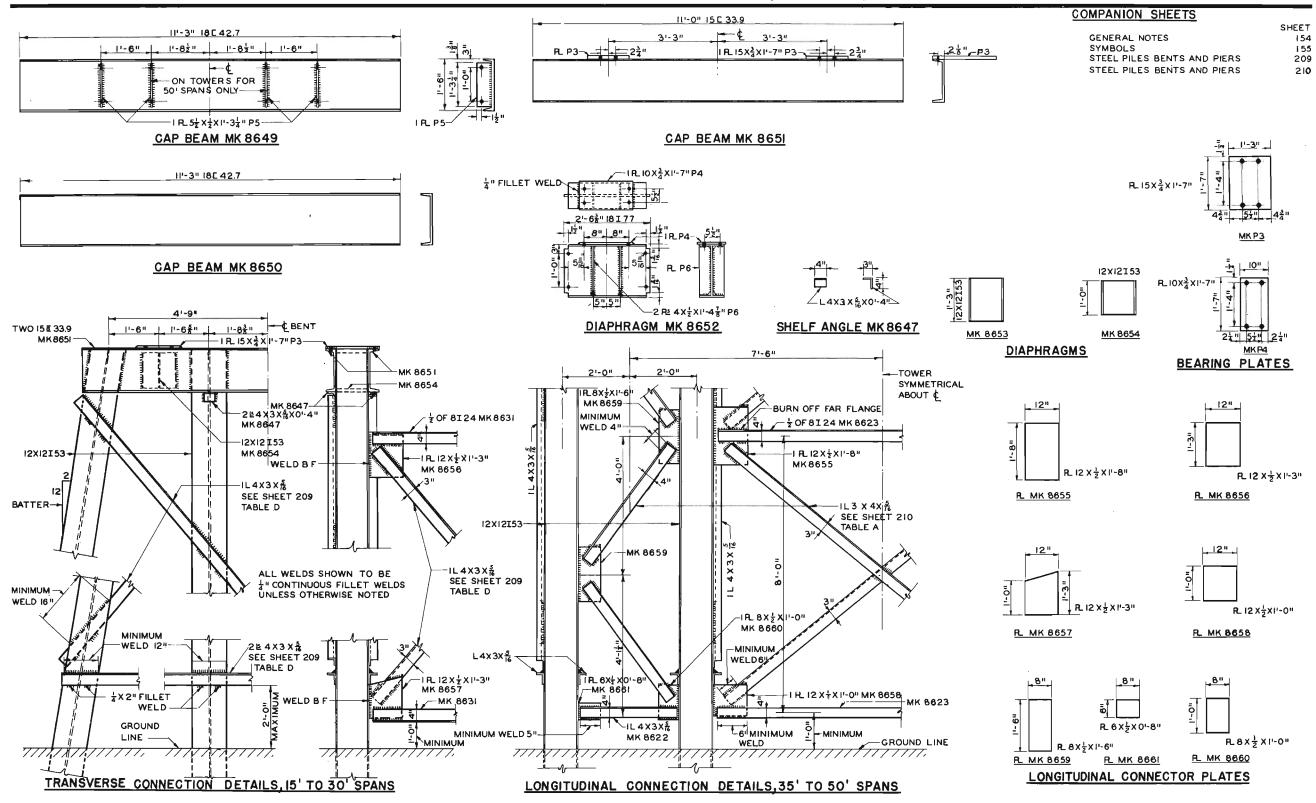
IABLE	U									
	F	PIECE MARK								
TOWER	TRANS		LONGITUDINAL							
HEIGHT	STRUT	BRACE	BRACE							
8'-0"	8630	8630	8632							
10'-0"	8632	8632	8634							
12'-0"	8633	8634	8635							
14'-0"	8635	8637	8637							
16-0"	8636	8641	8640							
18'-0"	8638	8643	8642							
20'-0"	8640	8646	8645							



154

155





GROUND

LINE

GROUND

DRIFT BOLT 3 × 22" D22

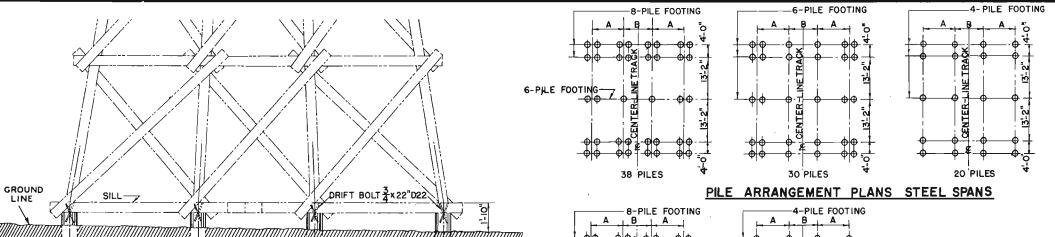
DRIFT BOLT

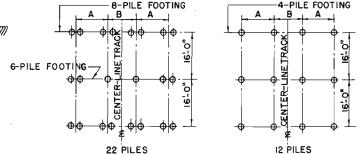
- ء x 22" D22-

4-PILE FOOTING

6-PILE FOOTING

8-PILE FOOTING





PILE ARRANGEMENT PLANS TIMBER SPANS 22-PILE FOUNDATION FOR TOWERS 20'TO 80'HIGH

12-PILE FOUNDATION FOR TOWERS 15'TO 20'HIGH

TOWER HEIGHT AND DIMENSIONS

HEIGHT OF TOWER	А	В	HEIGHT OF TOWER	A	В
13'- 4"	3'- 5 ½"	4'- 113"	46'	7'-62"	7'-8"
16'	3'- 9-½"	5'- 2"	48'	7'-97"	7'-10"
18'	4-0-	5-4"	50'- 10"	8-14"	8- I
20'	4'- 3 2"	5-6"	53' .	8-5"	8-3"
22'	4-6 2	5-8"	55'	8-8"	8-5
24'	4'-9+	5- 10	57'	8'-11"	8'-7"
25'- 10"	5-04"	6-04"	59'	9'-2"	8'-9"
28'	5-32	6'- 2"	61'	9'-5"	8'-11"
30'	5-62	6'- 4"	63'-4"	9'-8 2 "	9-134
32'	5-9-	6'-6"	65'	9'-11"	9-3
34'	6'-0 ½"	6'-8"	67'	10'-2"	9-5"
36'	6'- 3 1 "	6'-10"	69'	ю'-5"	9'-7"
38'- 4"	6-7"	7'- 0 3 "	71'	10'- 8"	9-9"
40'	6'-9 1 "	7- 2"	73'	10'-11"	9'-11"
42'	7-02	7'-4"	75 <u>'-</u> 10"	11- 34"	10-24
44'	$7' - 3\frac{1}{2}''$	7'-6"			

COMPANION SHEETS

SHEET TIMBER TOWERS FOR TIMBER SPANS 175 TIMBER TOWERS FOR STEEL SPANS 179 GENERAL NOTES 154 155 SYMBOLS

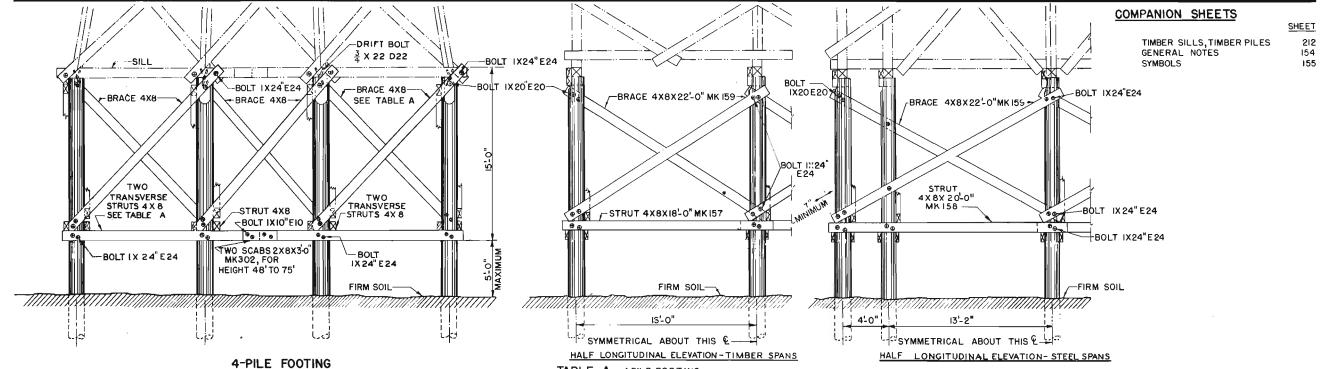
PILE SCHEDULE FOR TOWERS WITH STEEL SPANS

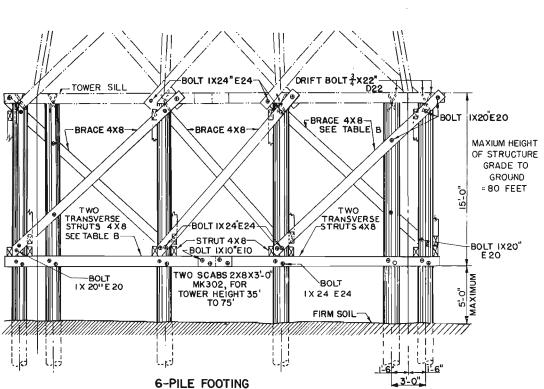
SPAN	TOWER	PILES PER
LENGTH	HEIGHT	TOWER
	30' TO 80'	38
50'	20' TO 30'	30
	15' TO 20'	20
	35 ' TO 80'	38
45'	25' TO 35'	30
	15' TO 25'	20
	40' TO 80'	38
40'	30' TO 40	30
	15' TO 30'	20
	45' TO 80'	38
35 '	35' TO 45'	30
	15' TO 35'	20
	55' TO 80'	38
30'	40' TO 55'	30
	15' TO 40'	20
	65' TO 80'	38
25'	45'TO 65'	30
	15' TO 45'	20
	55' TO 80	30
20'	15'TO 55'	20

BILL OF MATERIALS

MATERIALS FOR FOUNDATION UNDER ONE TOWER

						UNIT	12- PIL FOUNDA		22 -P IL FOUNDAT		20-PIL FOUNDA		30-PIL FOUNDAT		38-PIL FOUNDAT	
LINE	DESCRIPTION	STOCK NO	MARK	SIZE	LENGTH	WEIGHT	QUANTITY	WEIGHT	QUANTITY	WEIGHT	QUANTITY	WEIGHT	QUANTITY	WEIGHT	QUANTITY	WEIGHT
1	PILE						12		22		20		30		38	
2	DRIFT BOLT	43-1636.07-22	D 22	<u>3</u> 4	22"	3 LB	24	72 LB	44	132 LB	40	I20 LB	60	180 LB	76	228LB

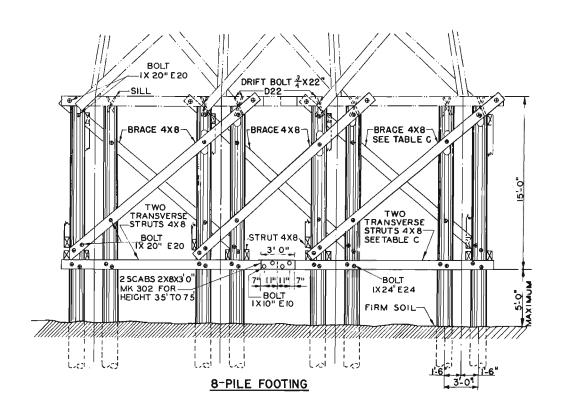


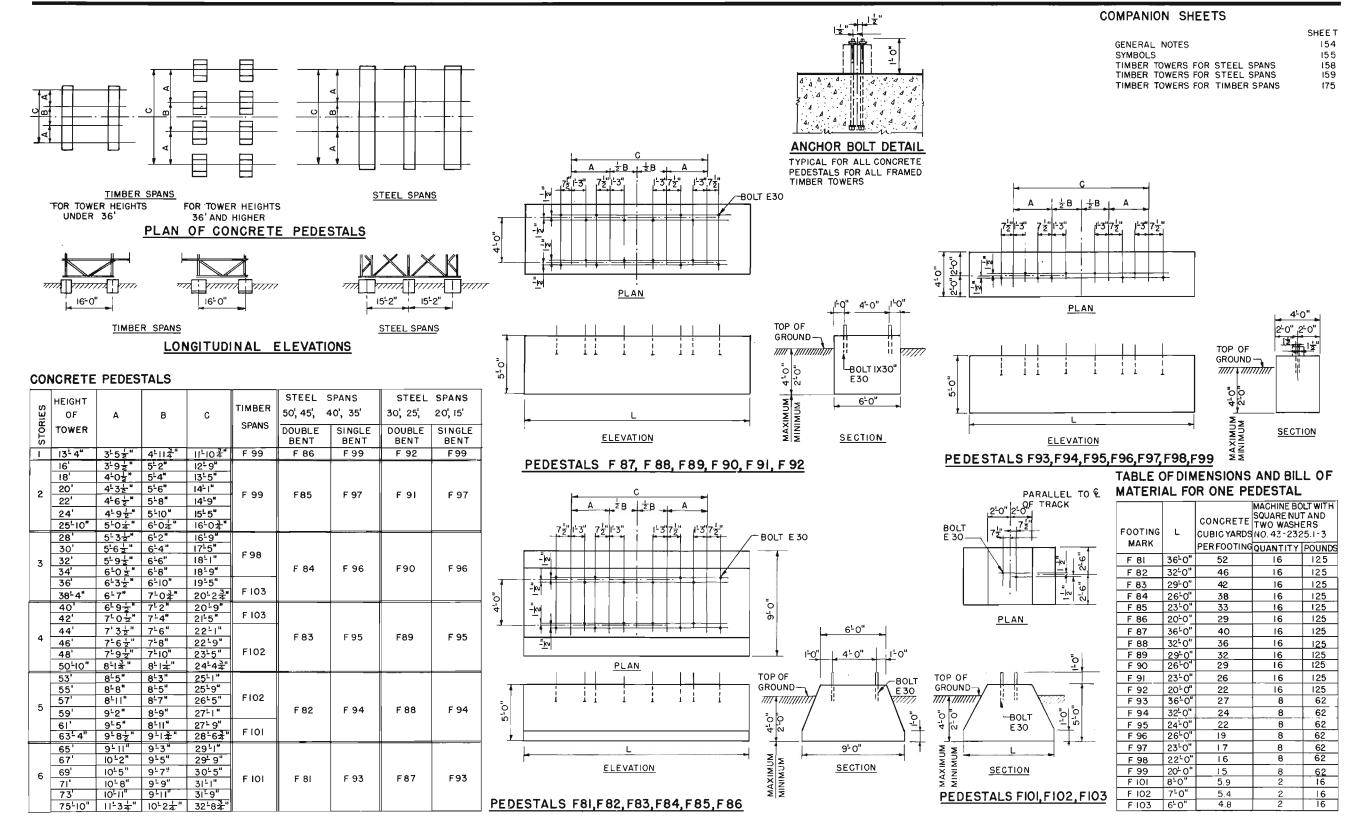


ABLE A	4-PIL	E F007	TING						
LENGTH OF TRANSVERSE BRACING									
TOWER	BRAC	E	STRUT						
HEIGHT	LENGTH	MARK	LENGTH	MARK					
15'T021'	16'-0"	156	16'-0"	156					
23'TO27'	16'-0"	156	18'-0"	157					
29'TO33'	16'-0"	156	20'-0"	158					
35'T040'	18-0"	157	22'-0"	159					
42'T046	18'-0"	157	24'-0"	160					
48'TO 56'	18'-0"	157	14'-0"	155					
58'T069'	20'-0"	158	16'-0"	156					

LENGTH OF TRANSVERSE BRACING									
TOWER	BRAC	E	STRU	Т					
HEIGHT	LENGTH	MARK	LENGTH	MARK					
15'T021'	16'-0"	156	20'-0"	158					
23'T027'	18'-0"	157	22'-0"	159					
29'T033'	18'-0"	157	24'-0"	160					
35'T040'	18-0"	157	14'-0"	155					
42'TO 46'	18'-0"	157	14'-0"	155					
48'TO 56'	20'-0"	158	16-0"	156					
58'T069'	20'-0"	158	18'-0"	157					

C 8-PIL 8	FOOT	ING						
LENGTH OF TRANSVERSE BRACING								
BRAC	Ε	STRUT	Γ					
LENGTH	MARK	LENGTH	MARK					
18'-0"	157	20'-0"	158					
18'-0"	157	22'-0"	159					
20'-0"	158	24-0"	160					
20-0"	158	14'-0"	155					
20'-0"	158	14'-0"	155					
20'-0"	158	16'-0"	156					
22'-0"	159	18'-0"	157					
	OF TRANS BRAC LENGTH 18'-0" 18'-0" 20'-0" 20'-0" 20'-0"	OF TRANSVERSE BRACE LENGTH MARK 18'-0" 157 18'-0" 158 20'-0" 158 20'-0" 158 20'-0" 158	BRACE STRUT LENGTH MARK LENGTH 18'-0" 157 20'-0" 18'-0" 157 22'-0" 20'-0" 158 24'-0" 20'-0" 158 14'-0" 20'-0" 158 16'-0"					

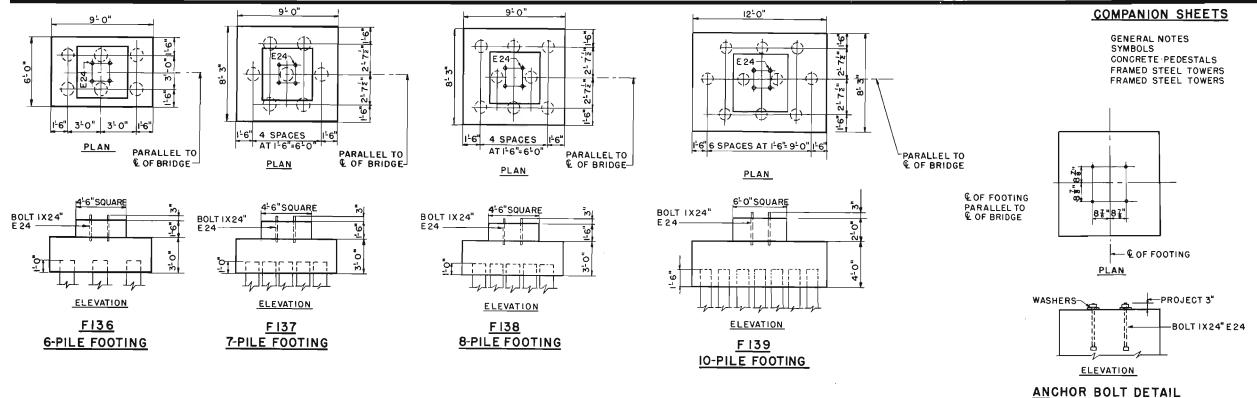




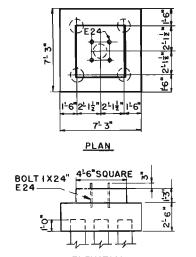
SHEET

154 155

216 184 185



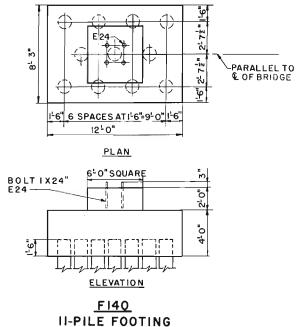


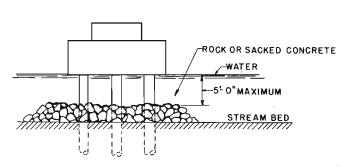




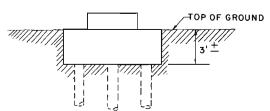
	BILL OF MA	TERIA	L FOR	ONE F	OOTING
I	HEIGHT	FOOTING	NUMBER	CONCRET	MACHINE WITH SO

ADJACENT SPAN	HEIGHT OF TOWER	FOOTING MARK NUMBER	NUMBER OF PILES	CONCRETÉ	MACHINE BOLT IX24" E24 WITH SQUARE NUT AND TWO WASHERS STOCK NUMBER 43-2325.1 -24		
				YARDS)	QUANTITY	POUNDS EACH	
25'	41' OR LOWER	F135	5	5.8	4	6.5	
	43' TO 57'	F136	6	7.1	4	6.5	
	59' TO 77'	F137	7	9.3	4	6.5	
30'	21' OR LOWER	F 135	5	5.8	4	6.5	
	23' TO 41'	F 136	6	7.1	4	6.5	
	43' TO 77'	F 137	7	9.3	4	6.5	
35'	21'OR LOWER	F 135	5	5.8	4	6.5	
	23' TO 41'	F 136	6	7.1	4	6.5	
	43' TO 57'	F 137	7	9.3	4	6.5	
	59' TO 77'	F 138	8	9.3	4	6.5	
40'	21' OR LOWER	F 136	6	7. l	4	6.5	
	23' TO 41'	F 137	7	9. 3	4	6.5	
	43' TO 77'	F 138	8	9. 3	4	6.5	
45'	21'OR LOWER	F 137	7	9.3	4	6.5	
	23' TO 57'	F 138	8	9.3	4	6.5	
	59' TO 77'	F 139	10	17.3	4	6.5	
50'	41'OR LOWER	F 138	8	9.3	4	6.5	
	43' TO 57'	F 139	10	17.3	4	6.5	
	59' TO 77'	F 140	11	17.3	4	6.5	





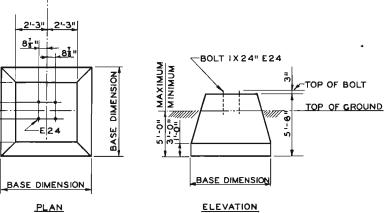
TYPICAL ELEVATION **FOOTINGS IN WATER**



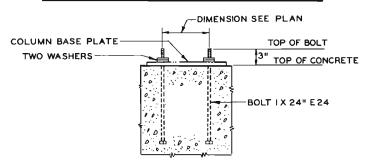
TYPICAL ELEVATION FOOTINGS IN SOIL

SHEET GENERAL NOTES 154 155 SYMBOLS

PARALLEL TO & OF BRIDGE -BOLT 1X 24" E24



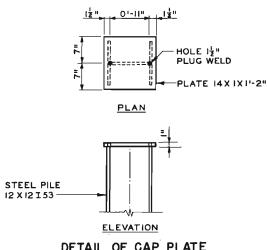
CONCRETE PEDESTAL FOR STEEL TOWERS

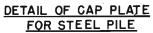


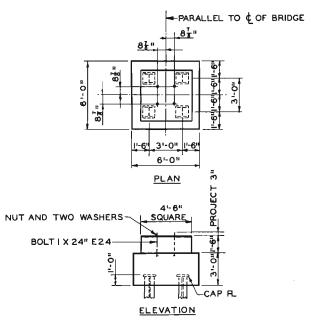
TYPICAL ANCHOR BOLT DETAIL

TABLE OF DIMENSIONS FOR ONE PEDESTAL

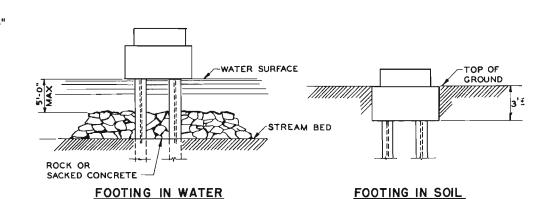
ADJACENT SPAN	HEIGHT OF TOWER	MARK	BASE DIMENSION	CUBIC YARDS CONCRETE	STOCK NO 43	IX 24" WITH ID TWO WASHERS . 2325.100-240
(FEET)	1011411				QUANTITY	POUNDS
25	39'OR LOWER	F123	9'-0"	10.8	4	26
2.5	41' TO 77'	F124	10'-0"	12.9	4	26
30	39'OR LOWER	F123	9'-0"	10.8	4	26
30	41' TO 77'	F124	10'-0"	12.9	4	26
	21'OR LOWER	F123	9'-0"	10.8	4	26
35	23' TO 57'	F124	10'-0"	12.9	4	26
	59' TO 77'	F125	111-0"	15.1	4	26
40	39'OR LOWER	F124	10'-0"	12.9	4	26
40	41' TO 77'	F125	11'-0"	15.1	4	26
4.5	21' OR LOWER	F124	10'-0"	12.9	4	26
45	23' TO 77'	F 125	11'-0"	15,1	4	26
5.0	21'OR LOWER	F124	10'-0"	12.9	4	26
50	23' TO 77'	F125	11'-0"	15.1	4	26







4-PILE FOOTING



REQUIRED BEARING CAPACITY OF PILES

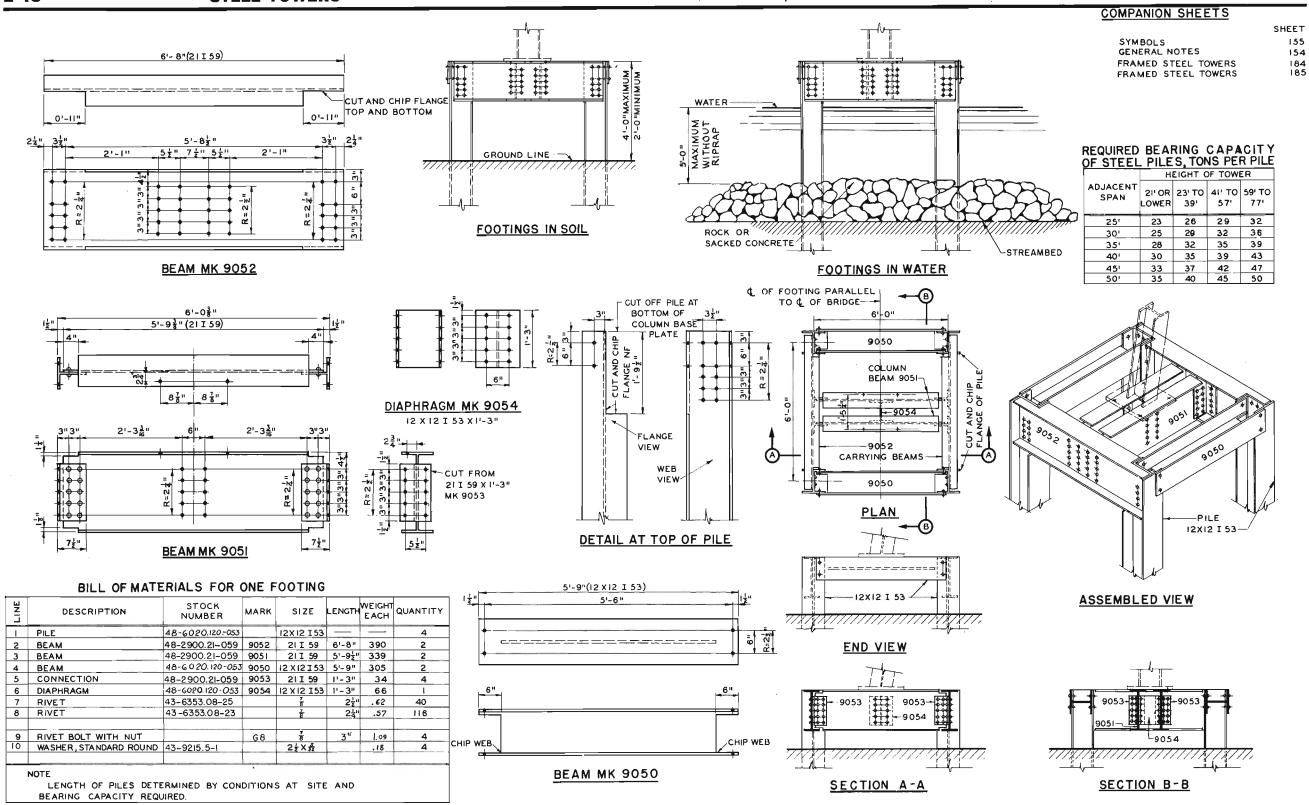
TONS PER PILE

ONS FER FILE									
ADJACENT	HEIGHT OF TOWER								
SPAN (FEET)	21' OR LOWER	23 ' TO 39 '	41' TO 57'	59' TO 77'					
251	23	26	29	32					
301	25	29	32	36					
351	28	32	35	39					
401	30	35	39	43					
451	33	37	42	47					
501	35	40	45	50					

BILL OF MATERIALS FOR ONE FOOTING WITH STEEL PILES

DESCRIPTION	STOCK NUMBER	MARK	SIZE	LENGTH	EACH	NUMBER OF PIECES	UNIT	AMOUNT
CONCRETE							CU YDS	5. I
PILE	48-6020.120.053		12X12I53			4		
CAP PLATE	47-7844.1		14 X I	1'-2"	55	4		
MACHINE BOLT WITH SQUARE								
NUT AND TWO WASHERS	43-2325.100-240	E 24	I	24"	6.4	4	POUNDS	26
WELDING ELECTRODE	46-3772.25-5		<u>7</u> 32				POUNDS	4

LENGTH OF PILES DETERMINED BY CONDITIONS AT SITE AND BEARING CAPACITY REQUIRED.



9003 |2X|2 | 53 | 6-6"

48-2900.21-059

48-6020.12-053

9004 I2XI2I53 6-6" 345

9005 | 12X|2 | 153 | 6'-6" | 345

9007 21 1 59 9-2" 541

9008 |2X|2|53 |9-2" | 243

9009 12X12I53 8-6" 450

9010 12X12I53 8-6" 450

90II |2X|2I53 8-6" 450

9013 | 12X12 | 153 | 16" | 80 9016 | 12X12 | 153 | 16" | 80

9030 |2X|2I53 |-6" 53

48-2900.2I-059 903I 2I I 59 I-II"

G 5

G8

345

50 UNIT WEIGHT

94

2½" .97 2½" 1.00 3 1 1.09 .97

2

48

24

16

2

4

2

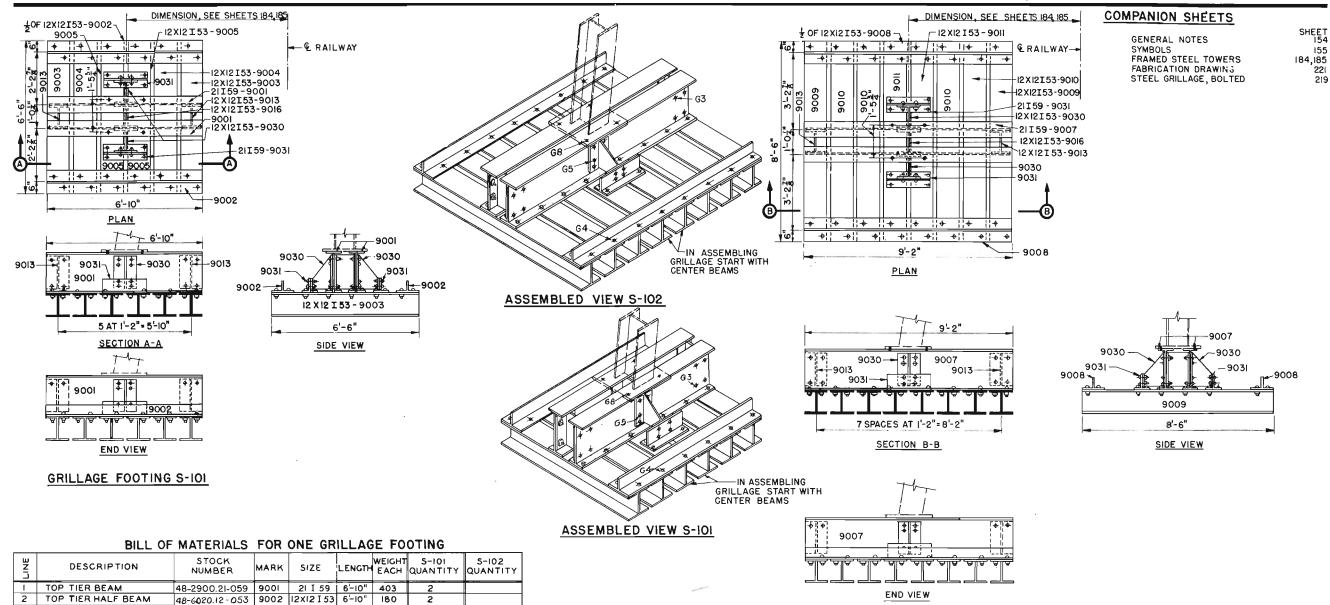
1

56

28

16

155



GRILLAGE FOOTING S-102

SCHEDULE FOR SELECTION OF GRILLAGE FOOTING FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

- ON MILOWIT OF AIR ELECTION AND TOWER TIETOTT										
	FOOT	INGS	ON S	OIL	FOOTINGS ON ROCK					
SPAN	HEIGH	IO TE	TOV	VER	HEIGHT OF TOWER					
BETWEEN	UP	23'	41'	59'	UP	23'	41'	59'		
TOWERS	то	TO	то	то	то	TO	то	TO		
	21'	39'	50'	77'	21'	39'	59'	77'		
15'TO 25'	S-102	S-102	S-102	S-102	S-10I	S-101	S-101	S-10I		
30'	S-102	S-102	S-102	S-103	S-101	S-101	S-101	S-102		
35'	5-102	5-102	S-103	S-103	S-101	S-101	5-102	S-102		
40'	S-102	S-103	S-103	S-103	S-101	S-102	S-102	\$-102		
45'	S-102	S-103	S-103	S-103	S-101	S-102	S-102	5-102		
50'	S-103	S-103	S-103	S-103	S-102	S-102	S-102	S-102		

3 BOTTOM TIER BEAM

4 BOTTOM TIER BEAM

9 BOTTOM TIER BEAM

6 TOP TIER BEAM

SEPARATOR 12 SEPARATOR

13 BRACE

14 BRACE

15 RIVET BOLT

16 RIVET BOLT

17 RIVET BOLT

BOTTOM TIER BEAM

TOP TIER HALF BEAM

BOTTOM TIER BEAM

BOTTOM TIER BEAM

18 RIVET BOLT AND WASHER

(A)

221

TABLE FOR SELECTION OF GRILLAGE FOOTINGS FOR KNOWN SPAN LENGTH AND TOWER HEIGHT

VIOMIA	SPAN	LEN	GIT .	ANU	IOME	K HE	IGHI		
	FOOT	INGS	ON S	OIL	FOOTINGS ON ROCK				
SPAN	HEIGHT OF TOWER				HEIGHT OF TOWER				
BETWEEN	UP	23'	41'	59'	UP	23'	41'	59'	
TOWERS	то	то	то	то	то	то	то	то	
	51,	39'	50'	77'	21'	39'	59'	77'	
15' TO 25'	S-102	S-102	S-102	S-102	S-101	S-101	S-101	S-101	
30'	S-102	S-102	S-102	S-103	S-101	S-101	9-101	S-102	
35'	S-102	S-102	S-103	S-103	S-101	S-101	s-102	S-I02	
40'	S-I02	S-103	s-103	S-103	S-101	S-102	S-102	S-102	
45'	S-102	S-103	S-103	S-I03	S-101	S-I02	S-102	\$-102	
E 01	C 103	6 100	C 100	C 103	C 100	6 100	20	6. 100	

COMPANION SHEETS

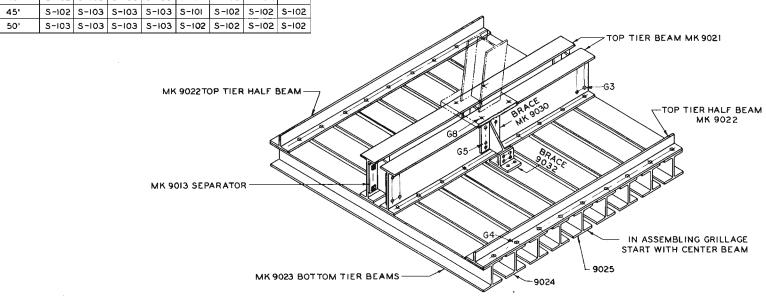
SHEET

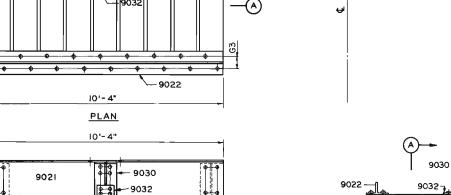
FRAMED STEEL TOWERS
GENERAL NOTES
SYMBOLS

SYMBOLS

SHEET
184,185
154
154
155

FABRICATION DRAWING





DIMENSIONS SEE SHEET 184,185

9023 9024 9024 9024 9025 9024 9024 9024 9023

9021

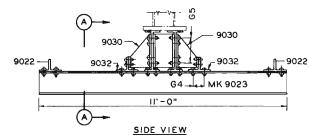
30 8 8

8 SPACES AT 1'-2" = 9'-4"

SECTION A-A

END VIEW
GRILLAGE FOOTING S-103

9021



BILL OF MATERIALS FOR ONE GRILLAGE FOOTING S-103

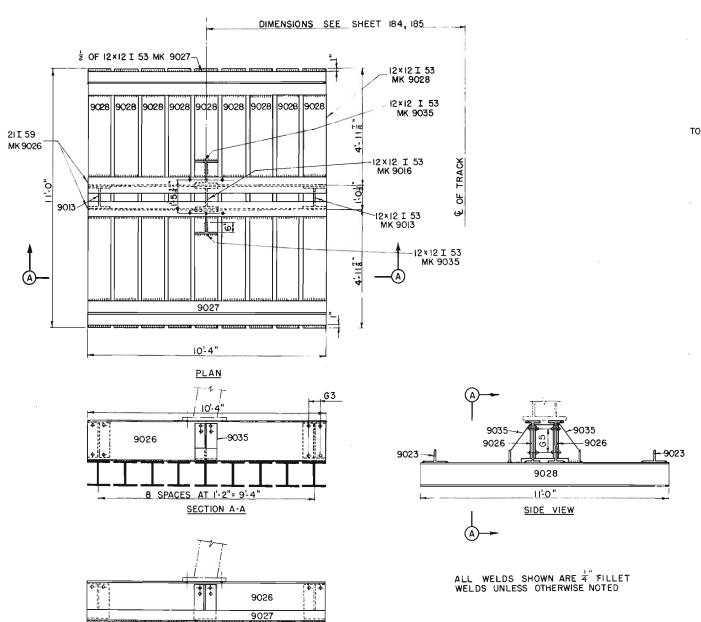
ASSEMBLED VIEW

LINE	DESCRIPTION	STOCK NO	MARK	QUANTITY	SIZE	LENGTH	WEIGHT EACH
ł	TOP TIER BEAM	48-2900.21-059	9021	2	21159	10'-4"	610
2	TOP TIER HALF BEAM	48-6020.12-053	9022	2	½-12×12 I 53	10'-4"	274
3	BOT TOM TIER BEAM		9023	2	12×12 I 53	11 '~ 0"	583
4	BOTTOM TIER BEAM		9024	6	12×12 I 53	11'- 0"	583
5	BOTTOM TIER BEAM		9025	1	12×12 I 53	11'- 0"	583
6	SEPARATOR		9013	2	12×12 I 53	1'-6"	80
7	SEPARATOR		9016	1	12×12 I 53	1'-6"	80
8	BRACE		9030	2	PC 12×12 I 53	1'-6"	53
9	BRACE	48-2900.21-059	9032	2	PC 21 I 59	0'-9"	22
10			I Krisovice				
Ш							TOTAL WT LBS
12	RIVET BOLT		G 3	60	78	216	56
13	RIVET BOLT		G4	32	78	21"	31
14	RIVET BOLT		G5	16	78	2 [6]	16
15	RIVET BOLT AND WASHER		Gв	4	7 B	3"	5

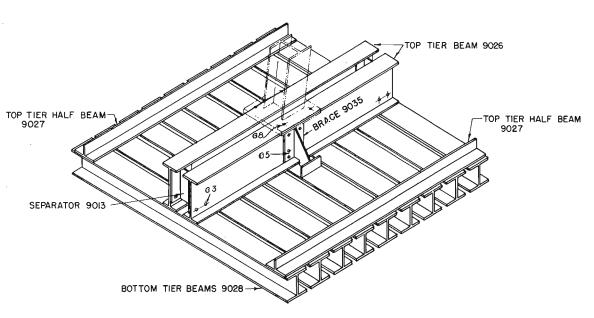
RAILWAY E-45

COMPANION SHEETS

	SHEET
GENERAL NOTES	154
SYMBOLS	155
FRAMED STEEL TOWERS	184
FRAMED STEEL TOWERS	185
FABRICATION DRAWING	221
STEEL GRILLAGE, BOLTED	219



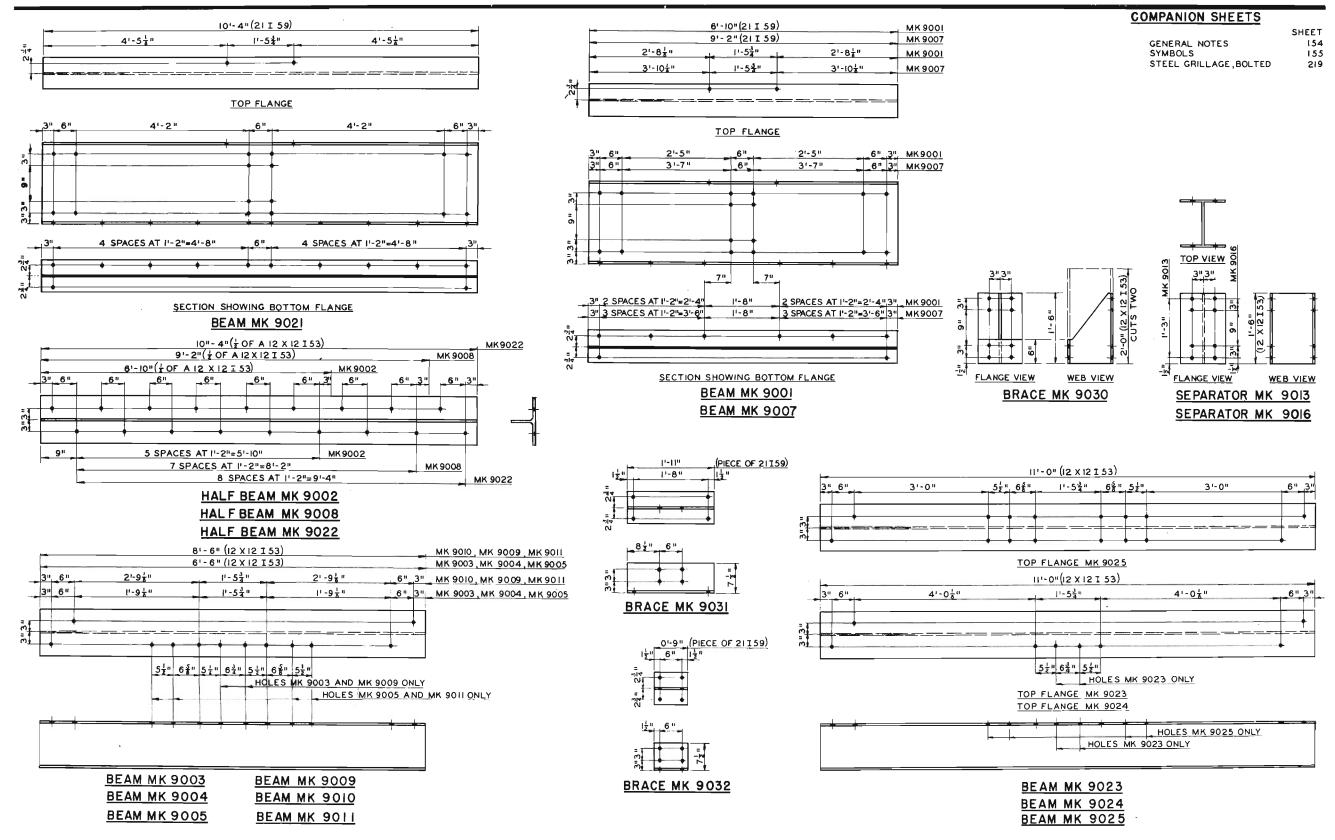
END VIEW GRILLAGE FOOTING SIG3



BILL OF MATERIALS FOR ONE GRILLAGE FOOTING S-103

ASSEMBLED VIEW

DESCRIPTION	STOCK NO	MARK	QUANTITY	SIZE	LENGTH	WEIGHT EACH
TOP TIER BEAM	48-2900.21-059	9026	2	21 I 59	10'-4"	610
TOP TIER HALF BEAM		9027	2	½-12×12 I 53	10'-4"	274
BOTTOM TIER BEAM		9028	9	12×12 I 53	11'-0"	583
SEPARATOR		9013	2	12×12 I 53	1'- 6"	80
SEPARATOR		9016	i	12×12 I 53	ı'- 6"	80
BRACE		9035	2	12×12 I 53	1'-7½"	56
						TOTAL WEIGHT
					•	POUNDS
RIVET BOLT		G 3	16	78	2 16'	15
RIVET BOLT		G 5	16	7 8	2 16	16
RIVET BOLT AND WASHER		G8	4	78	3"	5
WELDING ELECTRODE	46-3772.2-7			<u>3</u> !6		13
	TOP TIER BEAM TOP TIER HALF BEAM BOTTOM TIER BEAM SEPARATOR SEPARATOR BRACE RIVET BOLT RIVET BOLT RIVET BOLT AND WASHER	TOP TIER BEAM 48-2900.21-059 TOP TIER HALF BEAM BOTTOM TIER BEAM SEPARATOR SEPARATOR BRACE RIVET BOLT RIVET BOLT RIVET BOLT AND WASHER	TOP TIER BEAM 48-2900.21-059 9026 TOP TIER HALF BEAM 9027 BOTTOM TIER BEAM 9028 SEPARATOR 9013 SEPARATOR 9016 BRACE 9035 RIVET BOLT 63 RIVET BOLT AND WASHER 68	TOP TIER BEAM 48-2900.21-059 9026 2 TOP TIER HALF BEAM 9027 2 BOTTOM TIER BEAM 9028 9 SEPARATOR 9013 2 SEPARATOR 9016 1 BRACE 9035 2 RIVET BOLT 63 16 RIVET BOLT 65 16 RIVET BOLT AND WASHER 68 4	TOP TIER BEAM 48-2900.21-059 9026 2 21 1 59 TOP TIER HALF BEAM 9027 2 ½-12×12 1 53 BOTTOM TIER BEAM 9028 9 12×12 1 53 SEPARATOR 9013 2 12×12 1 53 SEPARATOR 9016 1 12×12 1 53 BRACE 9035 2 12×12 1 53 RIVET BOLT 63 16 7/8 RIVET BOLT G5 16 7/8 RIVET BOLT AND WASHER G8 4 7/8	TOP TIER BEAM 48-2900.21-059 9026 2 21 159 10'-4" TOP TIER HALF BEAM 9027 2 ½-12 × 12 153 10'-4" BOTTOM TIER BEAM 9028 9 12 × 12 153 11'-0" SEPARATOR 9013 2 12 × 12 153 1'-6" SEPARATOR 9016 1 12 × 12 153 1'-6" BRACE 9035 2 12 × 12 153 1'-7½" RIVET BOLT 63 16 7 2 16 216 RIVET BOLT AND WASHER 68 4 7 3"



RAILWAY

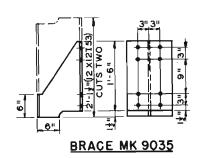
E-45

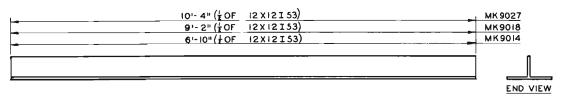
SHEET

154 155 220

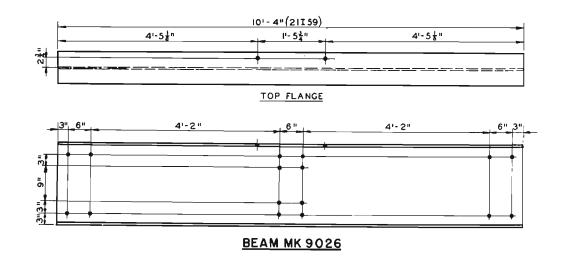
COMPANION SHEETS

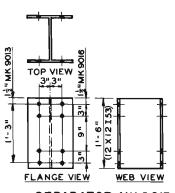
GENERAL NOTES SYMBOLS STEEL GRILLAGES,WELDED

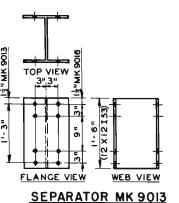




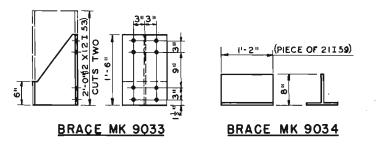
HALF BEAM MK 9014 HALF BEAM MK 9018 HALF BEAM MK 9027

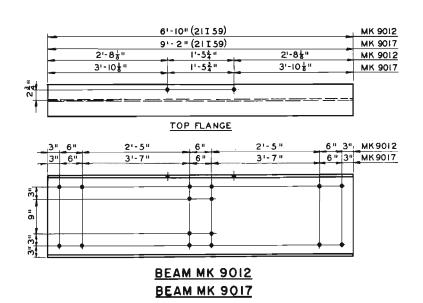


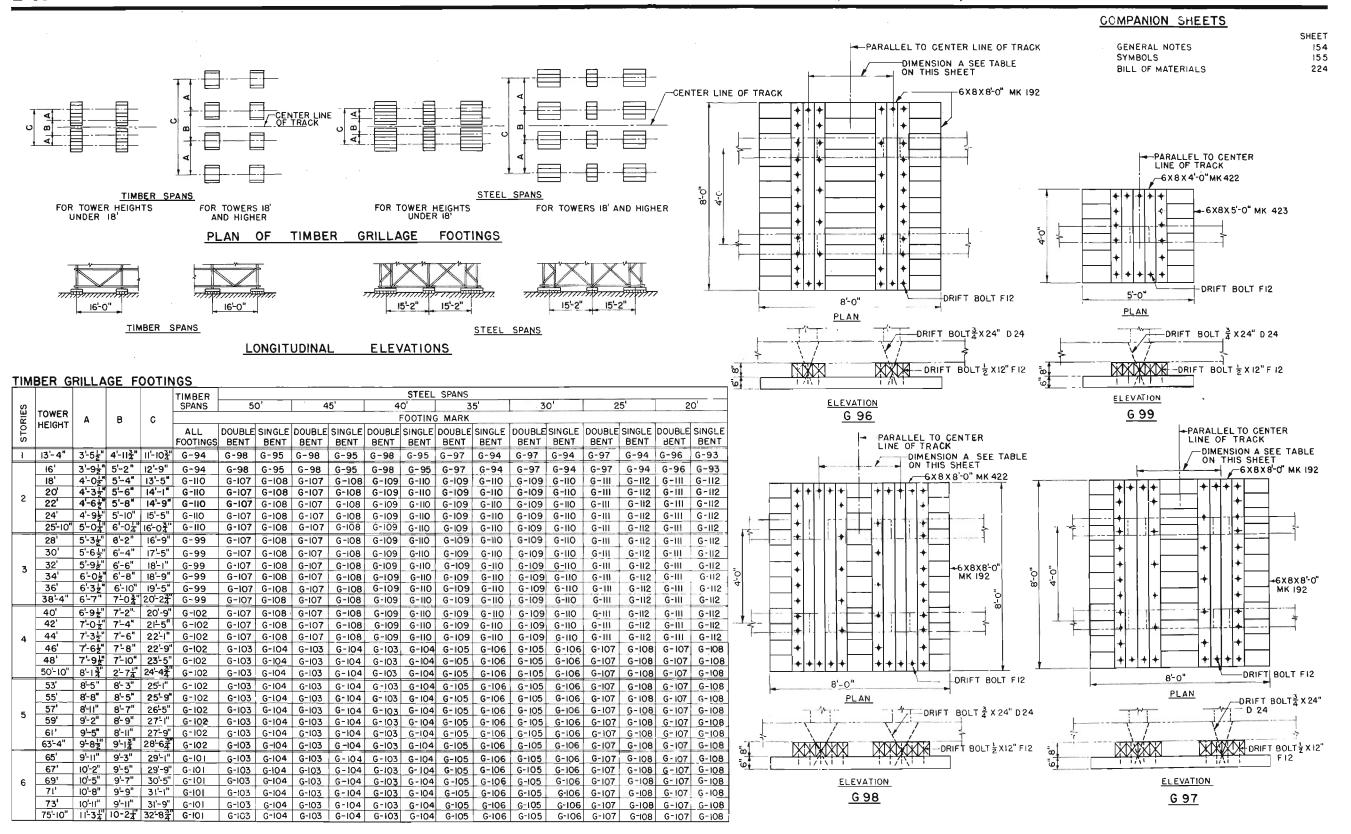


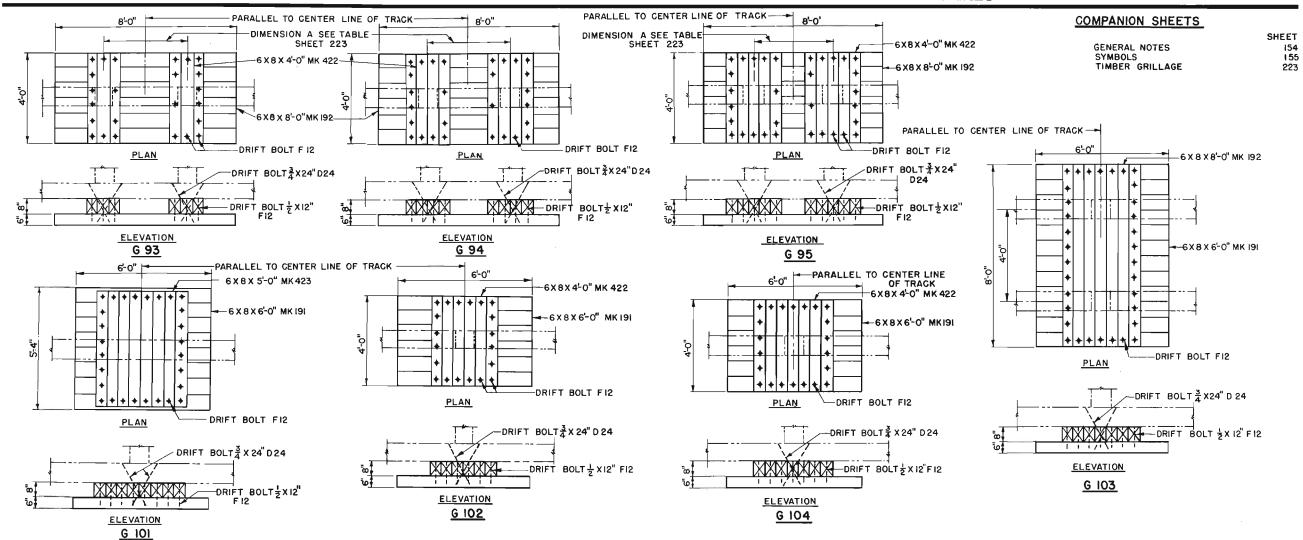


SEPARATOR MK 9016

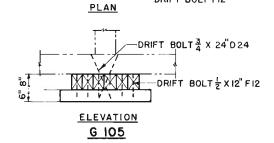




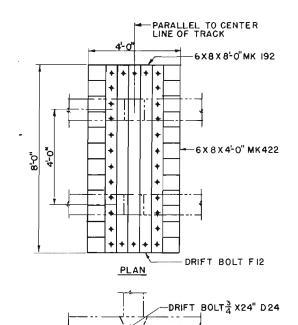




				GRILL	AGE NUMBER	₹	G:	93	G94	4	G9	5	G9	6	G97	,	G9	98	G9	9	G10	1	G10:	2	Gi	3	
IHE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENG TH	UNIT WEIGHT (POUHOS)	CLITHENC	FBM	QUANTITY	FBM	CHAMILIA	F3M	QUQUELITY	FBM	QU'NIT I TY	FBM	QUANTI TY	FBM	CUANTITY	FBM	QUANTITY	FBM	QUANTITY	FBM	(QUANTI TY	FBM	LINE
	LUMBER, SOFT WOOD							-																			-
1	GRILLAGE	39-9352.68	192	6 X 8	8'-0"	120	6	192	6	192	6	192	18	576	20	640	22	704				anous S			7	222	T 1
2		39-9352.68	191	6 X 8	6'-0"	90									1						8	192	6	144	12	288	2
3	DO	39-9352.68	423	6 X 8	5'-0*	75	l								1				6	120	8	160					3
4	DO	39-9352.58	422	5 X 8	4'-0"	60	6	96	8	128	10	160							5	80			6	96	1 1		4
	STEEL HARDWARE, BLACK	· -			•																•						
5	DRIFT BOLT	43-1636.07-2	4 D24	3/4	24*	3.15	4		4		4		а		в		8		2		2		2		4		1 5
6	00_	43-1636.05-1	2 F12	1/2	12"	1.65	24		28		32		42		46		50		18		28		20		34		6
				GRILL	IGE NUMBER		G	104	G10)5	Gl	0.5	G1	07	GI	.08	G1	.09	Gl	10	Gl	11	G112	2			
	LUMBER, SOFT WOOD																										
7	GRILLAGE	39-9352.68	192	6 X 8	8'-0"	120			6	192			5	160			4	128			3	96					7
8	00	39-9352.68	191	6 X 8	6'-0*	90	6	144																			8
9	DO	39-9352.68	422	6 X 8	4'-0"	60	7	112	12	192	12	192	12	192	11	176	12	192	10	160	12	192	9	144	1		9
	STEEL HARDWARE, BLACK																										
0	DRIFT BOLT	43-1636.07-2	4 D24	3/4	24"	3.15	2		4		2		4		2		4		2	12.000	4		2				10
a l	00	43-1636.05-1	2 F12	1/2	12*	1.65	22	T	32		20		30		18		28		16		26		14				11



-DRIFT BOLT FI2

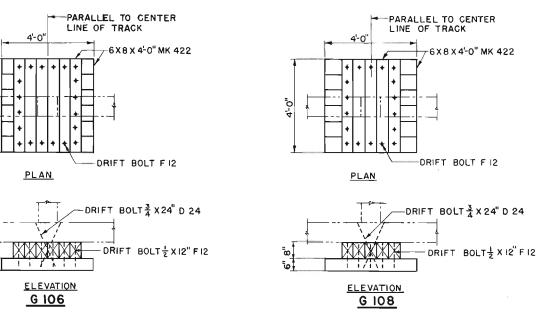


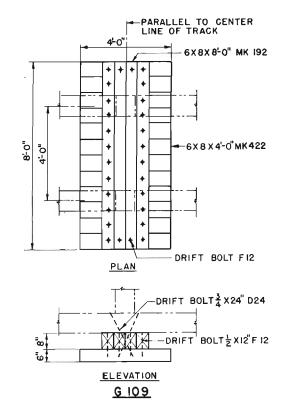
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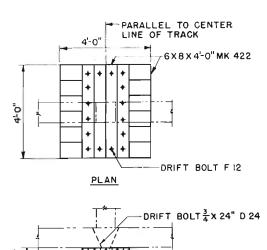
ELEVATION

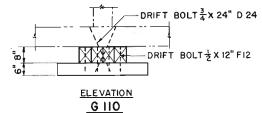
G 107

DRIFT BOLT 2 X 12" F 12



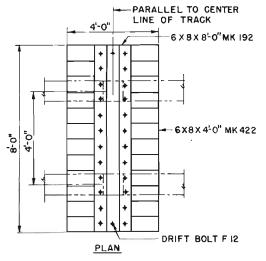


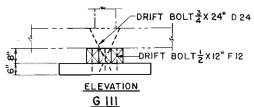


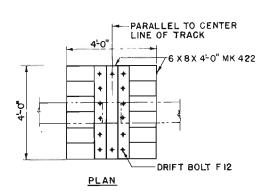


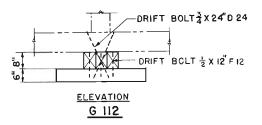
COMPANION SHEETS

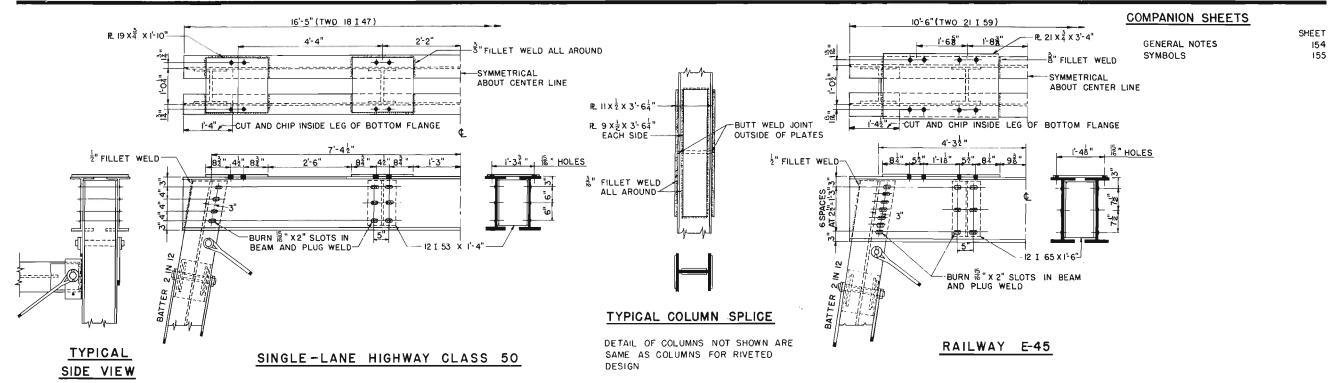
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SYMBOLS	155
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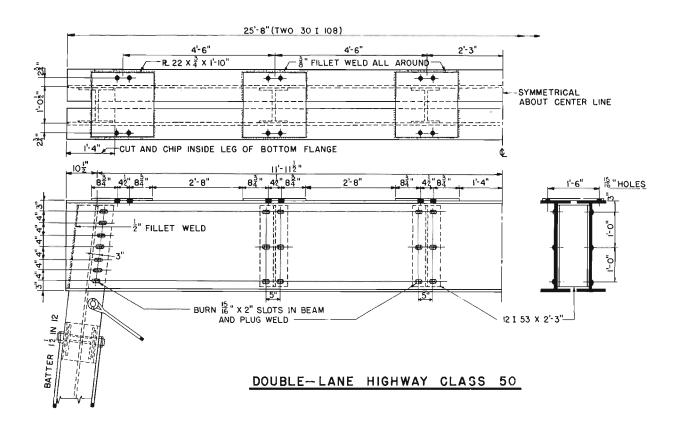


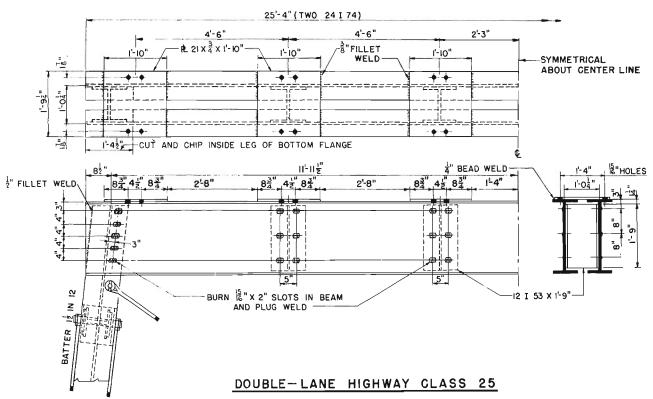


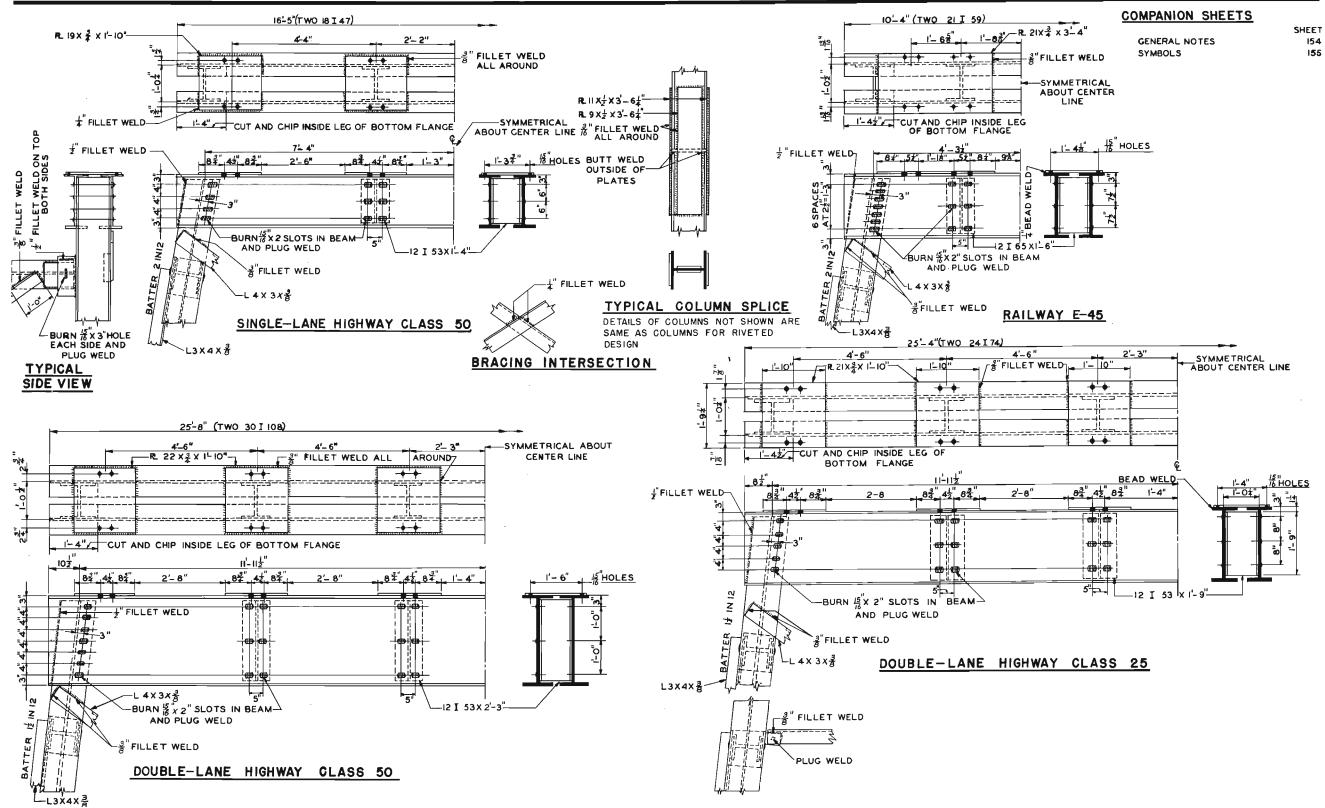


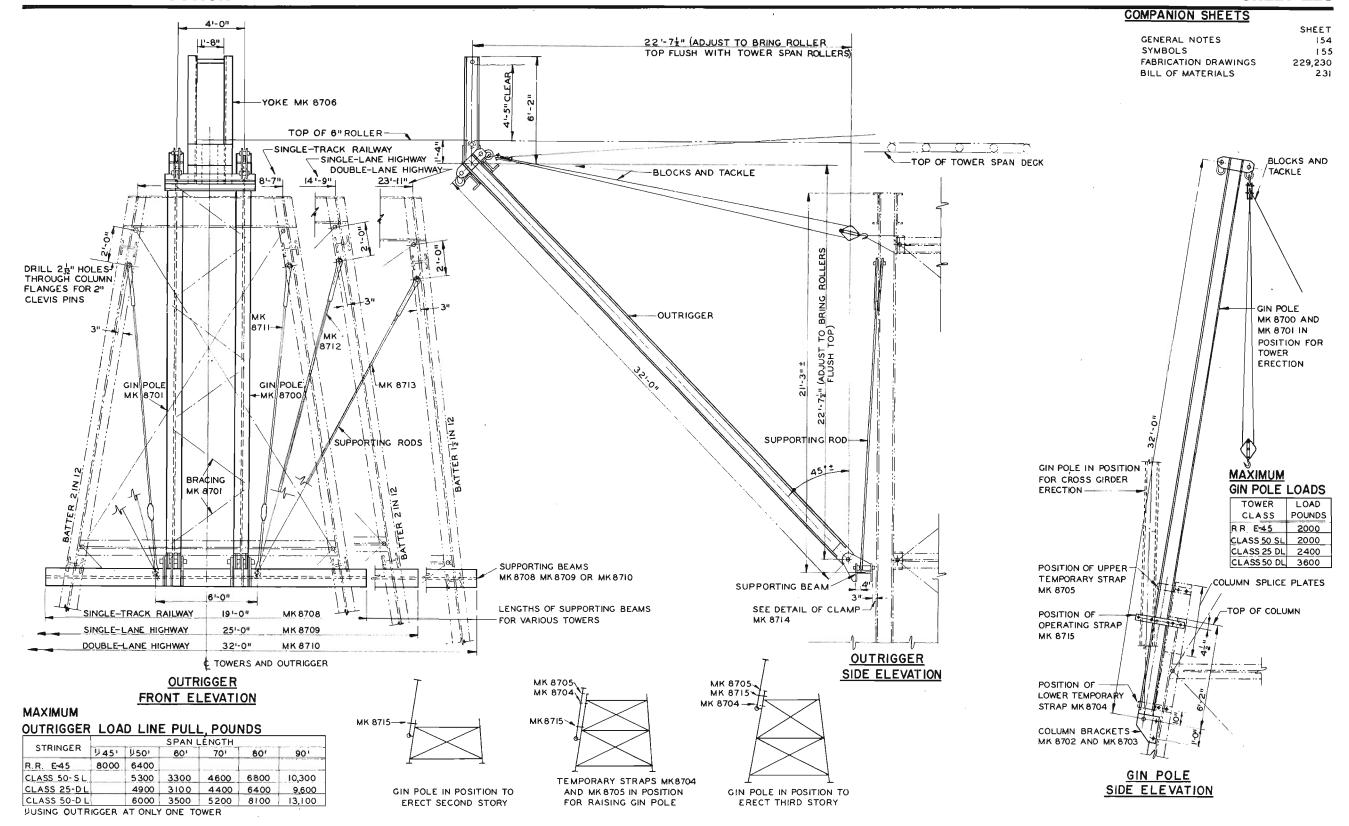


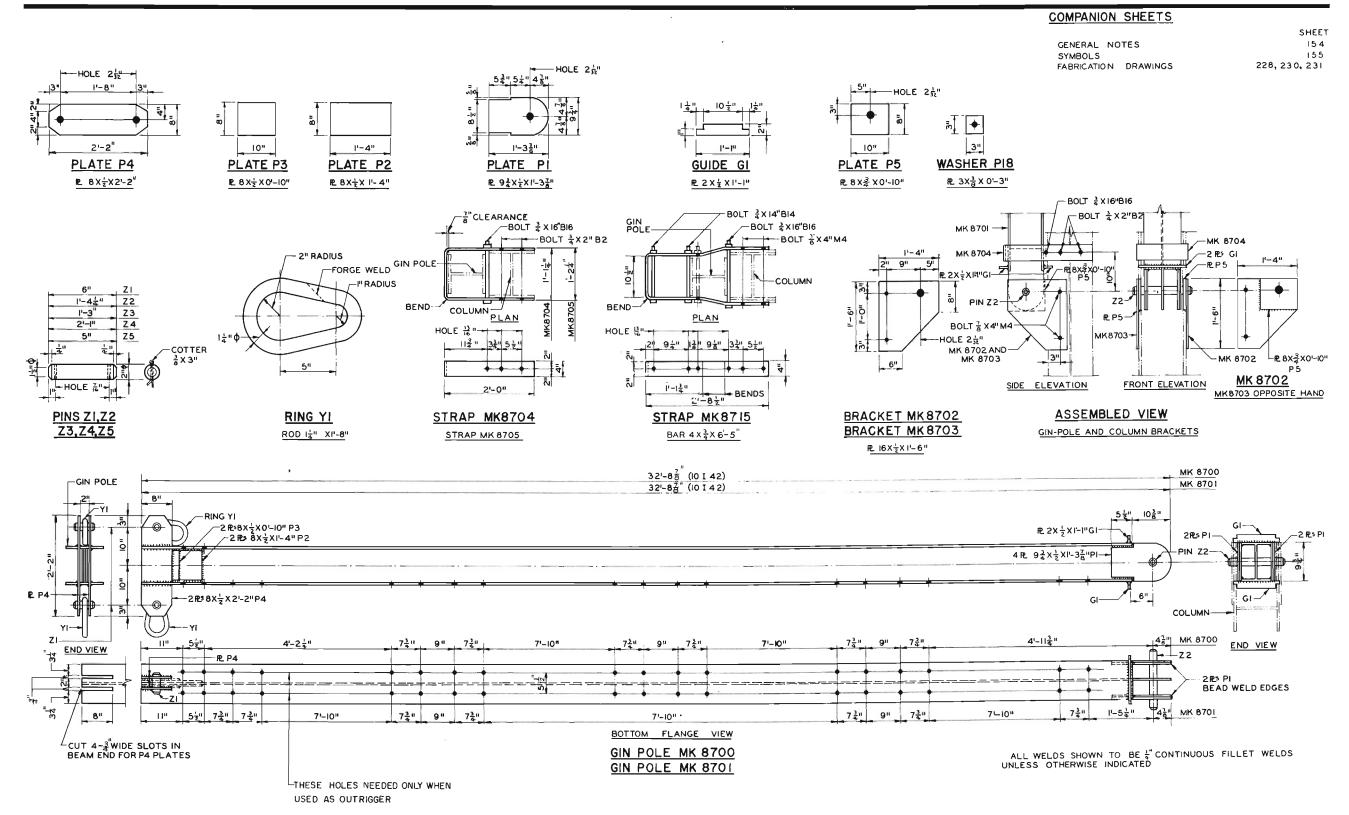




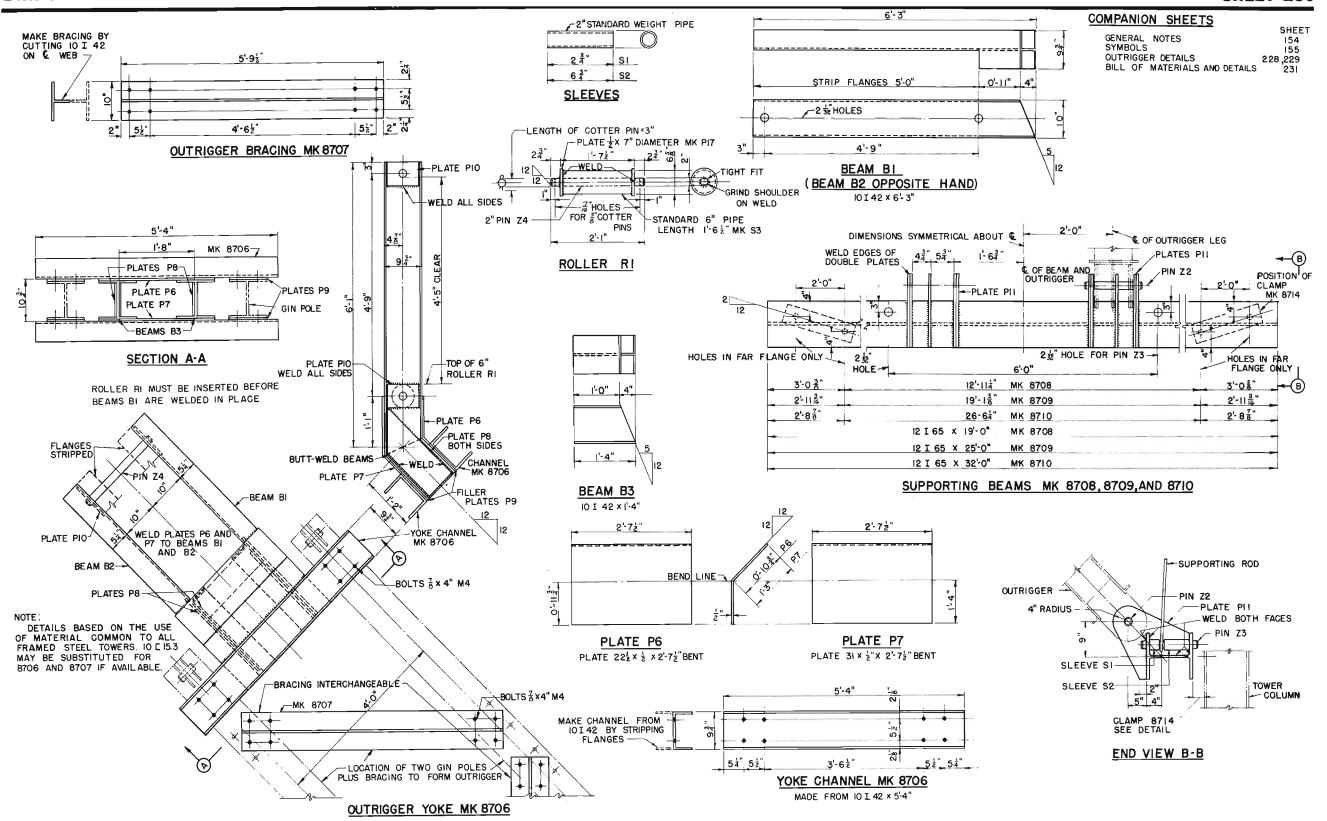








BRIDGE CONSTRUCTION



FABRICATION OF PARTS FOR

STEEL GIN-POLE OUTRIGGER

COMPANION SHEETS

BILL OF MATERIALS FOR ONE OUTRIGGER CONSISTING OF 2 GIN POLES, 1 YOKE, 6 OUTRIGGER BRACES, 1 SUPPORTING BEAM, 2 SUPPORTING RODS, 4 TEMPORARY STRAPS, 2 OPERATING STRAPS, 4 COLUMN BRACKETS AND 2 CLAMPS

MATERIAL COMMON TO ERECTION OF ANY STEEL TOWER OR STEEL STRINGER

		TO ERECTION OF ANY STE		LEE SIK	INGEN	SIZE		UNIT	
LINE	ITEM	DESCRIPTION	STOCK NO	MARK	QUANTITY	(INCHES)	LENGTH	WEIGHT (POUNDS)	LINE
1	GIN POLE	BEAM		8700	1	10 I 42	32'-8 7/8*	1375	1
2		DO	_	8701	1	10 I 42	32'-8 7/8"	1375	2
3		RING	46-6375.5-13	Y1	4	1 1/4	1'-8"	7	3
4		д ЫИ		Z 1	4	2	0'-6"	5	4
_ 5				Z 2	2	2	1'-4 1/4*	15	5
-6		GUIDE	47-7844.05	G1	4	2 X 1/2	1'-1"	4	6
_7		PLATE	47-7844.05	Pl	8	9 3/4 × 1/2	1'-3 7/8"	22	7
8		DO	47-7844.05	P2	4	8 X 1/2	1,-44	18	8
9		00	47-7844.05	Р3	4	8 X 1/2	0'-10"	11	9
10		DO_	47-7844.05	Рц	4	8 x 1/2	2'-2"	30	10
11	COLUMN BRACKET	DO	47-7844.05	8702	2	16 X 1/2	1'-6"	41	11
12		DO	47-7844.07	.65	2	8 x 3/4	0'-10"	17	12
13	_	BOLT AND ONE NUT	43-2219.08-04	M4	2	7/8	4.	1 5	12.
14	COLUMN BRACKET	PLATE	47-7844.05	8703	2	16 X 1/2	1'-6"	41	14
15		DO	47-7844.07	Ρ5	2	8 X 3/4	0'-10"	17	15
16		BOLT AND ONE NUT	43-2219.08-04	M4	2	7/8	ц.	<u>l</u> 5	16
17	TEMPORARY STRAP	BAR	47-7844.05	8704	2	4 X 1/2	5'-0"	34	17
18		00	47-7944.05	8705	2	4 X 1/2	5'-0"	34	18
19		BOLT AND ONE NUT	43-2325.07-02	B2	16	3/4	` 2*	1 14	19
20			43-2325.07-16	816	4	5/4	15"	10	20
21	OPERATING STRAP	8AR	47-7844.07	8715	2	3/4	6'-5"	66	21
22		BOLT AND ONE HUT	43-2219.08-04	M4	8	7/8	ц =	1 14	22
23		DO	43-2325.07-16	816	2	3/4	15"	1 5	23
24		00	43-2325.07-144	B14	4	3/4	14"	1 9	24
25	YOKE	CHANNEL (CUT I BEAM)		8706	2	10 I 42	51-4"	112	25
26		8E4M		B1	1	10 I 42	5'-3"	168	26
27		00		B2	1	10 I 42	5'-3"	158	27
28		00		B3	2	10 I 42	1'-4"	49	28
29		≇ PIN		Z 4	1	2 *	2'-1"	22	29
30	ROLLER	STANDARD PIPE	44-6246.3-06	S3	1	6"	1'-6 1/2"	29	30
<u> 51</u>		PLATE	47-7844.05	P17	2	7" DIA X 1/2			51
32		DO	47-7844.05	P6	1	22 1/2 × 1/2	2'-7 1/2"	100	32
33		DO	47-7844.05	Ρ7	1	31 X 1/2	2'-7 1/2*	138	33
34		DO	47-7944.05	P8	4	8 X 1/2	1'-11"	25	34
35		DO	47-7944.05	Ρ9	4	9 3/4 X 1/2	0'-9 3/4"	13	35
36		DO	47-7844.05	P10	4	5 X 1/2	0'-8*	7	35
37		ZI PIN		Z 4	1	2 *	2'-1"	22	57
38		BOLT AND ONE NUT	43-2219.08-04	M4	16	7/8	4 *	1 33	38
39	BRACING	TEE (SPLIT I-BEAM)		8707	6	10 I 42	5'-9 1/2"	168	39
40		BOLT AND ONE NUT	43-2219.08-04	M4	24	7/8	ű ×	Al 55	40
41	SUPPORTING BEAM	PLATE	47-7844.05	P11	10	18 X 1/2	1'-6 1/2"	47	41
42		21 PIN		23	2	2 -	1'-3-	13	42
43		SLEEVE STANDARD PIPE	44-6246.7-02	Sl	2	2 *	0'-2 3/4"	1	43
44		DO	44-6246.7-02	S 2	2	2 *	0'-6 3/4"	2	44
45	SUPPORTING ROD	CLEVIS PLATE	47-7844.05	Cl	4	4 1/2 x 1/2	2'-6"	19	45
46		SQUARE ROD		L1	2	3/4 □	5'-6'	11	46
47		TURNBUCKLE, STANDARD		Tl	2	1 1/8"	0'-9 1/8-	3	47
48		2 PIN		Z5	2	2 #	0'-5"	5	48
49	CLAMP	PLATE	47-7844.05	8714	. 2	5 X 1/2	2'-6"	21	49
50		DO	47-7844.05	P12	2	2 1/2 × 1/2	0'-3 1/2"	1	50
51		DO	47-7844.05	P13	2	2 7/6 X 1/2	0'-3 1/2"	2	51
52		00	47-7844.05	P14	ц	2 1/2 × 1/2	0'-8 1/2-	3	52
53		DO	47-7844.05	Ρ15	8	2 1/2 X 1/2	0'-2 7/8"	ı	53
				P16	2	4 × 1/2	0'-6 3/4"	4	54
54		DO	47-7844.05	1 - 10					
			47-7844.05 45-2219.08-04	M4	2	7/8	-	I 5	55
54		DO					-	1 5 1 8	55 56
54 55	MISCELLANEOUS	DO BOLT AND ONE NUT	45-2219.08-04	M4	2	7/8	-	1 8	
54 55 56	MISCELLANEOUS	BOLT AND ONE NUT	45-2219.08-04 43-2219.03-07	M4 M7	2	7/8 7/8	-	1 á	56 57 58
54 55 56 57	MISCELLANEOUS	DO BOLT AND ONE NUT DO WASHER	45-2219.08-04 43-2219.08-07 47-7844.04	M4 M7	2	7/8 7/8 3 X 3/8	-	1 8	56 57

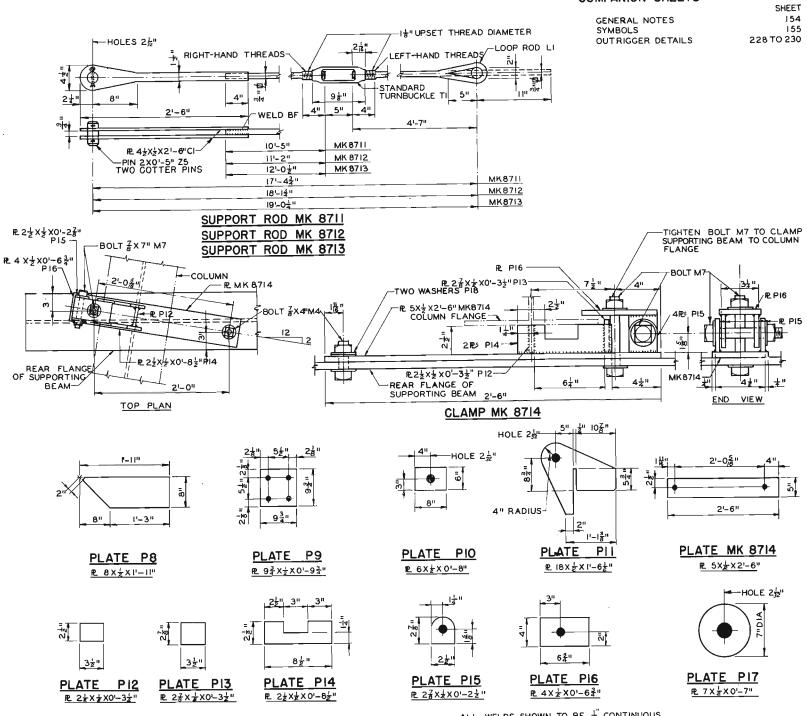
ADDITIONAL MATERIAL REQUIRED FOR ERECTION OF SINGLE TRACK RAILWAY STEEL

1 SUPPORTING ROD SOUARE ROD
2 SUPPORTING BEAM BEAM ADDITIONAL MATERIAL REQUIRED FOR ERECTION OF SINGLE LANE HIGHWAY STEEL TOWER AND STEEL STRINGER 1 SUPPORTING ROD SQUARE ROD 3/4 0 11'-2* 21 1 12 I 65 25'-0" 1625 2 8712 2

2 SUPPORTING BEAM BEAM 48-2900.12-065 8709 ADDITIONAL MATERIAL REQUIRED FOR ERECTION OF DOUBLE LANE HIGHWAY STEEL TOWER AND STEEL STRINGER 8715 2 3/4 11 12'-0 1/2" 23 1 5 8710 1 12 I 55 32'-0" 2075 2 1 SUPPORTING ROD SQUARE ROD

48-2900.12-065 8710 1

2 SUPPORTING BEAM BEAM

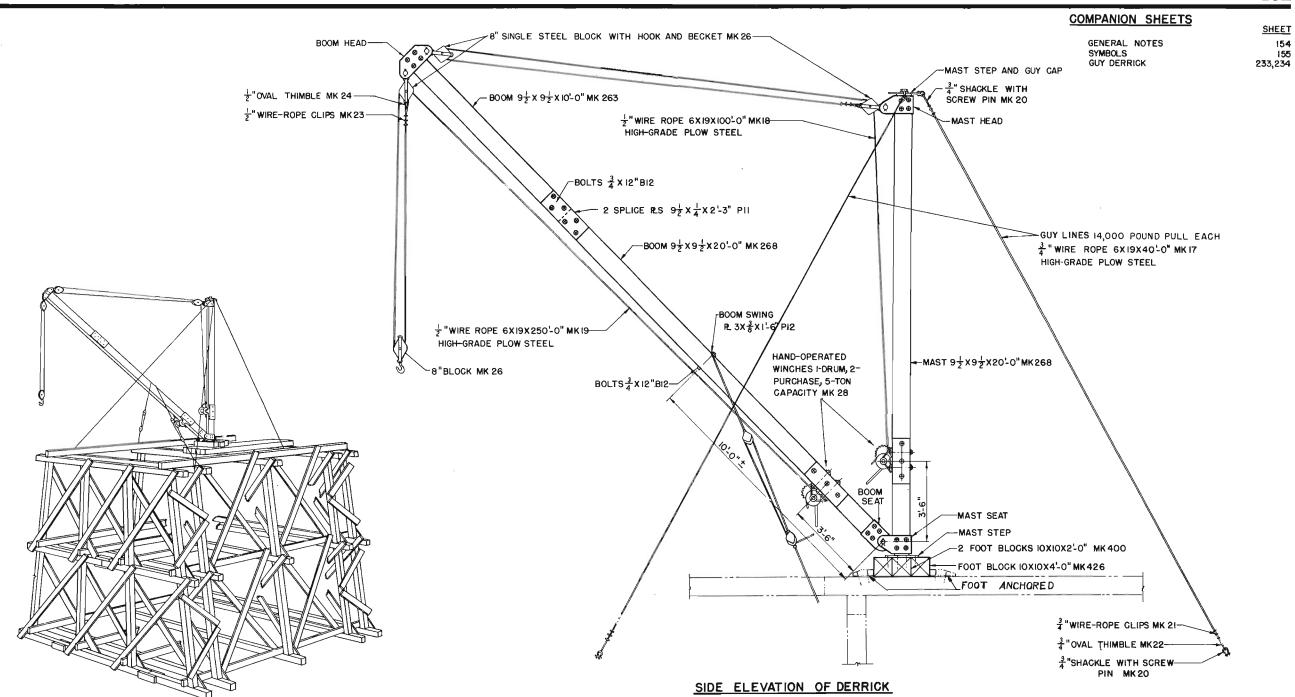


TOTAL WEIGHT
21 EACH PIN TO HAVE TWO COTTER KEYS (BILLED IN LINE 59)

BRIDGE CONSTRUCTION

ASSEMBLED VIEW IN ERECTION

SHEET



6,000-POUND PICKUP CAPACITY

GUY CONNECTION AT MAST HEAD

80'

901

UP TO 601

70'

90'

UP TO 401

11400

17840

4120

6320

7830

10240

5380

7820

6740

COMPANION SHEETS

	SHEET
GENERAL NOTES	154
SYMBOLS	155
TIMBER DERRICK	232,233

-BOOM GIN POLE B SUPPORT LINE B-MAST GIN POLE A-MAST GUY CAP GUY LINES B GUY LINES A- 19 SNUB LINE -BRIDGE DECK GROUND--TIMBER GROUND ANCHORAGE -TIMBER ANCHORAGE TOWER SHACKLE 3" TOWER MK 20 OVAL THIMBLE 1 "-TABLE OF STRESSES CLIP3" MK 21-CLASS 50-SINGLE LANE AND DOUBLE LANE MAX STRESS MAX STRESS MAX TOTAL GUY LINE GUY WIRE ROPE 4" MK17 STRESSES - 0=45° SUPPORT LINE PULL LINE B GUY LINES A GUY LINES B HORIZONTAL UP TO 60' 5980 1500 4720 1810 3475 70' 8775 2440 6790 3040 4610

6460

9160

2390

3320

4440

5260

3330

4740

3440

4870

7600

1250

2190

3350

4360

3140

5320

1510

SPANS UP TO 30' CAN BE ERECTED BY DERRICK
TIMBER GUY DERRICK MAST AND BOOM USED AS GIN
POLES FOR LAUNCHING STEEL STRINGERS

3850

5920

1030

1760

2640

3400

3140

5120

1410

10240

16270

3250

4890

7030 9340

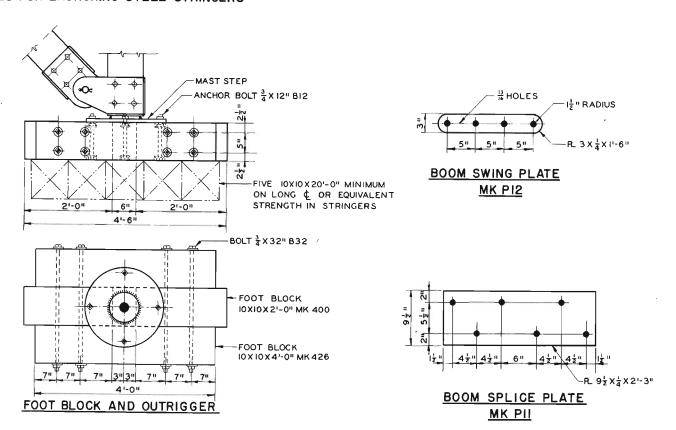
3400

5330

4170

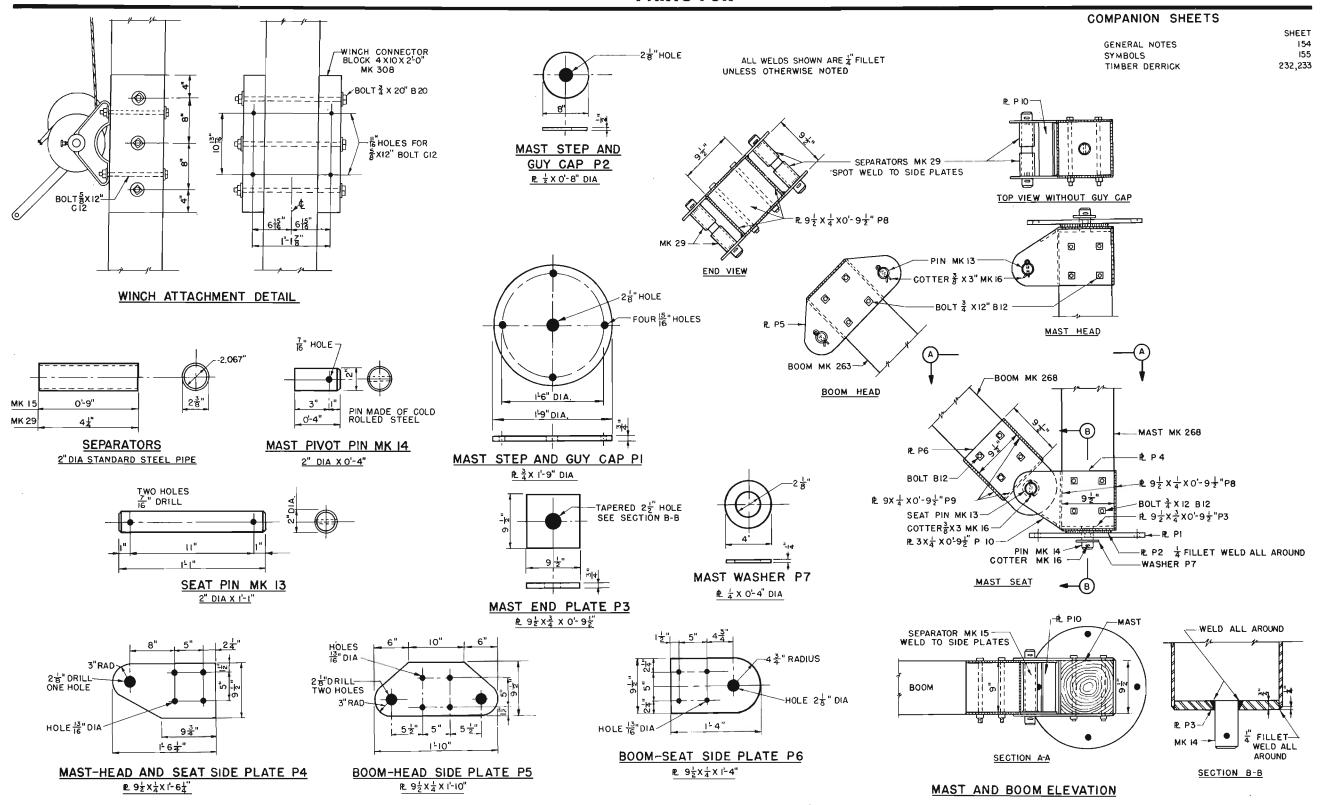
CLASS 25-DOUBLE LANE

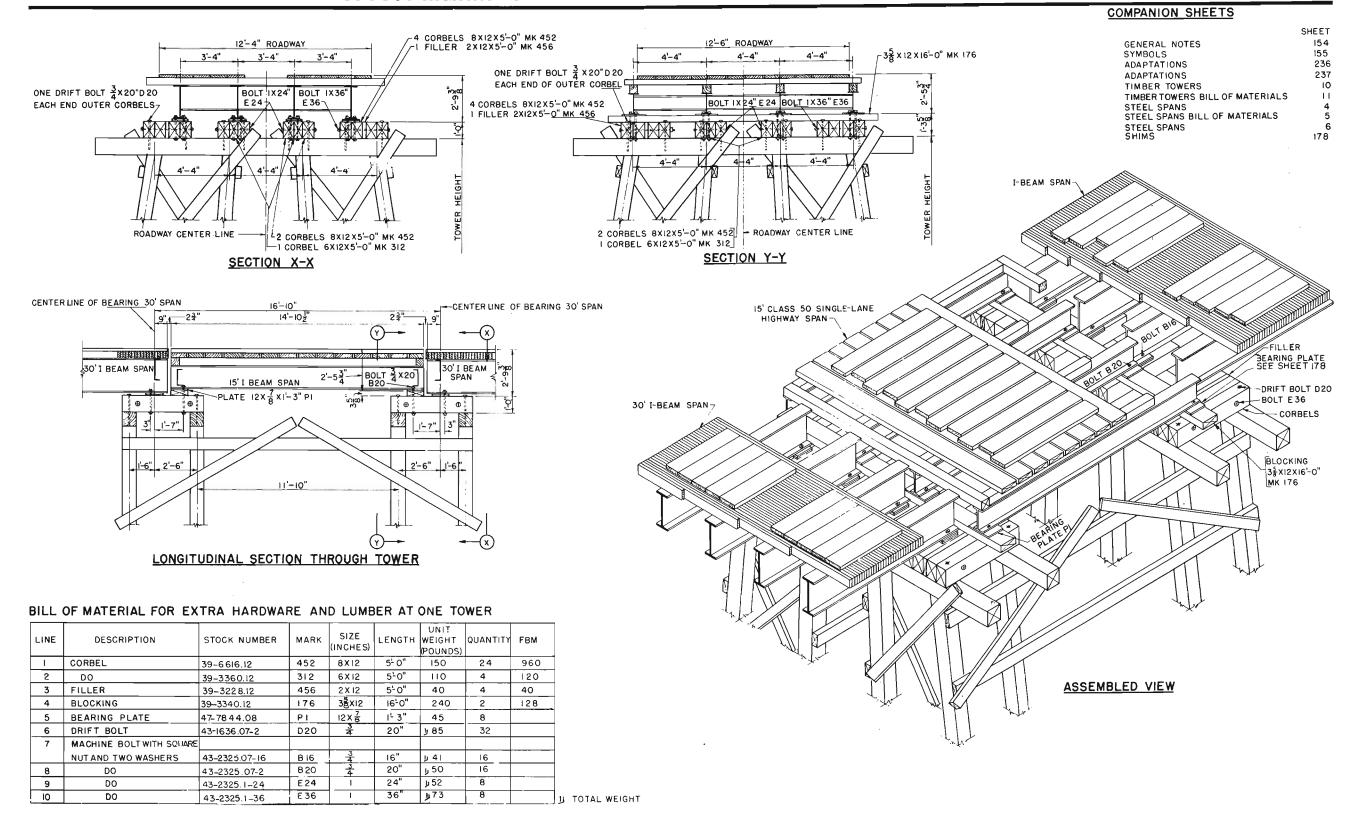
RAILROAD - E45



LINE	DESCRIPTION	STOCK NO	MARK	SIZE (INCHES)	LENGTH	UNIT WEIGHT (POUNDS)	QUANTITY	FBM
1	MAST STEP AND GUY CAP	47-7844.07	PI	3/4 X 1'-9" DIA	-	72	2	
2	DO	47-7344.05	P2	1/2 × 0'-8" DIA		6	2	
3	MAST HEAD AND SEAT END PLATE	47-7844.07	Р3	9 1/2 x 3/4	0'-9 1/2"	18	2	
4	MAST HEAD AND SEAT SIDE PLATE	47-7344.03	P4	9 1/2 × 1/4	1'-5 V4"	12	4	
5	BOOM-HEAD SIDE PLATE	47-7844.03	ρ5	9 1/2 X 1/4	1'-10-	19	2	
6	BOOM-SEAT SIDE PLATE	47-7344.03	96	9 1/2 × 1/4	1'-4"	10	2	
7	MAST WASHER	47-7844.03	Ρ7	1/4 × 0'-4" 313		1	2	
в	MAST HEAD AND SEAT SIDE PLATE AND BOOM-HEAD SIDE AND END PLATE	47-7844.03	P8	9 1/2 X 1/4	J'-9 1/2"	6	7	
9	BOOM- SEAT SIDE AND END PLATE	47-7344.03	29	9 X 1/4	0'-9 1/2"	6	3	
10	MAST SEAT AND HEAD BRACE PLATE	47-7844.03	P10	3 × 1/4	0'-9 1/2"	2	2	
11	BOOM SPLICE PLATE	47-7844.03	P11	9 1/2 × 1/4	2'-3"	18	2	
12	SOOM SWING PLATE	47-7844.04	P12	3 x 3/8	1'-6"	6	1	
13	PIN, COLD ROLLED STEEL	45-6375.5-15	13	1 1/2" 014	1'-1"	11	ц	
14	MAST PIVOT PIN, COLD ROLLED STEEL	46-6375.5-15	14	1 1/2" 014	0'-4"	4	2	
15	PIPE SPREADER, BOOM-SEAT	44-6246.7-02	15	2" STANDARD	0'-9"	3	1	
16	PIPE-SLEEVE HEAD PINS	44-6246.7-02	29	2" STANDARD	0'-4"	1	6	
17	COTTER PIN		16	3/8 Ø	3*	1 1	10	
18	MACHINE BOLF WITH SQUARE NUT AND TWO WASHERS	45-2325.07-124	812	3/4	12.	_1 59	28	
19	00	45-2325.07-2	320	3/4	20 •	18	6	
20	DO	43-2325.07-32	832	3/4	32*	1 56	8	
21	00	43-2525.06-12	C12	5/8	12*	10	8	
22	SHACKLE	12-4372.5-07	20	3/4		1 18	8	
23	BLOCK, SINGLE, STEEL, WITH HOOK AND BECKET	19-3755.05-08	26	8			ц	
24	DO	19-3267.05-04	25	4			4	
25	WIRE-ROPE GUY	22-4321.4-07	17	3/4	40'-0"	36	4	
26	WIRE-ROPE SOCM LINE	22-4321.4-05	18	1/2	100'-0"	40	1	
27	WIRE-ROPE LOAD LINE	22-4321.4-05	19	1/2	250'-0"	100	1	
28	MANILLA-ROPE BOOM SWING LINE	21-7555.3-05	27	1/2	30'-0"	2	2	
29	HAND WINCH, SINGLE DRUM	66-9450.05·	28	5_TON		110	2	
30	THIMBLE OVAL, GALVANIZED	12-6587.5-07	22	3/4		<u></u> ,	8	
31	00	12-6587.5-05	24	1/2			2	
32	CLIP, WIRE-ROPE, GALVANIZED	42-3544.5-08	21	7/8		1 42	24	
33	90	42-3544.5-05	23	1/2		_1 ,	6	
34	ELECTRODE WELDING	46-3772.2-7		3/15		1 7		
35	800M	39-6520.1-1	263	9 1/2 × 9 1/2	10'-0"	313	1	83
36	DO	39-6620.1-2	268	9 1/2 X 9 1/2	20'-0"	625	1	167
37	MAST	39-6620.1-2	268	9 1/2 × 9 1/2	20'-0"	625	1	167
38	BLOCK WINCH CONNECTOR	39-3340.1	310	4 × 10	2'-0"	25	4	27
39	FOCT BLOCK	39-6620.1	400	10 × 10	2'-0"	62	2	33
40	DO	39-6620.1	426	10 × 10	4'-0"	124	2	67

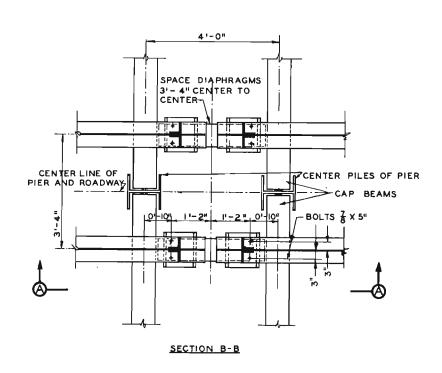
__ I TOTAL WEIGHT

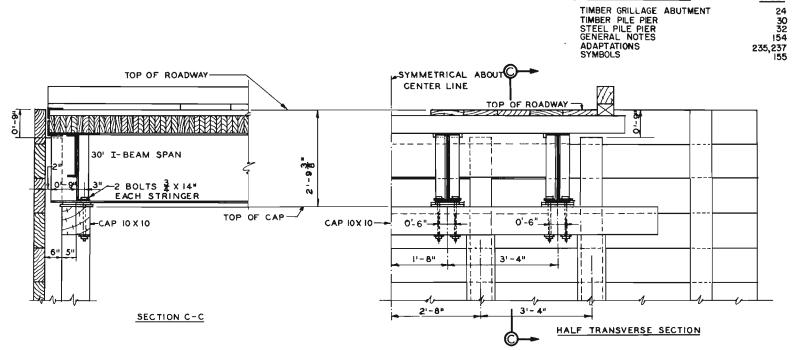




SHEET

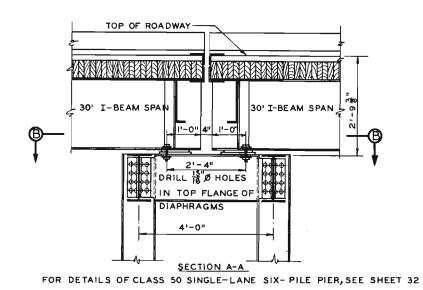
COMPANION SHEETS





FOR DETAILS AND DIMENSIONS NOT SHOWN, SEE CLASS 50 SINGLE-LANE ABUTMENT SHEET 23

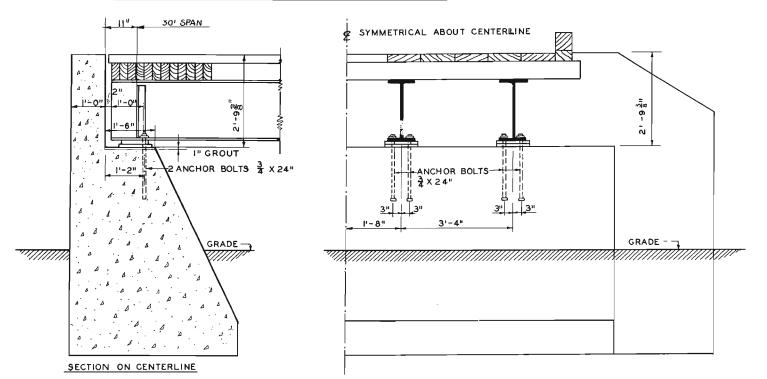
TIMBER GRILLAGE ABUTMENT



TOP OF ROADWAY-SYMMETRICAL ABOUT TOP OF ROADWAY CENTER LINE Y//// 30' I-BEAM SPA 30' I-BEAM SPAN 2 BOLTS X X 16" BOLTS IX 18" BOLTS IX 18" -2 CORBELS .8X 12 X 5'-0" 7-6" 0:-10 n 1'- 8" PIE PIER HEIGHT 4'-0" 21-2" 41 - 41 -CAP 12 X 12 SECTION D-D FOR DETAILS OF CLASS 50 SINGLE-LANE 8-PILE PIER, SEE SHEET 30 HALF TRANSVERSE SECTION

TIMBER PILE PIER

STEEL PILE PIER



 COMPANION SHEETS
 SHEET

 GENERAL NOTES
 15 4

 SYMBOLS
 155

 ADAPTATIONS
 235,236

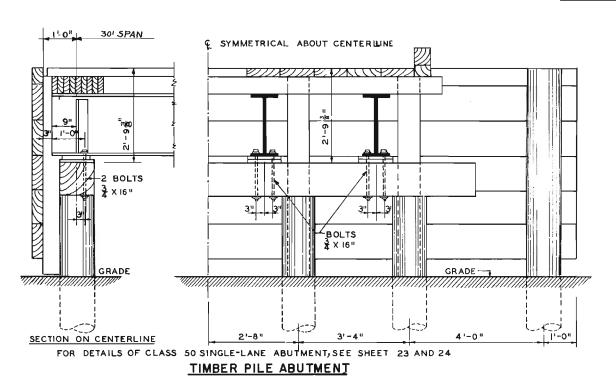
 CONCRETE ABUTMENT
 27

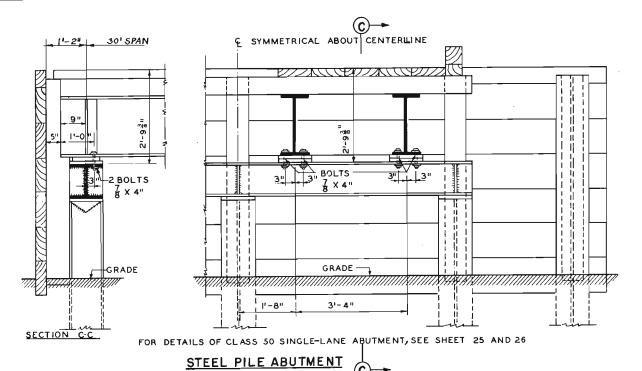
 TIMBER PILE ABUTMENT
 23,24

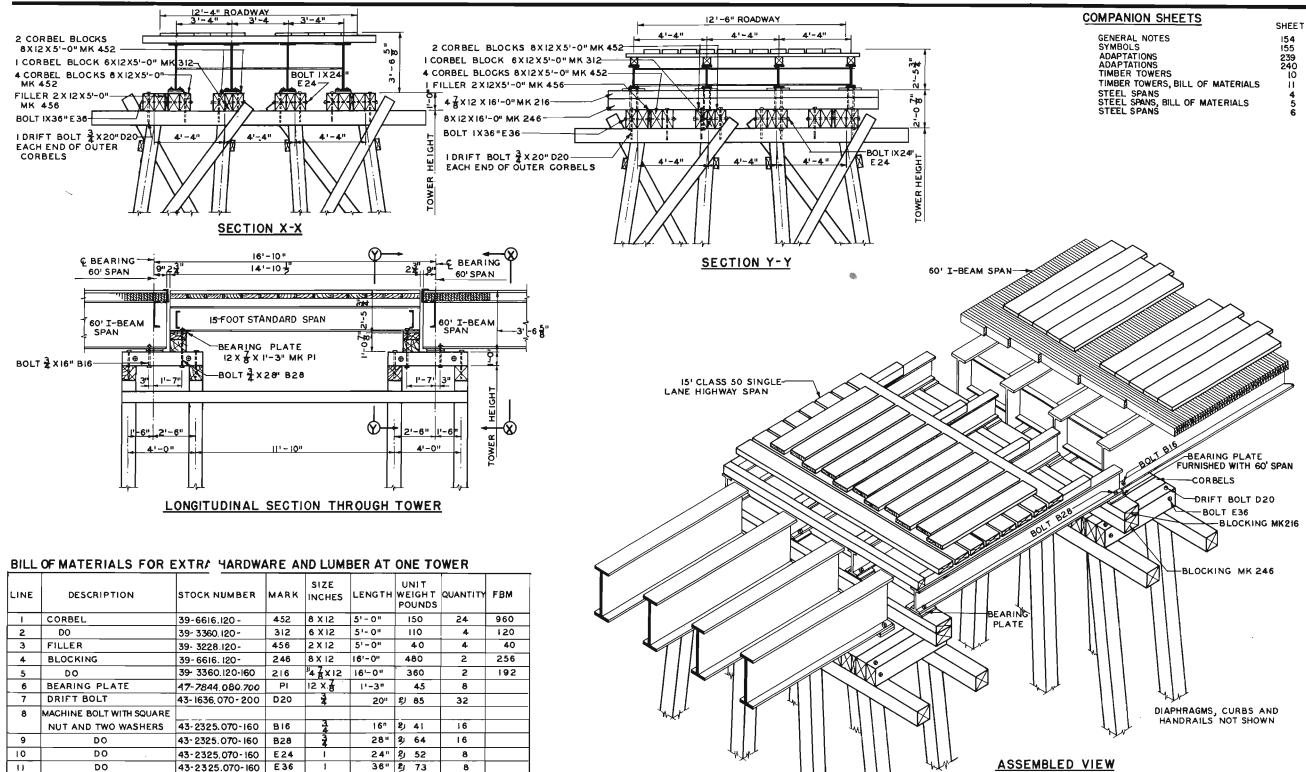
 STEEL PILE ABUTMENT
 25,26

FOR DETAILS OF CLASS 50 SINGLE-LANE ABUTMENT, SEE SHEET 27

CONCRETE ABUTMENT

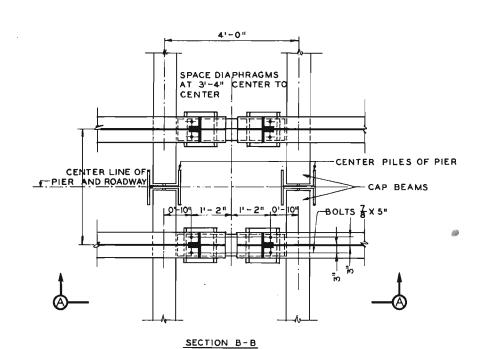


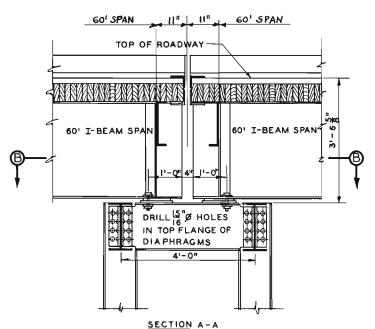




りTO BE CUT FROM 6 X 12 X 16'-0"

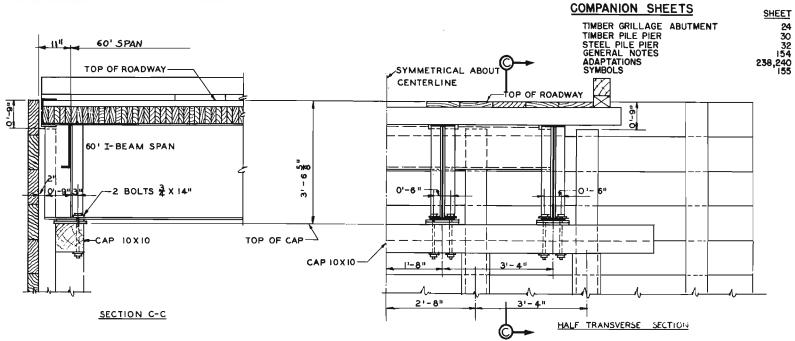
2) TOTAL WEIGHT





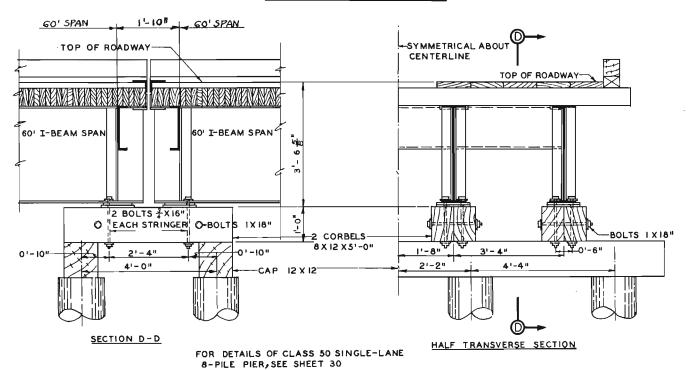
FOR DETAILS OF CLASS 50 SINGLE-LANE SIX-PILE PIER, SEE SHEET 32

STEEL PILE PIER



FOR DETAILS OF CLASS 50 SINGLE-LANE ABUTMENT, SEE SHEET 24

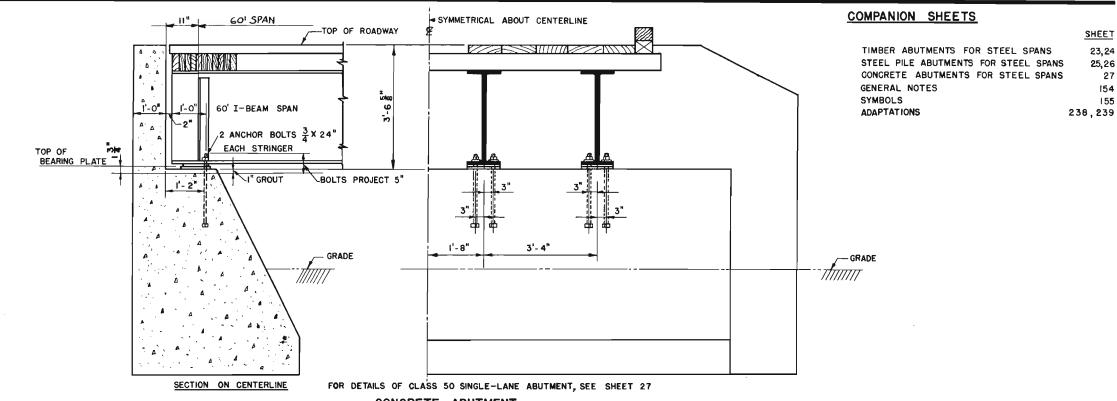
TIMBER GRILLAGE ABUTMENT

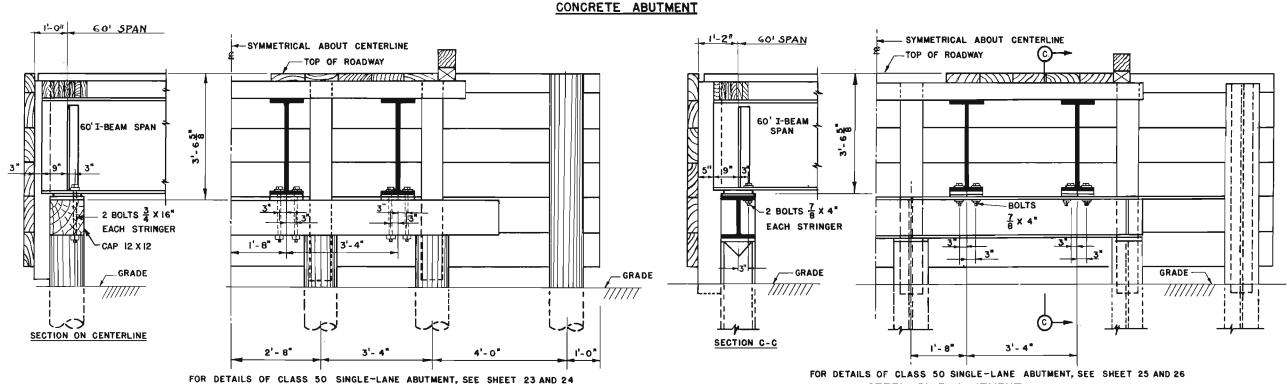


TIMBER PILE PIER

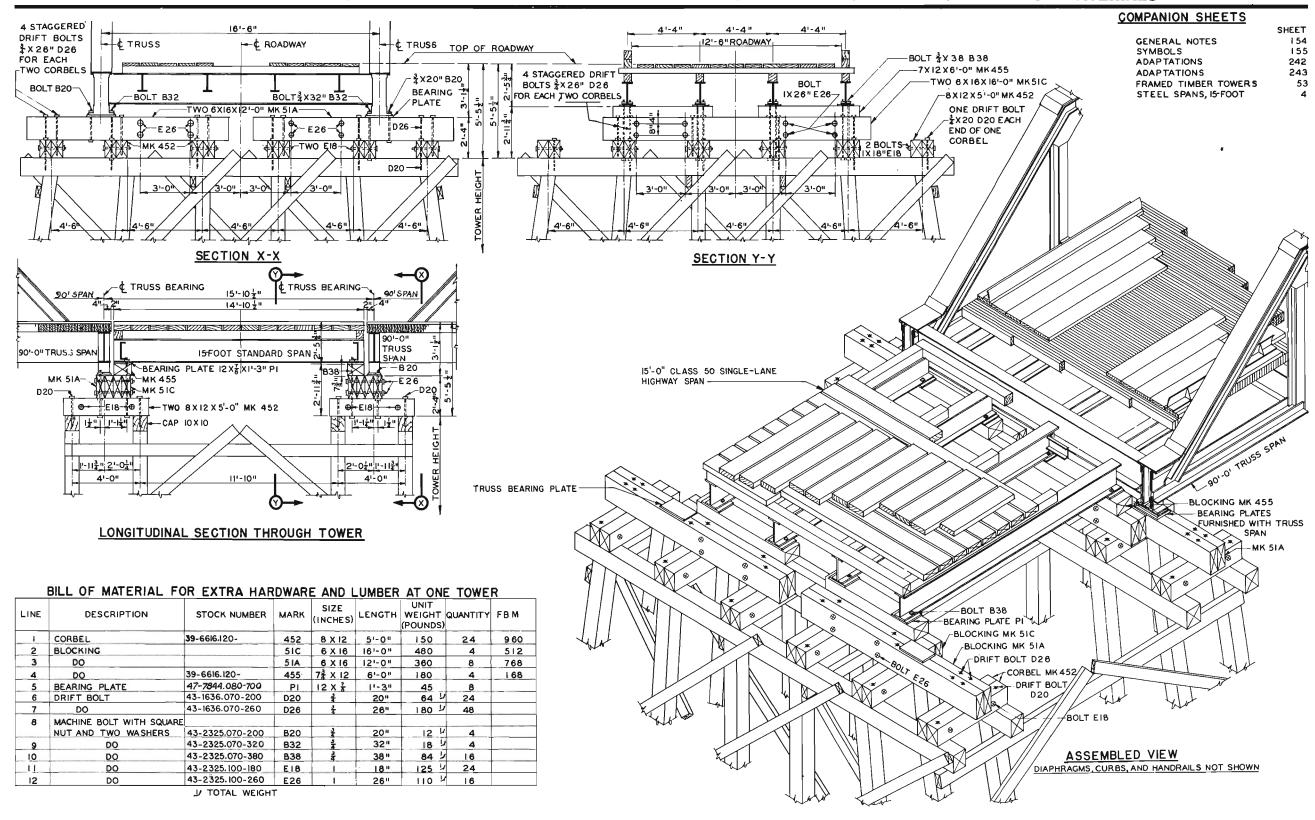
TIMBER PILE ABUTMENT

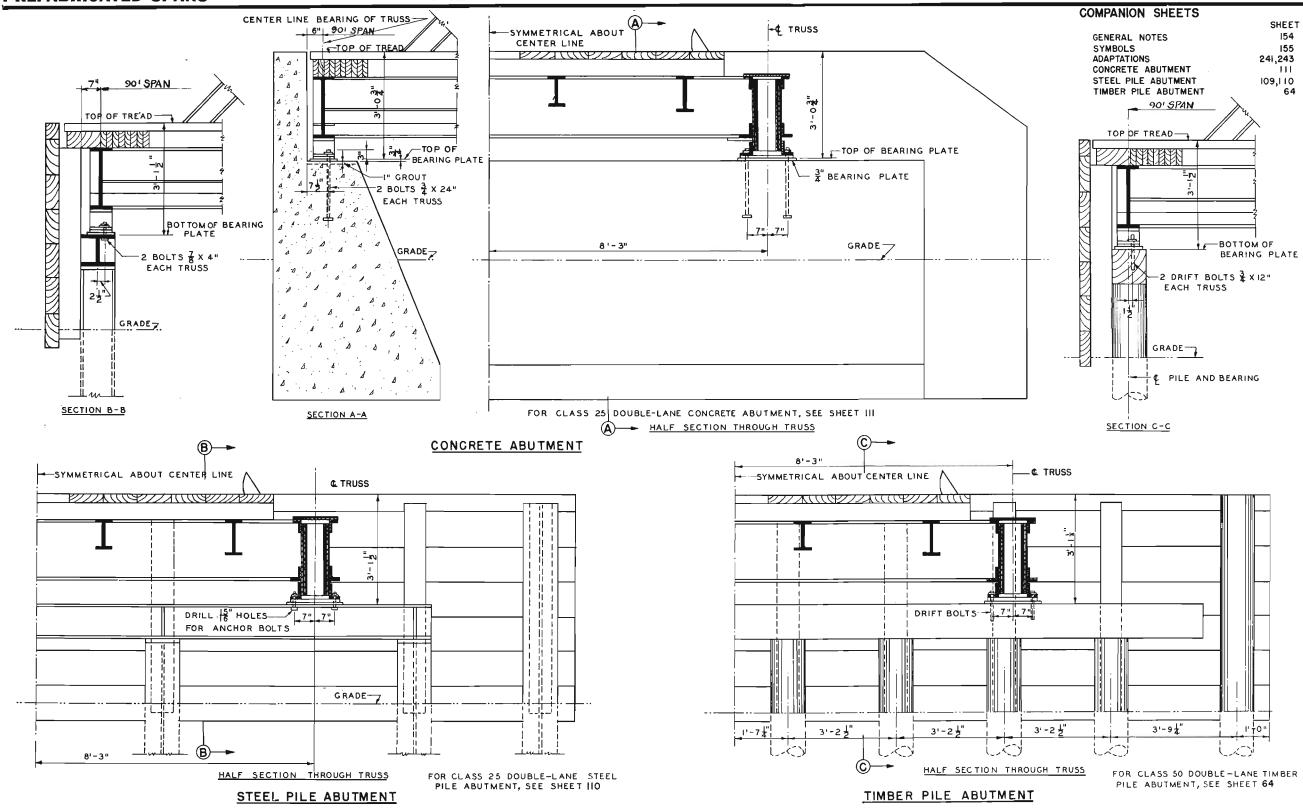
STEEL PILE ABUTMENT

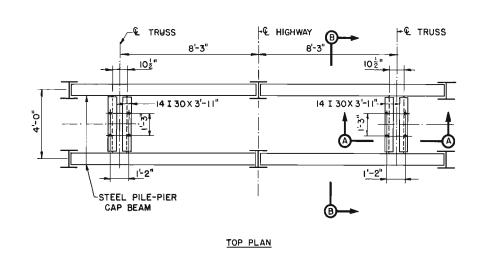


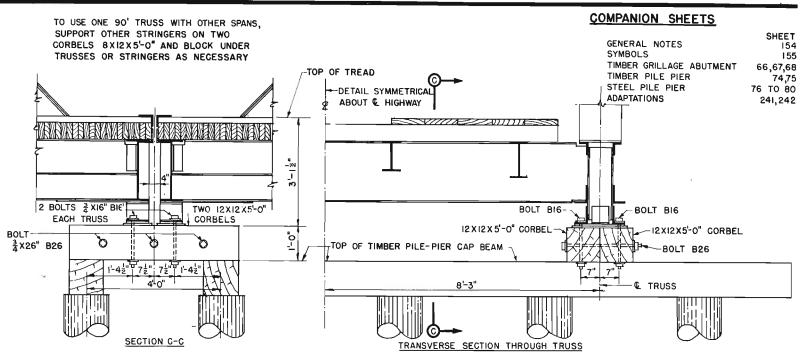


SHEET 241



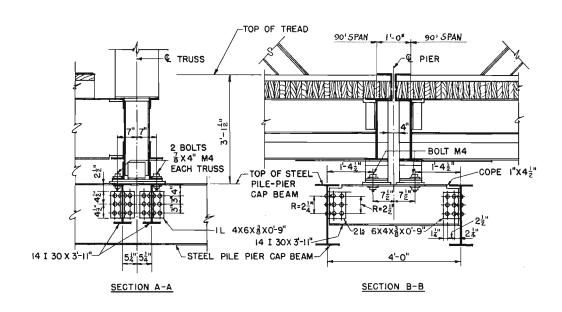






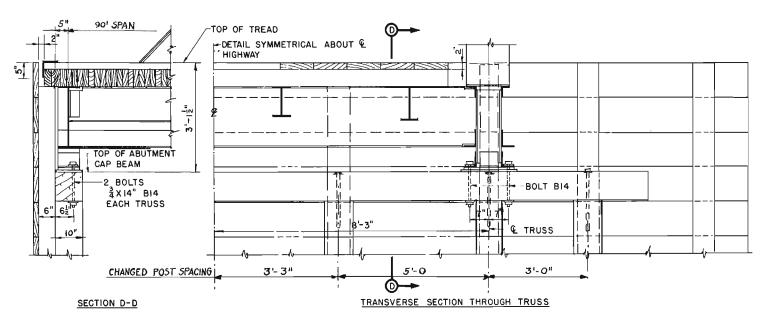
MODIFIED TIMBER PILE PIER

(SEE SHEET 75 FOR DIMENSIONS OF CLASS 50 DOUBLE-LANE HIGHWAY TIMBER PILE PIER NOT SHOWN THIS DETAIL)



MODIFIED STEEL PILE PIER

(SEE SHEETS 76 TO 80 FOR DIMENSIONS OF CLASS 50 DOUBLE-LANE HIGHWAY STEEL PILE PIER NOT SHOWN THIS DETAIL)



MODIFIED TIMBER GRILLAGE ABUTMENT

(SEE SHEET 67 FOR DIMENSIONS OF CLASS 50 DOUBLE-LANE HIGHWAY TIMBER GRILLAGE ABUTMENT NOT SHOWN THIS DETAIL) .

SHEET

154

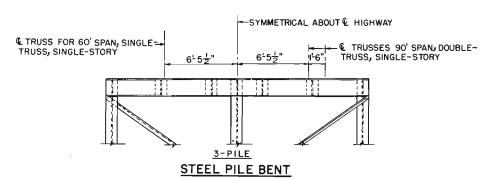
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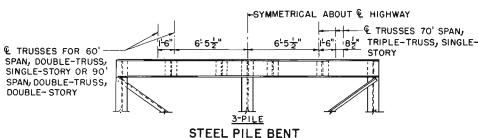
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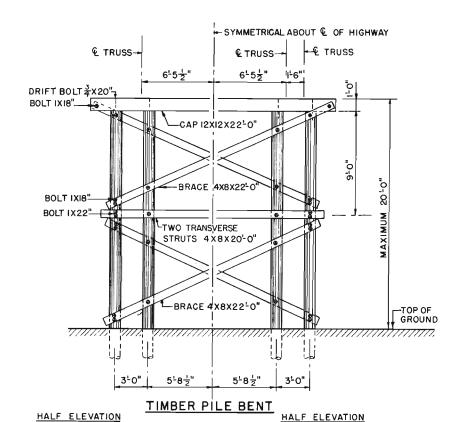
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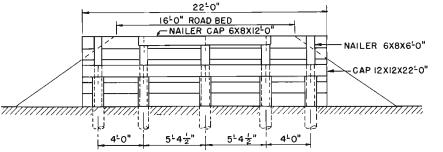




FOR DETAILS OF STEEL PILE BENT, SEE SHEET 116



60' SPAN, SINGLE-TRUSS, SINGLE-STORY; REQUIRED PILE BEARING CAPACITY 18 TONS 90'SPAN, DOUBLE-TRUSS, SINGLE-STORY; REQUIRED PILE BEARING CAPACITY 16 TONS



ELEVATION, TIMBER PILE ABUTMENT
DETAILS NOT SHOWN ARE SAME AS SHEET 21

CONCRETE ABUTMENT SEE SHEET III
STEEL PILE ABUTMENT SEE SHEET 69

REQUIRED PILE BEARING CAPACITIES (TONS)

TYPE OF SPAN		STEEL PILE ABUTMENT	TIMBER PILE ABUTMENT
60' SPAN, SINGLE-TRUSS, SINGLE STORY	25 TONS	16 TONS	16 TONS
90' SPAN, DOUBLE-TRUSS, DO	29 DO	16 DO	14 DO
60'SPAN.DOUBLE-TRUSS, DO	37 DO	24 DO	20 DO
70'SPAN, TRIPLE - TRUSS, DO	42 DO	25 DO	20 D0
90'SPAN, DOUBLE-TRUSS, DOUBLE-STORY	50 DO	31 DO	20 00

COMPANION SHEETS

TIMBER PILE ABUTMENT

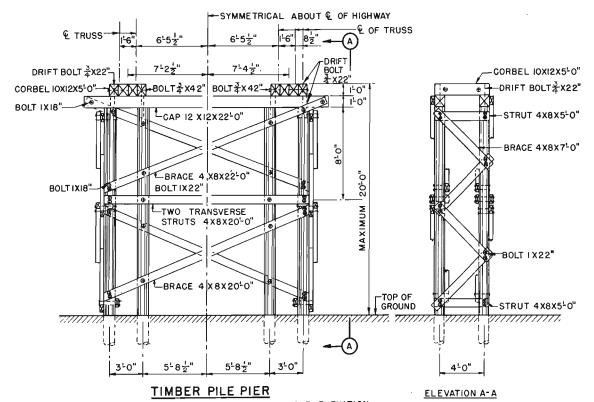
STEEL PILE ABUTMENT

CONCRETE ABUTMENT

STEEL PILE BENT

GENERAL NOTES

SYMBOLS



HALF ELEVATION

60' SPAN, DOUBLE-TRUSS, SINGLE-STORY;
REQUIRED PILE BEARING CAPACITY II TONS
OR

90' SPAN, DOUBLE-TRUSS, DOUBLE-STORY; REQUIRED PILE BEARING CAPACITY 15 TONS 70' SPAN, TRIPLE-TRUSS SINGLE-STORY; REQUIRED PILE BEARING CAPACITY IS TONS

STEEL- PILE PIER

TIMBER-PILE ABUTMENT A

TIMBER-PILE ABUTMENT B

STEEL-PILE ABUTMENT

20

20

36

17

20

25

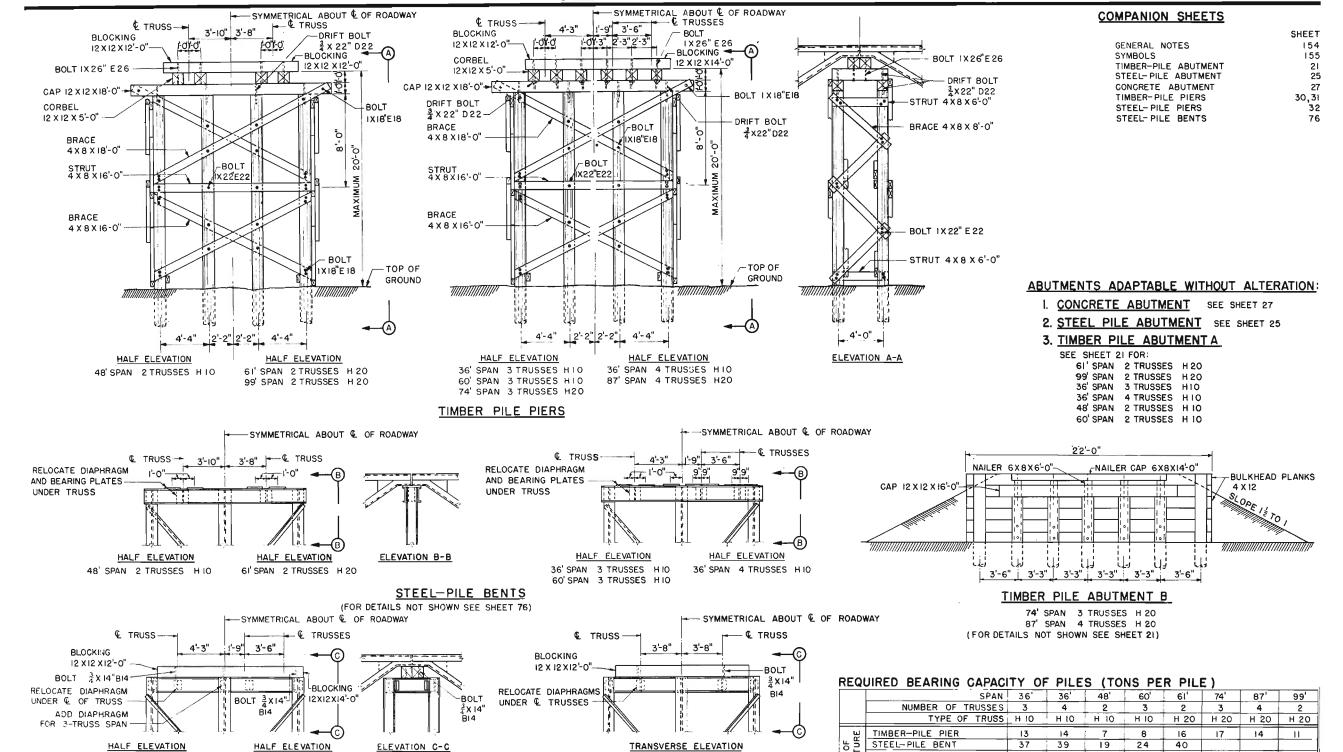
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24

45 42

19 20

35



99' SPAN 2 TRUSSES H 20

74 SPAN 3 TRUSSES H20

87 SPAN 4 TRUSSES H 20

STEEL-PILE PIERS

(FOR DETAILS NOT SHOWN SEE SHEET 32)

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